

Illinois Power Generating Company 1500 Eastport Plaza Dr. Collinsville, IL 62234

October 25, 2021

Illinois Environmental Protection Agency
DWPC – Permits MC #15
Attn: Part 845 Coal Combustion Residual Rule Submittal
1021 North Grand Avenue East
P.O. Box 19276
Springfield, IL 62794-9276

Re: Coffeen Power Plant Ash Pond No. 1; IEPA ID # W1350150004-01

Dear Mr. LeCrone:

In accordance with 35 I.A.C. § 845.200, Illinois Power Generating Company (IPGC) is submitting an operating permit application for the Coffeen Power Plant Ash Pond No. 1 (IEPA ID # W1350150004-01). One hardcopy and one digital copy are provided with this submittal.

The permit application was prepared in accordance with 35 I.A.C. § 845.230(d)(2) (Existing, Inactive and Inactive Closed CCR Surface Impoundment that have not completed an Agency approved closure before July 30, 2021). This submittal includes the completed permit forms as required by § 845.210.

Sincerely,

Cynthia Vodopivec

Cynthin E Way

SVP-Environmental Health and Safety

Enclosures

6555 SIERRA DRIVE IRVING, TEXAS 75039 **o** 214-812-4600 VISTRAENERGY.COM

Prepared for

Illinois Power Generating Company

1500 Eastport Plaza Drive Collinsville, Illinois 62234

INITIAL OPERATING PERMIT COFFEEN ASH POND NO.1

Prepared by



425 South Woods Mill Road, Suite 300 St. Louis, MO 63017

October 25, 2021

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| | |

ii October 2021



1. INTRODUCTION

Illinois Power Generating Company operates the coal-fired Coffeen Power Plant located in Montgomery County, Illinois. The IEPA assigned identification number assigned to this impoundment is: W1350150004-01 for the Ash Pond No.1. The National Inventory of Dams (NID) number assigned for the Ash Pond No.1 by the Illinois Department of Natural Resources (IDNR) is IL50715.

This initial operating permit application was developed in accordance with 35 Ill. Admin. Code 845, Standards for the Disposal of Coal Combustion Residuals in Surface Impoundments (Part 845).

This initial operating permit application is for the Ash Pond No.1.

1.1. <u>Facility Information</u>

<u>Section 845.210(b)(1):</u> All permit applications must contain the name, address, email address and telephone number of the operator, or duly authorized agent, and the property owner to whom all inquiries and correspondence shall be addressed.

Facility: Coffeen Ash Pond No.1

Coffeen Power Plant

134 Cips Lane Coffeen, IL 62017

Owner/Operator: Illinois Power Generating Company

1500 Eastport Plaza Drive Collinsville, Illinois 62234



1.2. Owner Signatures

<u>Section 845.210(b)(2):</u> All permit applications must be signed by the owner, operator or a duly authorized agent of the operator.

The owner of the Coffeen Power Plant is a corporation.

<u>Section 845.210(b)(3):</u> An application submitted by a corporation must be signed by a principal executive officer of at least the level of vice president, or his or her duly authorized representative, if that representative is responsible for the overall operation of the facility described in the application form..

The signature of Cynthia Vodopivec on behalf of Illinois Power Generating Company can be found in the permit applications located in Section 3.

1.3. Legal Description

<u>Section 845.210(c):</u> All permit applications must contain a legal description of the facility boundary and a description of the boundaries of all units included in the facility.

A legal description has been developed in compliance with Section 845.210(c) and is included in Attachment A.

1.4. Previous Assessments

<u>Section 845.210(d):</u> Previous Assessments, Investigations Plans, and Programs

Previous assessments were performed in accordance with 40 CFR § 257 and are referenced within the permit application and included in the appropriate Attachments.

<u>Section 845.210(d)(1):</u> The Agency may approve the use of any hydrogeologic site investigation or characterization, groundwater monitoring well or system, or groundwater monitoring plan, bearing the seal and signature of an Illinois Licensed Professional Geologist or Licensed Professional Engineer, completed before April 21, 2021 to satisfy the requirements of this Part.

A previous hydrogeologic site investigation or characterization, groundwater monitoring well or system, or groundwater monitoring plan have been completed with a seal from an Illinois Licensed Professional Geologist or Licensed Professional Engineer. However, field investigations have been completed that supplement that work that will be utilized in the following sections of this report.



<u>Section 845.210(d)(2):</u> For existing CCR surface impoundments, the owner or operator of the CCR surface impoundment may use a previously completed location restriction demonstration required by Section 845.300 (Placement Above the Uppermost Aquifer), Section 845.310 (Wetlands), Section 845.320 (Fault Areas), Section 845.330 (Seismic Impact Zones), and Section 845.340 (Unstable Areas) provided that the previously completed assessments meet the applicable requirements of those Sections.

Previous assessments are provided for Section 845.300 (Placement Above the Uppermost Aquifer), Section 845.310 (Wetlands), Section 845.320 (Fault Areas), Section 845.330 (Seismic Impact Zones), and Section 845.340 (Unstable Areas) in Attachment D.

<u>Section 845.210(d)(3):</u> For existing CCR surface impoundments, the owner or operator of the CCR surface impoundment may use a previously completed assessment to serve as the initial assessment required by Section 845.440 (Hazard Potential Classification Assessment), Section 845.450 (Structural Stability Assessment) and Section 845.460 (Safety Factor Assessment) provided that the previously completed assessment: A) Was not completed more than five years ago; and B) Meets the applicable requirements of those Sections.

Previous assessments are provided for Section 845.440 (Hazard Potential Classification Assessment), Section 845.450 (Structural Stability Assessment) and Section 845.460 (Safety Factor Assessment) in Attachments O, P, and Q respectively. The addendum and certification for the Hazard Potential Classification Assessment, Structural Stability Assessment and Safety Factor Assessment are located in Attachment U.

<u>Section 845.210(d)(4):</u> For inactive closed CCR surface impoundments, the owner or operator of the CCR surface impoundment may use a post-closure care plan previously approved by the Agency.

No post-closure care plan was previously approved by the Agency.



2. OPERATING PERMIT

2.1. Initial Operating Permit

<u>Section 845.230(d):</u> Initial Operating Permit for Existing, Inactive and Inactive Closed CCR Surface Impoundments

The Coffeen Ash Pond No.1 as defined by IEPA is an existing CCR surface impoundment that has not completed post-closure care. Per Part 845, Dynegy is submitting an initial operating permit application to IEPA by October 31, 2021. The following sections contain information or references to documents required for the Operating Permit application (Section 845.230).

2.2. History of Construction

<u>Section 845.230(d)(2)(A):</u> The history of construction specified in Section 845.220(a)(1);

The history of construction prepared in 2016 pursuant to 40 CFR § 257.73(c) is provided in Attachment B. An amendment to the history of construction has been prepared in compliance with Section 845.220(a)(1) and is provided in Attachment U.

2.3. Chemical Constituents

<u>Section 845.230(d)(2)(B):</u> An analysis of the chemical constituents found within the CCR to be placed in the CCR surface impoundment;

An analysis of the chemical constituents found within the CCR placed within the Coffeen Ash Pond No.1 is provided in Attachment C.

<u>Section 845.230(d)(2)(C):</u> An analysis of the chemical constituents of all waste streams, chemical additives and sorbent materials entering or contained in the CCR surface impoundment;

An analysis of the chemical constituents of all waste streams, chemical additives and sorbent materials entering or contained within the Coffeen Ash Pond No.1 is provided in Attachment C.

2.4. Location Standards Demonstration

<u>Section 845.230(d)(2)(D):</u> A demonstration that the CCR surface impoundment, as built, meets, or an explanation of how the CCR surface impoundments fails to meet, the location standards in the following Sections:



The Coffeen Ash Pond No.1 location standards as specified in Section 845.230(d)(2)(D) are described in the following sections.

<u>Section 845.230(d)(2)(D)(i):</u> Placement Above the Uppermost Aquifer;

The previous upper aquifer demonstration was certified by a qualified professional engineer stating that the demonstration meets the requirements of 40 C.F.R. § 257.60. The requirements described in 40 C.F.R. § 257.60 are identical to the requirements contained in Section 845.300. Pursuant to Section 845.210(d)(2), a certification is not required for this demonstration. The previously completed upper aquifer demonstration is included in Attachment D.

Section 845.230(d)(2)(D)(ii): Wetlands;

The previous wetlands demonstration was certified by a qualified professional engineer stating that the demonstration meets the requirements of 40 C.F.R. § 257.61. The requirements described in 40 C.F.R. § 257.61 are identical to the requirements contained in Section 845.310. Pursuant to Section 845.210(d)(2), a certification is not required for this demonstration. The previously completed wetlands demonstration is included in Attachment D.

Section 845.230(d)(2)(D)(iii): Fault Areas;

The previous fault area demonstration was certified by a qualified professional engineer stating that the demonstration meets the requirements of 40 C.F.R. § 257.62. The requirements described in 40 C.F.R. § 257.62 are identical to the requirements contained in Section 845.320. Pursuant to Section 845.210(d)(2), a certification is not required for this demonstration. The previously completed fault area demonstration is included in Attachment D.

Section 845.230(d)(2)(D)(iv): Seismic Impact Zone; and

The previous seismic impact zone demonstration was certified by a qualified professional engineer stating that the demonstration meets the requirements of 40 C.F.R. § 257.63. The requirements described in 40 C.F.R. § 257.63 are identical to the requirements contained in Section 845.330. Pursuant to Section 845.210(d)(2), a certification is not required for this demonstration. The previously completed seismic impact zone demonstration is included in Attachment D.

<u>Section 845.230(d)(2)(D)(v):</u> Unstable Areas and Floodplains;

The previous unstable area demonstration was certified by a qualified professional engineer stating that the demonstration meets the requirements of 40 C.F.R. § 257.64. The requirements described in 40 C.F.R. § 257.64 are identical to the requirements contained in Section 845.340. Pursuant to



Section 845.210(d)(2), a certification is not required for the unstable area demonstration. The previously completed unstable area demonstration is included in Attachment D.

The boundaries of the impoundment were determined by a survey conducted by a professional surveyor licensed in the State of Illinois. The boundaries of the Ash Pond No.1 were compared to the existing FEMA floodplain map, and it was determined that the Ash Pond No.1 is not located within the floodplain. A certification attesting to this is provided in Attachment D.

2.5. Permanent Markers

<u>Section 845.230(d)(2)(E):</u> Evidence of permanent markers required by Section 845.130 have been installed:

Evidence of permanent markers at the Coffeen Ash Pond No.1 as required by Section 845.130 is provided in Attachment E.

2.6. Slope Maintenance

<u>Section 845.230(d)(2)(F):</u> Documentation that the CCR surface impoundment, if not incised, will be operated and maintained with one of the forms of slope protection specified in Section 845.430;

The Coffeen Ash Pond No.1 is not incised. Documentation of slope protection as required by Section 845.430 is provided in Attachment J.

2.7. Initial Emergency Action Plan

<u>Section 845.230(d)(2)(G):</u> Initial Emergency Action Plan and accompanying certification (see Section 845.520(e));

The initial emergency action plan and certification has been completed as specified by Section 845.520(e) and is provided in Attachment F.

2.8. Fugitive Dust Control Plan

<u>Section 845.230(d)(2)(H):</u> Fugitive dust control plan and accompanying certification (see Section 845.500(b)(7));

The fugitive dust control plan and certification has been completed as specified by Section 845.500(b)(7) and is provided in Attachment G.



2.9. Groundwater Monitoring

Section 845.230(d)(2)(I): Groundwater monitoring information:

The groundwater monitoring information for the Coffeen Ash Pond No.1 is described in the following sections.

<u>Section 845.230(d)(2)(I)(i):</u> Hydrogeologic site characterization (see Section 845.620);

Hydrogeologic site characterization for the Coffeen Ash Pond No.1 is provided in Attachment H.

<u>Section 845.230(d)(2)(I)(ii):</u> Design and construction plans of a groundwater monitoring system (see Section 845.630);

Design and construction plans of a groundwater monitoring system are provided in Attachment I.

<u>Section 845.230(d)(2)(I)(iii):</u> A groundwater sampling and analysis program that includes selection of the statistical procedures to be used for evaluating groundwater monitoring data (see Section 845.640); and

A groundwater sampling and analysis program that meets the requirements of Section 845.640 is provided in Attachment I.

<u>Section 845.230(d)(2)(I)(iv):</u> Proposed groundwater monitoring program that includes a minimum of eight independent samples for each background and downgradient well (see Section 845.650(b));

A proposed groundwater monitoring program that meets the requirements of Section 845.650(b) is provided in Attachment I.

2.10. Initial Post-Closure Care Plan

<u>Section 845.230(d)(2)(K):</u> Initial written post-closure care plan, if applicable (see Section 845.780(d));

The Coffeen Ash Pond No.1 closure will be completed by capping the CCR in place. The initial post closure care plan was developed in accordance with Section 845.780 and is provided in Attachment K.



2.11. History of Groundwater Exceedances

<u>Section 845.230(d)(2)(M):</u> History of known exceedances of the groundwater protection standards in Section 845.600, and any corrective action taken to remediate the groundwater;

A history of known exceedances and any corrective action taken is provided in Attachment M.

2.12. Financial Assurance Requirements

<u>Section 845.230(d)(2)(N):</u> A certification that the owner or operator meets the financial assurance requirements of Subpart I;

A certification meeting the requirement of Section 845.230(d)(2)(N) stating that the Owner meets the financial assurance requirements of *Subpart I* is provided in Attachment N.

2.13. Hazard Potential Classification

<u>Section 845.230(d)(2)(O):</u> Hazard potential classification assessment and accompanying certification (see Section 845.440(a)(2));

The previous Hazard Potential Classification Assessment completed in compliance with 40 CFR §257.73(a) is provided in Attachment O. The addendum to the Hazard Potential Classification Assessment and certification as required by Section 845.440(a) is provided in Attachment U.

2.14. Structural Stability Assessment

<u>Section 845.230(d)(2)(P):</u> Structural stability assessment and accompanying certification (see Section 845.450(c));

The previous Structural Stability Assessment completed in compliance with 40 CFR §257.73(d) is provided in Attachment P. The addendum to the Structural Stability Assessment and certification as required by Section 845.450(c) is provided in Attachment U.

2.15. Safety Factor Assessment

<u>Section 845.230(d)(2)(Q):</u> Safety factor assessment and accompanying certification (see Section 845.460(b));

The previous Safety Factor Assessment completed in compliance with 40 CFR §257.73(e) is provided in Attachment Q. The addendum to the Safety Factor Assessment and certification as required by Section 845.460(b) is provided in Attachment U.



2.16. Inflow Design Flood Control System Plan

<u>Section 845.230(d)(2)(R):</u> Inflow design flood control system plan and accompanying certification (see Section 845.510(c)(3));

The previous Inflow Design Flood Control System Plan Assessment completed in compliance with 40 CFR §257.82 is provided in Attachment R. The addendum to the Inflow Design Flood Control Plan Assessmentas required by Section 845.510(c)(3) is provided in Attachment U.

2.17. Safety and Health Plan

Section 845.230(d)(2)(S): Safety and health plan (see Section 845.530); and

The safety and health plan in accordance with Section 845.530 is included in Attachment S.

2.18. Proposed Closure Priority Categorization

<u>Section 845.230(d)(2)(T):</u> For CCR surface impoundments required to close under 845.700, the proposed closure priority categorization required by Section 845.700(g).

A CCR Surface Impoundment Category Designation and Justification letter was submitted to IEPA on May 19, 2021. The Coffeen Ash Pond No.1 was designated as Category 5 Existing CCR surface impoundment with exceedances of the groundwater protection standards in Section 845.600. This letter is provided in Attachment T.



3. PERMIT APPLICATION

All permit applications must be made on the forms prescribed by the Agency and must be mailed or delivered to the address designated by the Agency on the forms. The permit applications (CCR-1 and CCR-2E) are provided below.

Form CCR 1



Illinois Environmental Protection Agency CCR Surface Impoundment Permit Application Form CCR 1 – General Provisions

| Bu | reau of | Water ID Number: | For IE | PA Use Only | |
|---|------------|---|-------------------------------|---------------------|--|
| CC | | | | | |
| - - | ailitu Ala | | | | |
| ra | cility Na | me: | | | |
| S | ECTION | 1: FACILITY, OPERATOR, AND C | WNER INFORMATION (35 III. Adn | n. Code 845.210(b)) | |
| | 1.1 | Facility Name | | | |
| | | | | | |
| | 1.2 | Illinois EPA CCR Permit Number (if ap | oplicable) | | |
| | | | | | |
| ition | 1.3 | Facility Contact Information | | | |
| | | Name (first and last) | Title | Phone Number | |
| Facility, Operator, and Owner Information | | Email address | | | |
| wner | 1.4 | Facility Mailing Address | | | |
| , and 0 | | Street or P.O. box | | | |
| perator | | City or town | State | Zip Code | |
| ty, o | 1.5 | Facility Location | | | |
| Facili | | Street, route number, or other specific | dentifier | | |
| | | County name | County code (if known) | | |
| | | City or town | State | Zip Code | |
| | 1.6 | Name of Owner/Operator | | | |
| | | | | | |

| ıfο | 1.7 | Owner/Operator Contact Ir | nformation | | |
|------------------------------------|--|--|---------------------------|--------------------|--------------------------------------|
|)wner li | | Name (first and last) | Title | | Phone Number |
| r, and C | | Email address | | | |
| erato | 1.8 | Owner/Operator Mailing Ad | ddress | | |
| Facility, Operator, and Owner Info | | Street or P.O. box | | | |
| Faci | | City or town | | State | Zip Code |
| | | SECTION 2: LEGA | L DESCRIPTION (35 | III. Adm. Code | 845.210(c)) |
| tion | 2.1 | Legal Description of the fac | ility boundary | | |
| Legal Description | | | | | |
| SE | CTION 3 | B: PUBLICLY ACCESSIBI | LE INTERNET SITE I | REQUIREMENTS | 6 (35 III. Adm. Code 845.810) |
| | 3.1 | Web Address(es) to publicly | y accessible internet sit | e(s) (CCR website) | |
| nternet Site | | | | | |
| _ | 3.2 Is/are the website(s) titled "Illinois CCR Rule Compliance Data and Information" | | | | formation" |
| | | Yes | No | | |
| | | SECTION | 4: IMPOUNDMENT | IDENTIFICATIO | N |
| ation | 4.1 | List all the impoundment ide indicate that you have attack | | | neck the corresponding box to dment. |
| Impoundment Identification | | | | Attache | ed written description |
| | | | | Attache | ed written description |
| lmen | | | | Attache | ed written description |
| punc | | | | | ed written description |
| lmpc | | | | | ed written description |
| | | | | Attache | ed written description |

| | | 1 | | | | |
|---------------------------------------|-----|---|--|--|---|--------------------------------|
| | | | Attached wri | tten desc | ription | |
| | | Attached written description | | | | |
| | | | Attached wri | tten desc | ription | |
| | | | Attached wri | tten desc | ription | |
| | | SECTION 5: CHECKLIST AND CERTIFICATION | STATEM | ENT | | |
| | 5.1 | In Column 1 below, mark the sections of Form 1 that you have application. For each section, specify in Column 2 any attachr | | | | n your |
| | | Column 1 | | | Column 2 | |
| ınt | | Section 1: Facility, Operator, and Owner Information | | w/attacl | nments | |
| teme | | Section 2: Legal Description | | w/attacl | nments | |
| Sta | | Section 3: Publicly Accessible Internet Site Requirement | | w/attacl | nments | |
| ation | | Section 4: Impoundment Identification | | w/attacl | nments | |
| tifica | 5.2 | Certification Statement | | | | |
| Checklist and Certification Statement | | I certify under penalty of law that this document and all attachmor supervision in accordance with a system designed to assure and evaluate the information submitted. Based on my inquiry system, or those persons directly responsible for gathering the to the best of my knowledge and belief, true, accurate, and consignificant penalties for submitting false information, including for knowing violations. | that qualifient of the person information inplete. I am | ed person n or perso , the infor n aware th | nel properly ons who manamation submation are | gather age the itted is, |
| | | Name (print or type first and last name) of Owner/Operator | | | Official Title | e |
| | | Signature Cyrthin E Wdy | | | Date Signe | d |

Form CCR 2E

Illinois Environmental Protection Agency



CCR Surface Impoundment Permit Application Form CCR 2E – Initial Operating Permit for Existing or Inactive CCR Surface Impoundments That Have Not Completed an Agency-approved Closure Before July 30, 2021

| | Agonoy approvod Glocal | bololo daly do, zoz i |
|----------------------------|------------------------|-----------------------|
| Bureau of Water ID Number: | | For IEPA Use Only |
| CCR Perr | mit Number: | |
| Facility N | ame: | |

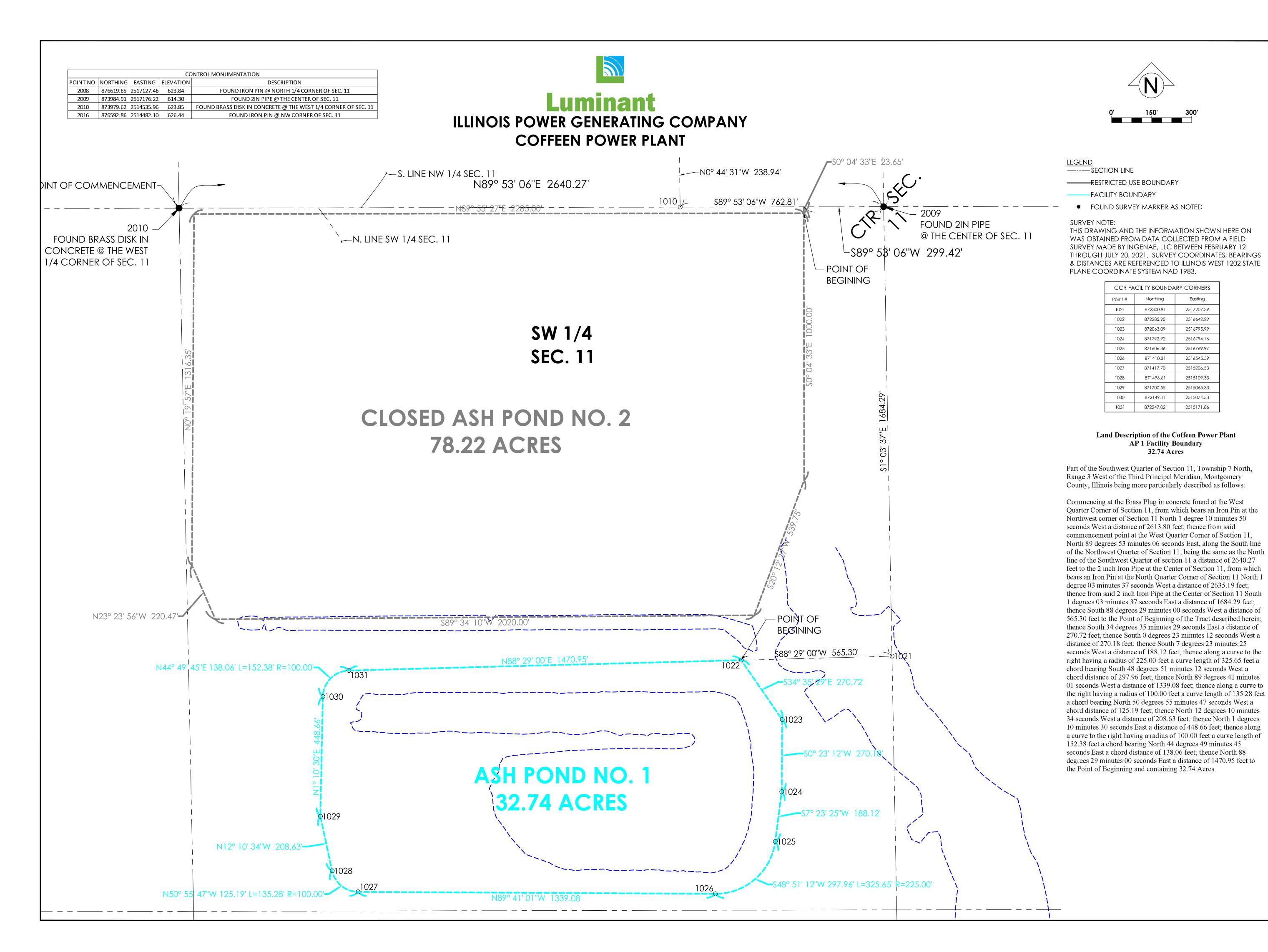
| SEC | TION 1: | CONSTRUCTION HISTORY (35 III. Adm. Code 845.220 AND 35 III. Adm. Code 845.230) |
|----------------------|---------|--|
| | 1.1 | CCR surface impoundment name. |
| | 1.2 | Identification number of the CCR surface impoundment (if one has been assigned by the Agency). |
| listory | 1.3 | Description of the boundaries of the CCR surface impoundment (35 III. Adm. Code 845.210(c)). |
| Construction History | 1.4 | State the purpose for which the CCR surface impoundment is being used. |
| | 1.5 | How long has the CCR surface impoundment been in operation? |
| | 1.6 | List the types of CCR that have been placed in the CCR surface impoundment. |
| | | |

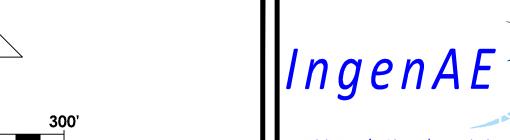
| | 1.7 | List name of the watershed within which the CCR surface impoundment is located. | | | |
|----------------------------------|--------|--|--|--|--|
| | | | | | |
| | 1.8 | Size in acres of the watershed within which the CCR surface impoundment is located. | | | |
| | | | | | |
| | 1.9 | Check the corresponding box to indicate that you have attached the following: | | | |
| | | Description of the physical and engineering properties of the foundation and abutment materials on which the CCR surface impoundment is constructed. | | | |
| | | Description of the type, size, range, and physical and engineering properties of the materials used in constructing each zone or stage of the CCR surface impoundment. | | | |
| (pər | | Describe the method of site preparation and construction of each zone of the CCR surface impoundment. | | | |
| Construction History (Continued) | | A listing of the approximate dates of construction of each successive stage of construction of the CCR surface impoundment. | | | |
| ory (| | Drawing satisfying the requirements of 35 III. Adm. Code 845.220(a)(1)(F). | | | |
| Hist | | Description of the type, purpose, and location of existing instrumentation. | | | |
| tion | | Area capacity curves for the CCR Impoundment. | | | |
| nstruc | | Description of each spillway and diversion design features and capacities and provide the calculations used in their determination. | | | |
| ပိ | | Construction specifications and provisions for surveillance, maintenance, and repair of the CCR surface impoundment. | | | |
| | 1.10.1 | Is there any record or knowledge of structural instability of the CCR surface impoundment? | | | |
| | | Yes No | | | |
| | 1.10.2 | If you answered yes to Item 1.10.1, provide detailed explanation of the structural instability. | | | |
| | | See Attachment B. | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | N 2: ANALYSIS OF CHEMICAL CONSTITUENTS (35 III. Adm. Code 845.230(d)(2)(B)) | | | |
| ents | 2.1 | Check the corresponding boxes to indicate you have attached the following: | | | |
| Constituents | | An analysis of the chemical constituents found within the CCR to be placed in the CCR surface impoundment. | | | |
| Con | | An analysis of the chemical constituents of all waste streams, chemical additives and sorbent materials entering or contained in the CCR surface impoundment. | | | |

| | SECTIO | ON 3: DEMONSTRATIONS AND CERTIFICATIONS | TIONS (35 III. Adm. Code 8 | 345.230(d)(2)(D)) | | | |
|--|--------|--|---------------------------------|------------------------|--|--|--|
| | 3.1 | Indicate whether you have attached a demonstrative meets, or an explanation of how the CCR surface the following sections: | | | | | |
| Demonstrations | | 35 III. Adm. Code 845.300 (Placement Above the Uppermost Aquifer) | Demonstration | Explanation | | | |
| stra | | 35 III. Adm. Code 845.310 (Wetlands) | Demonstration | Explanation | | | |
| mon | | 35 III. Adm. Code 845.320 (Fault Areas) | Demonstration | Explanation | | | |
| 35 III. Adm. Code 845.330 (Seismic Impact Zones) | | Demonstration | Explanation | | | | |
| | | 35 III. Adm. Code 845.340 (Unstable Areas and Floodplains) | Demonstration | Explanation | | | |
| | | SECTION 4: ATTA | CHMENTS | | | | |
| | 4.1 | Check the corresponding boxes to indicate that y | ou have attached the following | g: | | | |
| | | Evidence that the permanent markers re installed. | quired by 35 III. Adm. Code 84 | 5.130 have been | | | |
| | | pe operated and Adm. Code 845.430. | | | | | |
| | | by 35 III. Adm. Code | | | | | |
| ents | | Fugitive dust control plan and accompanying certification required by 35 III. Adm. Code 845.500(b)(7). Preliminary written closure plan as specified in 35 III. Adm. Code 845.720(a). | | | | | |
| hm | | | | | | | |
| Attachments | | 45.780(d), if applicable. | | | | | |
| , | | A certification as specified in 35 III. Adm. impoundment does not have a liner than 845.400(b) or (c). | | | | | |
| | | History of known exceedances of the gro 845.600, and any corrective action taken | | | | | |
| | | Safety and health plan, as required by 35 | 5 III. Adm. Code 845.530. | | | | |
| | | For CCR surface impoundments require proposed closure priority categorization | | | | | |
| | | SECTION 5: GROUNDWATER MONITORING | | | | | |
| Groundwater | 5.1 | Check the corresponding boxes to indicate you hinformation: | ave attached the following gro | undwater monitoring | | | |
| nnd | | A hydrogeologic site characterization me | eting the requirements of 35 II | I. Adm. Code 845.620. | | | |
| Gro | | Design and construction plans of a groun of 35 III. Adm. Code 845.630. | ndwater monitoring system me | eting the requirements | | | |

| | | A groundwater sampling and analysis program that includes section of the statistical procedures to be used for evaluating groundwater monitoring data, required by 35 III. Adm. Code 845.640. |
|----------------|-----|---|
| | | Proposed groundwater monitoring program that includes a minimum of eight independent samples for each background and downgradient well, required by 35 III. Adm. Code 845.650(b). |
| | | SECTION 6: CERTIFICATIONS |
| | 6.1 | Check the corresponding boxes to indicate you have attached the following certifications: |
| v | | A certification that the owner or operator meets the financial assurance requirements of Subpart I, as required by 35 III. Adm. Code 845.230(d)(2)(N). |
| Certifications | | Hazard potential classification assessment and accompanying certifications required by 35 III. Adm. Code 845.440(a)(2). |
| Certifi | | Structural stability assessment and accompanying certification, required by 35 III. Adm. Code 845.450(c). |
| | | Safety factor assessment and accompanying certification, as required by 35 III. Adm. Code 845.460(b). |
| | | Inflow design flood control system plan and accompanying certification, as required by 35 III. Adm. Code 845.510(c)(3). |

ATTACHMENT A





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Submissions / Revisions:



Project Name & Location:

COFFEEN POWER PLANT

134 CIPS Lane Coffeen, IL 62017

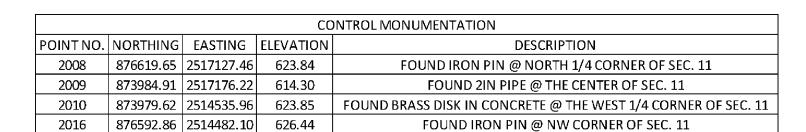
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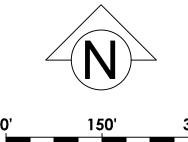
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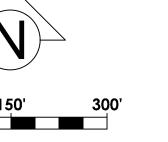
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ILLINOIS POWER GENERATING COMPANY





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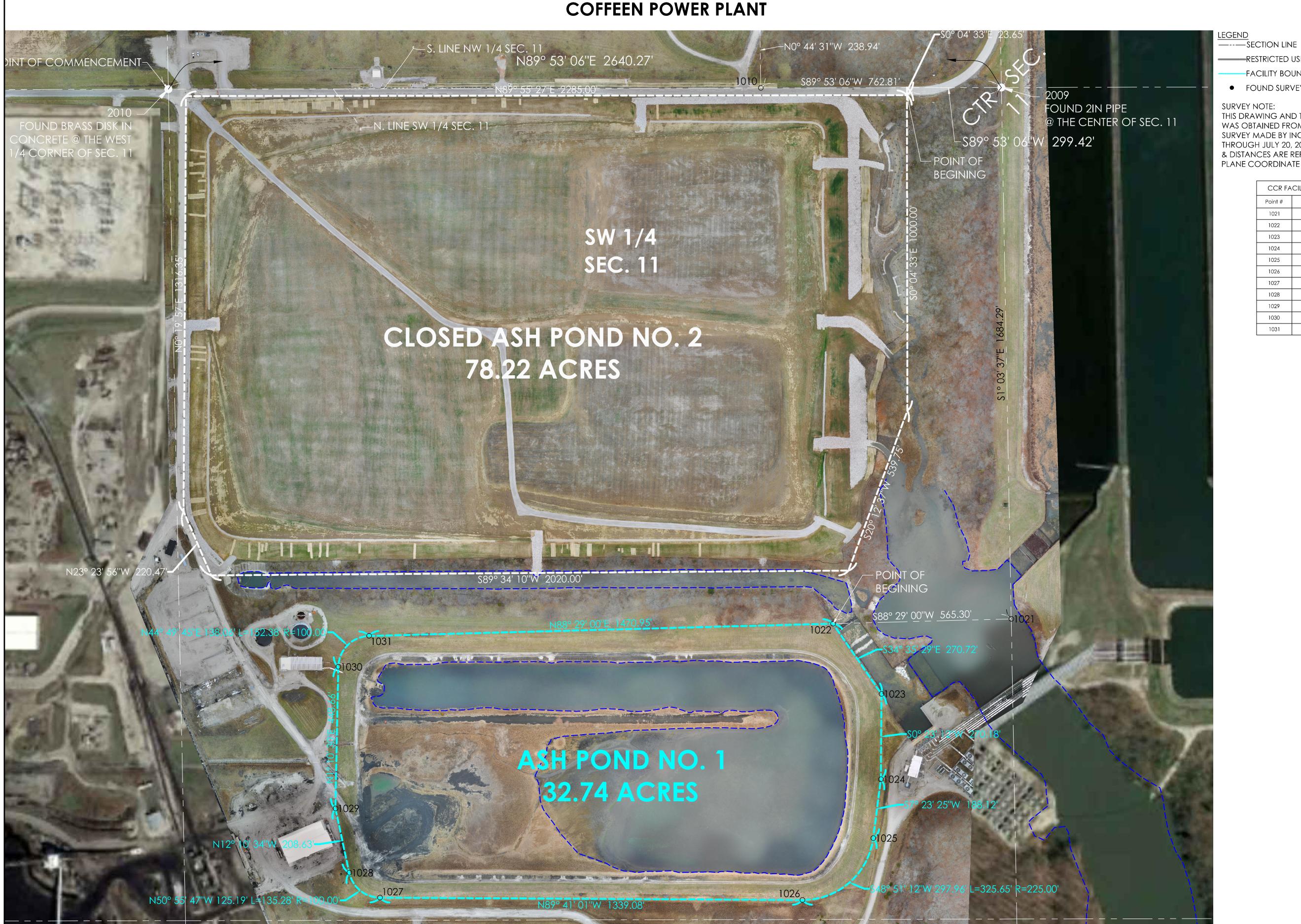
COFFEEN POWER PLANT

134 CIPS Lane Coffeen, IL 62017

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ATTACHMENT B



October 2016

Illinois Power Generating Company 134 CIPS Lane Coffeen, IL 62017

RE: History of Construction

USEPA Final CCR Rule, 40 CFR § 257.73(c)

Coffeen Power Station

Coffeen, Illinois

On behalf of Illinois Power Generating Company, AECOM has prepared the following history of construction for Ash Pond No. 1, Ash Pond No. 2, the GMF Pond, and the GMF Recycle Pond at the Coffeen Power Station in accordance with 40 CFR § 257.73(c).

BACKGROUND

40 CFR § 257.73(c)(1) requires the owner or operator of an existing coal combustion residual (CCR) surface impoundment that either (1) has a height of five feet or more and a storage volume of 20 acre-feet or more, or (2) has a height of 20 feet or more to compile a history of construction by October 17, 2016 that contains, to the extent feasible, the information specified in 40 CFR § 257.73(c)(1)(i)–(xii).

The history of construction presented herein was compiled based on existing documentation, to the extent that it is reasonably and readily available (see 80 Fed. Reg. 21302, 21380 [April 17, 2015]), and AECOM's site experience. AECOM's document review included record drawings, geotechnical investigations, construction specifications, etc. for Ash Pond No. 1, Ash Pond No. 2, the GMF Pond, and the GMF Recycle Pond at the Coffeen Power Station.



HISTORY OF CONSTRUCTION

§ 257.73(c)(1)(i): The name and address of the person(s) owning or operating the CCR unit; the name associated with the CCR unit; and the identification number of the CCR unit if one has been assigned by the state.

Owner: Illinois Power Generating Company

Address: 1500 Eastport Plaza Drive

Collinsville, IL 62234

CCR Units: Ash Pond No. 1

Ash Pond No. 2

GMF Pond, IDNR Dam ID No. IL50579

GMF Recycle Pond, IDNR Dam ID No. IL50578

Ash Pond No. 1 and Ash Pond No. 2 do not have a state assigned identification number.

§ 257.73(c)(1)(ii): The location of the CCR unit identified on the most recent USGS $7^{1}/_{2}$ or 15 minute topographic quadrangle map or a topographic map of equivalent scale if a USGS map is not available.

The locations of Ash Pond No. 1, Ash Pond No. 2, the GMF Pond, and the GMF Recycle Pond have been identified on an USGS 7-1/2 minute topographic quadrangle map in **Appendix A**.

§ 257.73(c)(1)(iii): A statement of the purpose for which the CCR unit is being used.

The following captures the purposes of the CCR units:

- Ash Pond No. 1 is being used to store and dispose of bottom ash and other-non-CCR waste and to clarify recycled process water for plant operations. Ash Pond No. 2 (inactive) was used to store and dispose of bottom ash and fly ash.
- The GMF Pond is being used to store and dispose of gypsum and to clarify recycled process water for plant operations.
- The GMF Recycle Pond was used to store and dispose of gypsum from the plant's scrubber operations prior to the in-service date of the GMF Pond in 2010. The GMF Recycle Pond currently only receives and stores clear process water from the GMF Pond.

Notice of intent to close Ash Pond No. 2 was provided in November, 2015.1

¹ This history of construction report was prepared on a facility-wide basis for CCR surface impoundments at the Coffeen Power Station. The inclusion of Ash Pond No. 2 in this history of construction report does not concede and should not be construed to concede that Ash Pond No. 2 is subject to the Design Criteria or all Operating Criteria in the CCR Rule.



§ 257.73(c)(1)(iv): The name and size in acres of the watershed where the CCR unit is located.

Ash Pond No. 1, Ash Pond No. 2, the GMF Pond, and the GMF Recycle Pond are located in the Coffeen Lake Watershed with a 12-digit Hydrologic Unit Code (HUC) of 071402030304 and a drainage area of 11,695 acres (USGS, 2016).

§ 257.73(c)(1)(v): A description of the physical and engineering properties of the foundation and abutment materials on which the CCR unit is constructed.

The foundation and abutment materials of Ash Pond No. 1, Ash Pond No. 2, the GMF Pond, and the GMF Recycle Pond consist of native fine-grained soils of wind-blown origin (loess), with some coarse-grained layers, underlain by glacial till. The physical properties of the finegrained soils are described as low- to medium-plasticity silty clay, sandy lean clay, or lean clay with sand, often with trace amounts of gravel; or high plasticity fat clay, often with trace amounts of sand. The clay soils vary from soft to very stiff, moist to wet, and brown to gray. The physical properties of the coarse-grained soils are described as clayey sand, silty sand, or fine to coarse sand, with trace amounts of gravel. The sand is wet and varies from loose to dense and brown to gray. A thin layer of native silty or sandy lean clay is located immediately above the glacial till deposits. The clay is very soft to medium stiff, low to medium plasticity, wet, and orange brown to gray. The physical properties of the glacial till are described as lean clay, or silty to sandy lean clay, with trace amounts of fine gravel, hard, low plasticity, moist to wet, and brown to gray. An available summary of the engineering property typical ranges of the foundation and abutment materials is presented in Table 1 below. The engineering properties are based on previous geotechnical explorations and laboratory testing.

Ash Pond No. 1 and Ash Pond No. 2 are enclosed impoundments with embankments and do not have abutments. The GMF Pond and GMF Recycle Pond were constructed as incised impoundments enclosed by embankments.

Table 1. Summary of Foundation and Abutment Material Engineering Properties

| Material | Unit Weight | | rained) Shear Parameters | Total (undrained) Shear Strength Parameters | Post-Earthquake Shear Strength |
|------------------------------------|----------------|--------------------|--------------------------------|--|---|
| | (pcf) | Cohesion, c' (psf) | Friction Angle, ¢' (deg) | S _u /p' | S _{ur} /p' |
| Foundation Clay (Under Embankment) | 125 | 0 | 32 | $S_u/p' = 0.39-0.45$, Min. $S_u = 700 \text{ psf}$ | Peak Undrained |
| Foundation Clay (Free Field) | 125 | 0 | 30 | $S_u/p' = 0.24-0.28$, Min. $S_u = 450 \text{ psf}$ | Peak Undrained |
| Soft Foundation Clay | 125 | 0 | 30 | $S_u/p' = 0.22-0.28$, Min. $S_u = 275 \text{ psf}$ | $S_u/p' = 0.13-0.16$, Min. $S_{ur} = 200 \text{ psf}$ |
| Glacial Till | 135 | 0 | 40 | $S_u/p' = 0.45-0.64$, Min. $S_u = 700 \text{ psf}$ | Peak Undrained |



§ 257.73(c)(1)(vi): A statement of the type, size, range, and physical and engineering properties of the materials used in constructing each zone or stage of the CCR unit; the method of site preparation and construction of each zone of the CCR unit; and the approximate dates of construction of each successive stage of construction of the CCR unit.

Physical properties for the embankment construction materials for Ash Pond No. 1, Ash Pond No. 2, GMF Pond, and GMF Recycle Pond are described as silty clay, sandy lean clay, or lean clay with sand, with trace amounts of fine gravel. The fill is soft to very stiff in consistency, low to medium plasticity, moist to wet, and brown to gray. Trace amounts of organic material and ash are present. The embankment fill generally appears to be well-compacted. An available summary of the engineering properties of the embankment construction materials is presented in **Table 2** below. The engineering properties are based on previous geotechnical explorations and laboratory testing.

Table 2. Summary of Construction Material Engineering Properties for Embankments

| Material | Unit Weight | | Peak Drained Peak Undi Shear Strength Shear Stre | | Post- Earthquake Shear Strength |
|-----------------|----------------|--------------------------|---|---|---------------------------------------|
| Material | (pcf) | Cohesion, c' (psf) | Friction Angle, f' (deg) | S _u /p' | S _{ur} /p' |
| Embankment Fill | 135 | 0 | 31 | $S_u/p' = 0.60$, Min. $S_u = 450 \text{ psf}$ | Peak Undrained |

The GMF Pond and GMF Recycle Pond contain liner systems. The liner system within the GMF Pond consists of a 60-mil textured high density polyethylene (HDPE) geomembrane underlain by a 3-foot thick layer of compacted clay. A typical cross section profile of the GMF Pond liner system is shown on drawing C-10206 (sh. 9) presented in **Appendix B**. An available summary of the engineering properties of the GMF Pond liner construction materials from Hanson (2008) is presented in **Table 3** below. The liner system within the GMF Recycle Pond consists of a 60-mil textured HDPE geomembrane underlain by smooth-drum rolled native soil. A typical cross section profile of the GMF Recycle Pond liner system is shown on drawing C-10206 (sh. 20) presented in **Appendix B**.

Table 3. Summary of Construction Material Engineering Properties for Liner

| Material | Unit Weight | Effective (dr Strength F | ained) Shear Parameters | Total (undrained) Shea Strength Parameters | |
|------------|----------------|-----------------------------|----------------------------|---|-------|
| | (pcf) | c' (psf) | Ф' (°) | c (psf) | Ф (°) |
| Clay Liner | 121.2 | 0 | 28.3 | 1950 | 0 |

The method of site preparation and construction of Ash Pond No. 1 and Ash Pond No. 2 is not reasonably and readily available. Site preparation and construction of the GMF Pond and GMF Recycle Pond were completed in accordance with the applicable construction specification (see § 257.73(c)(1)(xi) below).



The approximate dates of construction of each successive stage of construction of Ash Pond No. 1, Ash Pond No. 2, the GMF Pond, and the GMF Recycle Pond are provided in **Table 4** below.

Table 4. Approximate dates of construction of each successive stage of construction.

| Date | Event | | |
|-----------|--|--|--|
| 1964 | Construction of Ash Pond No. 1 | | |
| 1971 | Construction of Ash Pond No. 2 | | |
| 1978-1979 | Installation of internal embankment and new recycle intake structure in Ash Pond No. 1 and abandonment of existing outfall structure | | |
| 1984-1985 | Closure of Ash Pond No. 2 by installing a clay cover | | |
| 2000 | Installation of a sheet pile wall to facilitate construction of drainage flume along the northeast corner of the Ash Pond No. 1 | | |
| 2009 | Installation of well dewatering system in Ash Pond No. 2 | | |
| 2008-2010 | Construction of the GMF Pond and the GMF Recycle Pond | | |

§ 257.73(c)(1)(vii): At a scale that details engineering structures and appurtenances relevant to the design, construction, operation, and maintenance of the CCR unit, detailed dimensional drawings of the CCR unit, including a plan view and cross sections of the length and width of the CCR unit, showing all zones, foundation improvements, drainage provisions, spillways, diversion ditches, outlets, instrument locations, and slope protection, in addition to the normal operating pool surface elevation and the maximum pool surface elevation following peak discharge from the inflow design flood, the expected maximum depth of CCR within the CCR surface impoundment, and any identifiable natural or manmade features that could adversely affect operation of the CCR unit due to malfunction or mis-operation.

Drawings that contain items pertaining to the requested information for Ash Pond No. 1, Ash Pond No. 2, the GMF Pond, and the GMF Recycle Pond are listed in **Table 5** below. Items marked as "Not Available" are items not found during a review of the reasonably and readily available record documentation.



Table 5. List of drawings containing items pertaining to the information requested in

§ 257.73(c)(1)(vii).

| § 257.73(C)(1)(VII). | | | | |
|--|-----------------------|-------------------------|-----------------------------|------------------------|
| | Ash Pond No. 1 | Ash Pond No. 2 GMF Pond | | GMF Recycle Pond |
| Dimensional plan view (all zones) | B-35, S-44, S-45 | B-560, A1000 (sh. 1) | C-10206 (sh. 4, 9, 10) | C-10206 (sh. 4, 19) |
| Dimensional cross sections | B-35, S-47 to S-50 | B-561 | C-10206 (sh. 9) | C-10206 (sh. 20) |
| Foundation Improvements | Not Applicable | Not Applicable | C-10206 (sh. 10) | C-10206 (sh. 20) |
| Drainage Provisions | Not Applicable | A1000 (sh. 4) | C-10206 (sh. 15, 16, 20) | C-10206 (sh. 21) |
| Spillways and Outlets | S-8, S-49 | W1008 (sh. 2) | C-10206 (sh. 20) | C-10206 (sh. 22) |
| Diversion Ditches | Not Applicable | A1000 (sh. 1) | Not Applicable | Not Applicable |
| Instrument Locations | Plate 2, Figure 2A | Figure 2B | Not Applicable | C-10206 (sh. 19) |
| Slope Protection | S-49 | B-561 | C-10206 (sh. 9) | C-10206 (sh. 20) |
| Normal Operating Pool Elevation | S-8, S-49 | Not Applicable | C-10201-25 | Not Available |
| Maximum Pool Elevation | S-8 | Not Applicable | C-10201-25 | Not Available |
| Approximate Maximum Depth of CCR in 2016 | 15 feet | 28 feet | 16 feet | 12 feet |

All drawings referenced in **Table 5** above can be found in **Appendix B** and **Appendix C**.

Based on the review of the drawings listed above, no natural or manmade features that could adversely affect operation of these CCR units due to malfunction or mis-operation were identified.



§ 257.73(c)(1)(viii): A description of the type, purpose, and location of existing instrumentation.

Existing instrumentation at Ash Pond No. 1 and Ash Pond No. 2 include vibrating-wire and open-standpipe piezometers. The purpose of the piezometers is to measure the phreatic surface within and around the impoundments. Two (2) open-standpipe piezometers (AP-P1 and AP-P2) were installed at Ash Pond No. 2 in 2009 and the locations are presented on Figure 2A in **Appendix C**. Two (2) open-standpipe piezometers (B-2 and B-4) were installed at Ash Pond No. 1 in 2010 and the locations are presented on Plate 2 in **Appendix C**. Twelve (12) open-standpipe and vibrating-wire piezometers were installed at Ash Pond No. 1 and Ash Pond No. 2 in 2015 and the locations are presented on Figure 2A in **Appendix C**.

The GMF Pond does not contain existing instrumentation. Existing instrumentation at the GMF Recycle Pond consists of one (1) ultrasonic level transmitter. The purpose of the ultrasonic level transmitter is to measure the water level within the GMF Recycle Pond. The location of the ultrasonic level transmitter is shown on drawing C-10206 (sh. 19) presented in **Appendix B**.

§ 257.73(c)(1)(ix): Area-capacity curves for the CCR unit.

Area-capacity curves for Ash Pond No. 2 and the GMF Recycle Pond are not reasonably and readily available. The area-capacity curves for Ash Pond No. 1 and the GMF Pond are presented in **Figures 1** and **2**, respectively, below. "Area-capacity curves", as defined by 40 CFR § 257.53, "means graphic curves which readily show the reservoir water surface area, in acres, at different elevations from the bottom of the reservoir to the maximum water surface, and the capacity or volume, in acre-feet, of the water contained in the reservoir at various elevations."

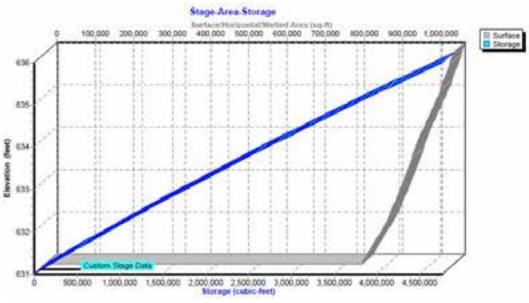


Figure 1. Area-capacity curve for Ash Pond No. 1



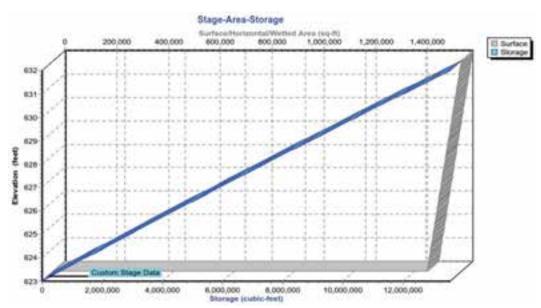


Figure 2. Area-capacity curve for GMF Pond

The area-capacity curves shown were taken from the pond modeling analysis. Actual pond capacity is limited to the approximate berm elevation listed in **Table 6** below. Any information above berm elevation should be disregarded.

§ 257.73(c)(1)(x): A description of each spillway and diversion design features and capacities and calculations used in their determination.

Ash Pond No. 1 contains a concrete intake structure that drains into a 48-inch diameter (dia.) steel pipe. The steel pipe leads to the recycle pump house. In 2016, the discharge capacity of Ash Pond No. 1 was evaluated using HydroCAD 10 software modeling a 1,000-year, 24-hour rainfall event. The results of the HydroCAD 10 analysis are presented below in **Table 6**.

Ash Pond No. 2 was closed in 1984-1985 by installing a clay cover. Non-contact stormwater is collected in ditches along the clay cover and drain off the pond cover via concrete-lined ditch outlets. CCR-contact stormwater collected within the pond is pumped into the GMF Pond via the well dewatering system at the discretion of plant personnel. The capacity of the diversion ditches and well pumps during a model rainfall event has not been evaluated.

The GMF Pond contains a 14-inch high-density polyethylene (HDPE) pipe culvert for normal flow and a weir-like spillway for high water flow. The GMF Pond also contains a 10-inch dia. HDPE siphon pipe used for dewatering. In 2016, the discharge capacity of the GMF Pond was evaluated using HydroCAD 10 software modeling a 1,000-year, 24-hour rainfall event. The results of the HydroCAD 10 analysis are presented below in **Table 6**.

The GMF Recycle Pond contains a decant structure that drains into two (2) 18-inch dia. HDPE pipes that lead to a pump house. The capacity of the decant structure during a model rainfall event has not been evaluated.



Table 6. Results of HydroCAD 10 analyses

| | Ash Pond No. 1 | GMF Pond |
|--|----------------|----------|
| Approximate Minimum Berm Elevation ¹ (ft) | 635.0 | 631.0 |
| Approximate Emergency Spillway Elevation ¹ (ft) | Not Applicable | 624.0 |
| Starting Pool Elevation ¹ (ft) | 631.0 | 621.2 |
| Peak Elevation ¹ (ft) | 632.0 | 623.8 |
| Time to Peak (hr) | 24.4 | 24.1 |
| Surface Area (ac) | 20.4 | 33.4 |
| Storage ² (ac-ft) | 19.5 | 88.3 |

Note:

- 1. Elevations are based on NAVD88 datum
- 2. Storage given is from Starting Pool Elevation to Peak Elevation.

§ 257.73(c)(1)(xi): The construction specifications and provisions for surveillance, maintenance, and repair of the CCR unit.

The construction specifications for Ash Pond No. 1 and Ash Pond No. 2 are not reasonably and readily available. The construction specifications for the GMF Pond and the GMF Recycle Pond are located in *Project Specifications, Gypsum Stack and Recycle Pond Construction* presented in **Appendix D**.

The provisions for surveillance, maintenance, and repair of Ash Pond No. 1 are located in *Operation & Maintenance Manual for #1 Ash Pond* presented in **Appendix E**. The provisions for surveillance, maintenance, and repair of Ash Pond No. 2 are not reasonably and readily available. The provisions for surveillance, maintenance, and repair of the GMF Pond and the GMF Recycle Pond are located in *Operation and Maintenance Manual, Gypsum Management Facility* presented in **Appendix F**.

The operations and maintenance plans for the CCR units identified in this report are currently being revised by Illinois Power Generating Company.

§ 257.73(c)(1)(xii): Any record or knowledge of structural instability of the CCR unit.

In March, 2009, shallow sloughing was observed along the eastern embankment of Ash Pond No. 2. The sloughing was inspected by Hanson Professional Services Inc. A dewatering



system was installed in Ash Pond No. 2 to lower the phreatic surface within the pond. In December, 2015, additional sloughing was observed on the embankment of Ash Pond No. 2 and on the embankment of Ash Pond No. 1. The sloughing was believed to be caused by recent heavy rains and was repaired. Photos of the 2015 sloughing repair are presented in Appendix G.

There is no record or knowledge of structural instability at the GMF Pond and the GMF Recycle Pond at Coffeen Power Station.

LIMITATIONS

The signature of AECOM's authorized representative on this document represents that to the best of AECOM's knowledge, information and belief in the exercise of its professional judgment, it is AECOM's professional opinion that the aforementioned information is accurate as of the date of such signature. Any recommendation, opinion or decisions by AECOM are made on the basis of AECOM's experience, qualifications and professional judgment and are not to be construed as warranties or guaranties. In addition, opinions relating to environmental, geologic, and geotechnical conditions or other estimates are based on available data and that actual conditions may vary from those encountered at the times and locations where data are obtained, despite the use of due care.

Sincerely,

Claudia Prado

Program Manager

Victor Modeer, P.E., D.GE Senior Project Manager



REFERENCES

Hanson Professional Services Inc. (2008), Support Document for IDNR/OWR Permit Application, Coffeen Power Generating Station Gypsum Management Facility Montgomery County, Illinois

United States Environmental Protection Agency (USEPA). (2015). *Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals From Electric Utilities; Final Rule.* 40 CFR Parts 257 and 261, 80 Fed. Reg. 21302, 21380 April 17, 2015.

United States Geological Survey (USGS). (2016). The National Map Viewer. http://viewer.nationalmap.gov/viewer/. USGS data first accessed in March of 2016.

APPENDICES

Appendix A: History of Construction Vicinity Map Appendix B: Coffeen Power Station Drawings

Appendix C: Coffeen Power Station Boring and Piezometer Locations

Appendix D: Project Specifications, Gypsum Stack and Recycle Pond Construction (Hanson 2008)

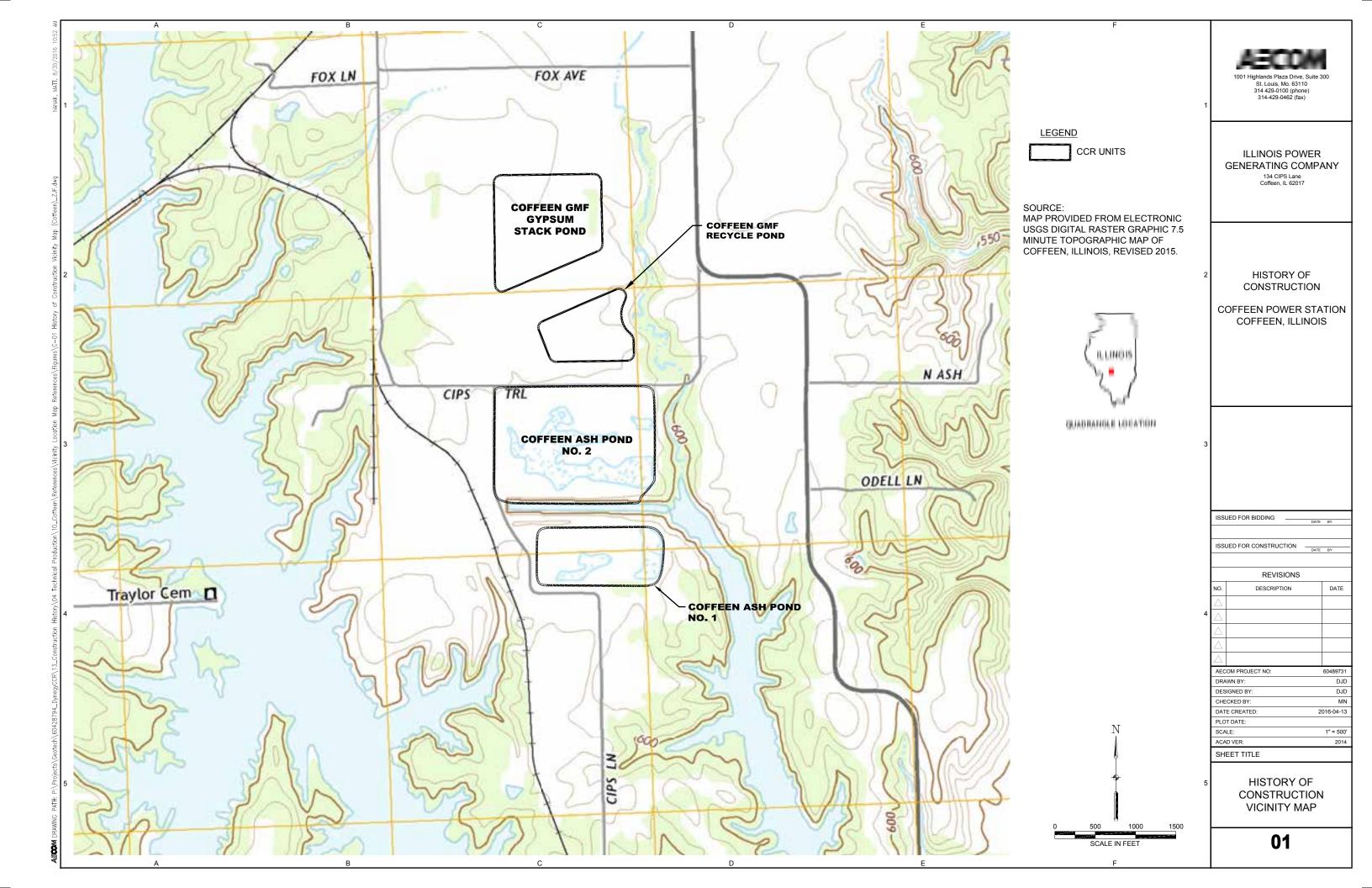
Appendix E: Operation & Maintenance Manual for #1 Ash Pond

Appendix F: Operation and Maintenance Manual, Gypsum Management Facility Operation (2015)

Appendix G: Photos of 2015 Sloughing Repair



Appendix A: History of Construction Vicinity Map





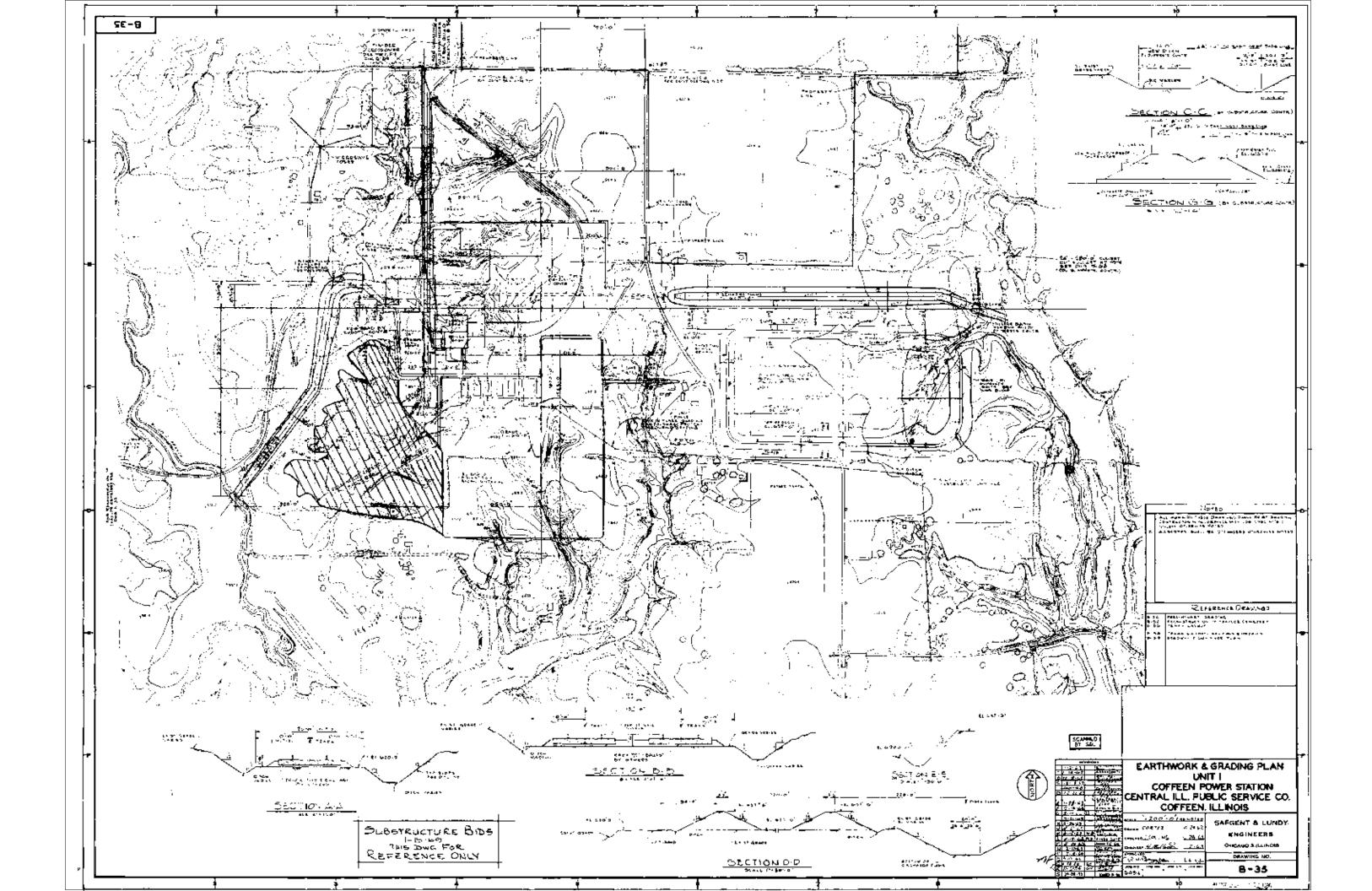
Appendix B: Coffeen Power Station Drawings

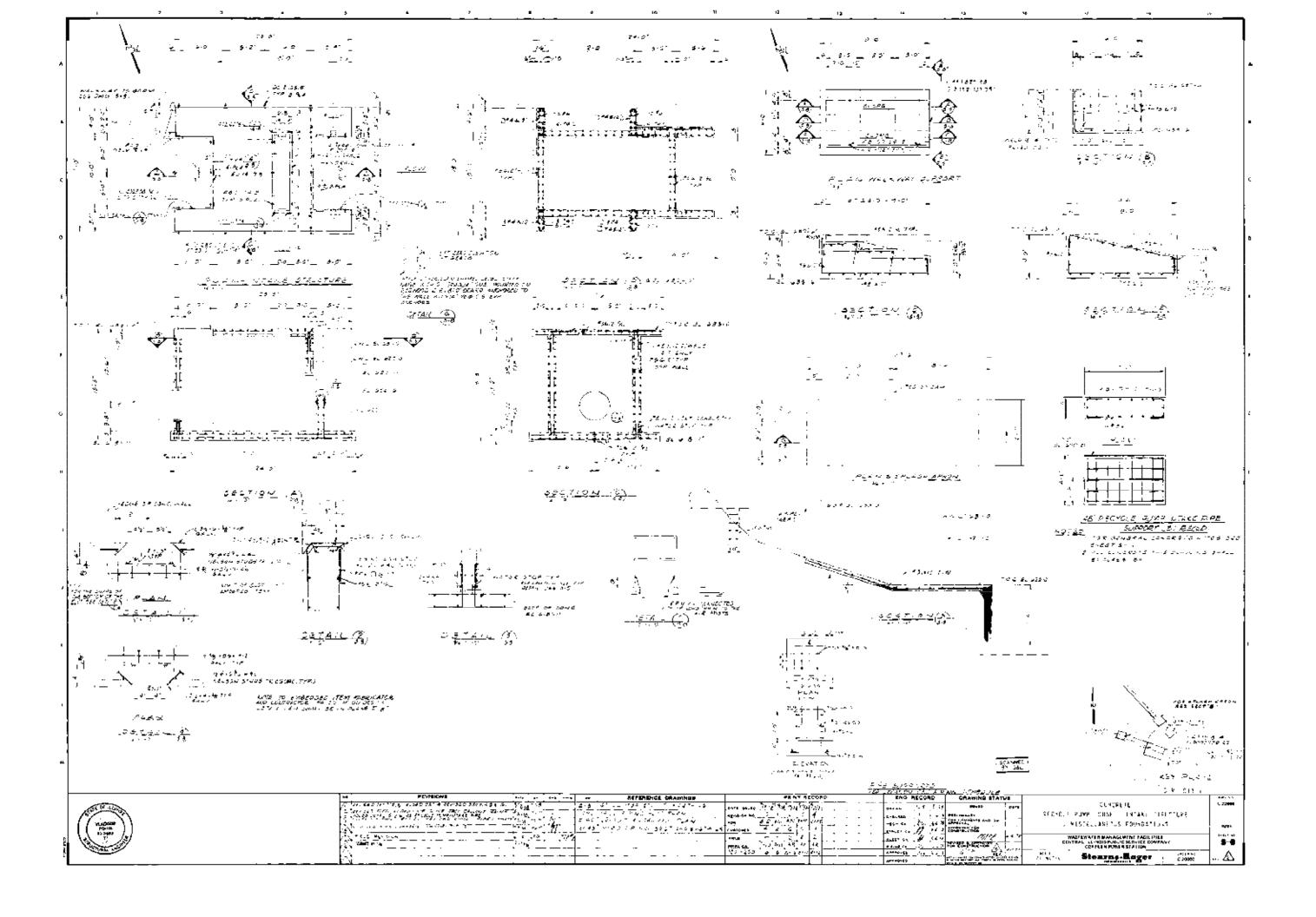
- 1. "Earthwork & Grading Plan", Drawing No. B-35, Revision S, 8 September, 1995, Sargent & Lundy Engineers.
- 2. "Concrete Recycle Pump House Intake Structure", Drawing No. S-8, Revision 6, 23 February, 1996, Stearns-Roger Incorporated.
- 3. "Civil Layout & Grading Plan Sheet 4", Drawing No. S-44, Revision 6, 23 February, 1996, Stearns-Roger Incorporated.
- 4. "Civil Layout & Grading Plan Sheet 5", Drawing No. S-45, Revision 9, 23 February, 1996, Stearns-Roger Incorporated.
- 5. "Civil Miscellaneous Sections and Details, Sheet 2", Drawing No. S-47, Revision 2, 23 February, 1996, Stearns-Roger Incorporated.
- 6. "Civil Ash Pond No 1 Sections and Details", Drawing No. S-48, Revision 2, 23 February, 1996, Stearns-Roger Incorporated.
- 7. "Civil Miscellaneous Sections and Details, Sheet 4", Drawing No. S-49, Revision 4, 23 February, 1996, Stearns-Roger Incorporated.
- 8. "Civil Miscellaneous Sections and Details", Drawing No. S-50, Revision 4, 23 February, 1996, Stearns-Roger Incorporated.
- 9. "Ash Storage Area, Plan", Drawing No. B-560, Revision A, 9 February, 1971, Sargent & Lundy Engineers.
- 10. "Ash Storage Area, Sections & Details", Drawing No. B-561, Revision A, 9 February, 1971, Sargent & Lundy Engineers.
- 11. "Overall Site Plan, Dewatering System, Ash Pond #2", Drawing No. A1000 (sh. 1), Revision A, 12 October, 2009, Ameren Energy Resources Generating.
- 12. "Site Details, Dewatering System, Ash Pond #2", Drawing No. A1000 (sh. 4), Revision A, 12 October, 2009, Ameren Energy Resources Generating.
- 13. "Proposed Site Plan, CCB Management Facility", Drawing No. C-10206 (sh. 4), Revision 0, 5 January, 2011, Ameren Energy Generating.
- 14. "Groundwater Monitoring & Boring Plan, CCB Management Facility", Drawing No. C-10206 (sh. 5), Revision 0, 5 January, 2011, Ameren Energy Generating.
- 15. "Anchor Trench and Liner System, CCB Management Facility", Drawing No. C-10206 (sh. 9), Revision 0, 5 January, 2011, Ameren Energy Generating.
- 16. "Cell G1-Foundation Grade & Control Data, CCB Management Facility", Drawing No. C-10206 (sh. 10), Revision 0, 5 January, 2011, Ameren Energy Generating.
- 17. "Cell G1-Process Water Recovery System, CCB Management Facility", Drawing No. C-10206 (sh. 15), Revision 0, 5 January, 2011, Ameren Energy Generating.
- 18. "Cell G1-PWRS Drain Details, CCB Management Facility", Drawing No. C-10206 (sh. 16), Revision 0, 5 January, 2011, Ameren Energy Generating.
- 19. "Recycle Pond Plan & Control Data, CCB Management Facility", Drawing No. C-10206 (sh. 19), Revision 0, 5 January, 2011, Ameren Energy Generating.
- 20. "Recycle Pond Process Water Transfer Channel Details, CCB Management Facility", Drawing No. C-10206 (sh. 20), Revision 0, 5 January, 2011, Ameren Energy Generating.

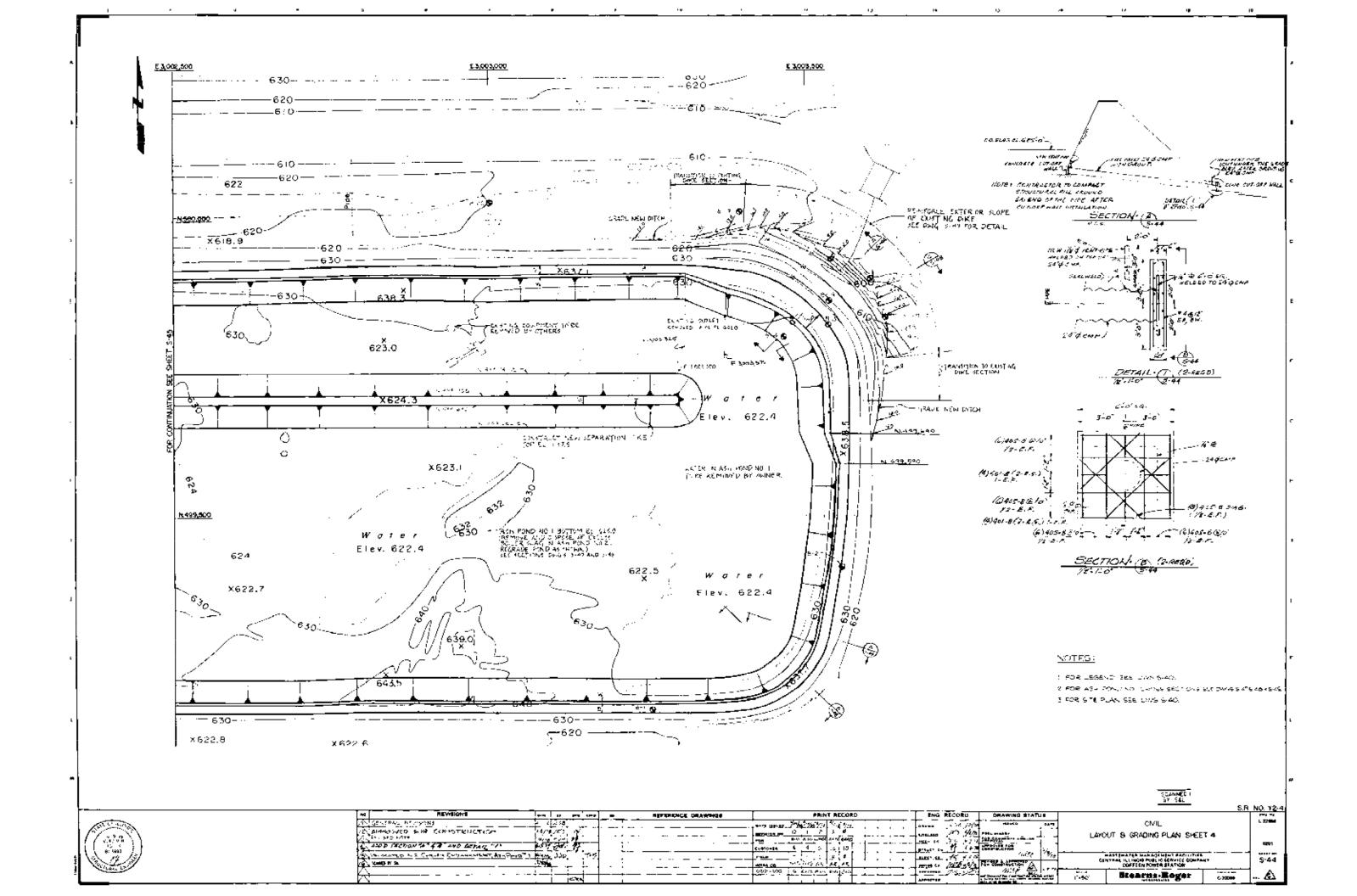


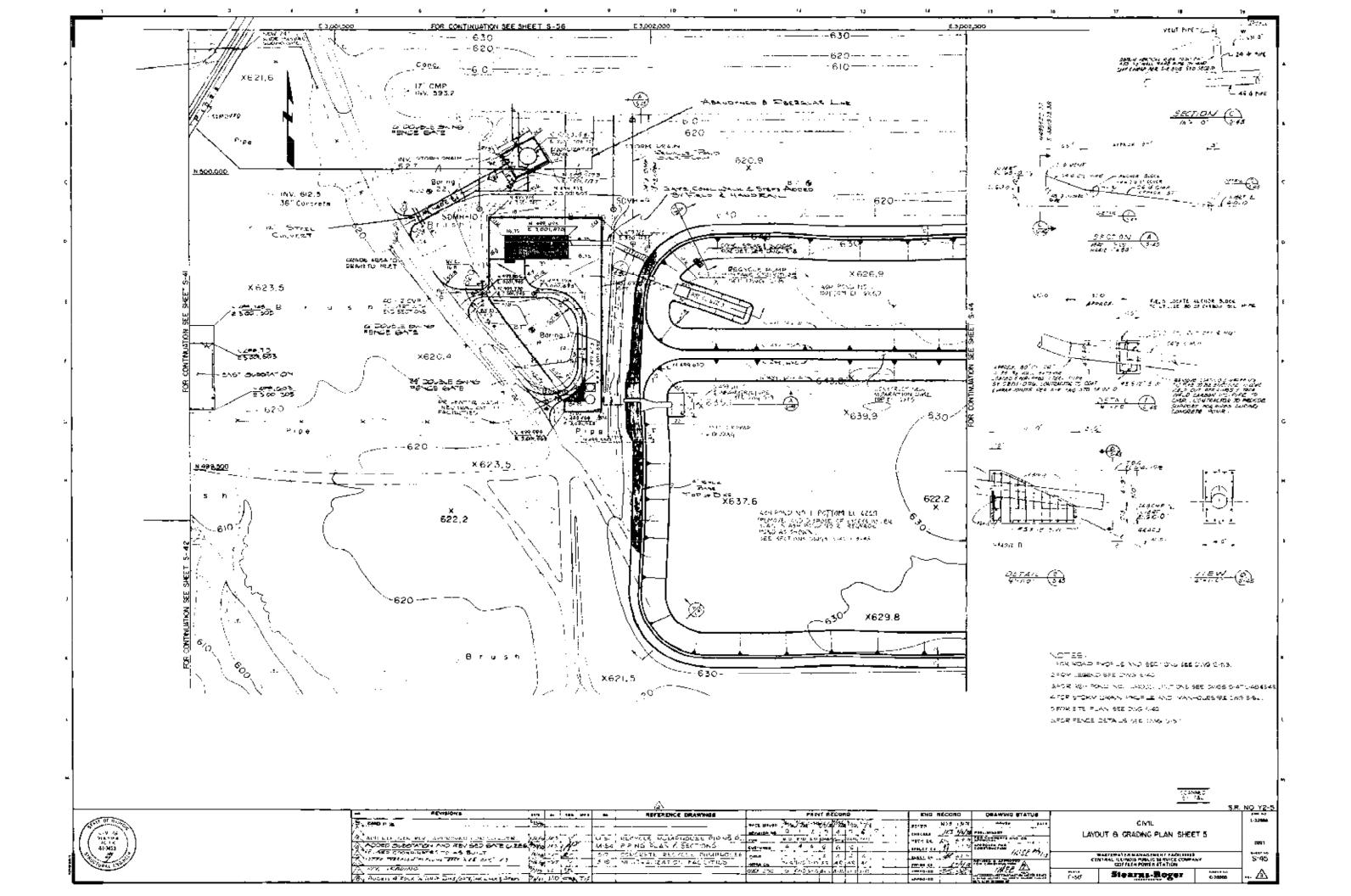
Appendix B: Coffeen Power Station Drawings (continued)

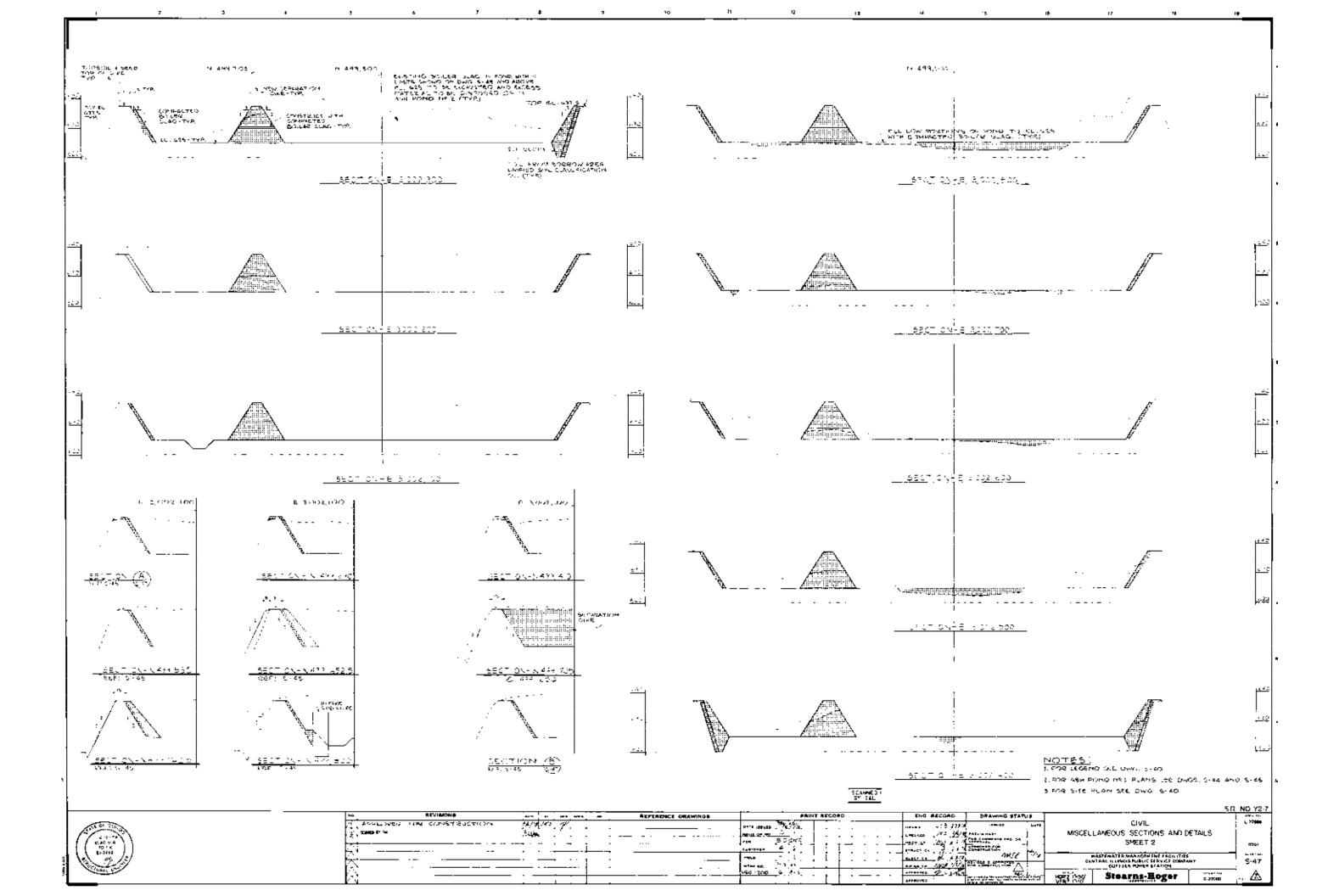
- 21. "Recycle Pond–Process Water Decant Sections & Details, CCB Management Facility", Drawing No. C-10206 (sh. 21), Revision 0, 5 January, 2011, Ameren Energy Generating.
- 22. "Recycle Pond Emergency Spillway Sections & Details, CCB Management Facility", Drawing No. C-10206 (sh. 22), Revision 0, 5 January, 2011, Ameren Energy Generating.
- 23. "Ash Pond #2, Drainage Modifications", Drawing No. W1008 (sh. 2), Ameren Energy Generating.

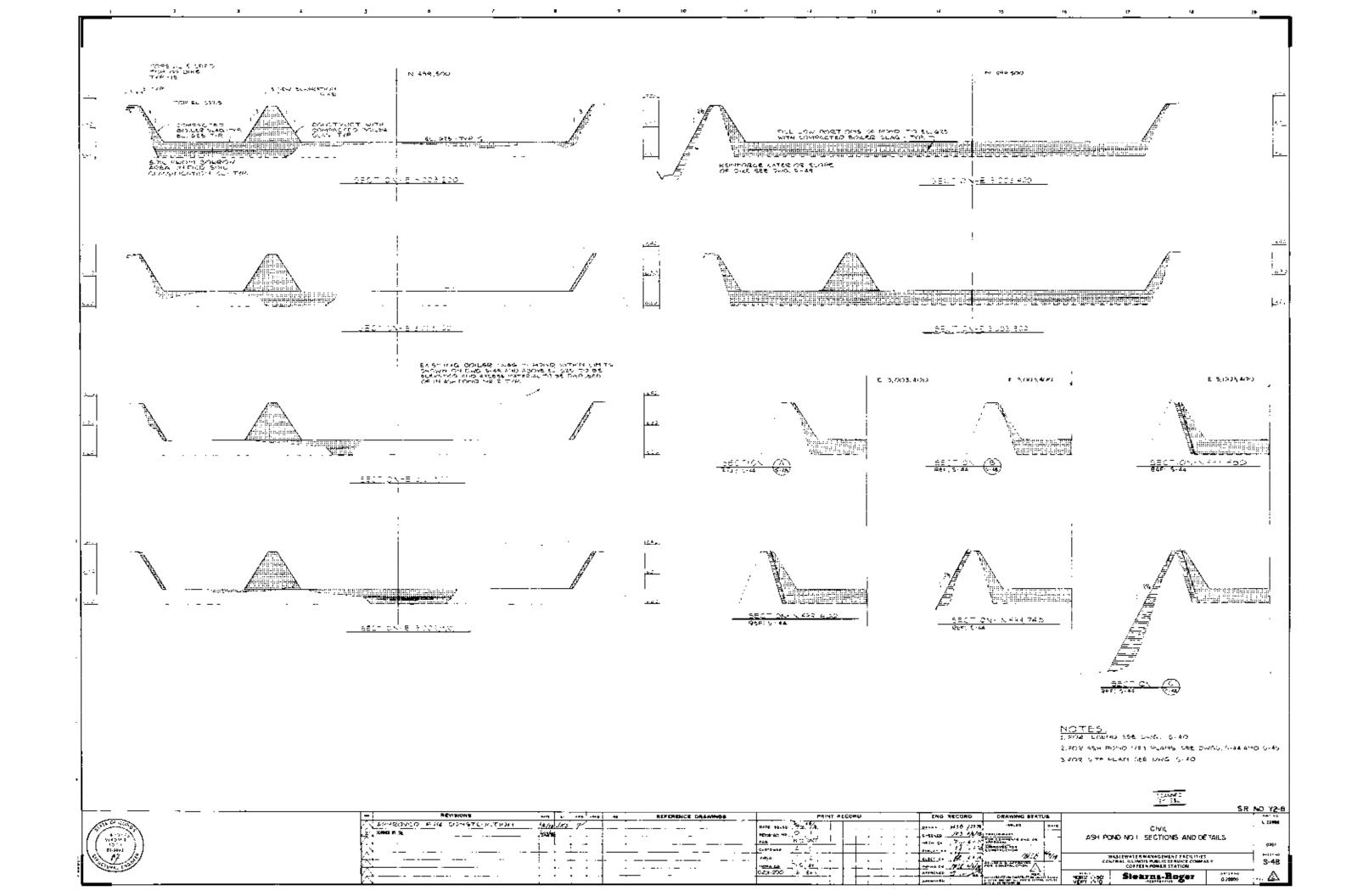


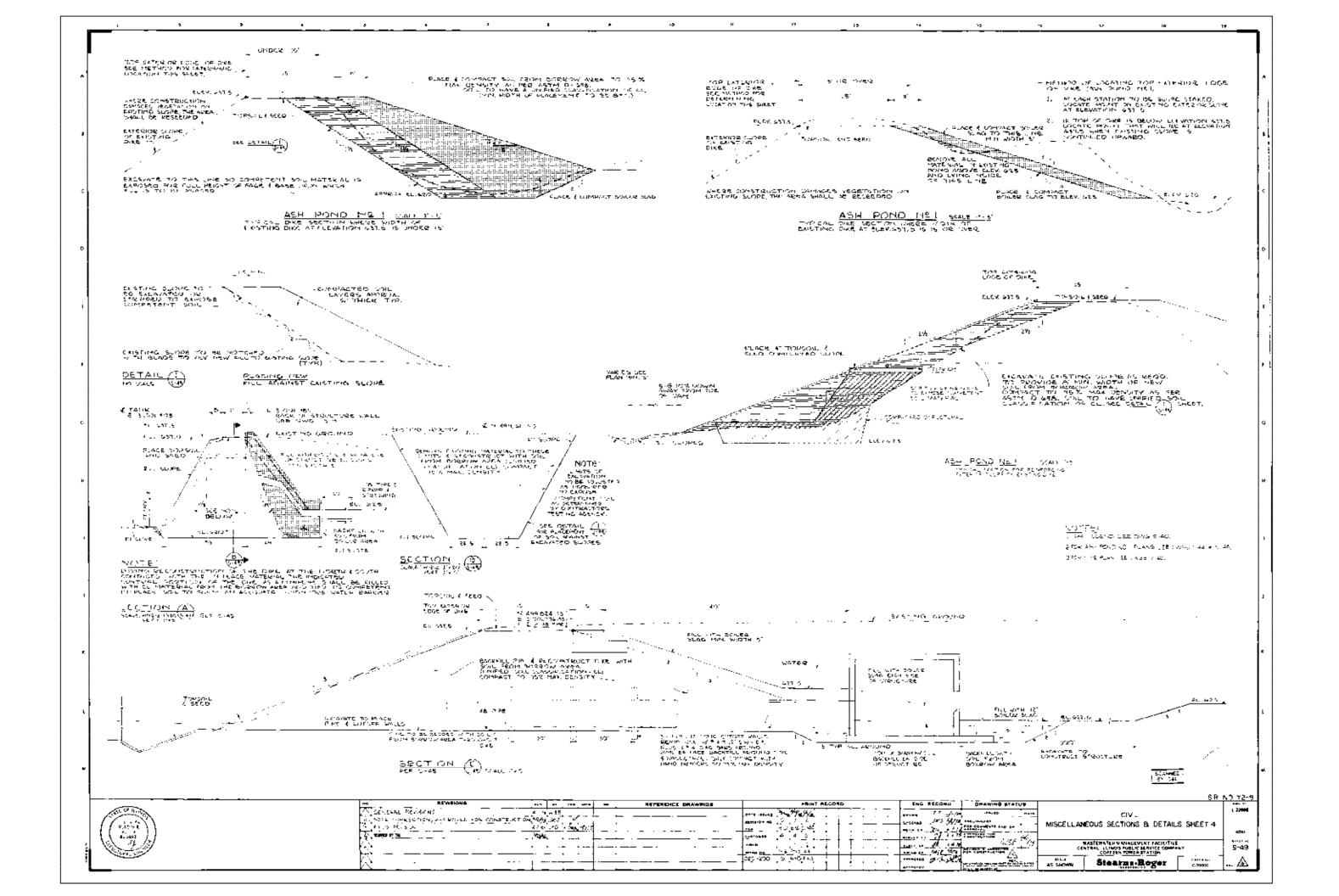


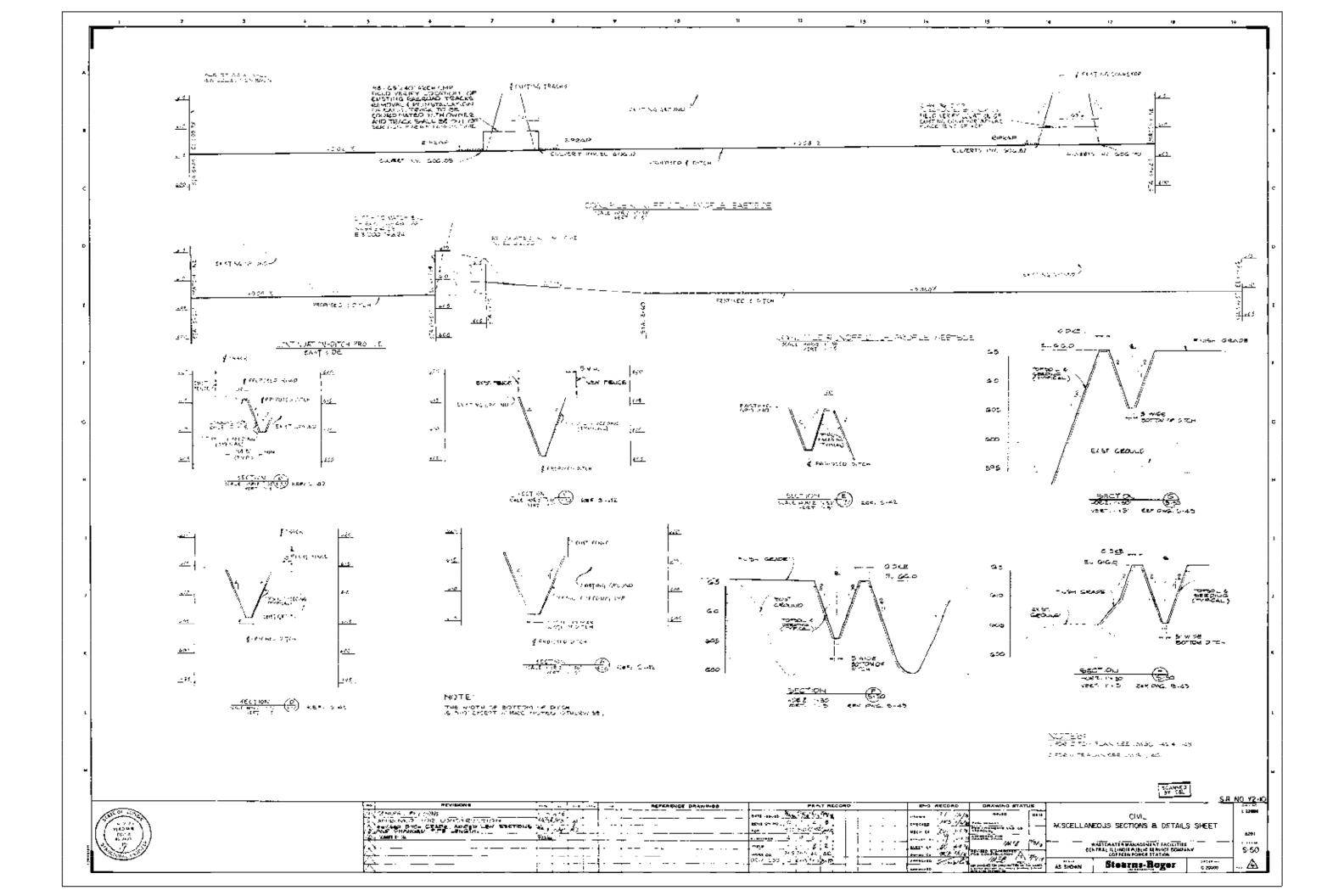


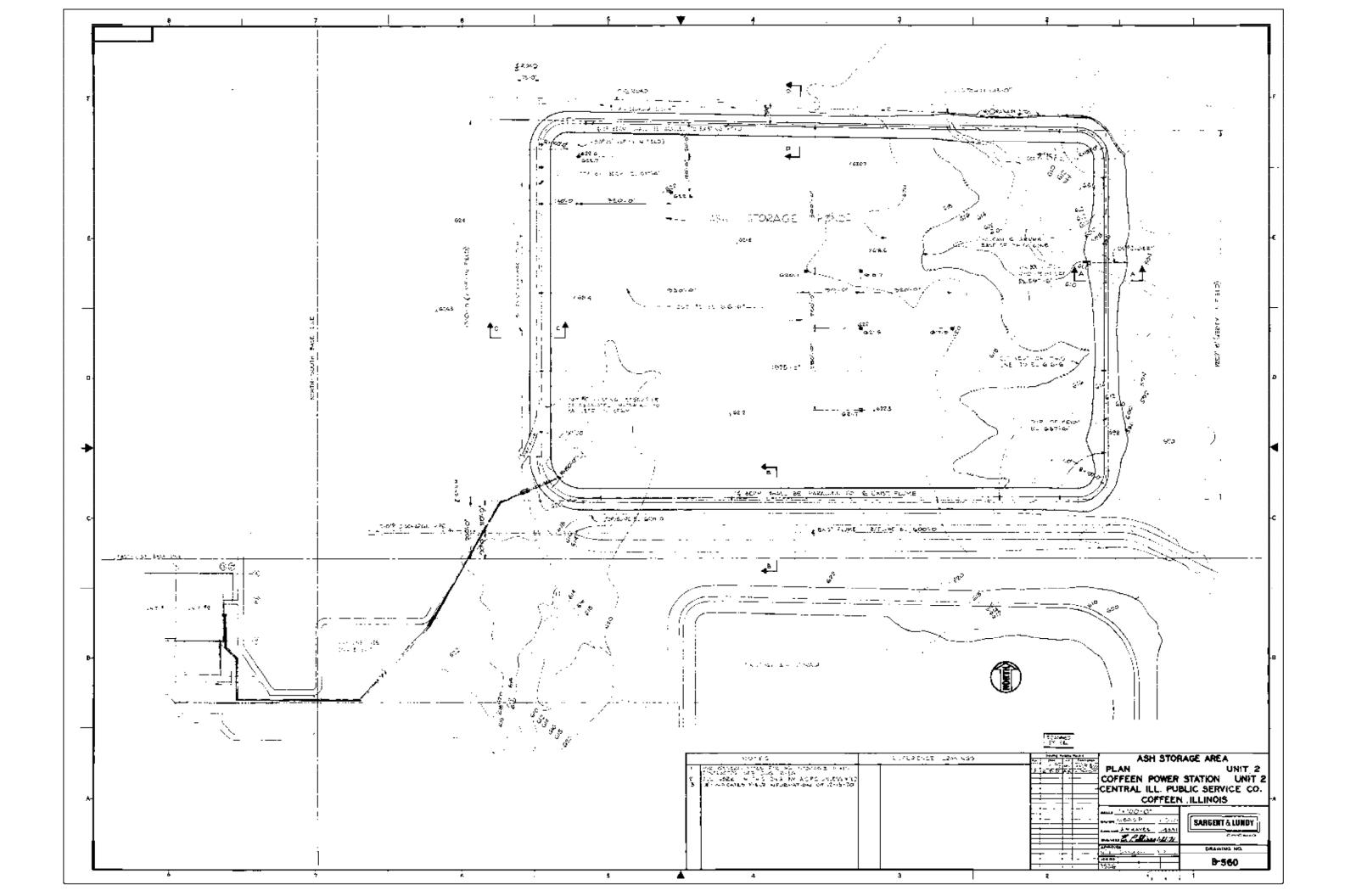


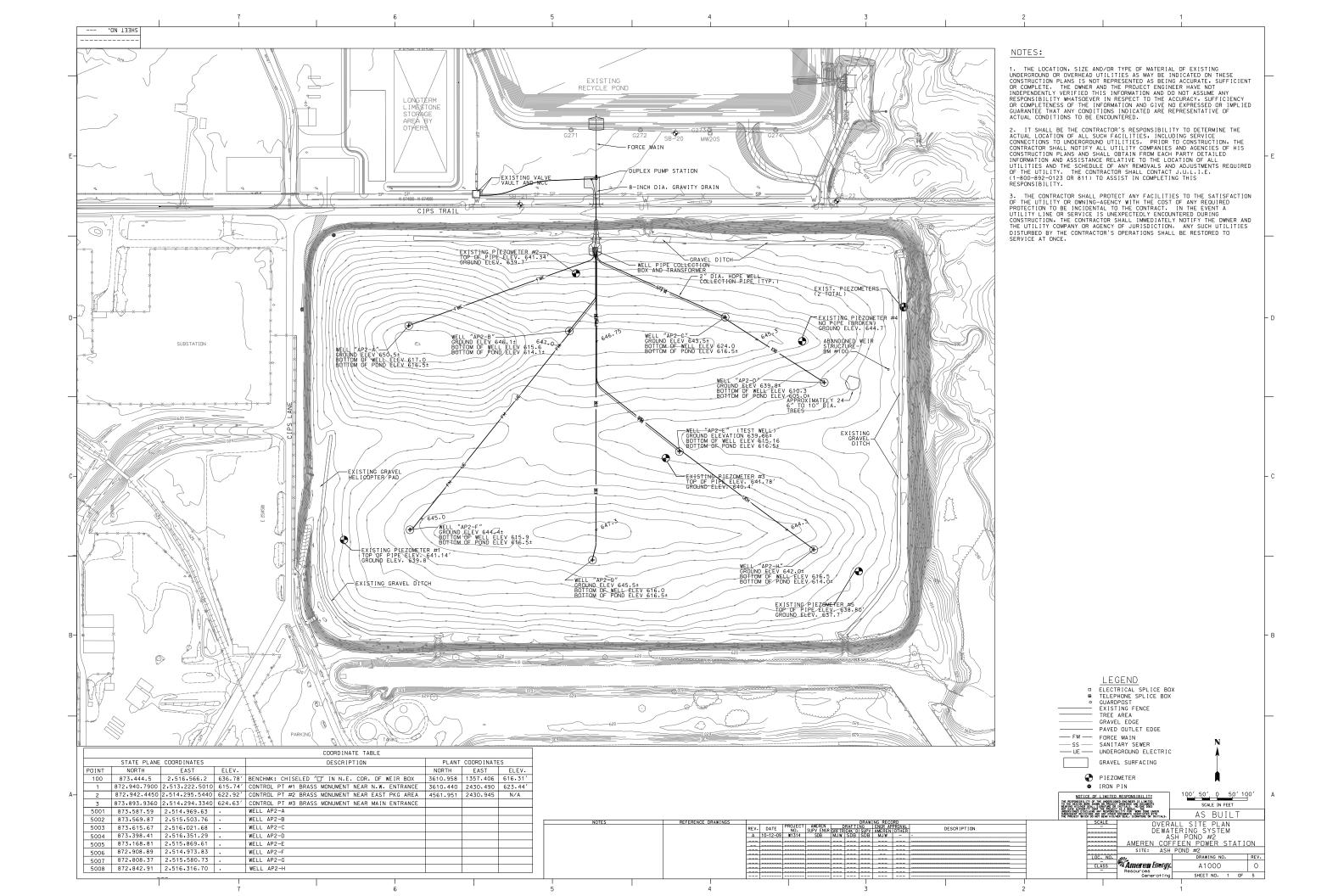


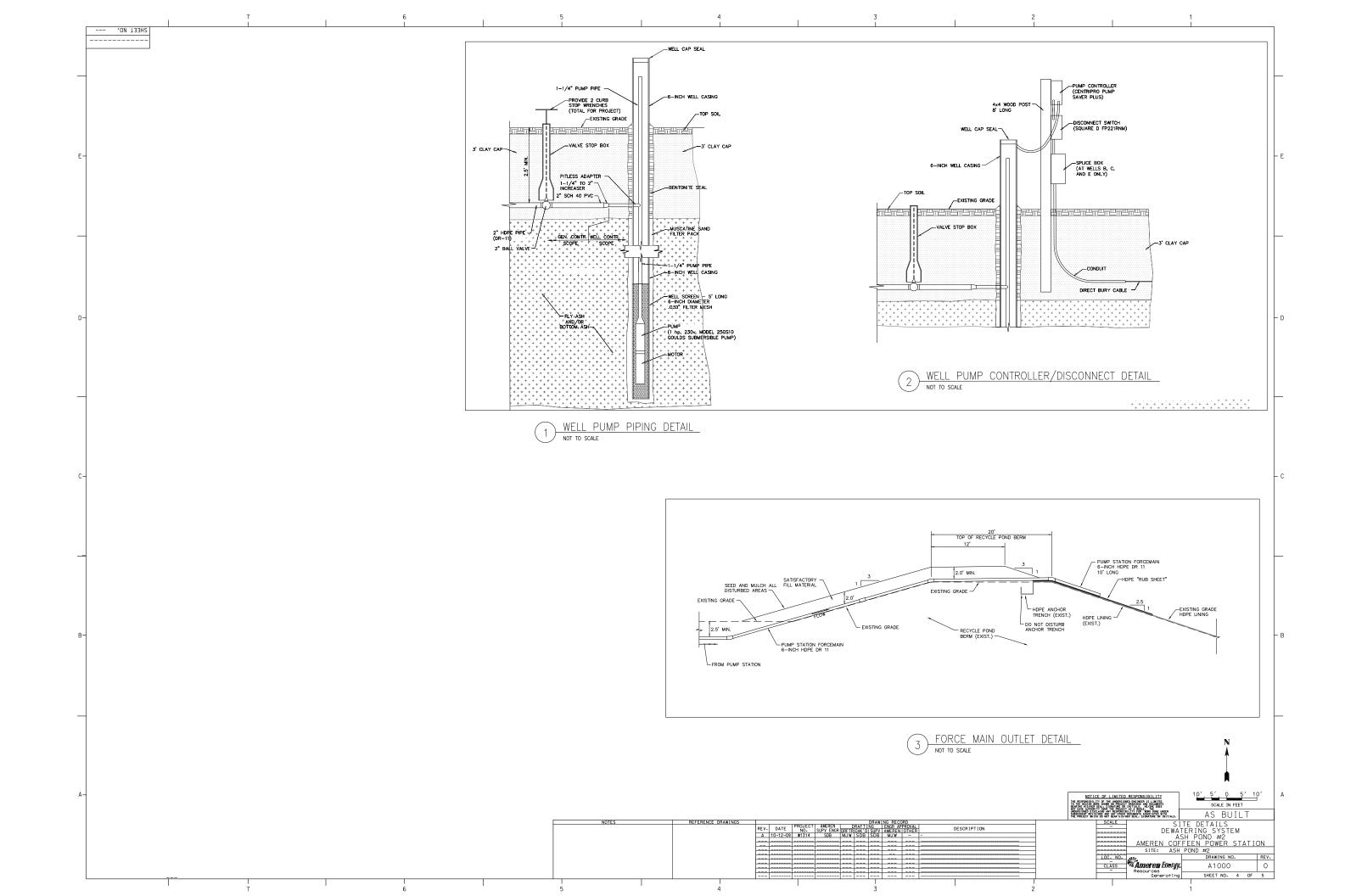


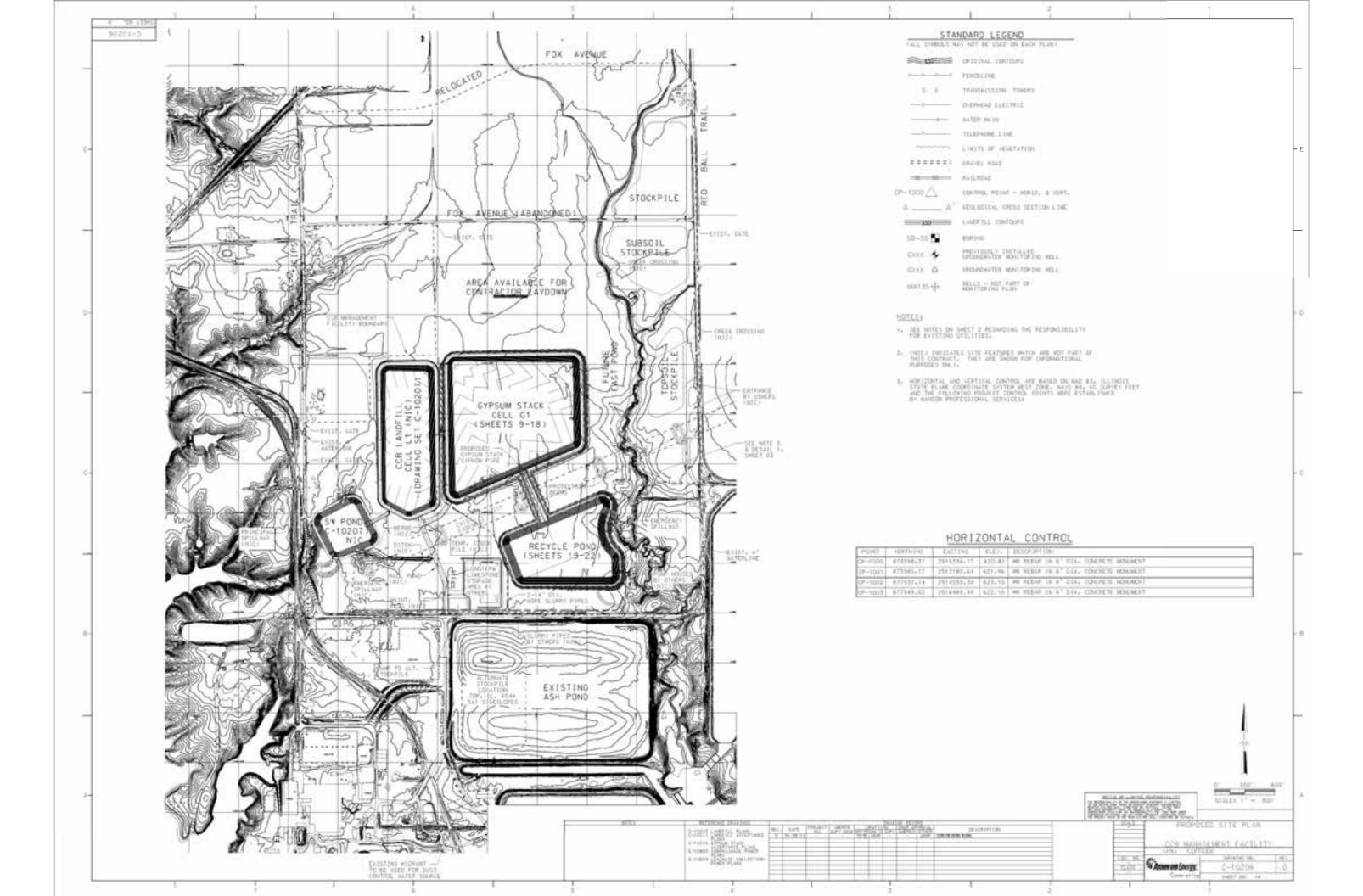


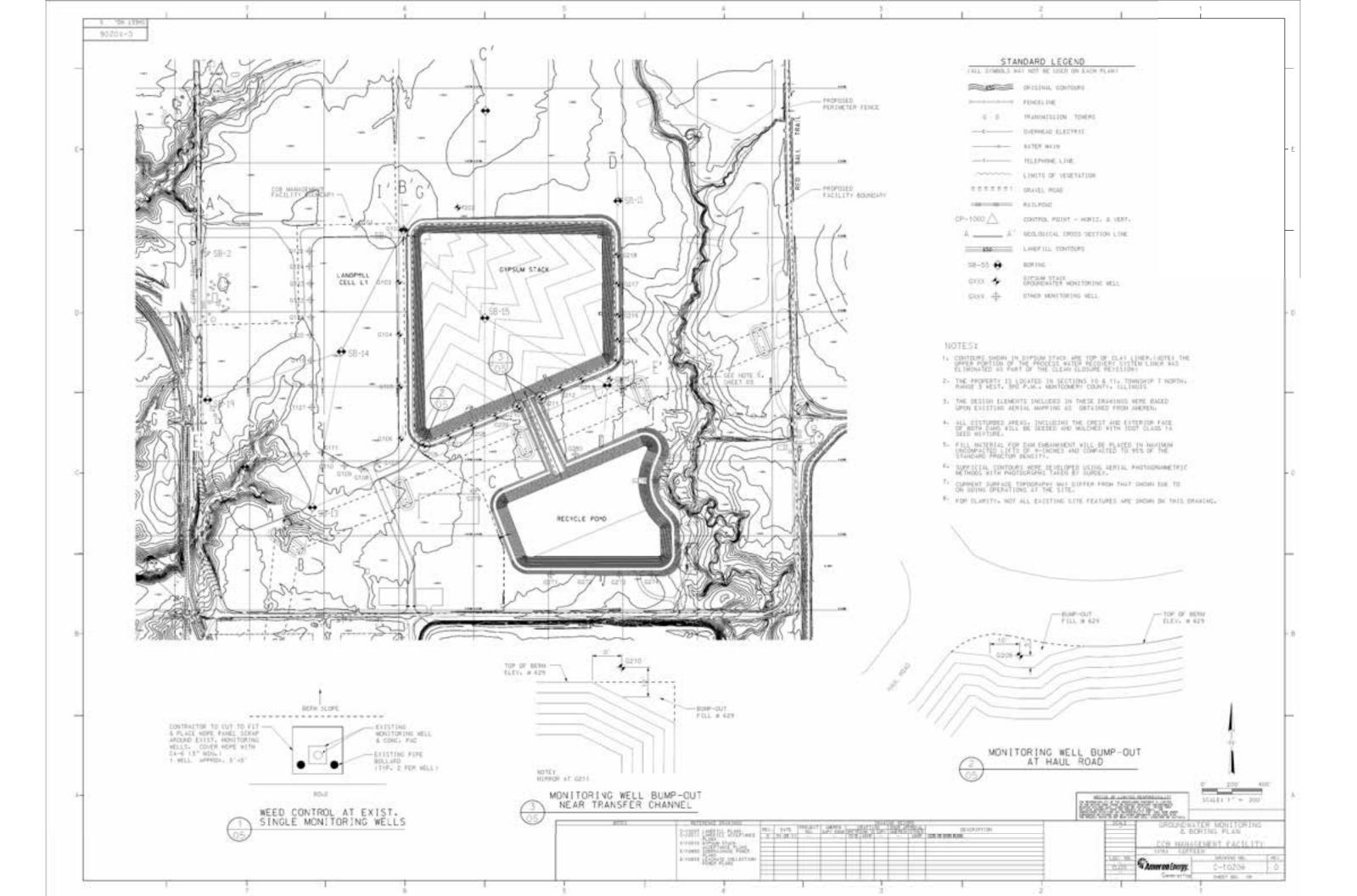


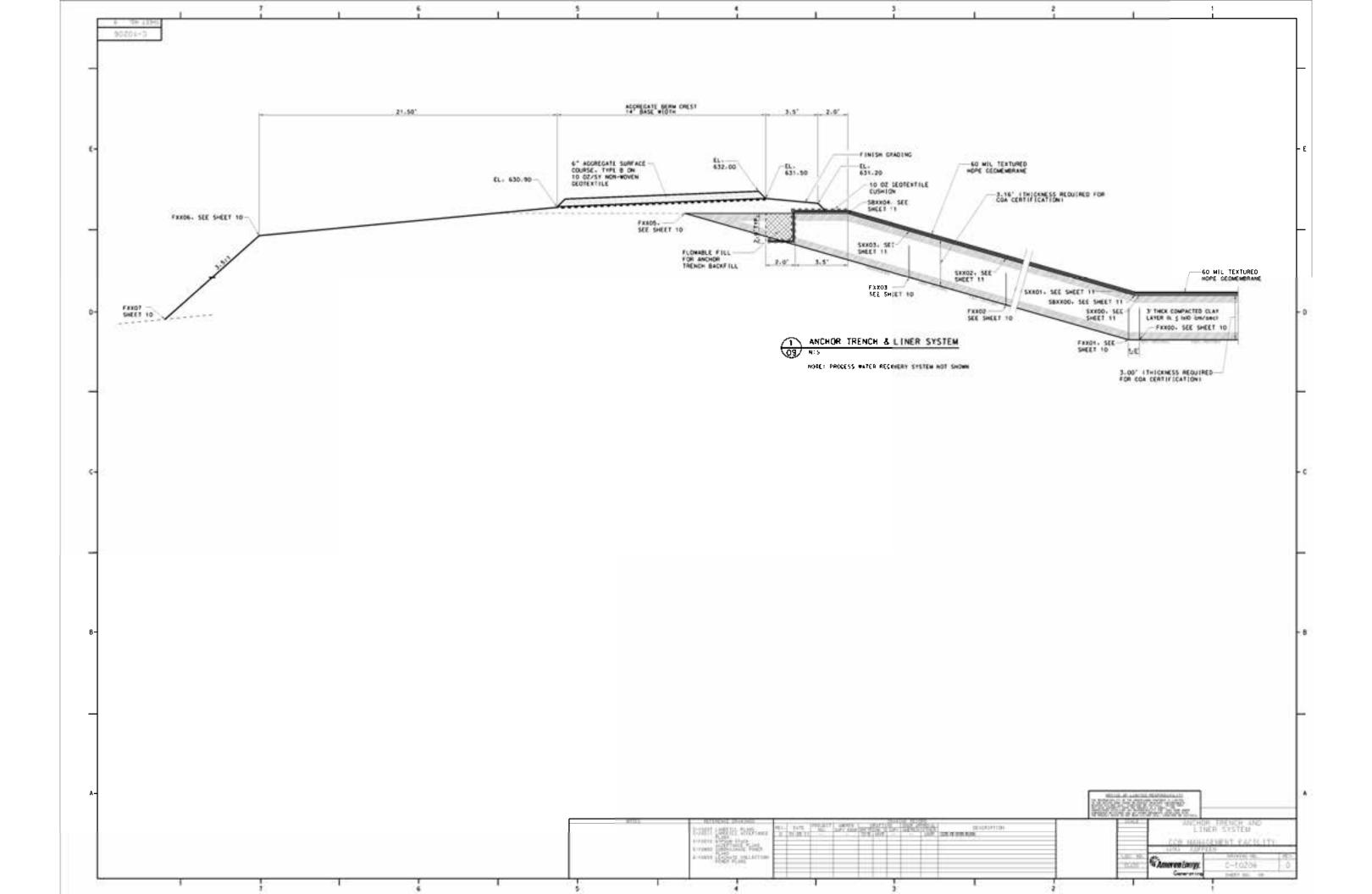


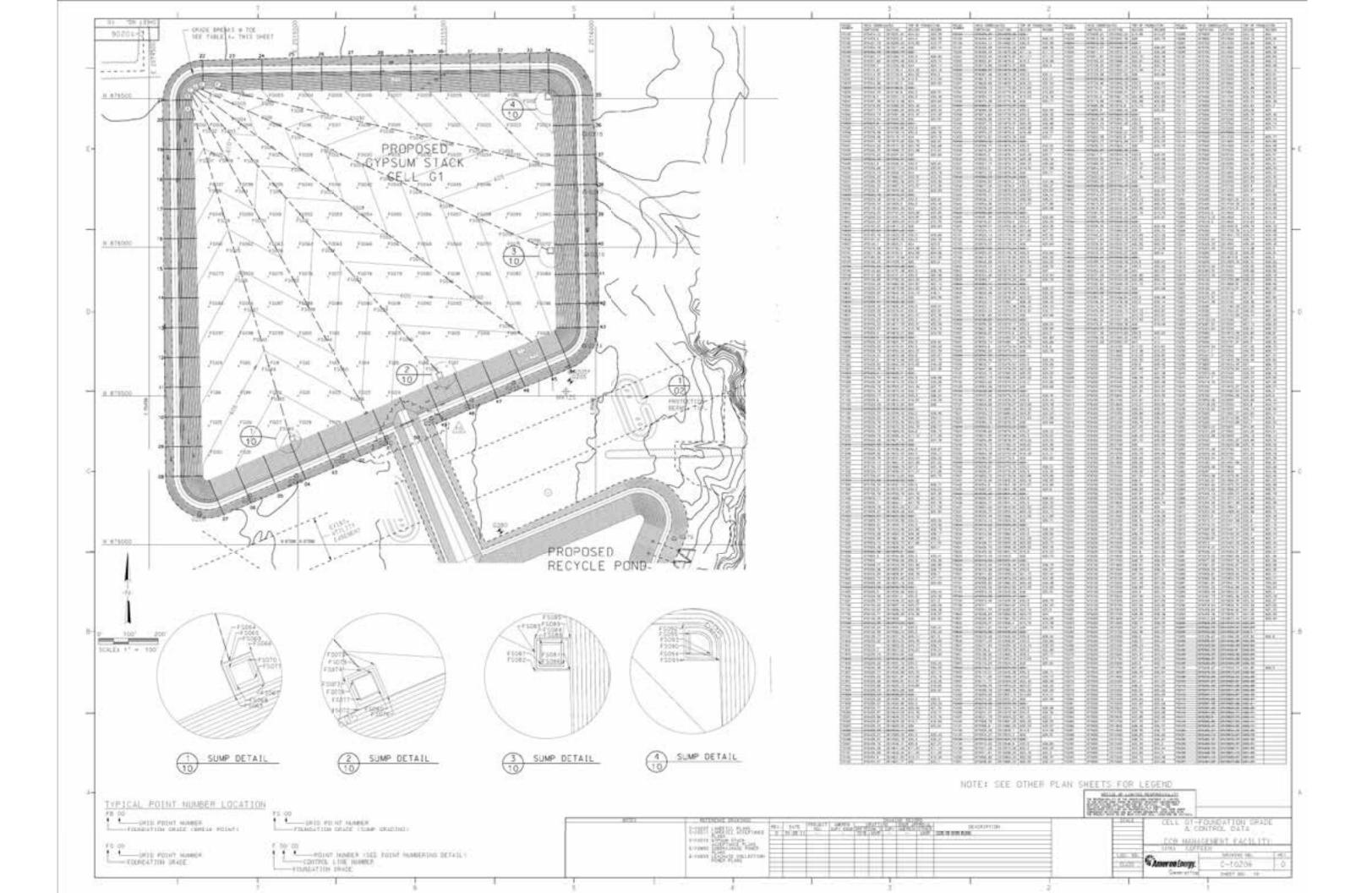


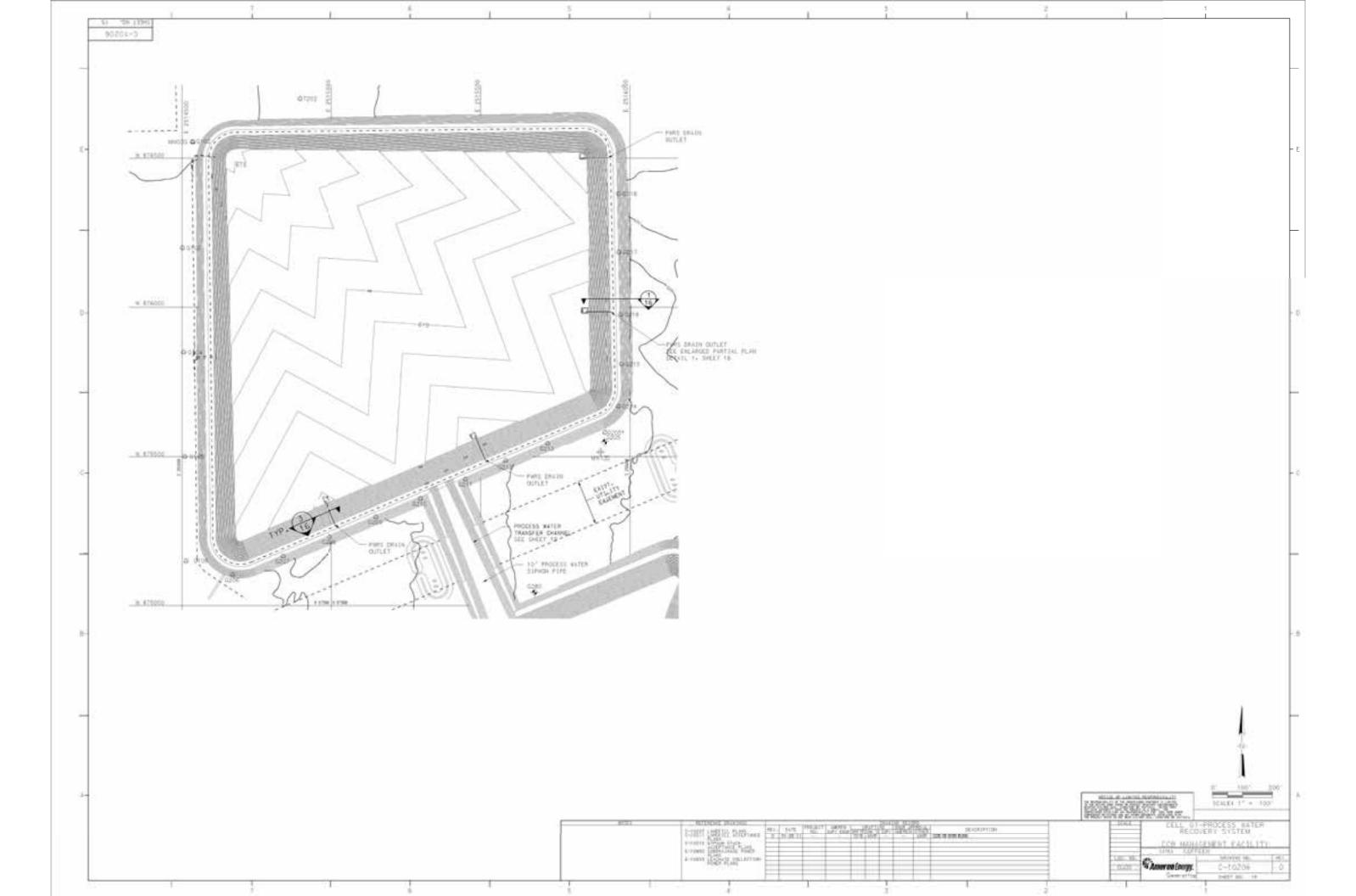


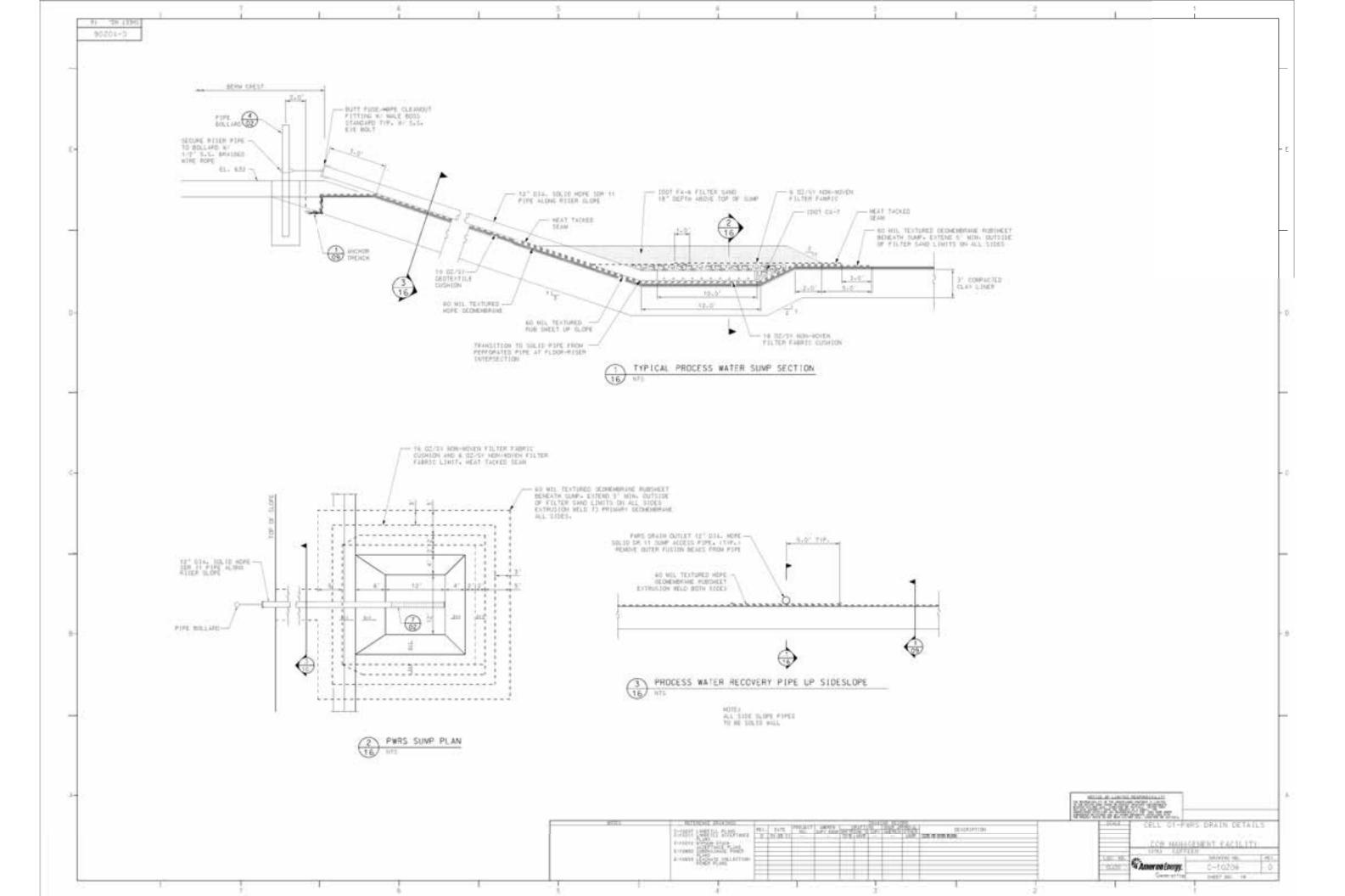


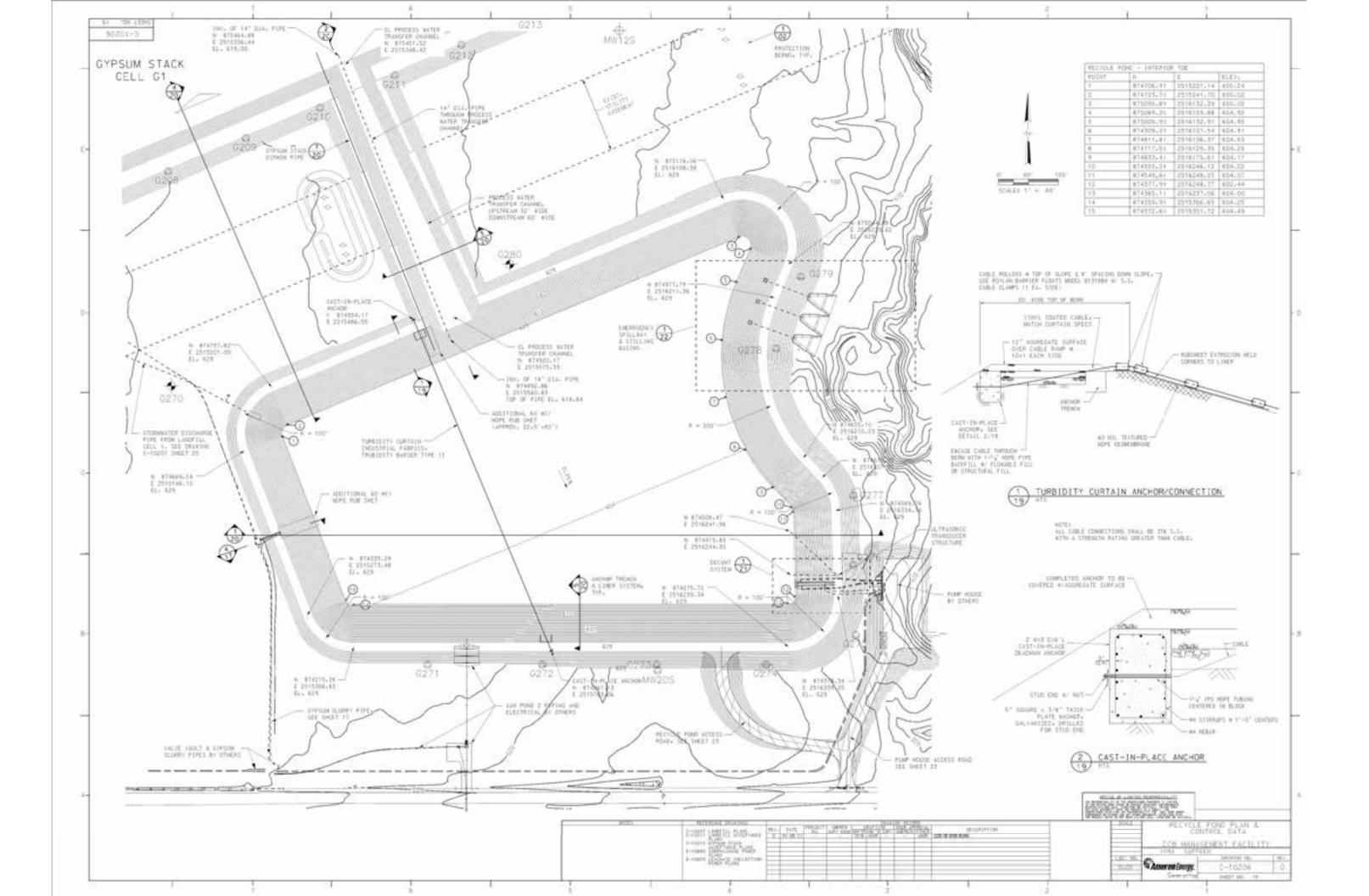


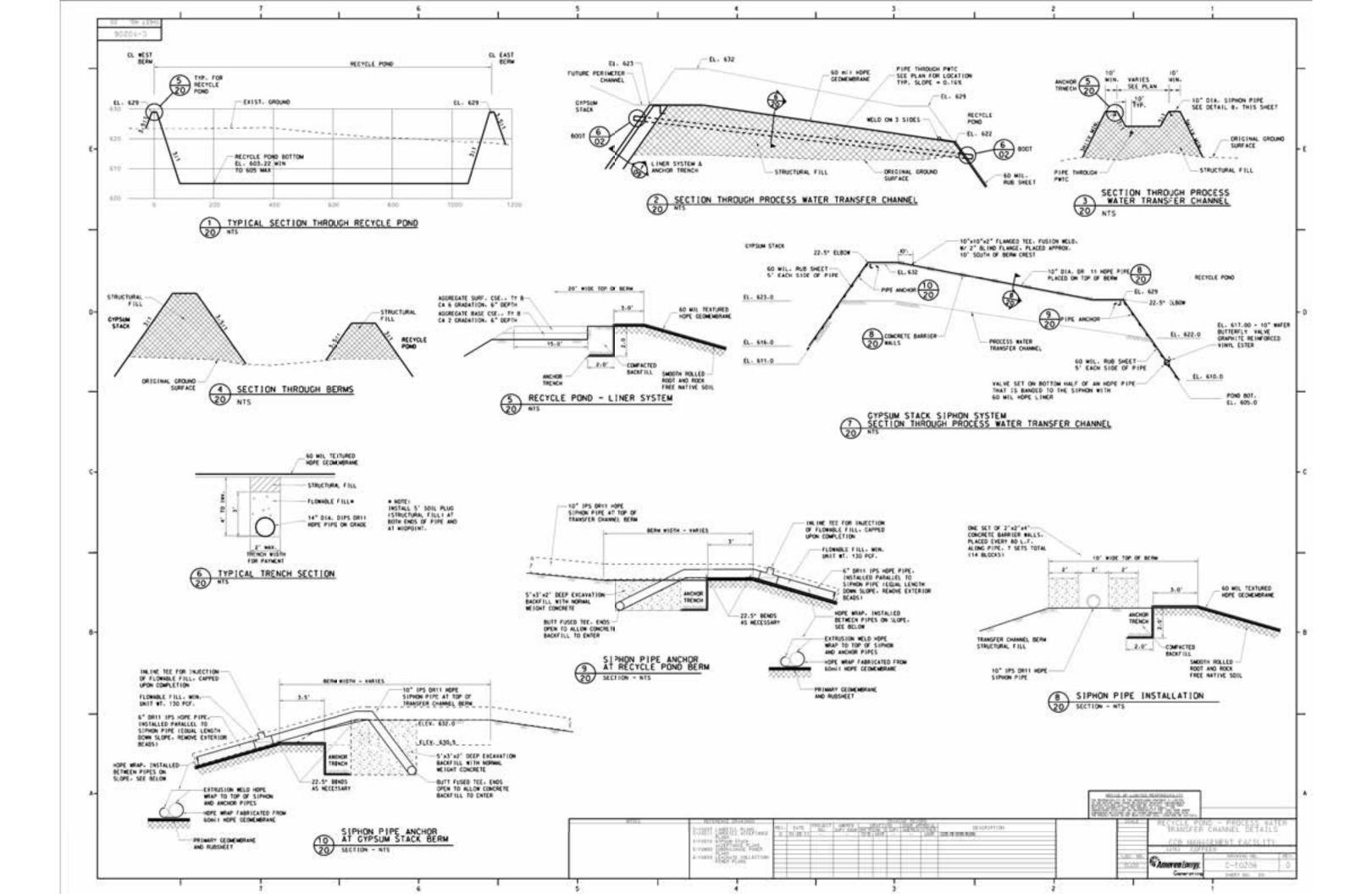


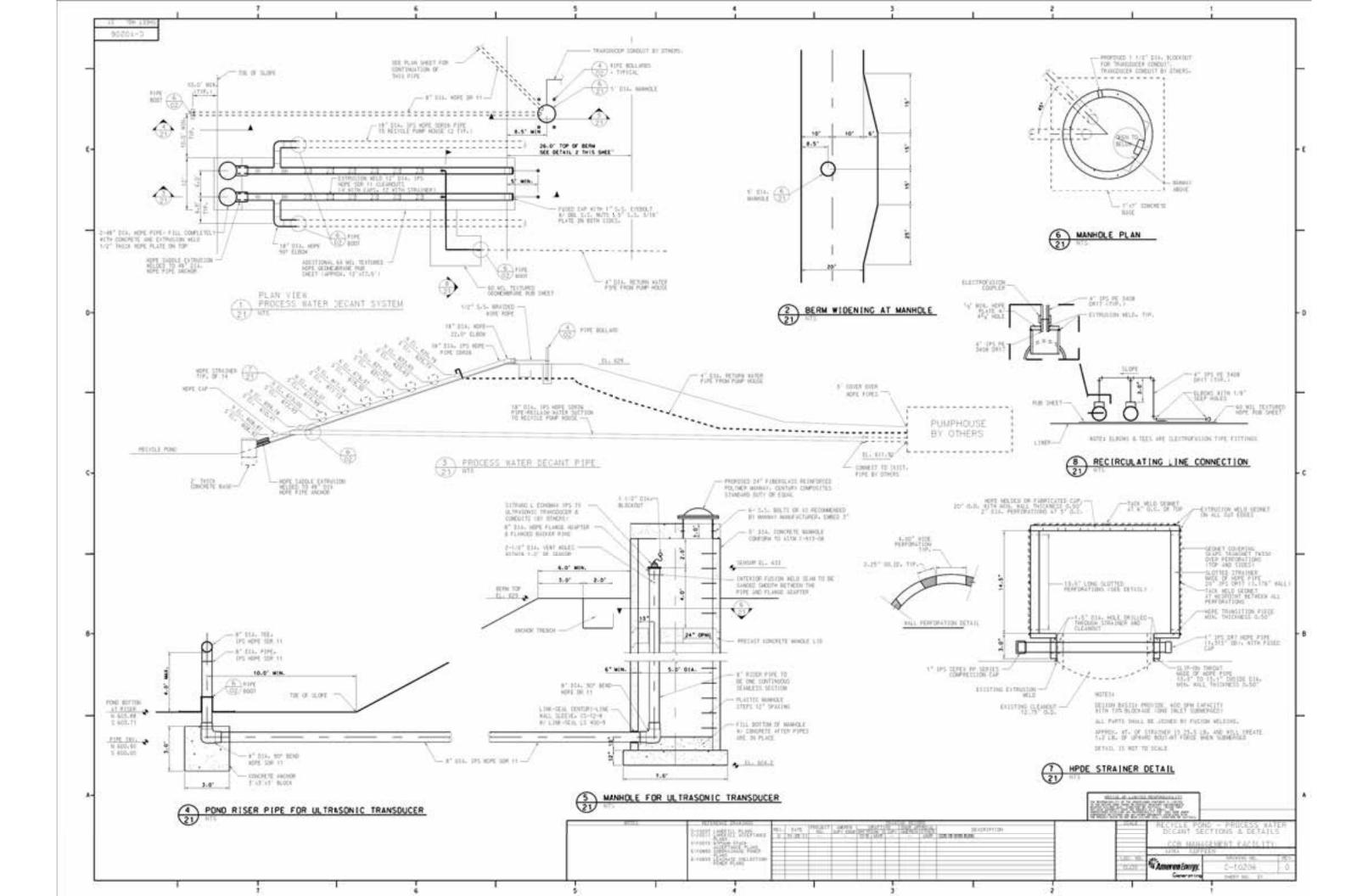


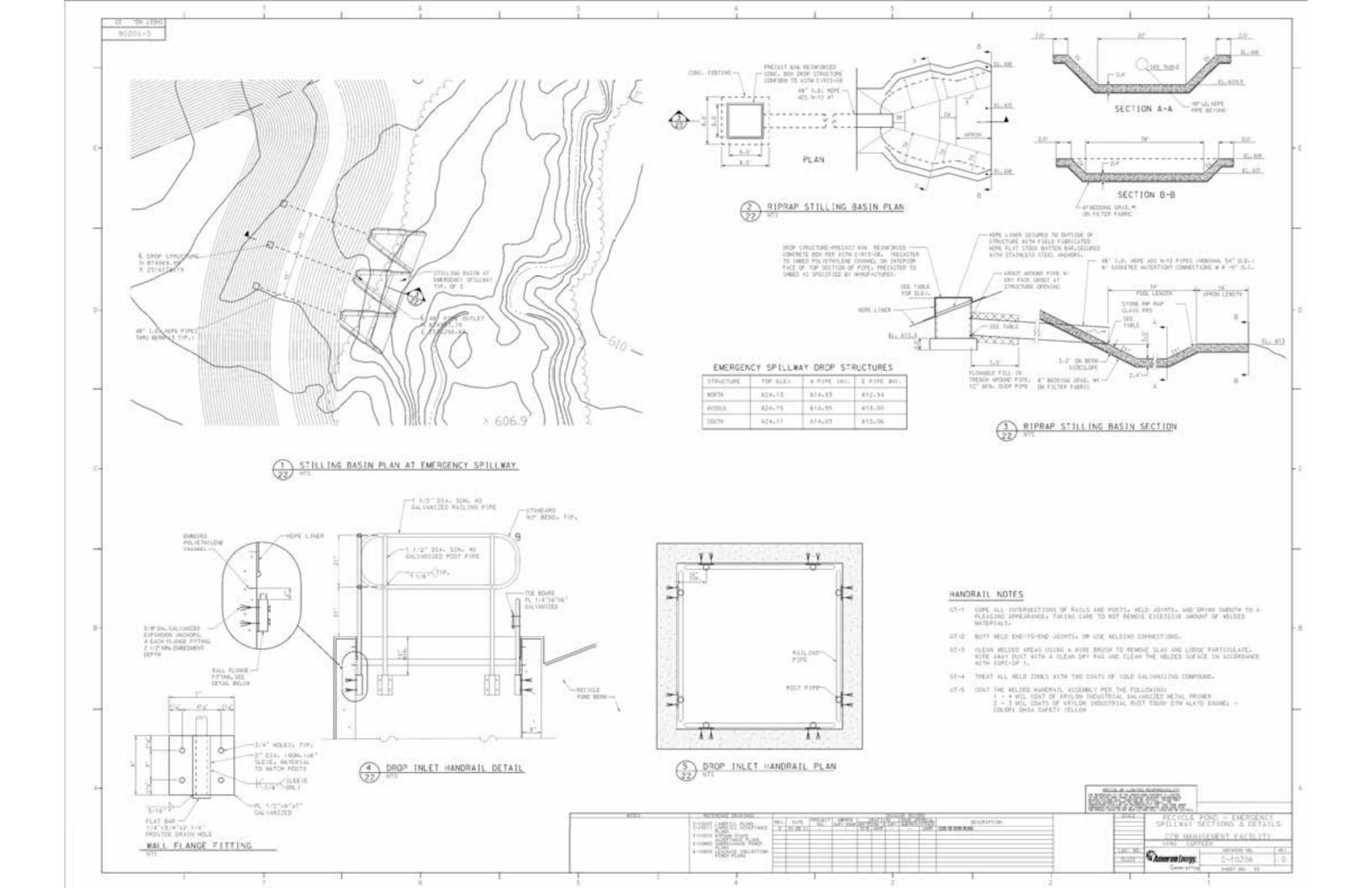


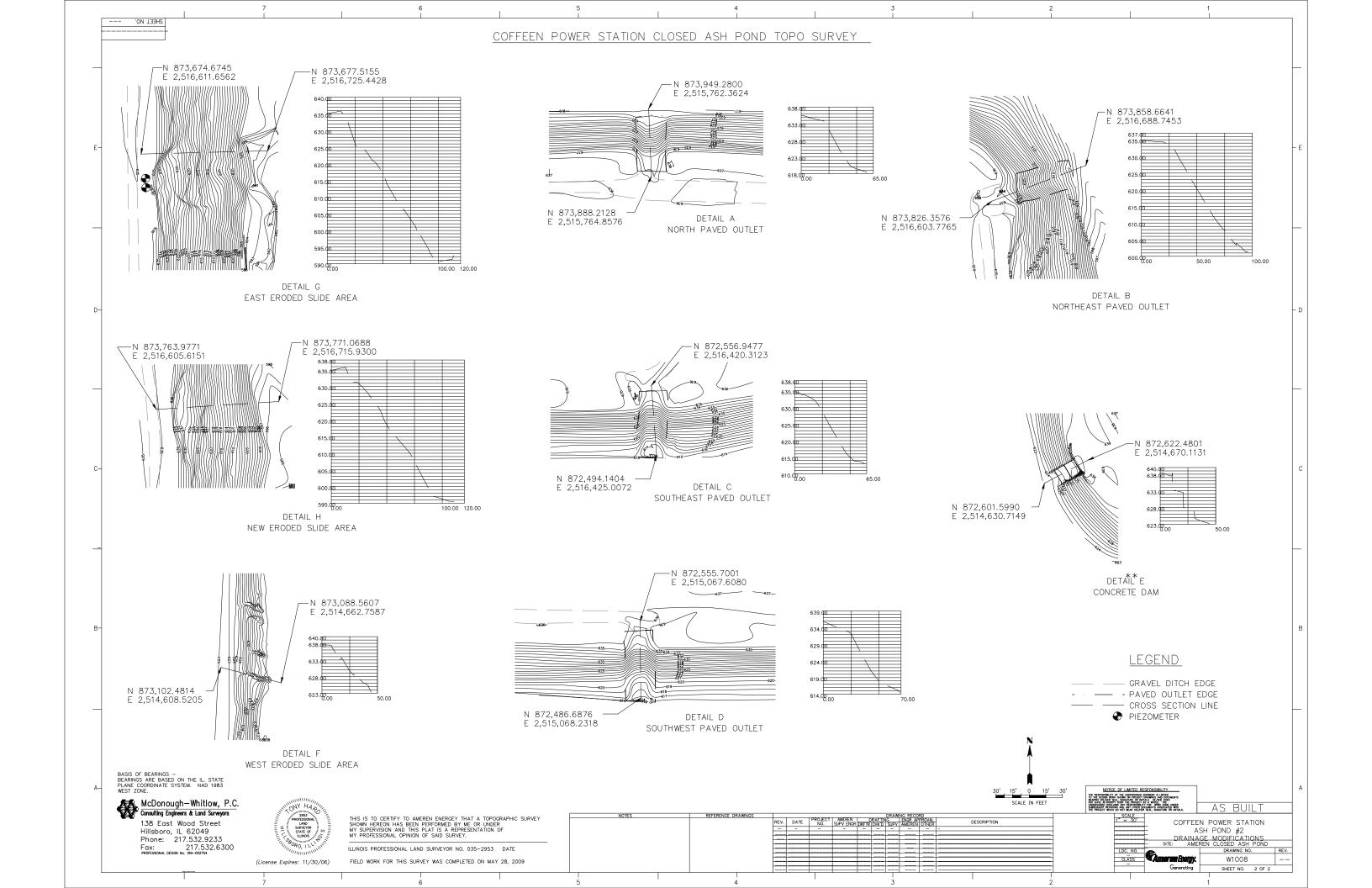






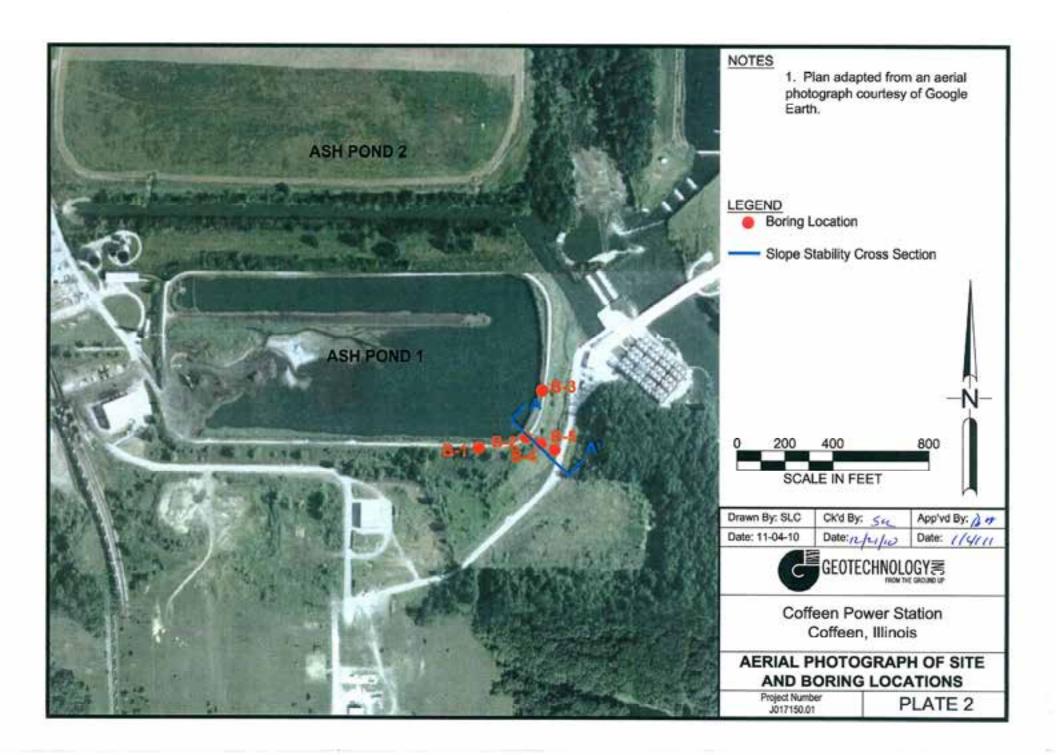


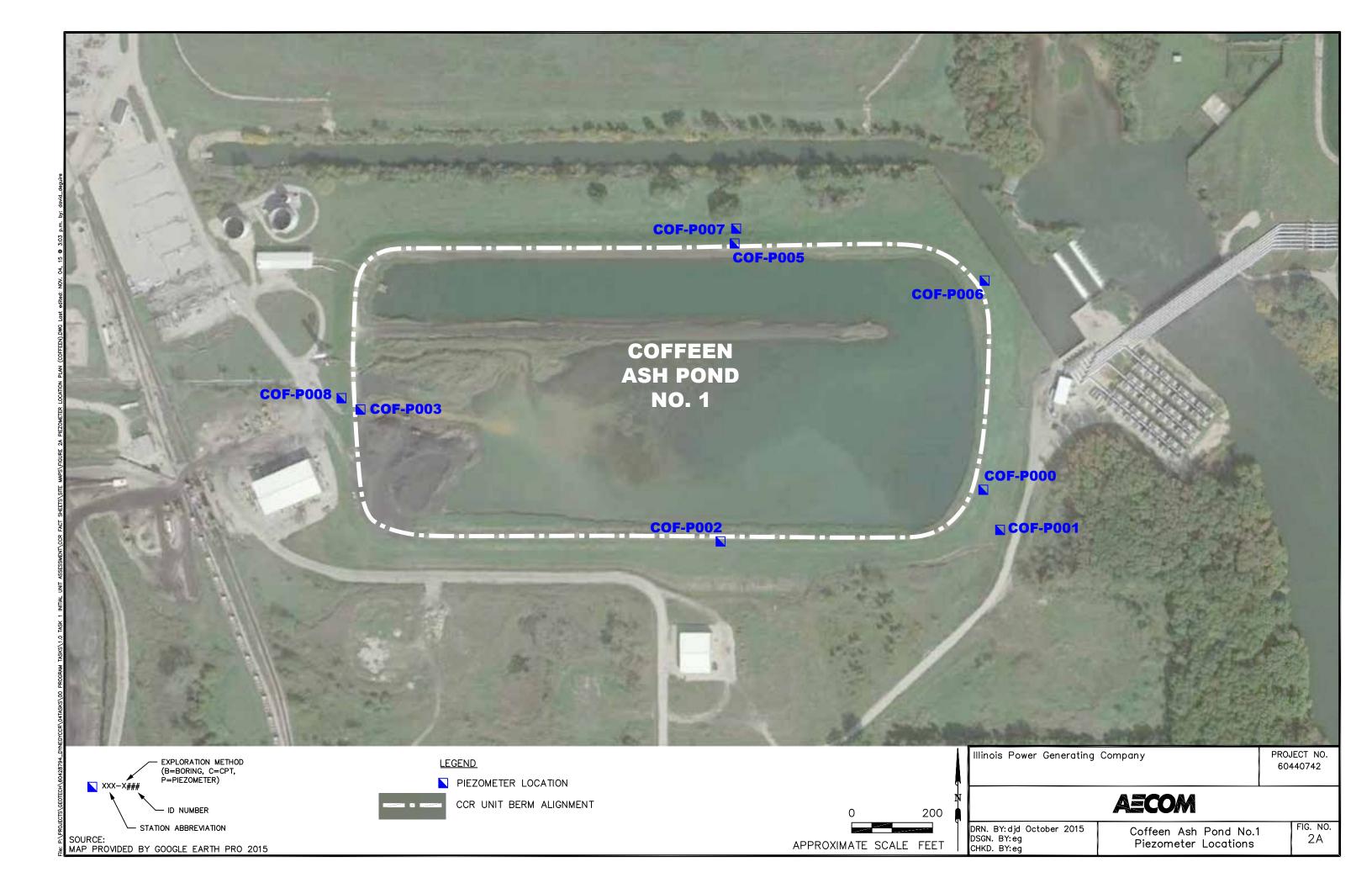


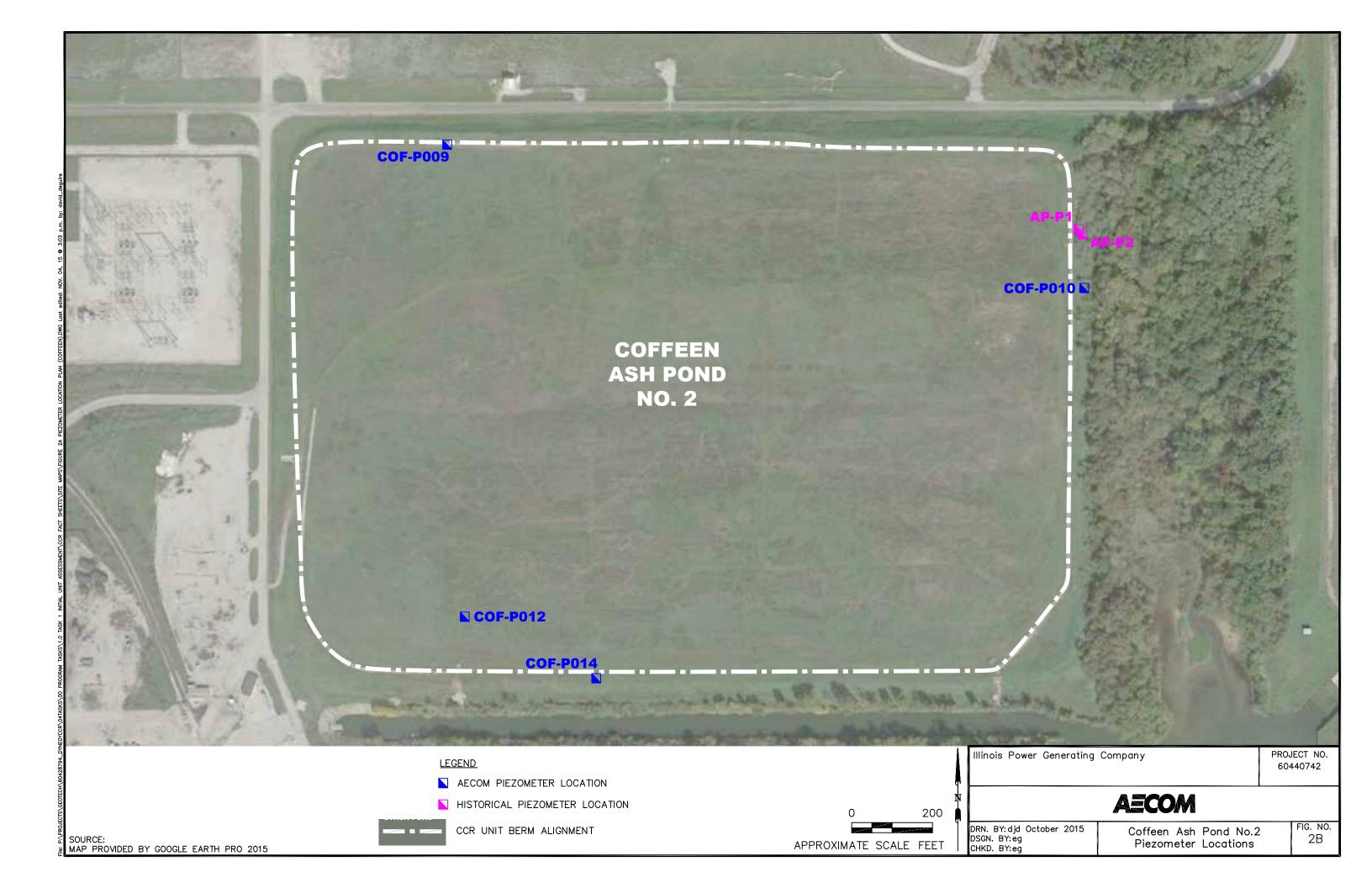




Appendix C: Coffeen Power Station Boring and Piezometer Locations









Appendix D: Project Specifications, Gypsum Stack and Recycle Pond Construction (Hanson 2008)

PROJECT SPECIFICATIONS GYPSUM STACK AND RECYCLE POND CONSTRUCTION GYPSUM MANAGEMENT FACILITY COFFEEN POWER STATION MONTGOMERY COUNTY, ILLINOIS

Prepared For:

AMEREN ENERGY GENERATING COMPANY

Prepared By:

HANSON PROFESSIONAL SERVICES INC. 1525 South Sixth Street Springfield, Illinois 62703

GYPSUM STACK AND RECYCLE POND CONSTRUCTION GYPSUM MANAGEMENT FACILITY COFFEEN POWER STATION MONTGOMERY COUNTY, ILLINOIS

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DIVISION1-GENERAL REQUIREMENTS

Section 01356 - Storm Water Pollution Prevention Measures

PART 1. GENERAL

1.01 DESCRIPTION

A. This section pertains to the construction and maintenance of temporary erosion control systems to control erosion and sediment damage to adjacent properties and water resources, and the removal of erosion control devices when they are no longer required.

1.02 RELATED SECTIONS

The following sections contain items which are related to the work in this section:

02936 - Topsoil, Seeding, and Mulching.

1.03 REFERENCES

The following reference, or cited portions thereof, governs the work:

Illinois Department of Transportation (IDOT): Standard Specifications for Road and Bridge Construction, adopted January 1, 2007.

1.04 SUBMITTALS

- Submittals shall follow the provisions of Section 01010.
- B. Preconstruction Submittals: A storm water best management practices (BMP) plan shall be submitted that includes the following items:
 - Site drawing showing anticipated locations of structural erosion controls, areas of disturbed soils, and drainage patterns;
 - Inspection and record-keeping procedures; and
 - Maintenance procedures for erosion controls.

PART 2. PRODUCTS

2.01 EROSION CONTROL SYSTEMS

Materials for erosion control systems shall be in accordance with Article 280.02 of the IDOT Standard Specifications.

PART 3. EXECUTION

3.01 EXAMINATION

The site shall be examined to determine the extent of work required.

3.02 PRECONSTRUCTION JOBSITE INSPECTION

- A. The person who shall be at the jobsite during construction and who shall be responsible for insuring that erosion control work is completed in a timely manner shall be identified at the preconstruction meeting.
- B. A jobsite inspection shall be conducted with the Owner's Representative to review and designate the locations and types of erosion protection to be placed. The inspection shall be scheduled at the preconstruction conference and carried out on the job site before beginning any work that will disturb existing drainage or potentially create erodible conditions.

3.03 CONSTRUCTION

- A. Temporary erosion control systems shall be constructed in accordance with IDOT Standard 280001 and Article 280.04 of the Standard Specifications and as directed by the Owner's Representative. Erosion control devices shall be in place and approved by the Owner's Representative prior to beginning other work.
- B. Incorporate permanent erosion control features into the project at the earliest practicable time to minimize the need for temporary erosion controls.

3.04 MAINTENANCE

- A. Temporary erosion control systems shall be maintained in accordance with Article 280.05 of the Standard Specifications, except that measurement and payment provisions shall not apply.
- B. Temporary erosion control systems for unprotected disturbed areas shall be cleaned of trapped sediment and repaired immediately prior to project close out.
- Temporary seeding shall be applied to all disturbed areas except the gypsum stack excavation and the future fill and topsoil stockpiles.

3.05 REMOVAL AND DISPOSAL

When the Owner's Representative deems that temporary erosion control systems are no longer needed, they shall be removed and properly disposed, and silt deposits shall be removed or regarded as directed by the Owner's Representative, and the area seeded. Non-biodegradable temporary erosion control materials shall be disposed of off site. Biodegradable erosion control devices may be disposed of in spoil areas designated by the Owner's Representative. All laws and regulations in disposing of the materials shall be obeyed.

END OF SECTION 01356

1:05jobs/05s3004A\Gypsum Stacking\IDNR Dum Safety Permit Application\Specs\S01356_Storm Water Pollution Prevention Measures.doc

PART 1. GENERAL

1.01 DESCRIPTION

This section pertains to stripping of topsoil and vegetation from areas of the site that are to be excavated.

1.02 RELATED SECTIONS

No related sections.

PART 2. PRODUCTS

No products used.

PART 3. EXECUTION

3.01 EXAMINATION

The Contractor shall examine the site to determine the extent of work required.

3.02 SITE PREPARATION - STRIPPING

- A. All vegetation and topsoil encountered within the Gypsum Stack grading limits shall be stripped. Topsoil shall be kept clean and free of all foreign material, and stored in separate stockpiles from vegetation and common excavations. Stockpiles shall be located as indicated on the drawings or as directed by the Owner's Representative.
- Payment for stripping shall be based upon removal of 24 inches of topsoil in areas that require stripping.

3.03 DISPOSAL

All materials resulting from site preparation operations shall be stockpiled in the designated spoil area. Contractor shall obey all laws and regulations when disposing of the materials.

END OF SECTION 02100

1:\03jobs\03s5010\Gypsum Stack\Specs\Gypsum Mangement Facility\Pre-Final Specs\S02100_Site Preparation.doc

PART 1. GENERAL

1.01 DESCRIPTION

This section pertains to excavation, fill, and backfill required for foundation preparation, construction of low-permeability soil layer, anchor trench construction, miscellaneous site grading and berm construction.

1.02 RELATED SECTIONS

- A. The following sections contain items which are related to the work in this section:
 - 01356 Storm Water Pollution Prevention Measures
 - 2. 02100 Site Preparation
 - 02373 Geotextiles
 - 4. 02936 Topsoil, Seeding, and Mulching

1.03 REFERENCES

The following references, or cited portions thereof, govern the work:

- Illinois Department of Transportation (IDOT): Standard Specifications for Road and Bridge Construction, adopted January 1, 2007
- Department of Sustainable Natural Resources, Soil Survey Standard Test Method, Unified Soil Classification System: Field Method (USCS).

1.04 MEASUREMENT AND PAYMENT

- A. The Contractor shall be responsible for estimating the extent of excavation and fill required to complete the work, including, but not limited to, excavation to required elevations; loading, transporting, placing, and compacting low permeability soil; excavation and backfill of anchor trench; and miscellaneous site grading and berm construction. The Contractor shall include the dollar amount associated with all earthwork in his Lump Sum Bid amount.
- B. Removal and replacement of unsuitable foundation material and subgrade stabilization measures directed by the Owner's Representative will be paid for on a time and material basis.

1.06 COORDINATION

Existing utilities or other plant facilities shall not be interrupted, except when permitted in writing by the Owner's Representative and then only after acceptable

temporary services have been provided. A minimum 48-hour notice shall be provided prior to proceeding with an approved temporary interruption.

1.08 SUBMITTALS

Materials Handling Plan.

A materials handling plan shall be submitted for construction and protection of the low permeability soil liner. The plan shall describe the following:

- Processing and placement of the low permeability soil type, model number, weight, and critical dimensions of equipment to be used for soil processing, compaction, scarification, and smooth rolling;
- Method of protecting low permeability soil from changes in moisture content and freezing after placement.

B. Construction Access Ramp Layout.

Layout drawings shall be submitted showing alignment, profile, and typical section of the construction access ramps from the haul road into the bottom of the Gypsum Management Facility excavation. The minimum width of the ramp shall be 50 ft., and the longitudinal grade shall not exceed 8 percent.

PART 2. PRODUCTS

2.01 MATERIALS

A. Earth Fill Material

Earth Fill Material shall consist of a mixture of clay, silt, sand, and gravel-sized particles obtained from previously constructed subsoil stockpiles. These materials can be used separately or mixed as required for best results. When placed, Embankment Material shall have a USCS classification of SM, ML, or CL and shall be uniform. This material shall be free of ice, snow, organic matter, rubbish, and debris. Coarse-grained particles shall be well dispersed to prevent the development of segregated pockets or zones with insufficient fine material to fill the interstices.

B. Soil Liners

The Soil Liner for the Gypsum Management Facility is considered a Clay Liner, and shall be soil classification CL, CL-ML, or CH. The material shall be free of roots, debris, organic or frozen material, and shall have a maximum clod size no greater than the length of the compactor foot for the compaction equipment proposed by the Contractor. When compacted, the material shall have a hydraulic conductivity of less than 1 x 10⁻⁴ cm/sec.

C. Soil Stabilizers and Moisture Conditioning Agents

Additives to accelerate drying or to improve stability and workability of soil shall not be permitted unless approved in writing by the Owner's Representative.

2.02 EQUIPMENT

A. Compaction Equipment

Tamping foot rollers

Compaction equipment shall consist of tamping foot rollers which have a minimum weight of 40,000 pounds. At least one tamping foot shall be provided for each 110 square in. of drum surface. The length of each tamping foot, measured from the outside surface of the drum, shall be at least 1 in. longer than the loose lift thickness.

Steel-Wheeled Rollers

Equipment used to produce a smooth compacted surface shall be a smooth, non-vibratory steel wheeled roller weighing not less than 1,000 lb. per lineal ft.

B. Scarification Equipment

Discs, rotor tillers, or other equipment used to scarify the surface shall be capable of uniformly disturbing the upper 6 in. of surface to provide good bonding between lifts.

C. Mixing and Spreading Equipment

Discs, harrows, and motor graders or other similar equipment shall be available at the site for use in spreading, mixing, and drying Compacted Subsoil Stockpile Material.

PART 3. EXECUTION

3.01 PREPARATION

A. Control of Work

Benchmarks, monuments, and other reference points shall be maintained throughout the work area.

B. Utility Location

Before starting excavation, the location and extent of underground utilities in the work area shall be established.

3.02 EXCAVATION

A. General

Excavation consists of removal and redistribution of material encountered when establishing required grade and subgrade elevations. The Contractor shall be responsible for dewatering, protection, shoring, and disposal of excavated materials as necessary to complete the excavation.

B. Procedures

Excavation may be accomplished by any method and by use of any equipment that is suitable to the work, except that blasting will not be permitted. Based on previous construction experience at the site, it is recommended that excavation to the foundation grade be completed as far in advance of low permeability soil placement as possible to allow the foundation surface to dry and form a "crust" capable of sustaining compactive effort.

C. Overexcavation

All excavation shall be performed to the lines and grades indicated on the plans. Any overexcavation or excess excavation not requested by the Owner's Representative shall be at the expense of the Contractor.

D. Disposal of Excavated Materials

Contractor shall utilize excavated material as stockpile materials for future use as specified in paragraph E.

E. Stockpile Requirements

- Excavated clay and silty clay materials are to be stockpiled in the shortterm subsoil stockpile area.
- Excess excavated materials are to be stockpile in the areas designated on the drawings.
- Materials not suitable for use as fill or backfill shall be disposed of onsite in the locations specified by the Owner's Representative.
- Spread fill material for use by others, topsoil, and low permeability soil are to be stockpiled in layers not to exceed 1 ft loose thickness.
- Tops of stockpiles are to be graded to ensure positive drainage. Side slopes for stockpiles shall be no steeper than 3H:1V.
- Perimeter ditches are to be excavated to intercept runoff flowing toward stockpile areas and to route it to outlet locations approved by the Owner's Representative.

3.03 SUBGRADE PREPARATION

- A. Areas to receive fill shall be proof rolled under the observation of the Owner's Representative. Soft, loose, weak, or wet materials shall be removed and replaced with compacted fill or stabilized with geotechnical fabric or geogrid as directed by the Owner's Representative. Joints, fractures, and moisture seeps shall be repaired, and local sand deposits, if present at foundation grade, shall be removed and backfilled with compacted fill material as directed by the Owner's Representative.
- B. The Owner's Representative may recommend additional drying time for soft, wet subgrade that has not been exposed long enough to permit "crust" formation. If approved by the Owner's Representative, the Contractor may install, at his own expense, geotechnical fabric or geogrid to stabilize the wet subgrade and expedite construction.
- C. No fill shall be placed until the subgrade has been examined and approved.

3.04 GENERAL FILL

A. Placement

- Unless otherwise indicated on the plans, all fill shall be composed of Earth Fill Material.
- 2. Fill materials used in embankment construction shall normally be placed in lanes parallel to the embankment axis and shall be placed in conformance with the lines, grades, and slopes as indicated on the plans. Placement of fill materials in lanes which are not parallel to the embankment will be allowed only where working room is too restricted for normal placement as determined by the Owner's Representative.
- 3. Fill shall be spread in approximately flat layers in such a manner as to obtain lifts of relatively uniform thickness without spaces between successively deposited loads. Segregation shall be prevented during placing and spreading. Hauling equipment shall be routed across the fill in such a way as to promote uniform compaction and to prevent the formation of ruts.
- 4. The maximum compacted thickness of each lift shall not exceed 8 in. where heavy compaction equipment will be used. The maximum compacted thickness shall not exceed 3 in. where power tampers or similar smaller equipment will be used. It may be necessary to reduce the thickness of lifts in order to obtain the required minimum density.
- Where compacted earth fill is to be placed against existing slopes, each lift shall be keyed into existing slope by removing existing slope material in steps as each new lift is placed.
- 6. The surface of the fill shall be kept reasonably smooth. The fill surface shall be sloped transverse to the axis of the embankments to allow drainage. If the compacted surface is, in the opinion of the Owner's Representative, too smooth or too dry to bond properly with the

succeeding lift, it shall be roughened by scarifying, light discing, or other acceptable means, and it shall be sprinkled before the succeeding lift is placed thereon. If the surface becomes rutted or uneven subsequent to compaction, it shall be flattened and leveled before placing the next lift. This extra work shall be at the Contractor's expense.

- 7. Fill operations shall be suspended during periods of extended wet weather. Upon resuming operations, all fill materials that are excessively wet or soft shall be reprocessed in place or removed and stockpiled for reprocessing. The removal of soft material shall be carried to such depth as is necessary to expose firm materials. Fill shall not be placed on frozen surfaces.
- 8. When filling operations at any section will be suspended for any period in excess of 12 hours or in wet weather, the surface of the fill shall be rolled smooth to seal it against excessive absorption of moisture and to facilitate runoff. Prior to resuming fill placement and compaction, the fill surface shall be scarified and/or disced and moisture conditioned as required.
- The Contractor will receive no additional compensation for any removal, reprocessing, stockpiling, recompaction, wasting, or similar operation related to suspensions or conditions due to weather or other causes unless caused by the Owner.
- Earth fill access ramps shall not be constructed within the limits of the compacted embankments without prior approval. When such ramps are approved, they shall be constructed of low permeability soil (in-board of the perimeter berm) or compacted fill (out-board of the perimeter berm).

B. Compaction -

- Fill materials shall be compacted to a dry density equal to or greater than the following:
 - The Gypsum Management Facility: 95 percent of the maximum dry density obtained from the Standard Proctor Test, ASTM D698.

In order to insure uniform coverage and to facilitate construction inspection and control, the compaction of each layer shall proceed in a systematic, orderly, and continuous manner. Rolling shall be parallel to the embankment axis, except where there is insufficient working room for such operations.

- The moisture content of all earth fill materials shall be as uniform as
 practicable throughout each lift. Fill shall be compacted at a moisture
 content that is no more than 2 percent below and no more than 2 percent
 above optimum moisture content.
- Moisture conditioning of fill materials shall be performed by discing, harrowing, plowing, blading, or other suitable means prior to excavation. Moisture conditioning where the fill is placed shall be limited to minor adjustments prior to compaction. Addition of moisture shall be by using a

- pressure spray bar mounted in front of or to one side of a water tanker so that water will not collect in the tracks of the truck.
- 4. Compaction of fill materials shall not commence if the moisture content is not within the specified limits. Any materials that are placed but not compacted prior to drying out or becoming too wet shall be removed and replaced or reprocessed at the Contractor's expense.
- No admixtures as drying agents or to improve the workability of the soil will be allowed.

3.05 SOIL LINERS

A. Sources

The Soil Liners for the Gypsum Management Facility shall be constructed from Soil Liner Material as described in paragraph 2.01(B) above.

B. Test Liner

A compacted low permeability soil test liner of the actual full scale liner shall be constructed in accordance with the following requirements:

- Test liner will be constructed from the same soil material sources, to the same design specifications, and with similar equipment and procedures as are proposed for the full scale liner.
- Test liner will be at least four times the width of the widest piece of equipment to be used.
- Test liner will be no less than 100 ft long to allow equipment to reach normal operating speed before reaching a central 40-ft test area.
- Test liner will be constructed with maximum 8-in. compacted lifts for a total liner thickness of 3 ft.
- Test liner will be tested by the Owner's Testing Consultant as described below for each of the following physical properties:
 - a. Multiple two-stage Boutwell permeameter tests will be used on the test liner to determine the hydraulic conductivity. The two-stage field hydraulic conductivity test is a falling head infiltration test conducted in a cased borehole, typically 4 in. in diameter. The test is cited in the U.S. EPA Technical Guidance Document: Quality Assurance and Quality Control for Waste Containment Facilities, September 1993 (EPA/600/R-93/182).
 - Undisturbed samples (Shelby tubes) will be tested in the laboratory for hydraulic conductivity to determine if there is a statistical correlation to the field testing results.
 - c. Other engineering parameters including, but not limited to, particle size analysis, liquid limits, plasticity, water content, and in-place density that are needed to evaluate the full scale liner will be determined.

 Additional test fills will be constructed for each new soil type or for each change in equipment or procedures.

C. Full Scale Liner Construction:

- Full scale liner construction shall not be commenced until the results of the in-place compaction testing and Boutwell permeameter tests on the test liner confirm that the construction procedures and specified compaction requirements produce a in-situ hydraulic conductivities as specified in Section 2.01(B) above.
- 2. The liner shall be constructed according to the placement and compaction requirements for general fill, except the material shall be compacted to a density of no less than 95 percent of maximum dry density at a moisture content between 100 percent and 105 percent of optimum. The same compaction procedures, such as number of passes, speed, and compaction equipment used on construction of the test liner shall be used. Grade stakes shall not be driven into the clay liner.
- The completed liner shall be smooth rolled to limit moisture loss and promote run-off of surface water. Moisture content shall be maintained within the specified range and erosion or other damage that occurs in the soil liner shall be repaired as directed by the Owner's Representative until the geosynthetic liner is placed.
- Repair of any rutting or other damage caused by the installation of the geosynthetic liner will be paid for on a time and material basis.
- 5. Voids created in the clay barrier layer during construction (including, but not limited to, penetrations for test samples, and other penetrations necessary for construction) shall be repaired by removing material that does not meet the requirements for low permeability soil, placing low permeability soil backfill, granular or pelletized bentonite, or a mixture of bentonite and low permeability soil in lifts no thicker than 2 in. and tamping each lift with a steel rod. Each lift shall be tamped a minimum of 25 times altering the location of the rod within the void for each blow. Other ruts and depressions in the surface of the lifts shall be scarified, filled, and then compacted to grade.

3.06 CUSHION DIRT

Cushion Dirt to be placed beneath the upper High Density Polyethylene (HDPE) Geomembrane is to be placed to the specifications for General Fill in Section 3.04 above, except fill materials for Cushion Dirt shall be compacted to a dry density equal to or greater than 90 percent of the maximum dry density obtained from the Standard Proctor Test, ASTM D698.

3.07 ANCHOR TRENCH CONSTRUCTION

A. Gypsum Management Facility

- A ledge at the bottom of the anchor trench elevation shall be excavated.
 Low permeability soil shall be placed and compacted on the ledge as shown on the anchor trench details in the plans.
- The anchor trench shall be excavated to the depth and width shown on the anchor trench details. The front edge of the trench shall be rounded to eliminate any sharp corners that could cause excessive stress to the geosynthetic liners. Loose soil shall be removed or compacted into the floor of the trench.
- 3. Subsequent to Geosynthetic Clay Liner (GCL), Bottom HDPE Geomembrane and Geotextile Cushion installation, it shall be verified that the liners cover the entire trench floor, but do not extend up the back of the trench wall. After the liner installation in the trench has been inspected and approved by the Owner's Representative, the trench shall be backfilled with 1 ft. of low permeability soil. The backfill shall be deposited and compacted according to the requirements for general fill in such a manner as to prevent damage to the GCL and liner materials.
- 4. Subsequent to installation of separation geotextile on top of drainage layer, it shall be verified that the fabric extends across the top of the initial 1 ft layer of trench backfill, but does not extend up the back of the trench wall. After the fabric installation in the trench has been inspected and approved by the Owner's Representative, the trench shall be backfilled with 1 ft of low permeability soil. The backfill shall be deposited and compacted according to the requirements for general fill in such a manner as to prevent damage to the geotextile fabric.
- 5. Subsequent to installation of the upper HDPE Geomembrane, verify that the liner extends across the top of the initial 1 ft layer of trench backfill, but does not extend up the back of the trench wall. After the liner installation in the trench has been inspected and approved by the Owner's Representative, backfill the remainder of the trench to the top of the low permeability soil layer. Deposit and compact the backfill according to the requirements for general fill in such a manner as to prevent damage to the HDPE Geomembrane.

3.08 TESTING

A. Construction Quality Assurance (CQA) compaction and permeability tests will be made by the Owner's Testing Consultant during the progress of the work as indicated in Appendix 2. The Contractor shall cooperate with the Testing Consultant and allow such tests to be performed. B. If tests indicate that an area of fill or low permeability soil liner does not meet the specified requirements, additional tests shall be performed to determine the extent of non-compliance. The Contractor shall moisture condition and recompact that area until a passing test result is obtained.

3.08 FINISH GRADING

All excavated and filled areas shall be fine graded and leveled to provide a smooth finish free of debris, foreign matter, objectionable stones, clods, lumps, pockets, or high spots, properly drained and true to indicated elevations. Finish grading shall be only near completion of work or when requested. Any portions of the berm damaged by construction shall be restored. The berm ditch shall be finished to design grade, and the ditch side slopes shaped and trimmed to provide a uniform ditch cross section.

3.09 CONSTRUCTION TOLERANCES

- A. The foundation grade and finished earthwork grades shall be no more than 0.4 ft below and not above plan grade.
- B. The minimum thickness of low permeability soil layer shall be 3 ft.

END OF SECTION 02200

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PART 1. GENERAL

1.01 DESCRIPTION

This section pertains to the placement of riprap for erosion control.

1.02 RELATED SECTIONS

The following section contains items which are related to the work in this section:

02200 - Earthwork

1.03 REFERENCES

Specified references or cited portions thereof, current at date of bidding documents unless otherwise specified, govern the work.

A. Illinois Department of Transportation (IDOT): Standard Specifications for Road and Bridge Construction, adopted January 1, 2007.

1.04 SUBMITTALS

Product Data: Provide quarry name and material type prior to delivery.

PART 2. PRODUCTS

2.01 MATERIALS

- A. Stone Riprap and Bedding materials according to Article 1005.01 of the Illinois Standard Specifications for Road and Bridge Construction.
- B. Filter Fabric material for Stone Riprap according to Article 1080.03, with an AOS (Apparent Opening Size) as indicated on the plans.
- Supplier shall be listed on the current IDOT Approved Aggregate Source List.
- D. Gradation as indicated in the drawings. Quality shall be Class A.

PART 3. EXECUTION

3.01 CONSTRUCTION REQUIREMENTS

- A. Stone Riprap and Bedding shall be installed in accordance with Section 281 of the Illinois Standard Specifications for Road and Bridge Construction for the placement of Stone Riprap. Measurement and payment provisions of Section 281 shall not apply.
- Filter Fabric for Stone Riprap shall be installed in accordance with Section 282 of the Illinois Standard Specifications for Road and Bridge Construction.
- C. The Owner's Representative shall be allowed to visually inspect Riprap for compliance with specifications prior to placement.

END OF SECTION 02275

DIVISION 2 – SITEWORK Section 02315 – Granular Materials

PART 1. GENERAL

1.01 DESCRIPTION

A. Gypsum Management Facility

This section pertains to the following:

- Furnishing and placing granular drainage materials for the drainage layer and leachate collection system.
- Furnishing and placing coarse aggregate for encasement of the ring drain collection piping.
- Furnishing and installing materials for roadbed construction related to the Gypsum Management Facility access roads and the McKinley Road relocation.
- 4. Recycle Pond Drain.

1.02 RELATED SECTIONS

The following sections contain items which are related to the work in this section:

- 02300 Earthwork
- 02373 Geotextiles
- 02640 HDPE Piping

1.03 REFERENCES

The following references, or cited portions thereof, govern the work:

- Illinois Department of Transportation (IDOT): Standard Specifications for Road and Bridge Construction, adopted January 1, 2007.
- American Society for Testing and Materials (ASTM):
 - ASTM D 75 (2003) Practice for Sampling Aggregates.
 - ASTM D 422 (1963; R 2002) Test Method for Particle-Size Analysis of Soils.
 - ASTM D 2434 (1968, R 2000) Test Method for Permeability of Granular Soils (Constant Head).
 - d. ASTM D 3042 (2003) Test Method for Insoluble Residue in Carbonate Aggregates.
 - e. ASTM C 1260 (2005) Standard Test Method for Potential Alkali Reactivity of Aggregates (Mortar-Bar Method).

 American Geological Institute (AGI). Geoscience Handbook AGI Data Sheets, 4th Edition.

1.04 MEASUREMENT AND PAYMENT

The Contractor shall be responsible for estimating the extent of granular materials required to complete the work including, but not limited to, construction of drainage layer, encasement of leachate collection piping, and road-bed construction. The Contractor shall include the dollar amount associated with furnishing and placing all granular materials in his Lump Sum Bid amount.

1.05 COORDINATION

A. The geosynthetic liner shall be covered with granular materials as soon as practicable after a section of liner has been approved by the Owner's Representative.

1.06 SUBMITTALS

A. Product Data:

- Aggregate source list: Submit a list of proposed aggregate sources.
- Shipping Tickets: Submit shipping tickets for the granular materials delivered to the site. Shipping tickets shall be according to paragraph 1004.01f of the IDOT Standard Specifications.

B. Test Reports.

 Submit results of grain size analysis (ASTM D422) and hydraulic conductivity testing (ASTM D2434) for gradations established by the Contractor that provide the specified hydraulic conductivity. Test results are required for each proposed source and gradation. Submit test results for each source demonstrating compliance with reactivity, soundness, and abrasion requirements specified herein.

C. Samples:

 Submit one sample per source for each gradation proposed for use on the project. Samples shall be at least one pound and shall be obtained and shipped according to ASTM D75. Submit samples at least 15 days prior to starting construction of the drainage layer and coarse aggregate encasement for leachate piping.

1.07 STORAGE AND HANDLING

A. Storage and handling of granular materials shall be according to paragraph 1004.01e of the IDOT Standard Specifications.

1.01

PART 2. PRODUCTS

2.01 MATERIALS

A. General

- Unless otherwise approved by the Owner's Representative, granular materials shall be obtained from sources listed on the current IDOT Approved Aggregate Source List (www.dot.il.gov\materials\) approvedaggregatesources.pdf).
- Coarse Granular materials shall be meet the Description of Gravel, as described in Section 1004.01(a)(1) of the IDOT Standard Specifications, and shwll be spherical to sub-discoidal, sub-rounded to well rounded particles as defined by AGI Data Sheet, 4th Edition, Sheet 8.4 – Comparison Charts for Estimating Roundness and Sphericity.
- Granular materials shall experience no more than 15 percent carbonate loss per ASTM D3042.
- Granular materials shall be free of deleterious material, and shall meet the Na₂SO₄ soundness and Los Angeles Abrasion Specifications for Class B quality aggregate per paragraph 1004.01 of the IDOT Standard Specifications.
- All material shall pass the 2 in. sieve, and no greater than 5 percent shall be retained on the No. 200 sieve.
- Granular materials shall be innocuous to alkali-silica reactivity, and shall exhibit internal expansions of less than 0.10 percent at 16 days after casting as determined by ASTM C 1260.

B. Gypsum Management Facility Granular Materials

Granular Materials for Drainage Layer

Gradation for granular material for drainage layer shall be as required to provide a minimum hydraulic conductivity (ASTM D2434) of 1 x 10⁻³ cm/sec.

Coarse Aggregate around Ring Drain Collection Piping

Coarse Aggregate used to encase the ring drain collection piping shall be IDOT Gradation CA 7 material as outlined in Article 1004.01 of the IDOT Standard Specifications for Road and Bridge Construction.

Filter Sand

Filter Sand used for protective cover over the ring drain collection system shall be IDOT Gradation FA 1, Class B or better according to Article 1003 of the IDOT Standard Specifications for Road and Bridge Construction.

Aggregate Base Course, Type B

Aggregate Base Course, Type B used for base material for all new access roads and shall be IDOT Gradation CA 2, in accordance with Section 1004.04 of the IDOT Standard Specifications for Road and Bridge Construction. The material shall originate from an IDOT approved source. The Na₂SO₄ soundness and Los Angeles Abrasion Specifications for Class B quality aggregate per paragraph 1004.01 of the IDOT Standard Specifications shall not apply.

Aggregate Surface Course, Type B

Aggregate Surface Course, Type B used for surface material for all new access roads and the McKinley Road relocation shall be IDOT Gradation CA 6, in accordance with Section 1004.04 of the IDOT Standard Specifications for Road and Bridge Construction. The material shall originate from an IDOT approved source. The Na₂SO₄ soundness and Los Angeles Abrasion Specifications for Class B quality aggregate per paragraph 1004.01 of the IDOT Standard Specifications shall not apply.

2.02 EQUIPMENT

Equipment for spreading and compacting granular materials shall be low ground pressure equipment to prevent damage to the underlying geosynthetic liners.

PART 3. EXECUTION

3.01 PROTECTION OF GEOSYNTHETICS

- A. Protection of the geosynthetic liners is critically important. Approved geosynthetic liner shall be covered by granular material as soon as practicable. Granular material shall be placed to a minimum thickness of 1 ft before any heavy equipment or loaded trucks are allowed on the lined area.
- No equipment will be permitted directly on the geosynthetic liner.
- C. Any damage to the geosynthetic liner system shall be repaired, as directed by the Owner's Representative, at the expense of the Contractor.

3.02 GRANULAR DRAINAGE LAYER (GYPSUM MANAGEMENT FACILITY)

A. Placement on Cell Floor

- The granular material shall be back-dumped on the geotextile cushion fabric in a sequence of operations beginning at the perimeter of the liner on the cell floor.
- 2. Placement of material on the fabric shall be accomplished by spreading dumped material off of previously placed material with a bulldozer blade or endloader, in such a manner as to prevent tearing or shoving of the cloth. Dumping of material directly on the fabric will only be permitted to establish an initial working platform. No vehicles or construction equipment shall be allowed on the fabric prior to placement of the granular blanket to a minimum thickness of 1 ft.

B. Placement on Cell Side Slopes

- Placement of granular material on cell side slopes shall be accomplished using methods and equipment similar to that specified for placement of material on cell floor.
- The Contractor may place gypsum underlain with separation geotextile fabric to buttress the granular material on the slope:
 - The Construction Quality Assurance (CQA) survey to certify thickness of drainage material shall be completed within the footprint of the gypsum stack before gypsum placement.

b. Separation geotextile fabric shall extend beyond the toe of gypsum buttress a sufficient distance to prevent contamination of the granular drainage layer. See Sections 02373 and 02320 for construction of separation geotextile fabric and gypsum, respectively.

3.04 COARSE AGGREGATE FOR ENCASEMENT OF RING DRAIN COLLECTION PIPING (GYPSUM MANAGEMENT FACILITY)

- A. The geotextile filter fabric for encasement of leachate collection piping shall be placed on the approved cushion geotextile fabric according to Section 02373 – Geotextiles.
- B. The coarse aggregate shall be placed on the encasement fabric to the width shown on the plans to the level of the bottom of the ring drain collection piping.
- C. Course aggregate shall be placed and tamped along the pipe during pipe installation. The coarse aggregate shall be placed longitudinally along the pipe in lifts not to exceed 8 in. thick to a height of at least the center of the pipe. The aggregate shall be maintained at equal elevation on each side of the pipe, and the first lift of material shall be mechanically tamped to ensure that the space under the pipe is completely filled. The top of pipe shall not be covered until the CQA survey certifies leachate piping grade has been completed.
- C. After the CQA survey has been completed, coarse aggregate material shall continue to be placed in lifts not to exceed 8 in. thick, as specified in the previous paragraph until the minimum cover height shown in the plans is attained.
- D. The running of trucks or heavy equipment over leachate piping shall be avoided until there is at least a 12 in. cover of Filter Sand over the completed geotextile envelop. Temporary ramps no steeper than 10H:1V transverse to the piping shall be provided for temporary equipment crossings until the first lift of gypsum is placed.

3.03 ROADWAY CONSTRUCTION

- Prepare the roadway subgrade as shown on the plans, in accordance with Section 02200 – Earthwork.
- Furnish Geotechnical Fabric for Ground Stabilization in accordance with Section 02373 – Geotextiles.
- C. Furnish Aggregate Base Course, Type B in accordance with Article 351 of the IDOT Standard Specifications for Road and Bridge Construction.

D. Furnish Aggregate Surface Course, Type B in accordance with Article 402 of the IDOT Standard Specifications for Road and Bridge Construction.

3.04 TESTING

- A. CQA gradation and permeability tests will be made by the Owner's Testing Consultant during the progress of the work as indicated in Appendix 2. The Contractor shall cooperate with the Testing Consultant and allow such tests to be performed.
- B. If tests indicate that an area of granular material or coarse aggregate does not meet the specified requirements, then the Contractor shall remove the material and replace it with suitable material.

3.05 FINISH GRADING

The granular drainage layer shall be fine graded to provide a smooth finish before a CQA survey of the completed portion of the drainage layer is requested. Ruts or erosion damage shall be repaired before placement of the separation geotextile fabric.

3.06 CONSTRUCTION TOLERANCES

The minimum thickness of drainage layer shall be 1 ft.

END OF SECTION 02315

PART 1. GENERAL

1.01 DESCRIPTION

This section pertains to furnishing and installing geotextile fabrics on prepared surfaces.

1.02 RELATED SECTIONS

The following sections contain items which are related to the work in this section:

- 02300 Earthwork
- 02315 Granular Materials
- 02800 HDPE Geomembrane

1.03 REFERENCES

The following references, or cited portions thereof, govern the work:

- Illinois Department of Transportation (IDOT): Standard Specifications for Road and Bridge Construction, adopted January 1, 2007.
- American Society for Testing and Materials (ASTM):
 - a. ASTM 3776 (1996; R 2002) Standard Test Method for Mass per Unit Area (Weight) of Fabric;
 - ASTM D 3786 (2001) Test Method for Hydraulic Bursting Strength of Textile Fabrics – Diaphragm Bursting Strength Tester Method;
 - ASTM D 4533 (2004) Test Method for Trapezoid Tearing Strength of Geotextiles;
 - ASTM D 4632 (1991; R 2003) Test Method for Grab Breaking Load and Elongation of Geotextiles;
 - e. ASTM D 4751 (2004) Test Method for Determining Apparent Opening Size of Geotextile;
 - f. ASTM D 4833 (2000) Test Method for Index Puncture Resistance of Geotextiles, Geomembranes, and Related Products;
 - g. ASTM D 4873 (2002) Guide for Identification, Storage, and Handling of Geosynthetic Rolls;
 - ASTM D 4884 (1996; R 2003) Test Method for Strength of Sewn or Thermally Bonded Seams of Geotextiles;
 - ASTM D5261-92(2003) Standard Test Method for Measuring Mass per Unit Area of Geotextiles

ASTM D6241-04 Standard Test Method for the Static Puncture Strength of Geotextiles and Geotextile-Related Products Using a 50-mm Probe

1.04 MEASUREMENT AND PAYMENT

- A. The Contractor shall be responsible for estimating the extent of geotextile fabric required to complete the work including fabric for laps, anchorage, repairs, and samples for Construction Quality Assurance (CQA) testing. The Contractor shall include the dollar amount associated with all geotextile construction in his Lump Sum Bid amount, except as specified in paragraph B.
- B. Geotextile fabric for ground stabilization, when directed by the Owner's Representative, will be paid for on a time and materials basis.
- C. No additional payment will be made for geotextile fabric for ground stabilization installed at the Contractor's discretion.

1.05 SUBMITTALS

A. Product Data

- The manufacturer's list of guaranteed properties for each geotextile fabric or geogrid proposed for use on the project shall be submitted.
- The manufacturer's installation guidelines shall be submitted.

B. Samples

Samples of geotextile fabrics shall be submitted for CQA prequalification testing. Sample size and sampling frequency are specified in Appendix 2.

C. Inventory

A copy of the roll inventory that identifies, as a minimum, manufacturer or supplier, product or style number, roll number, width, and length of roll as identified on the roll label shall be submitted.

1.06 STORAGE AND HANDLING

Geotextiles shall be stored and handled according to ASTM D4873.

PART 2. PRODUCTS

2.01 MATERIALS

A. Geotextile Fabric for Liner System

Geotextile fabrics for use in the cell liner system shall consist of non-woven filaments of polypropylene, polyester, or polyethylene. Stabilizers and/or inhibitors shall be added to the base polymer if necessary to make the filaments resistant to deterioration caused by ultraviolet light and heat exposure. Reclaimed or recycled fibers or polymer shall not be added to the formulation. Non-woven fabric may be needle-punched, heat-bonded, or a combination thereof. The filaments shall be dimensionally stable (i.e., filaments shall maintain their relative position with respect to each other) and resistant to delamination. The edges of the geotextile shall be finished to prevent the outer fiber from pulling away from the geotextile. The filaments shall be free from any chemical treatment or coating that might significantly reduce porosity and permeability.

Fabric shall have the following physical properties:

| Physical Properties ⁽¹⁾ | 4 oz. (Separation) | 6 oz. (PWRS) | 16 oz. (CA Envelope) |
|---|-----------------------|-----------------|-------------------------|
| Mass/Unit Area (oz/yd²) ASTM D5261 | 4.0 | 6.0 | 16.0 |
| Grab Tensile Strength (lb.) ASTM D4632 | 115 | 160 | 380 |
| Grab Elongation (%) ASTM D4632 | 50 | 50 | 50 |
| Puncture Strength (lb.) ASTM D4833 | 65 | 85 | 240 |
| Puncture (CBR) Strength (lb.) ASTM D6241 | 310 | 410 | 1025 |
| Mullen Burst Strength (psi) ASTM D3786 | 210 | 280 | 750 |
| Trapezoidal Tear Strength (lb.) ASTM D4533 | 50 | 60 | 150 |
| Width (ft.) | 15 | 15 | 15 |
| Apparent Opening Size (AOS) Max. US Std. Sieve No. ASTM D4751 | 70 | 70 | 100 |
| UV Resistance ⁽²⁾ (%) ASTM D4355 | 70 | 70 | 70 |
| Roll Width (ft.) | 15 | 15 | 15 |

Notes:

All Values listed are Minimum Average Roll Values (MARV) unless otherwise noted, calculated as the typical minus two standard deviations.

⁽²⁾ UV Resistance is a minimum value and not a MARV. Evaluation to be on 2.0 inch strip tensile specimens after 500 hours exposure.

Cushion Geotextile Fabric.

Cushion geotextile fabric shall consist of non-woven filaments of polypropylene, polyester, or polyethylene. Stabilizers and/or inhibitors shall be added to the base polymer if necessary to make the filaments resistant to deterioration caused by ultraviolet light and heat exposure. Reclaimed or recycled fibers or polymer shall not be added to the formulation. Non-woven fabric may be needle-punched, heat-bonded, or a combination thereof. The filaments shall be dimensionally stable (i.e., filaments shall maintain their relative position with respect to each other) and resistant to delamination. The edges of the geotextile shall be finished to prevent the outer fiber from pulling away from the geotextile. The filaments shall be free from any chemical treatment or coating that might significantly reduce porosity and permeability.

Fabric shall have the following physical properties:

| Physical Properties ⁽¹⁾ | 10 oz. (Cushion) | |
|---|---------------------|--|
| Mass per unit area (oz/yd²) ASTM D5261 | | |
| Grab Tensile Strength (lb.) ASTM D4632 | 230 | |
| Grab Tensile Elongation (%) ASTM D4632 | 50 | |
| Trapezoidal Tear Strength (lb.) ASTM D4533 | 95 | |
| Puncture (CBR) Strength (lb.) ASTM D6241 | 700 | |
| Puncture (CBR) Elongation (in.) ASTM D6241 | 1.5 | |
| UV Resistance ⁽²⁾ (%) ASTM D4355 | 70 | |
| Apparent Opening Size (Max.) (AOS) Sieve No ASTM D4751 | *** | |
| Roll Width (ft.) | 15 | |

Notes:

B. Geotechnical Fabric for Ground Stabilization

Geotechnical fabric for ground stabilization shall conform to Article 1080.02 of the IDOT Standard Specifications for Road and Bridge Construction.

All Values listed are Minimum Average Roll Values (MARV) unless otherwise noted, calculated as the typical minus two standard deviations.

⁽²⁾ UV Resistance is a minimum value and not a MARV. Evaluation to be on 2.0 inch strip tensile specimena after 500 hours exposure.

C. Thread for Seams

High strength thread should be used such that seam test should conform to ASTM D4884. The thread shall meet the chemical, ultraviolet, and physical requirements of the geotextile, and the color shall be different from that of the geotextile.

D. Securing Devices

Pins, staples, and other devices that project through the geotextile fabric are not permitted for fabrics installed above the geomembrane. Sandbags, stone, or other appropriate means approved by the Owner's Representative shall be used to prevent movement of the geotextile.

2.02 EQUIPMENT

A. Equipment for spreading and compacting granular materials shall be low ground pressure equipment to prevent damage to the underlying geosynthetic liners.

PART 3. EXECUTION

3.01 SAMPLES FOR CQA TESTING

- Geotextile fabric samples shall be obtained, identified and packaged from rolls designated by the Owner's Representative according to ASTM D4873.
- Samples shall be 3 ft. wide by the full roll width.

3.02 BASE PREPARATION

- A. Surface on which the geotextile will be placed shall be prepared to a relatively smooth surface condition, and shall be free from obstruction, debris, depressions, erosion features, or any irregularities that would prevent continuous, intimate contact of the geotextile with the entire surface. Rills, gullies, and ruts must be graded out of the surface before geotextile placement. Areas on which geotextile are to be placed shall be graded and/or dressed in accordance with Section 02200 Earthwork and Section 02315 Granular Drainage Materials. Immediately prior to placing the geotextile, the prepared base will be inspected by the Owner's Representative, and no material shall be placed thereon until that area has been approved.
- B. Geotextile cushion fabric will be installed directly on the geosynthetic liner. Jointly inspect the liner with the Owner's Representative before commencing fabric installation each day. Notify the Owner's Representative promptly of any damage or defects observed in the liner as fabric installation progresses. Do not place fabric in the damaged or defective area until the liner has been repaired and

approved by the Owner's Representative. Submit a daily inspection report identifying the area of fabric placement and certifying that there were no visible defects in the area of fabric placement.

C. Do not run heavy vehicle traffic directly on the geosynthetic liner or cushion geotextile. Use vehicles and equipment as specified in paragraph 2.02 to transport and deploy fabric on the liner. Operate the equipment with care, and place protective cover over the geomembrane, if necessary, to avoid damaging the liner. Route traffic and personnel over installed cushion fabric and use the installed fabric as a working platform to the greatest extent possible.

3.03 INSTALLATION

A. General Requirements:

- Geotextile fabric shall be unrolled and laid out following these requirements to the greatest extent practical:
 - Orient panels with the longest dimension parallel to the slope.
 - Minimize the number of seams in corners and odd-shaped areas.
 - Extend panels on slopes a minimum of 5 ft onto a horizontal surface.

Geotextile panels shall be unrolled using methods that will not damage the fabric and will protect underlying surface from damage. While unrolling, the geotextile fabric shall be visually inspected for imperfections and faulty or suspect areas marked. Ballast shall be placed on fabric to prevent wind uplift. Expansion and contraction should be allowed for by leaving slack.

Heavy vehicle traffic shall not be run directly on geotextile fabric. Fabric in areas of heavy traffic shall be protected with protective cover over the fabric.

2. Laps

Individual panels of geotextile fabric shall be lapped according to manufacturer's instructions and as specified herein. Provide a minimum overlap of 3 in. unless otherwise specified herein or in the plans. Shingle overlaps so that water or other material cannot run down the slope between the two layers of fabric.

Field Seams

Continuously sew all laps on slopes steeper than 10H:1V. This requirement does not apply to the heavy geotextile fabric for envelopment of coarse aggregate around leachate piping.

Defects and Repairs

Examine the installed geotextile fabric for defects, holes discontinuous seams, puckered or separated laps, etc. Repair defective laps and seams. Patch holes and defects according to manufacturer's recommendations and as directed by the Owner's Representative. Do not cover suspect or patched areas until they have been inspected and approved by the Owner's Representative.

B. Geotextile Fabric for Separation

- Use low ground pressure equipment to avoid rutting the granular material.
- Horizontal seams (parallel to top of slope) will be permitted on cell side slopes to facilitate staged construction of the drainage layer on the side slope.
- Extend separation geotextile fabric into and across the bottom of the anchor trench and complete backfill of the trench according to Section 02200.

C. Geotextile Fabric for Coarse Aggregate Envelope

- Geotextile for coarse aggregate envelope will be installed directly on the cushion fabric. Remove any foreign materials from the cushion fabric within the footprint of the coarse aggregate leachate piping encasement before installing the geotextile envelope. Place sufficient width to completely envelop the coarse aggregate and provide a longitudinal lap of at least 6 in.
- After the coarse aggregate encasement has been completed, according to Section 02315, wrap the geotextile around the mounded aggregate, and cover the lap with at least 6 in. of material before permitting vehicle or equipment on the fabric.
- Any ballast material other than coarse aggregate, according to Section 02315, that is placed within the envelope will require removal during coarse aggregate construction.

D. Geotechnical Fabric for Ground Stabilization

 Install Geotechnical Fabric for Ground Stabilization in accordance with Section 210 of the IDOT Standard Specifications for Road and Bridge Construction.

- If approved by the Owner's Representative, the Contractor may, at his own expense, install geotextile or geogrid for ground stabilization outside the limits designated by the Owner's Representative.
- Submit as-built drawings that clearly delineate limits and type of ground stabilization.

3.04 PROTECTION

- A. Protect installed fabric until it is covered by at least 1 ft. of overlying material.
- B. Any damage to the geotextile during its installation or during placement of overlying materials shall be replaced by the Contractor at no cost to the Owner. Unless otherwise noted, the work shall be scheduled so that the covering of the geotextile with a layer of the specified material is accomplished within 14 calendar days after placement of the geotextile. Failure to comply shall require replacement of geotextile. The geotextile shall be protected from damage prior to and during the placement of overlying materials. Before placement of overlying materials, the Contractor shall demonstrate that the placement technique will not cause damage to the geotextile.

3.05 TESTING AND INSPECTION

A. Prequalification Testing

Geotextiles are subject to CQA testing by the Owner's Testing Consultant to verify conformance with the manufacturer's list of guaranteed properties according to Appendix 2. The Contractor shall provide samples as specified herein. If tests indicate nonconformance to the list of guaranteed properties, provide additional samples as directed by the Owner's Representative to determine the extent of the non-conformance. Any fabric that does not conform to the list of guaranteed properties shall be removed from the site.

- B. Installed fabric shall be inspected by the Owner's Representative. No material shall be placed on the fabric, other than ballast, until the installation has been approved by the Owner's Representative. Ballast shall not obscure seams or significant length of unseamed laps. The Owner's Representative may require removal of ballast to inspect suspect areas.
- C. If the Owner's Representative suspects that completed work has been damaged by construction methods that do not conform to the specifications, he may require removal of completed work to verify the integrity of the underlying materials. The Contractor shall bear the cost of removal and subsequent repair as directed by the Owner's Representative.

END OF SECTION 02373

PART 1. GENERAL

1.01 DESCRIPTION

- A. This section covers furnishing and installation of a reinforced needlepunched Geosynthetic Clay Liner (GCL) at the Gypsum Management Facility and the CCB Management Facility.
- B. The work includes furnishing all equipment and materials, providing all labor, supervision, administration and management necessary to perform the work as specified herein and as shown on the plans.

1.02 RELATED SECTIONS

None.

1.03 REFERENCES

The following references, or cited portions thereof, govern the work

- American Society for Testing and Materials (ASTM):
 - a. ASTM D 4632 (1991; R 2003), Standard Test Method for Grab Breaking Load and Elongation of Geotextiles;
 - ASTM D 4643 (2000), Test Method for Determination of Water (Moisture) Content of Soil by the Microwave Oven Method;
 - ASTM D 5084 (2003), Test Method for Measurement of Hydraulic Conductivity of Saturated Porous Materials Using a Flexible Wall Permeameter;
 - d. ASTM D 5261 (1992; R 2003), Test Method for Measuring Mass Per Unit Area of Geotextiles;
 - e. ASTM D 5321 (2002), Test Method for Determining the Coefficient of Soil and Geosynthetic or Geosynthetic and Geosynthetic Friction by the Direct Shear Method;
 - f. ASTM D 5887 (2004), Test Method for Measurement of Index Flux Through Saturated Geosynthetic Clay Liner Specimens Using a Flexible Wall Permeameter;
 - ASTM D 5888 (1995; R 2002), Practice for Storage and Handling of Geosynthetic Clay Liners;
 - ASTM D 5889 (1997; R 2003), Practice for Quality Control of Geosynthetic Clay Liners;

- ASTM D 5890 (2002), Test Method for Swell Index of Clay Mineral Component of Geosynthetic Clay Liners;
- ASTM D 5891 (2002), Test Method for Fluid Loss of Clay Component of Geosynthetic Clay Liners.

1.04 SUBMITTALS

- A. With the bid, the Contractor shall furnish the following information:
 - Conceptual description of the proposed plan for placement of the GCL panels over the areas of installation.
 - GCL Manufacturer's Quality Control (MQC) Plan for documenting compliance with Sections 2.01 and 2.02 of these specifications.
 - GCL manufacturer's historical data for reinforced GCL of a) 10,000-hour creep shear testing per Section 2.01 D, and b) seam flow data at 2 psi confining pressure per Section 2.01 E.
 - A copy of GCL manufacturer's International Standards Organization (ISO) Quality Certificate of Registration.
 - Statement of experience from the proposed GCL supplier.
 - Statement of experience from the proposed GCL installer.
- B. At the Owner Representative's or Owner's request, the Contractor shall furnish:
 - 1. A representative sample of the GCLs.
 - A project reference list for the GCL(s) consisting of the principal details of at least ten projects totaling at least 10 million sq. ft (100,000 sq. meters) in size.
- C. Upon shipment, the Contractor shall furnish:
 - The GCL manufacturer's Quality Assurance/Quality Control (QA/QC) certifications to verify that the materials supplied for the project are in accordance with the requirements of this specification.
 - Inventory of materials received.
- D. As installation proceeds, the Contractor shall submit certificates of subgrade acceptance, signed by the Contractor and Construction Quality Assurance (CQA) Inspector (see Sections 1.06 and 3.03) for each area that is covered by the GCL.
- E. Warranty

After construction, the contractor shall submit material and installation warranty certificates.

1.05 OUALIFICATIONS

- A. GCL Manufacturer must have produced at least 10 million sq. ft. (1 million sq. meters) of GCL, with at least 8 million sq. ft. (800,000 sq. meters) installed.
- B. The GCL Installer must either have installed at least 1 million sq. ft. (100,000 sq. meters) of GCL, or must provide to the Engineer satisfactory evidence, through similar experience in the installation of other types of geosynthetics, that the GCL will be installed in a competent, professional manner.

1.06 CONSTRUCTION QUALITY ASSURANCE (CQA)

- A. The Owner shall provide a third-party inspector for CQA of the GCL installation. The inspector shall be an individual or company who is independent from the manufacturer and installer and who shall be responsible for monitoring and documenting activities, related to the CQA of the GCL throughout installation.
- B. Testing of the GCL as necessary to support the CQA effort shall be performed by a third party laboratory retained by the Owner and independent from the GCL manufacturer and installer.

WARRANTY

The geomembrane material shall be warranted, on a pro-rata basis against manufacturer's defects for a period of five (5) years from the date of liner installation. The installation shall be warranted against defects in workmanship for a period of (1) year from the date of liner completion.

PART 2. PRODUCTS

2.01 MATERIALS

- A. Acceptable products for the GCL are GCL Bentomat® SDN, as manufactured by CETCO, 1350 West Shure Drive, Arlington Heights, Illinois 60004 USA (847-392-5800), or an engineer-approved reinforced needlepunched GCL material equal to Bentomat SDN.
- B. The delineation of areas to receive GCL shall be agreed by the Installer and the Engineer prior to installation.
- C. The GCL and its components shall have the properties shown in the GCL Certified Properties table at the end of this section.
- D. The reinforced GCL shall have 10,000 hour test data for large-scale constant-load (creep) shear testing for related products under hydrated conditions. The

- displacement shall be 0.13 in. (3.3 mm) or less at a constant shear load of 250 psf (12 kPa) and a normal load of 500 psf (24 kPa).
- E. The reinforced GCL shall have seam test data from an independent laboratory showing that the seam flow with a grooved cut in one of the nonwoven geotextiles is less than 1 x 10⁻⁸ m³/m²/s at 2 psi hydraulic pressure.
- F. The minimum acceptable dimensions of full-size GCL panels shall be 150 ft. (45.7 m) in length. Short rolls [(those manufactured to a length greater than 70 ft. (21 meters) but less than a full-length roll)] may be supplied at a rate no greater than three (3) per truckload or three (3) rolls every 36,000 sq. ft. (3,500 sq. meters) of GCL, whichever is less.
- G. A 6-inch (150 mm) overlap guideline shall be imprinted on both edges of the upper geotextile component of the GCL as a means for providing quality assurance of the overlap dimension. Lines shall be printed in easily visible, nontoxic ink.

2.02 PRODUCT QUALITY DOCUMENTATION

The GCL manufacturer shall provide the Contractor or other designated party with manufacturing QA/QC certifications for each shipment of GCL. The certifications shall be signed by a responsible party employed by the GCL manufacturer and shall include:

- A. Certificates of analysis for the bentonite clay used in GCL production demonstrating compliance with the swell index and fluid loss parameters shown in the GCL Certified Properties tables.
- B. Manufacturer's test data for finished GCL product(s) of bentonite mass/area, GCL tensile strength and GCL peel strength (reinforced only) demonstrating compliance with the index parameters shown in the GCL Certified Properties tables.
- GCL lot and roll numbers supplied for the project (with corresponding shipping information).

2.03 PRODUCT LABELING

- A. Prior to shipment, the GCL manufacturer shall label each roll, identifying:
 - Product identification information (Manufacturer's name and address, brand product code).
 - Lot number and roll number.
 - Roll length, width and weight.

2.04 PACKAGING

- A. The GCL shall be wound around a rigid core whose diameter is sufficient to facilitate handling. The core is not necessarily intended to support the roll for lifting but should be sufficiently strong to prevent collapse during transit.
- All rolls shall be labeled and bagged in packaging that is resistant to photodegradation by ultraviolet (UV) light.

2.05 ACCESSORY BENTONITE

A. The granular bentonite sealing clay used for overlap seaming, penetration sealing and repairs shall be made from the same natural sodium bentonite as used in the GCL and shall be as recommended by the GCL manufacturer. Seaming of GCLs shall be conducted in accordance with the manufacturer's guidelines for each particular GCL. Please refer to the installation guidelines for Bentomat /Claymax GCLs.

PART 3. EXECUTION

3.01 SHIPPING AND HANDLING

- A. The rolls of GCL shall be packaged and shipped by appropriate means to prevent damage to the material and to facilitate off-loading.
- B. The Installation Supervisor shall be present during delivery and unloading of the GCL. A visual inspection of each roll should be made during unloading to identify if any packaging has been damaged. Rolls with damaged packaging should be marked and set aside for further inspection. The packaging should be repaired prior to being placed in storage. The Installation Supervisor shall prepare and submit an inventory that includes lot and roll number for materials received.
- C. The Installer is responsible for unloading the GCL. The Owner will make available equipment and operators employed at the site to assist with unloading. The Installer shall coordinate with the Owner to determine equipment availability and should contact the Manufacturer prior to shipment to ascertain the appropriateness of the proposed unloading methods and equipment.

3.02 STORAGE

A. Storage of the GCL rolls shall be the responsibility of the Installer. A dedicated storage area shall be provided by the Owner at the job site. Submit storage area requirements (size and preferred location) with bid documents.

- B. Rolls should be stored in a manner that prevents sliding or rolling from the stacks and may be accomplished by the use of chock blocks. Rolls should be stacked at a height no higher than that at which the lifting apparatus can be safely handled (typically no higher than four).
- C. All stored GCL materials and the accessory bentonite must be covered with a plastic sheet or tarpaulin until their installation.
- The integrity and legibility of the labels shall be preserved during storage.

3.03 EARTHWORK

- A. The low permeability soil layer upon which the GCL is installed shall be prepared and compacted prior to installation. The surface shall be smooth, firm, and unyielding, and free of:
 - Vegetation.
 - Construction debris.
 - Sticks.
 - Sharp rocks.
 - Void spaces.
 - Ice.
 - Abrupt elevation changes.
 - Standing water.
 - Cracks larger than 0.25 in. (6 mm) in width.
 - 10. Any other foreign matter that could contact the GCL.
- B. Immediately prior to GCL deployment, the low permeability soil layer shall be final-graded by the contractor to fill in all voids or cracks and then smooth-rolled to provide the best practicable surface for the GCL. At completion of this activity, no wheel ruts, footprints or other irregularities shall exist in the subgrade. Furthermore, all protrusions extending more than 0.5 in. (12 mm) from the surface shall either be removed, crushed or pushed into the surface with a smoothdrum compactor.
- On a continuing basis, the project CQA inspector shall certify acceptance of the subgrade before GCL placement.
- D. It shall be the Installer's responsibility thereafter to indicate to the Owner's Representative any change in the condition of the low permeability soil layer that could cause the subgrade to be out of compliance with any of the requirements listed in this Section. The Installation Supervisor shall certify in the daily report that no GCL was placed over visibly defective low permeability soil surface.
- E. At the top of sloped areas of the job site, an anchor trench for the GCL shall be excavated by the contractor in accordance with the project plans. The trench shall

be excavated and approved by the CQA Inspector prior to GCL placement. No loose soil shall be allowed at the bottom of the trench and no sharp corners or protrusions shall exist anywhere within the trench.

3.04 GCL PLACEMENT

- A. GCL rolls shall be delivered to the working area of the site in their original packaging. Immediately prior to deployment, the packaging shall be carefully removed without damaging the GCL. The orientation of the GCL (i.e., which side faces up) shall be in accordance with the Owner Representative's recommendations.
- B. Equipment which could damage the GCL, shall not be allowed to travel directly on it. If the installation equipment causes rutting of the subgrade, the subgrade must be restored to its originally accepted condition before placement continues.
- C. Care must be taken to minimize the extent to which the GCL is dragged across the subgrade in order to avoid damage to the bottom surface of the GCL. A temporary geosynthetic subgrade covering commonly known as a slip sheet or rub sheet may be used to reduce friction damage during placement.
- D. The GCL panels shall be placed parallel to the direction of the slope.
- E. All GCL panels shall lie flat on the underlying surface, with no wrinkles or folds, especially at the exposed edges of the panels.
- F. Only as much GCL shall be deployed as can be covered at the end of the working day with soil, a geomembrane, or a temporary waterproof tarpaulin. The GCL shall not be left uncovered overnight. If the GCL is hydrated when no confining stress is present, the Installer shall remove and replace the hydrated material as directed by the Owner Representative.

3.05 ANCHORAGE

A. As directed by the project drawings and specifications, the end of the GCL roll shall be placed in an anchor trench at the top of the slope. The front edge of the trench shall be rounded so as to eliminate any sharp corners. Loose soil shall be removed from the floor of the trench. The GCL shall cover the entire trench floor, but shall not extend up the rear trench wall.

3.06 SEAMING

A. The GCL seams shall be constructed by overlapping their adjacent edges according to the manufacturer's recommendations. Care should be taken to ensure that the overlap zone is not contaminated with loose soil or other debris.

- B. The minimum dimension of the longitudinal overlap should be 6 in. (150 mm) for Bentomat SDN. If the GCL is manufactured with a grooved cut in the nonwoven geotextile that allows bentonite to freely extrude into the longitudinal overlap then no bentonite-enhanced seam is required for this overlap. If the GCL does not have a grooved cut in one of the nonwoven geotextiles in the longitudinal overlap, then bentonite-enhanced seams are required as described below.
- C. End-of-roll overlapped seams shall be constructed with a minimum overlap of 24 in. (600 mm) for Bentomat SDN. Seams at the ends of the panels should be constructed such that they are shingled in the direction of the grade to prevent the potential for runoff flow to enter the overlap zone. End-of-roll overlapped seams for all reinforced GCL seams require bentonite-enhanced seams as described below.
- D. Bentonite-enhanced seams shall be constructed between the overlapping adjacent panels as follows. The underlying edge of the longitudinal overlap is exposed and then a continuous bead of granular sodium bentonite is applied along a zone defined by the edge of the underlying panel and the 6-inch (150 mm) line. The granular bentonite shall be applied at a minimum application rate of one quarter pound per lineal ft. (0.4 kg/m). A similar bead of granular sodium bentonite is applied at the end-of-roll overlap.

3.07 DETAIL WORK

- There shall be no penetrations through the GCL.
- B. Cutting the GCL should be performed using a sharp utility knife. Frequent blade changes are recommended to avoid damage to the geotextile components of the GCL during the cutting process.

3.08 DAMAGE REPAIR

A. If the GCL is damaged (torn, punctured, perforated, etc.) during installation, it may be possible, if approved by the Owner's Representative, to repair it by cutting a patch to fit over the damaged area. The patch shall be obtained from a new GCL roll and shall be cut to size such that a minimum overlap of 12 in. (300 mm) is achieved around all of the damaged area. Granular bentonite or bentonite mastic shall be applied around the damaged area prior to placement of the patch. It may be desirable to use an adhesive to affix the patch in place so that it is not displaced during cover placement. Patching shall be observed and approved by the Owner's Representative.

GCL CERTIFIED PROPERTIES

| MATERIAL PROPERTY | TEST METHOD | TEST FREQUENCY ft ² (m ²) | REQUIRED VALUES | | |
|--|----------------------------|---|--|--|--|
| Bentonite Swell Index ¹ | ASTM D 5890 | 1 per 50 tonnes | 24 mL/2g min. | | |
| Bentonite Fluid Loss ¹ | ASTM D 5891 | 1 per 50 tonnes | 18 mL max. | | |
| Bentonite Mass/Area ² | ASTM D 5993 | 40,000 ft ² (4,000 m ²) | 0.75 lb/ft ² (3.6 kg/m ²) min | | |
| GCL Grab Strength ³ | ASTM D 6768 | 200,000 ft ² (20,000 m ²) | 30 lbs/in (53 N/cm) MARV | | |
| GCL Peel Strength ³ | ASTM D 6496 | 40,000 ft ² (4,000 m ²) | 2.5 lbs/in (4.4 N/cm) min | | |
| GCL Index Flux ⁴ | ASTM D 5887 | Weekly | $1 \times 10^{-8} \text{m}^3/\text{m}^2/\text{sec max}$ | | |
| GCL Hydraulic Conductivity ⁴ | ASTM D 5887 | Weekly | 5 x 10 ⁻⁹ cm/sec max | | |
| GCL Hydrated Internal Shear Strength ⁵ | ASTM D 5321 ASTM D 6243 | Periodic | 500 psf (24 kPa) typ @ 200 psf | | |

Notes

³ Bentonite mass/area reported at 0 percent moisture content.

Peak values measured at 200 psf (10 kPa) normal stress for a specimen hydrated for 48 hours. Site-specific materials, GCL products, and test conditions must be used to verify internal and interface strength of the proposed design.

END OF SECTION 02376

Bentonite property tests performed at a bentonite processing facility before shipment the manufacturer's production facilities.

³ All tensile strength testing is performed in the machine direction using ASTM D 6768. All peel strength testing is performed using ASTM D 6496. Upon request, tensile and peel results can be reported per modified ASTM D 4632 using 4 inch grips.

^{*} Index flux and permeability testing with deaired distilled/deionized water at 80 psi (551kPa) cell pressure, 77 psi (531 kPa) headwater pressure and 75 psi (517 kPa) tailwater pressure. Reported value is equivalent to 925 gal/scre/day. This flux value is equivalent to a permeability of 5x10° cm/sec for typical GCL thickness. Actual flux values vary with field condition pressures. The last 20 weekly values prior the end of the production date of the supplied GCL may be provided.

PART 1. GENERAL

1.01 DESCRIPTION

This section pertains to construction of the HDPE (High Density Polyethylene) Piping at the Gypsum Management Facility and the CCB Management Facility.

1.02 RELATED SECTIONS

None.

1.03 REFERENCES

The following references, or cited portions thereof, govern the work

A. American Society of Testing and Materials:

- ASTM D 2683 (2004); Specification for Socket-Type Polyethylene Fittings for Outside Diameter-Controlled Polyethylene Pipe and Tubing.
- ASTM D 3261 (2003); Specification for Butt Heat Fusion Polyethylene (PE) Plastic Fittings for Polyethylene (PE) Plastic Pipe and Tubing.
- ASTM D 3350 (2005); Specification for Polyethylene Plastics Pipe and Fittings Materials.
- ASTM F 412 (2001a); Terminology Relating to Plastic Piping System.
- ASTM F 1055 (1998); Specification for Electrofusion Type Polyethylene Fittings for Outside Diameter Controlled Polyethylene Pipe and Tubing.
- ASTM F 1056 (2004); Specification for Socket Fusion Tools for Use in Socket Fusion Joining Polyethylene Pipe or Tubing and Fittings.

1.04 SUBMITTALS

A. Qualifications

Submit qualifications of the Welding Supervisor who will be responsible for construction quality control of the pipe joining process.

B. Material Certifications

Submit manufacturer certifications that the pipe provided complies with the requirements herein.

C. Product Data

- Submit product data and operating instructions for pipe joining equipment.
- Submit pipe manufacturer's recommended procedures for storing, handling, and installing pipe and fittings.

1.05 QUALIFICATIONS

A. The Contractor or Subcontractor performing the work under this section shall have in his employ a Welding Supervisor who has completed a minimum of 1,000 ft of pipe joining work using the type of equipment proposed for use in this work. The Welding Supervisor shall be on site at all times during pipe line installation, and shall provide direct supervision over other employees.

1.06 WARRANTY

A. The pipe and fittings shall be warranted, on a pro-rata basis, against manufacturer's defects for a period of five (5) years from the date of pipe installation. The installation shall be warranted against defects in workmanship for a period of one (1) year from the date of completion of the leachate collection piping system.

PART 2. PRODUCTS

2.01 MATERIALS

A. Pipe

- Pipe material shall be High Density Polyethylene (HDPE) PE 3408, according to ASTM F412, with a cell class designation of 345464C, according to ASTM D3350. Iron pipe size (IPS) and standard dimension ratio (SDR) shall be as indicated in the plans.
- Size and spacing of holes in perforated pipe shall be as indicated in the plans.

B. Fittings

 Fittings shall be made of the same material, and shall have a pressure rating no less than 160 psi. Butt fusion, socket, or electrofusion fittings, according to ASTM D3261, ASTM D2683, and ASTM F1055, respectively, are acceptable.

2.02 EQUIPMENT

A. Butt Fusion Machine

The butt fusion machine shall include the following features:

- Facer with rotating planer block design.
- Heater faces coated by the manufacturer to prevent molten plastic from adhering to the heater face.
- Hydraulic-operated jaws suitable for use with the pipe sizes indicated in the plans.

B. Socket Fusion Equipment

Socket fusion heating tools and depth gauges shall be of the same manufacturer, unless they are all marked F1056, indicating compliance with ASTM F1056.

C. All equipment shall conform to any requirements specified in the pipe and socket manufacturer's installation instructions, and shall be approved by the Owner's Representative.

PART 3. EXECUTION

3.01 MATERIAL DELIVERY, STORAGE, AND HANDLING

- A. HDPE pipe and fittings shall be packaged and shipped by appropriate means to prevent damage to the material and to facilitate off-loading. The Owner will provide an on-site storage site. Storage site requirements (size and preferred location) shall be submitted with the bid documents.
- Storage and handling shall be according to manufacturer's recommendations.

3.02 BASE PREPARATION

All HDPE piping shall be installed on a layer of coarse aggregate placed by the Contractor in accordance with the plans. The grade of the coarse aggregate base shall be verified before installing the piping.

3.03 INSTALLATION

All pipe and fittings shall be installed according to the manufacturer's recommendations. Removal of weld beads is not required. Contractor shall place coarse aggregate along the pipe to provide lateral stability. Welds shall not be obscured until they have been approved by the Owner's Representative, the top of pipe shall not be covered until the Construction Quality Assurance (CQA) survey has been completed to verify conformance with specified tolerances.

3.04 INSPECTIONS

- A. The Owner's Representative shall shall be visually inspect pipe materials to verify that each pipe material is properly stamped (by the manufacturer) for ASTM acceptance before installation. Defective or damaged materials shall be removed from the site.
- B. Each weld and connection shall be visually inspected by the Owner's Representative. Defective welds shall be repaired as directed by the Owner's Representative and according to manufacturer's recommendations. Welds and connections shall not be covered until they have been approved by the Owner's Representative.

3.05 TOLERANCES

A. HDPE piping shall be located within 0.5 ft. of plan location, and elevation shall be within 0.1 ft. of plan elevation with no adverse slopes.

END OF SECTION 02936

PART 1. GENERAL

1.01 DESCRIPTION

- A. This section includes manufacturing, furnishing, and installing High Density Polyethylene (HDPE) Geomembranes for the Gypsum Management Facility and the Gypsum Management Facility Recycle Pond.
- B. The work includes furnishing all equipment and materials and providing all labor, supervision, administration and management necessary to perform the work as shown on the plans.

1.02 RELATED SECTIONS

- A. The following sections contain items which are related to the work in this section:
 - 02373 Geotextiles
 - 02376 Geosynthetic Clay Liner

1.03 REFERENCES

- A. The following references, or cited portions thereof, govern the work:
 - American Society for Testing and Materials (ASTM):
 - a. D 638, Standard Test Method for Tensile Properties of Plastics.
 - D 751, Standard Test Methods for Coated Fabrics.
 - D 792, Standard Test Methods for Density and Specific Gravity (Relative Density) of Plastics by Displacement.
 - D 1004, Standard Test Method for Initial Tear Resistance of Plastic Film and Sheeting.
 - D 1204, Standard Test Method for Linear Dimensional Changes of Non Rigid Thermoplastic Sheeting or Film at Elevated Temperature.
 - D 1238, Standard Test Method for Flow Rates of Thermoplastics by Extrusion Plastometer.
 - D 1505, Standard Test Method for Density of Plastics by Density-Gradient Technique.
 - D 1603, Standard Test Method for Carbon Black in Olefin Plastics.
 - D 3895, Test Method for Oxidative Induction Time of Polyolefins by Thermal Analysis.
 - D 4218, Test Method for Determination of Carbon Black Content in Polyethylene Compounds by the Muffle-Furnace Technique.

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- D 4437, Standard Practice for Determining the Integrity of Field Seams Used in Joining Flexible Polymeric Sheet Geomembranes.
- D 4833, Test Method for Index Puncture Resistance of Geotextiles, Geomembranes and Related Products.
- m. D 5199, Standard Test Method for Measuring Nominal Thickness of Smooth Geomembranes.
- D 5397, Standard Test Method for Evaluation of Stress Crack Resistance of Polyolefins using Notched Constant Tensile Load Test.
- D 5596, Standard Practice for Microscopical Examination of Pigment Dispersion in Plastic Compounds.
- D 5641, Standard Practice for Geomembrane Seam Evaluation by Vacuum Chamber.
- q. D 5721, Practice for Air-Oven Aging of Polyolefin Geomembranes.
- D 5820, Test Method for Air Testing.
- D 5885, Test Method for Oxidative Induction Time of Polyolefin Geosynthetics by High Pressure Differential Scanning Calorimetry.
- D 5994, Standard Test Method for Measuring Nominal Thickness of Textured Geomembranes
- D 6365, Standard Practice for the Nondestructive Testing of Geomembrane Seams using The Spark Test

Geosynthetic Research Institute (GRI):

- a. GRI GM 6, Pressurized Air Channel Test for Dual Seamed Geomembranes
- GRI GM 9, Cold Weather Seaming of Geomembranes
- GRI GM 10, Specification for Stress Crack Resistance of HDPE Geomembrane Sheet
- d. GRI GM 13, Test Properties, Testing Frequency and Recommended Warranty for High Density Polyethylene (HDPE) Smooth and Textured Geomembranes
- e. GRI GM 14, Test Frequencies for Destructive SeamTesting

1.04 SUBMITTALS

- A. Submit the following to the Engineer or Owner, for review and approval, within a reasonable time so as to expedite shipment or installation of the Geomembrane:
 - Documentation of manufacturer's qualifications as specified in subsection 1.05A of this Section.
 - Manufacturer's Quality Control program manual or descriptive documentation.
 - A material properties sheet, including at a minimum all properties specified in GRI GM 13, including test methods used.
 - Sample of the material.

- Documentation of Installer's qualifications, as specified below and in subsection 1.05B of this Section.
 - a. Submit a list of at least ten completed facilities. For each name and type of facility; its location; the date of installation; number of contact at the facility; type and thickness of geomembrane and; surface area of the installed geomembrane.
 - Submit resumes or qualifications of the Installation Supervisor,
 Master Seamer and Technicians to be assigned to this project.
 - c. Quality Control Program.
- Example Material Warranty and Liner Installation Warranty complying with subsections 1.07 and 1.08 of this Section.
- Resin Supplier's name, resin production plant identification, resin brand name and number, production date of the resin, resin Manufacturer's quality control certificates, and certification that the properties of the resin meet the requirements

B. Shop Drawings

- Submit copies of shop drawings for engineer's approval within a
 reasonable time so as not to delay the start of geomembrane installation.
 Shop drawings shall show the proposed panel layout identifying seams
 and details. Seams should generally follow direction of the slope. Butt
 seams or roll-end seams should not occur on a slope unless approved by
 the Owner's Representative. Butt seams on a slope, if allowed, should be
 staggered.
- Placement of geomembrane will not be allowed to proceed until Owner's Representative has received and approved the shop drawings.

C. Additional Submittals (In-Progress and at Completion)

- Manufacturer's warranty (refer to subsection 1.08).
- Geomembrane installation warranty (refer to subsection 1.09).
- Daily written acceptance of subgrade surface (refer to subsection 3.01.C).
- Low-temperature seaming procedures if applicable (refer to subsection 3.03.A)
- Prequalification test seam samples (refer to subsection 3.05.A.6).
- Field seam non-destructive test results (refer to subsection 3.05.B.1).
- Field seam destructive test results (refer to subsection 3.05.C.6).
- Daily field installation reports (refer to subsection 3.05.G).
- Installation record drawing, as discussed in subsection 3.05.G).

1.05 QUALITY CONTOL

A. Manufacturer's Qualifications:

The manufacturer of geomembrane of the type specified or similar product shall have at least five years experience in the manufacture of such geomembrane. In addition, the geomembrane manufacturer shall have manufactured at least 10,000,000 sq. ft. of the specified type of geomembrane or similar product during the last five years.

B. Installer's Qualifications:

- The Geomembrane Installer shall be the Manufacturer, approved Manufacturer's Installer or a contractor approved by the Owner's Representative to install the geomembrane.
- The Geomembrane Installer shall have at least three years experience in the installation of the specified geomembrane or similar. The Geomembrane Installer shall have installed at least 10 projects involving a total of 5,000,000 sq. ft. of the specified type of geomembrane or similar during the last three years.
- Installation shall be performed under the direction of a field Installation Supervisor who shall be responsible throughout the geomembrane installation, for geomembrane panel layout, seaming, patching, testing, repairs, and all other activities of the Geomembrane Installer. The Field Installation Supervisor shall have installed or supervised the installation and seaming of a minimum of 10 projects involving a total of 5,000,000 sq. ft. of geomembrane of the type specified or similar product.
- Seaming shall be performed under the direction of a Master Seamer (who may also be the Field Installation Supervisor or Crew Foreman) who has seamed a minimum of 3,000,000 sq. ft. of geomembrane of the type specified or similar product, using the same type of seaming apparatus to be used in the current project. The Field Installation Supervisor and/or Master Seamer shall be present whenever seaming, patching, other welding operations, and testing is performed.
- 5 All seaming, patching, other welding operations, and testing shall be performed by qualified technicians employed by the Geomembrane Installer.

1.06 DELIVERY, STORAGE AND HANDLING

- A. Each roll of geomembrane delivered to the site shall be labeled by the manufacturer. The label shall be firmly affixed and shall clearly state the manufacturer's name, product identification, material thickness, roll number, roll dimensions and roll weight.
- Geomembrane shall be protected from mud, dirt, dust, puncture, cutting or any other damaging or deleterious conditions.
- C. Rolls shall be stored away from high traffic areas. Continuously and uniformly support rolls on a smooth, level prepared surface.
- Rolls shall not be stacked more than three high.

1.07 PROJECT CONDITIONS

Geomembrane shall not be installed in the presence of standing water, while precipitation is occurring, during excessive winds, or when material temperatures are outside the limits specified in Section 3.03.

1.08 MATERIAL WARRANTY

As required by specification, or as required in GRI GM 13 (attachment A)

1.09 GEOMEMBRANE INSTALLATION WARRANTY

The Geomembrane Installer shall guarantee the geomembrane installation against defects in the installation and workmanship for 1 year commencing with the date of final acceptance.

1.10 GEOMEMBRANE PRE-CONSTRUCTION MEETING

- A. Geomembrane Pre-Construction Meeting shall be held at the site prior to installation of the geomembrane. At a minimum, the meeting shall be attended by the Geomembrane Installer, Owner, Owner's representative (Engineer and/or CQA Firm), and the General Contractor.
- B. Topics for this meeting shall include:
 - Responsibilities of each party.
 - Lines of authority and communication. Resolution of any project document ambiguity.
 - Methods for documenting, reporting and distributing documents and reports.
 - Procedures for packaging and storing archive samples.
 - Review of time schedule for all installation and testing.
 - Review of panel layout and numbering systems for panels and seams including details for marking on geomembrane.
 - Procedures and responsibilities for preparation and submission of as-built panel and seam drawings.
 - Temperature and weather limitations. Installation procedures for adverse weather conditions. Defining acceptable subgrade, geomembrane, or ambient moisture and temperature conditions for working during liner installation.
 - Subgrade conditions, dewatering responsibilities and subgrade maintenance plan.
 - Deployment techniques including allowable subgrade for the geomembrane.
 - Plan for controlling expansion/contraction and wrinkling of the geomembrane.
 - Covering of the geomembrane and cover soil placement.
 - Measurement and payment schedules.
 - Health and safety.
- C. The meeting shall be documented by the Owner's Representative and minutes shall be transmitted to all parties.

PART 2. PRODUCTS

2.01 SOURCE QUALITY CONTROL

Manufacturing Quality Control

- A. The test methods and frequencies used by the manufacturer for quality control/quality assurance of the above geomembrane prior to delivery, shall be in accordance with GRI GM 13, or modified as required for project specific conditions.
- B. The manufacturer's geomembrane quality control certifications, including results of quality control testing of the products, as specified in subsection 2.01.C of this Section, must be supplied to the Owner's Representative. The certification shall be signed by a responsible party employed by the manufacturer, such as the QA/QC Manager, Production Manager, or Technical Services Manager. Certifications shall include lot and roll numbers and corresponding shipping information.
- C. The Manufacturer will provide Certification that the geomembrane and welding rod supplied for the project have the same base resin and material properties.

2.02 GEOMEMBRANE

- A. The geomembrane shall consist of new, first quality products designed and manufactured specifically for the purpose of this work which shall have been satisfactorily demonstrated by prior testing to be suitable and durable for such purposes. The geomembrane rolls shall be seamless, high density polyethylene (HDPE- Density >0.94g/cm) containing no plasticizers, fillers or extenders and shall be free of holes, blisters or contaminants, and leak free verified by 100% in line spark or equivalent testing. The geomembrane shall be supplied as a continuous sheet with no factory seams in rolls. The geomembrane will meet the property requirements as shown in Table A. (GRI GM 13)
- Material shall be reviewed for conformance to the project specifications by the Owner's Representative
- The geomembrane seams shall meet the property requirements as shown in Table 2, (Attachment B).

PART 3. EXECUTION

3.01 SUBGRADE PREPARATION

Geomembrane installed over geosynthetic clay liner (GCL).

The area of GCL to be covered with geomembrane shall be jointly inspected daily with the Owner's Representative before commencing geomembrane installation for the day, and the condition of the GCL shall be continuously observed as geomembrane installation progresses. Rocks, stones, sticks, sharp objects and debris of any kind shall be removed from the surface of the GCL. The Owner's Representative shall be notified of any discontinuities, premature hydration, or

otherwise defective GCL. Geomembrane shall not be placed over suspect areas until they have been repaired to the satisfaction of the Owner's Representative. The Installation Supervisor shall certify daily in writing that the GCL surface was acceptable at the time of geomembrane installation.

B. Geomembrane installed over cushion dirt.

The area of cushion dirt to be covered with geomembrane shall be prepared in accordance with the Section 02200 – Earthwork. The surface shall be smooth and free of ruts and holes, rocks, stones, sticks, sharp objects and debris of any kind.

- C. The Geomembrane installer shall provide daily written acceptance for the surface to be covered by the geomembrane in that day's operations. The surface shall be maintained in a manner, during geomembrane installation, to ensure subgrade suitability.
- D. All subgrade damaged by construction equipment and deemed unsuitable by the Owner's Representative for geomembrane deployment shall be repaired prior to placement of the geomembrane. All repairs shall be reviewed by the Owner's Representative and approved by the Geomembrane Installer. This damage, repair, and the responsibilities of the contractor and Geomembrane Installer shall be defined in the preconstruction meeting.

3.02 GEOMEMBRANE PLACEMENT

- A. No geomembrane shall be deployed until the applicable certifications and quality control certificates listed in subsection 1.04 of this Section are submitted to and approved by the Owner's Representative. Should geomembrane material be deployed prior to approval by the Owner's Representative it will be at the sole risk of the Geomembrane Installer and/or Contractor. If the material does not meet project specifications it shall be removed from the work area at no cost to the owner.
- B. The geomembrane shall be installed to the limits shown on the project drawings and essentially as shown on approved panel layout drawings.
- C. No geomembrane material shall be unrolled and deployed if the material temperatures are lower than 0 degrees C (32 degrees F). Temperature limitations should be defined in the preconstruction meeting. Typically, only the quantity of geomembrane that will be anchored and seamed together in one day should be deployed.
- No vehicular traffic shall travel on the geomembrane other than an approved low ground pressure All Terrain Vehicle or equivalent.
- E. Sand bags or equivalent ballast shall be used as necessary to temporarily hold the geomembrane material in position under the foreseeable and reasonably - expected wind conditions. Sand bag material shall be sufficiently close- knit to prevent soil fines from working through the bags and discharging on the geomembrane.
- F. Geomembrane placement shall not be done if moisture prevents proper subgrade preparation, panel placement, or panel seaming. Moisture limitations

- should be defined in the preconstruction meeting.
- G. Damaged panels or portions of the damaged panels which have been rejected shall be marked and their removal from the work area recorded.
- H. The geomembrane shall not be allowed to "bridge over" voids or low areas in the subgrade. In these areas, the subgrade shall be prepared to allow the geomembrane to rest in intimate contact with the subgrade.
- Wrinkles caused by panel placement or thermal expansion should be minimized in accordance with section 1.10 B. 11.
- J. Considerations on Site Geometry: In general, seams shall be oriented parallel to the line of the maximum slope. In corners and odd shaped geometric locations, the total length of field seams shall be minimized. Seams shall not be located at low points in the subgrade.
- K. Overlapping: The panels shall be overlapped prior to seaming to whatever extent is necessary to effect a good weld and allow for proper testing. In no case shall this overlap be less than 75mm (3 in.).

3.03 SEAMING PROCEDURES

- Cold weather installations should follow guidelines as outlined in GRI GM9.
- No geomembrane material shall be seamed when liner temperatures are less than 0 degrees C (32 degrees F).
- C. No geomembrane material shall be seamed when the sheet temperature is above 75 degrees C (170 degrees F) as measured by an infrared thermometer or surface thermocouple.
- D. Seaming shall primarily be performed using automatic fusion welding equipment and techniques. Extrusion welding shall be used where fusion welding is not possible such as at pipe penetrations, patches, repairs and short (less than a roll width) runs of seams.
- E. Fishmouths or excessive wrinkles at the seam overlaps, shall be minimized and when necessary cut along the ridge of the wrinkles back into the panel so as to effect a flat overlap. The cut shall be terminated with a keyhole cut (nominal 10 mm (1/2 in) diameter hole) so as to minimize crack/tear propagation. The overlay shall subsequently be seamed. The key hole cut shall be patched with an oval or round patch of the same base geomembrane material extending a minimum of 150 mm (6 in.) beyond the cut in all directions.

3.04 PIPE AND STRUCTURE PENETRATION SEALING SYSTEM

- Provide penetration sealing system as shown in the Project Drawings.
- B. Penetrations shall be constructed from the base geomembrane material, flat stock, prefabricated boots and accessories as shown on the Project Drawings. The prefabricated or field fabricated assembly shall be field welded to the geomembrane as shown on the Project Drawings so as to prevent leakage. This assembly shall be tested as outlined in section 3.05.B. Alternatively, where field non destructive testing can not be performed, attachments will be field spark tested by standard holiday leak detectors in accordance with ASTM 6365 Spark testing should be done in areas where both air pressure testing and vacuum testing are not possible.
 - Equipment for Spark testing shall be comprised of but not limited to: A 02800-8

- hand held holiday spark tester and conductive wand that generates a high voltage.
- 2. The testing activities shall be performed by the Geomembrane Installer by placing an electrically conductive tape or wire beneath the seam prior to welding. A trial seam containing a non welded segment shall be subject to a calibration test to ensure that such a defect (non welded segment) will be identified under the planned machine settings and procedures. Upon completion of the weld, enable the spark tester and hold approximately 25mm (1 in) above the weld moving slowly over the entire length of the weld in accordance with ASTM 6365. If there is no spark the weld is considered to be leak free.
- A spark indicates a hole in the seam. The faulty area shall be located, repaired and retested by the Geomembrane Installer.
- Care should be taken if flammable gases are present in the area to be tested.

3.05 FIELD QUALITY CONTROL

The Owner's Representative shall be notified prior to all pre qualification and production welding and testing, or as agreed upon in the pre construction meeting.

A. Prequalification Test Seams

- Test seams shall be prepared and tested by the Geomembrane Installer to verify that seaming parameters (speed, temperature and pressure of welding equipment) are adequate.
- 2. Test seams shall be made by each welding technician and tested in accordance with ASTM D 4437 at the beginning of each seaming period. Test seaming shall be performed under the same conditions and with the same equipment and operator combination as production seaming. The test seam shall be approximately 3.3 meters (10 feet) long for fusion welding and 1 meter (3 feet) long for extrusion welding with the seam centered lengthwise. At a minimum, tests seams should be made by each technician 1 time every 4-6 hours; additional tests may be required with changes in environmental conditions.
- 3. Two 25 mm (1 in) wide specimens shall be die-cut by the Geomembrane Installer from each end of the test seam. These specimens shall be tested by the Geomembrane Installer using a field tensiometer testing both tracks for peel strength and also for shear strength. Each specimen shall fail in the parent material and not in the weld, "Film Tear Bond"(F.T.D. failure). Seam separation equal to or greater than 10% of the track width shall be considered a failing test.
- The minimum acceptable seam strength values to be obtained for all specimens tested are listed in Subsection 3.05.C.4 of this Section. All four specimens shall pass for the test seam to be a passing seam.
- If a test seam fails, an additional test seam shall be immediately conducted. If the additional test seam fails, the seaming apparatus shall be rejected and not used for production seaming until the deficiencies are

- corrected and a successful test seam can be produced.
- 6. A sample from each test seam shall be labeled. The label shall indicate the date, geomembrane temperature, number of the seaming unit, technician performing the test seam and pass or fail description. The sample shall then be given to the Owner's Representative for archiving.

B. Field Seam Non-destructive Testing

- All field seams shall be non-destructively tested by the Geomembrane Installer over the full seam length before the seams are covered. Each seam shall be numbered or otherwise designated. The location, date, test unit, name of tester and outcome of all non-destructive testing shall be recorded and submitted to the Owner's Representative.
- Testing should be done as the seaming work progresses, not at the
 completion of all field seaming. All defects found during testing shall be
 numbered and marked immediately after detection. All defects found
 should be repaired, retested and remarked to indicate acceptable
 completion of the repair.
- Non-destructive testing shall be performed using vacuum box, air pressure or spark testing equipment.
- Non-destructive tests shall be performed by experienced technicians familiar with the specified test methods. The Geomembrane Installer shall demonstrate to the Owner's Representative all test methods to verify the test procedures are valid.
- Extrusion seams shall be vacuum box tested by the Geomembrane Installer in accordance with ASTM D 4437 and ASTM D 5641 with the following equipment and procedures:
 - a. Equipment for testing extrusion seams shall be comprised of but not limited to: a vacuum box assembly consisting of a rigid housing, a transparent viewing window, a soft rubber gasket attached to the base, port hole or valve assembly and a vacuum gauge; a vacuum pump assembly equipped with a pressure controller and pipe connections; a rubber pressure/vacuum hose with fittings and connections; a plastic bucket; wide paint brush or mop; and a soapy solution.
 - The vacuum pump shall be charged and the tank pressure adjusted to approximately 35 kPa (5 psig).
 - c. The Geomembrane Installer shall create a leak tight seal between the gasket and geomembrane interface by wetting a strip of geomembrane approximately 0.3m (12 in) by 1.2m (48 in) (length and width of box) with a soapy solution, placing the box over the wetted area, and then compressing the box against the geomembrane. The Geomembrane Installer shall then close the bleed valve, open the vacuum valve, maintain initial pressure of approximately 35 kPa (5 psig) for approximately 5 seconds. The geomembrane should be continuously examined through the viewing window for the presence of soap bubbles, indicating a leak. If no bubbles appear after 5 seconds, the area shall be

- considered leak free. The box shall be depressurized and moved over the next adjoining area with an appropriate overlap and the process repeated.
- All areas where soap bubbles appear shall be marked, repaired and then retested.
- At locations where seams cannot be non destructively tested, such as pipe penetrations, alternate nondestructive spark testing (as outlined in section 3.04.B) or equivalent should be substituted.
- f. All seams that are vacuum tested shall be marked with the date tested, the name of the technician performing the test and the results of the test.
- Double Fusion seams with an enclosed channel shall be air pressure tested by the Geomembrane Installer in accordance with ASTM D 5820 and ASTM D 4437 and the following equipment and procedures:
 - a. Equipment for testing double fusion seams shall be comprised of but not limited to: an air pump equipped with a pressure gauge capable of generating and sustaining a pressure of 210 kPa (30 psig), mounted on a cushion to protect the geomembrane; and a manometer equipped with a sharp hollow needle or other approved pressure feed device.
 - b. The Testing activities shall be performed by the Geomembrane Installer. Both ends of the seam to be tested shall be sealed and a needle or other approved pressure feed device inserted into the tunnel created by the double wedge fusion weld. The air pump shall be adjusted to a pressure of 210 kPa (30 psig), and the valve closed,. Allow 2 minutes for the injected air to come to equilibrium in the channel, and sustain pressure for 5 minutes. If pressure loss does not exceed 28 kPa (4 psig) after this five minute period the seam shall be considered leak tight. Release pressure from the opposite end verifying pressure drop on needle to ensure testing of the entire seam. The needle or other approved pressure feed device shall be removed and the feed hole sealed.
 - c. If loss of pressure exceeds 28 kPa (4 psig) during the testing period or pressure does not stabilize, the faulty area shall be located, repaired and retested by the Geomembrane Installer.
 - Results of the pressure testing shall be recorded on the liner at the seam tested and on a pressure testing record.

C. Destructive Field Seam Testing

One destructive test sample per 150 linear m (500 linear ft) seam length or another predetermined length in accordance with GRI GM 14 shall be taken by the Geomembrane Installer from a location specified by the Owner's Representative. The Geomembrane Installer shall not be informed in advance of the sample location. In order to obtain test results prior to completion of geomembrane installation, samples shall be cut by the Geomembrane Installer as directed by the Owner's Representative as seaming progresses.

- 2. All field samples shall be marked with their sample number and seam number. The sample number, date, time, location, and seam number shall be recorded. The Geomembrane Installer shall repair all holes in the geomembrane resulting from obtaining the seam samples. All patches shall be vacuum box tested or spark tested. If a patch cannot be permanently installed over the test location the same day of sample collection, a temporary patch shall be tack welded or hot air welded over the opening until a permanent patch can be affixed.
- 3. The destructive sample size shall be 300 mm (12 in) wide by 1 m (36 in) long with the seam centered lengthwise. The sample shall be cut into three equal sections and distributed as follows: one section given to the Owner's Representative as an archive sample; one section given to the Owner's Representative for laboratory testing as specified in paragraph 5 below; and one section retained by the Geomembrane Installer for field testing as specified in paragraph 4 below.
- 4. For field testing, the Geomembrane Installer shall cut 10 identical 25 mm (1 in) wide replicate specimens from his sample. The Geomembrane Installer shall test five specimens for seam shear strength and five for peel strength. Peel tests will be performed on both inside and outside weld tracks. To be acceptable, 4 of 5 test specimens must pass the stated criteria in section 2.02 with less than 10% separation. If 4 of 5 specimens pass, the sample qualifies for testing by the testing laboratory if required.
- If independent seam testing is required by the specifications it shall be conducted in accordance with ASTM 5820 or ASTM D4437 or GRI GM
 6.
- Reports of the results of examinations and testing shall be prepared and submitted to the Owner's Representative.
- 7. For field seams, if a laboratory test fails, that shall be considered as an indicator of the possible inadequacy of the entire seamed length corresponding to the test sample. Additional destructive test portions shall then be taken by the Geomembrane Installer at locations indicated by the Engineer, typically 3 m (10 ft) on either side of the failed sample and laboratory seem tests shall be performed. Passing tests shall be an indicator of adequate seams. Failing tests shall be an indicator of non-adequate seams and all seams represented by the destructive test location shall be repaired with a cap-strip extrusion welded to all sides of the capped area. All cap-strip seams shall be non-destructively vacuum box tested until adequacy of the seams is achieved. Cap strip seams exceeding 50 M in length (150 FT) shall be destructively tested.

D. Identification of Defects

- Panels and seams shall be inspected by the Installer and Owner's Representative during and after panel deployment to identify all defects, including holes, blisters, undispersed raw materials and signs of contamination by foreign matter.
- E. Evaluation of Defects: Each suspect location on the liner (both in geomembrane 02800-12

seam and non-seam areas) shall be non-destructively tested using one of the methods described in Section 3.05.B. Each location which fails non-destructive testing shall be marked, numbered, measured and posted on the daily "installation" drawings and subsequently repaired.

- If a destructive sample fails the field or laboratory test, the Geomembrane Installer shall repair the seam between the two nearest passed locations on both sides of the failed destructive sample location.
- Defective seams, tears or holes shall be repaired by reseaming or applying a extrusion welded cap strip.
- Reseaming may consist of either:
 - Removing the defective weld area and rewelding the parent material using the original welding equipment; or
 - Reseaming by extrusion welding along the overlap at the outside seam edge left by the fusion welding process.
- Blisters, larger holes, and contamination by foreign matter shall be repaired by patches and/or extrusion weld beads as required. Each patch shall extend a minimum of 150 mm (6 in) beyond all edges of the defects.
- 5. All repairs shall be measured, located and recorded.
- F. Verification of Repairs on Seams: Each repair shall be non-destructively tested using either vacuum box or spark testing methods. Tests which pass the non-destructive test shall be taken as an indication of a successful repair. Failed tests shall be reseamed and retested until a passing test results. The number, date, location, technician and test outcome of each patch shall be recorded.
- G. Daily Field Installation Reports: At the beginning of each day's work, the Installer shall provide the Engineer with daily reports for all work accomplished on the previous work day. Reports shall include the following:
 - 1. Total amount and location of geomembrane placed;
 - Total length and location of seams completed, name of technicians doing seaming and welding unit numbers;
 - Drawings of the previous day's installed geomembrane showing panel numbers, seam numbers and locations of non-destructive and destructive testing:
 - Results of pre-qualification test seams;
 - 5. Results of non-destructive testing; and
 - Results of vacuum testing of repairs.
- H. Destructive test results shall be reported prior to covering of liner or within 48 hours.

3.06 LINER ACCEPTANCE

- A. Geomembrane liner will be accepted by the Owner's Representative when:
 - The entire installation is finished or an agreed upon subsection of the installation is finished;

- 2. All Installer's QC documentation is completed and submitted to the owner
- Verification of the adequacy of all field seams and repairs and associated geomembrane testing is complete.

3.07 ANCHOR TRENCH

Construct as specified on the project drawings.

3.08 DISPOSAL OF SCRAP MATERIALS

A. On completion of installation, the Geomembrane Installer shall dispose of all trash and scrap material in a location approved by the Owner, remove equipment used in connection with the work herein, and shall leave the premises in a neat acceptable manner. No scrap material shall be allowed to remain on the geomembrane surface.

PART 4. GRI GM13 SPECIFICATIONS

Geosynthetics Research Institute (GRI) Test Method GM13 – "Test Methods, Test Properties and Testing Frequency for High Density Polyethylene (HDPE) Smooth and Textured Geomembranes", Revision 8, Dated July 10, 2006.

ATTACHMENT A:

| Minimum Average Weld Pr Geome | operties for mbranes (En | | | and 7 | Textu | ired ! | HDP | E |
|---|-----------------------------|-----------|-----------|-----------|-----------|------------|------------|------------|
| Property | Test Method | 30 mil | 40 mil | 50 mil | 60 mil | 80 mil | 100 mil | 120 mil |
| Peel strength (fusion & extrusion) lb/in. Shear strength (fusion & extrusion) lb/in. | ASTM 4437 ASTM 4437 | 39 60 | 52 80 | 65 100 | 78 120 | 104 160 | 130 200 | 156 239 |

END OF SECTION 02800

DIVISION 2 - SITE WORK

Section 02936 - Topsoil, Seeding, and Mulching

PART 1. GENERAL

1.01 DESCRIPTION

This section pertains to seeding and placing mulch or erosion control blanket over seeded areas.

1.02 RELATED SECTIONS

- A. Specified elsewhere:
 - 02200 Earthwork

1.03 REFERENCES

The following reference or cited portions thereof, current at date of bidding documents unless otherwise specified, governs the work.

 Illinois Department of Transportation (IDOT): Standard Specifications for Road and Bridge Construction, adopted January 1, 2007.

1.04 SPECIFICATIONS

- A. Work shall conform to the applicable requirements of Sections 250 and 251 of Standard Specifications for Road and Bridge Construction and to the requirements hereinafter specified.
- Exceptions: All references in the IDOT specifications to methods of measurement and payment shall not apply.

1.05 WARRANTY

 Warranty for one (1) year plus one growing season from date of substantial completion shall be provided.

PART 2. PRODUCTS

2.01 MATERIALS

A. Seed: Seed shall conform to Article 1081.04 of the IDOT Standard Specifications. The composition of the Ameren Energy Resources Generating hay seeding mix shall

be as follows:

| Seed Type | Pounds/Acre | | | | |
|-------------------|-------------|--|--|--|--|
| Vernal Alfalfa | 12 | | | | |
| Wrangler Alfalfa | 8 | | | | |
| Medium Red Clover | 6 | | | | |
| Timothy | 4 | | | | |

- B. Mulch Material and Erosion Control Blanket: Mulch material shall conform to Article 1081.06 and the excelsior blanket/knitted straw mat shall conform to Article 1081.10 of the IDOT Standard Specifications.
- Fertilizer and agricultural ground limestone will not be permitted.

PART 3. EXECUTION

3.01 CONSTRUCTION

- A. Seed bed preparation and seeding methods shall conform to Section 250 of the IDOT Specifications. Seeding of areas disturbed by construction activities after September 30, 2008 may be deferred until Spring 2009.
- B. Seed shall be applied to the perimeter berm ditch, to disturbed portions of the perimeter berm, and to all disturbed earth surfaces outside of the existing perimeter berm. IDOT seeding mixture 7 shall be used on stockpiles. IDOT seeding mixture 1A shall be used on the gypsum stack perimeter earthen berm, the recycle pond dam embankment and on slopes that are 4H:1V or steeper. The Ameren hay seed mix shall be used on slopes flatter that 4H:1V.
- C. Application rates for IDOT seed mixtures shall be as specified in Section 250 of the IDOT Specifications. The application rate for the Ameren Energy Resources Generating's seed mix shall be as specified in the Ameren Energy Resources Generating's hay seeding mix.
- D. Seeded areas shall be mulched in accordance with Article 251.03. The Contractor may use either Method 2 or Method 3.

3.02 MAINTENANCE OF COMPLETED WORK

A. All areas seeded by the Contractor shall be maintained by the Contractor during the period between completion of such work and final completion and acceptance of the Contractor's work by the Owner. This maintenance shall be such that the completed work, at time of acceptance, complies in all respects with the requirements herein specified. B. The areas seeded will be required to germinate. If the seed does not germinate, the Contractor will be required to regrade and reseed at no additional cost.

END OF SECTION 02936

DIVISION 3 - CONCRETE Section 03100 - Concrete Formwork

PART 1. GENERAL

1.01 WORK INCLUDES

A. The complete installation of the formwork for cast-in-place concrete, with shoring, bracing and anchorage, openings for other work, form accessories, form stripping.

1.02 RELATED SECTIONS

- A. Section 03200 Concrete Reinforcement.
- B. Section 03300 Cast-In-Place Concrete.
- C. Section 03400 Concrete Embedment Liner.

1.03 REFERENCES

- ACI 347 Recommended Practice For Concrete Formwork.
- B. ACI 301 Specifications For Structural Concrete For Buildings.

1.04 DESIGN REQUIREMENTS

A. Design, engineer and construct formwork, shoring and bracing to conform to design and code requirements; resultant concrete to conform to required shape, line and dimension.

1.05 QUALITY ASSURANCE

Perform Work in accordance with ACI 347 and 301.

1.06 REGULATORY REQUIREMENTS

 Conform to applicable code for design, fabrication, erection and removal of formwork.

1.07 DELIVERY, STORAGE, AND HANDLING

 Store off ground in ventilated and protected manner to prevent deterioration from moisture.

1.08 COORDINATION

- Coordinate this Section with other Sections of work which require attachment of components of formwork.
- B. If formwork is placed which results in insufficient concrete cover over reinforcement, request instructions from Owner's Representative before proceeding.

PART 2. PRODUCTS

2.01 WOOD FORM MATERIALS

- A. Softwood Plywood: 3/4 in. PS 1-83 "B-B" (concrete form) plywood, Class I, exterior grade or better, mill-oiled and edge sealed with each piece bearing legible inspection trademark.
- B. Architectural Plywood: 3/4 in. PS 1-83 "B-B" plyform, Class I, with High Density smooth overlay, 1 surface, edge scaled with each piece bearing legible inspection trademark.

2.02 MANUFACTURERS - PREFABRICATED FORMS

- Weyerhauser Concrete Form.
- B. Georgia Pacific, G-P Exterior Soft Wood Plywood Product.
- C. Plywood and Door Corporation's Finn-Form.

2.03 PREFABRICATED FORMS

- A. Preformed Steel Forms: Minimum 16 gage matched, tight fitting, stiffened to support weight of concrete without deflection detrimental to tolerances and appearance of finished surfaces.
- B. Glass Fiber Fabric Reinforced Plastic Forms: Matched, tight fitting, stiffened to support weight of concrete without deflection detrimental to tolerances and appearance of finished concrete surfaces.

2.04 FORMWORK ACCESSORIES

A. Form Ties: Snap-off type, galvanized metal, adjustable length, 1 in. back break dimension, free of defects that could leave holes larger than 1 in. in concrete surface; Dayton-Sure Grip snap-in-form ties, as manufactured by Dayton Superior

- Corp., Symons Ties as manufactured by Symons Corporation, Snap-Tys as manufactured by Richmond Corporation. Ties shall be removed after forms are removed, and holes filled with mortar that matches the adjacent surfaces.
- B. Form Release Agent: Colorless mineral oil which will not stain concrete, or absorb moisture; by Magic Kote manufactured by Symons Manufacturing Co., Form Coat manufactured by Concrete Services Co., Formcel manufactured by Lambert Corp.
- C. Corners: Chamfered, wood strip type; 3/4 x 3/4 in. size on all exterior corners, 3 x 3 in. size where shown on the drawings; maximum possible lengths.
- D. Nails, Spikes, Lag Bolts, Through Bolts, Anchorages: Sized as required, of sufficient strength and character to maintain formwork in place while placing concrete.
- E. Concrete Embedment Liner, where required, shall be installed in accordance with Section 03400 – Concrete Embedment Liner.

PART 3. EXECUTION

3.01 EXAMINATION

 Verify lines, levels and centers before proceeding with formwork. Ensure that dimensions agree with drawings.

3.02 EARTH FORMS

Earth forms are not permitted, except for footings.

3.03 ERECTION - FORMWORK

- A. Erect formwork, shoring and bracing to achieve design requirements, in accordance with requirements of ACI 301. Metal forms shall be installed in strict accordance with manufacturer's directions and specifications.
- B. Provide bracing to ensure stability of formwork. Shore or strengthen formwork subject to overstressing by construction loads.
- C. Arrange and assemble formwork to permit dismantling and stripping. Do not damage concrete during stripping. Permit removal of remaining principal shores.
- Align joints and make watertight. Keep form joints to a minimum.
- Obtain approval before framing openings in structural members which are not indicated on drawings.

3.04 APPLICATION - FORM RELEASE AGENT

- Apply form release agent on formwork in accordance with manufacturer's recommendations.
- Apply prior to placement of reinforcing steel, anchoring devices, and embedded items.
- C. Do not apply form release agent where concrete surfaces will receive special finishes or applied coverings which are affected by agent.

3.05 INSERTS, EMBEDDED PARTS, AND OPENINGS

- Provide formed openings where required for items to be embedded in or passing through concrete work.
- Locate and set in place items which will be cast directly into concrete.
- C. Coordinate work of other Sections in forming and placing openings, slots, reglets, recesses, chases, sleeves, bolts, anchors, and other inserts.
- Install accessories in accordance with manufacturer's instructions, straight, level, and plumb. Ensure items are not disturbed during concrete placement.
- E. Provide temporary ports or openings in formwork where required to facilitate cleaning and inspection. Locate openings at bottom of forms to allow flushing water to drain.
- F. Close temporary openings with tight fitting panels, flush with inside face of forms, and neatly fitted so joints will not be apparent in exposed concrete surfaces.

3.06 FORM CLEANING

- Clean and remove foreign matter within forms as erection proceeds.
- Clean formed cavities of debris prior to placing concrete.
- C. Flush with water or use compressed air to remove remaining foreign matter. Ensure that water and debris drain to exterior through clean-out ports.
- D. During cold weather, remove ice and snow from within forms. Do not use de-icing salts or water to clean out forms. Use compressed air or other means to remove foreign matter.

3.07 FORMWORK TOLERANCES

Construct formwork to maintain tolerances required by ACI 301.

3.08 FIELD QUALITY CONTROL

- A. Inspect erected formwork, shoring, and bracing to ensure that work is in accordance with formwork design, and that supports, fastenings, wedges, ties, and items are secure.
- B. Do not reuse wood formwork more than three times for concrete surfaces to be exposed to view. Do no patch formwork.

3.09 FORM REMOVAL

- Do not remove forms or bracing until concrete has gained sufficient strength to carry its own weight and imposed loads.
- B. Loosen forms carefully. Do not wedge pry bars, hammers, or tools against finished concrete surfaces scheduled for exposure to view.
- C. Store removed forms in manner that surfaces to be in contact with fresh concrete will not be damaged. Discard damaged forms.

END OF SECTION 03100

DIVISION 3 - CONCRETE Section 03200 - Concrete Reinforcement

PART 1. GENERAL

1.01 WORK INCLUDES

 The complete installation of the reinforcing steel bars and accessories for cast-in-place concrete.

1.02 RELATED SECTIONS

- A. Section 03100 Concrete Formwork.
- B. Section 03300 Cast-in-Place Concrete.

1.03 REFERENCES

- A. ACI 301 Structural Concrete for Buildings.
- B. ACI 318 Building Code Requirements For Reinforced Concrete.
- C. ACI SP-66 American Concrete Institute Detailing Manual.
- D. ASTM A615 Deformed and Plain Billet Steel Bars for Concrete Reinforcement.
- E. CRSI Concrete Reinforcing Steel Institute Manual of Practice.

1.04 SUBMITTALS

- Submit under provisions of Section 01010.
- B. Shop Drawings: Indicate bar sizes, spacings, locations, and quantities of reinforcing steel, and bending and cutting schedules. Contract drawings shall not be reproduced as the basis for shop drawings.
- Manufacturer's Certificate: Certify that products meet or exceed specified requirements.

1.05 QUALITY ASSURANCE

- Perform Work in accordance with CRSI Manual of Standard Practice.
- Submit certified copies of mill test report of reinforcement materials analysis.

1.06 COORDINATION

Coordinate with placement of formwork, formed openings and other work.

PART 2. PRODUCTS

2.01 REINFORCEMENT

Reinforcing Steel: ASTM A615, 60 ksi yield grade; deformed billet steel bars.

2.02 ACCESSORY MATERIALS

- A. Tie Wire: Minimum 16 gage, annealed steel wire, epoxy coated when used with epoxy-coated reinforcement.
- Chairs, Bolsters, Bar Supports, Spacers: Sized and shaped for strength and support of reinforcement during concrete placement conditions.
- C. Special Chairs, Bolsters, Bar Supports, Spacers Adjacent to Weather Exposed Concrete Surfaces: Plastic coated steel type; size and shape as required.

2.03 FABRICATION

- Fabricate concrete reinforcing in accordance with CRSI Manual of Standard Practice and ACI SP-66.
- Splice reinforcement on at locations indicated on drawings. Indicate location of splices on shop drawings.

PART 3. EXECUTION

3.01 PLACEMENT

- Place, support and secure reinforcement against displacement. Do not deviate from required position. Clean reinforcement of foreign particles or coatings.
- Accommodate placement of formed openings.
- Conform to ACI 318 code for concrete cover over reinforcement.

3.02 FIELD QUALITY CONTROL

A. Contractor shall notify the Owner's Representative at least 24 hrs. in advance of concrete placement. Placement of reinforcing shall occur in such sequence that the Owner's Representative has sufficient time to inspect the correctness of the reinforcing within the placement area. The Owner's Representative retains the right to require necessary revisions be made before concrete is placed.

END OF SECTION 03200

DIVISION 3 - CONCRETE Section 03300 - Cast-In-Place Concrete

PART 1. GENERAL

1.01 WORK INCLUDES

 The complete installation of cast-in-place concrete structures, including joint scalants.

1.02 RELATED SECTIONS

- A. Section 03100 Concrete Formwork: Formwork and accessories.
- B Section 03200 Concrete Reinforcement.
- C. Section 03400 Concrete Embedment Liner

1.03 REFERENCES

- A. ACI 301 Structural Concrete for Buildings.
- B. ACI 302 Guide for Concrete Floor and Slab Construction.
- ACI 304 Recommended Practice for Measuring, Mixing, Transporting and Placing Concrete.
- D. ACI 305R Hot Weather Concreting.
- E. ACI 306R Cold Weather Concreting.
- F. ACI 308 Standard Practice for Curing Concrete.
- G. ACI 318 Building Code Requirements for Reinforced Concrete.
- H. ASTM C31 Concrete Test Specimens.
- ASTM C33 Concrete Aggregates.
- J. ASTM C94 Ready-Mixed Concrete.
- K. ASTM C150 Portland Cement.
- L. ASTM C260 Air Entraining Admixtures for Concrete.

M. ASTM C494 - Chemical Admixtures for Concrete.

1.04 SUBMITTALS

Product Data: Provide data on joint devices, attachment accessories, admixtures.

1.05 QUALITY ASSURANCE

- Perform Work in accordance with ACI 301.
- Acquire cement and aggregate from same source for all work.
- C. Conform to ACI 305R when concreting during hot weather.
- Conform to ACI 306R when concreting during cold weather.

1.06 COORDINATION

 Coordinate this Section with other Sections which require embedment of components in cast-in-place concrete.

1.07 PRODUCT DATA

- A. Submit proposed mix design to Owner's Representative for review prior to commencement of work. Identify source and provide material certificates for cement, fine and coarse aggregates. Provide recent laboratory gradation for fine and coarse aggregates and mix design information in accordance with ACI 301.
- B. Submit Construction joint plan.

PART 2. PRODUCTS

2.01 CONCRETE MATERIALS

- Cement: ASTM C150, Type I Normal Portland Type, Gray Color.
- B. Fine and Coarse Aggregates: ASTM C33.
- C. Water: Potable.

2.02 ADMIXTURES

A. Air Entrainment: ASTM C260.

- B. Chemical: ASTM C494. Maximum 0.05% Chloride Ion Contents.
- The use of calcium chloride in any concrete is not permitted.

2.03 ACCESSORIES

- A. Non-Shrink Grout: Premixed compound consisting of non-metallic aggregate, cement, water reducing and plasticizing agents; capable of developing minimum compressive strength of 2,400 psi in 48 hours and 7,000 psi in 28 days.
- B. Curing Compound: Dress and Seal No. 18 by L&M Construction Chemicals, MB-429 by Master Builders, or Sikagard Cure/Hard by the Sika Corporation.
- C. Epoxy Grouted Adhesive Anchors: Hilti, Red Head, Simpson, or Rawl.

2.04 CONCRETE MIX

- Mix concrete in accordance with ACI 304. Deliver concrete in accordance with ASTM C94.
- Select proportions for normal weight concrete in accordance with ACI 301.
- C. Provide normal weight concrete of the following characteristics:
 - Compressive strength at 28 days: 4,000 psi.
 - Slump: 4 in. A tolerance of up to 1 in. above the maximum shall be allowed for one batch in any five consecutive batches tested.
 - Water/cement ratios: 0.4 (max).
- D. Use accelerating admixtures in cold weather only when approved by Owner's Representative. Use of admixtures will not relax cold weather placement requirements.
- Use set-retarding admixtures during hot weather only when approved by Owner's Representative.
- F. Water-reducing admixtures may be used in all concrete except footings and in strict compliance with the manufacturer's directions.
- G. Add air-entraining agent to concrete mix for air content of 6% (± 1%).

PART 3. EXECUTION

3.01 EXAMINATION

- Verify requirements for concrete cover over reinforcement.
- B. Verify that anchors, seats, plates, reinforcement and other items to be cast into concrete are accurately placed, positioned securely, and will not cause hardship in placing concrete.

3.02 PLACING CONCRETE

- Place concrete in accordance with ACI 301.
- Notify Owner's Representative minimum of 24 hours prior to commencement of operations.
- Ensure reinforcement, inserts, and embedded parts are not disturbed during concrete placement.
- D. Maintain records of concrete placement. Record date, location, quantity, air temperature, and test samples taken.
- Place concrete continuously between predetermined expansion, control, and construction joints.
- F. When air temperature is between 80°F and 90°F, reduce the mixing and delivery time specified in ASTM C94 from 1-1/2 hours to 75 minutes. When the air temperature is above 90°F, reduce the mixing and delivery time to 60 minutes.
- G. Cold weather concreting. Comply with ACI 306 except as follows:
 - In freezing weather, provide suitable means for maintaining concrete temperature at a minimum of 70°F for three days, or 50°F for five days after placing.
 - Cooling of concrete to outside temperature: Not faster than 1° per hour for first day and 2° per hour thereafter until outside temperature is reached.
 - Maximum temperature of concrete produced with heated aggregated, heated water, or both, at any time during its production or transportation: 90°F.
 - Do not mix chemicals or other foreign materials in concrete to prevent freezing or to accelerate hardening of concrete, unless approved in writing by Owner's Representative.

- H. Hot weather concreting. Comply with ACI 305R.
 - ACI recommendations shall be observed when any combination of high air temperature, low relative humidity and wind velocity tend to impair the quality of fresh or hardened concrete.
 - Retarding and water reducing admixtures shall be approved in writing for each concrete mix design prior to placement.

3.03 CONCRETE FINISHING

- A. Provide exterior concrete formed surfaces to be left exposed with smooth rubbed finish in accord with ACI 301. All other formed surfaces shall have fins, projections and offsets removed.
- Provide Class A tolerances to exterior concrete slabs according to ACI 301.
 - Broom finish all exterior slabs. Broom out all tool marks.
- C. Pitch slabs to drain.

3.04 CURING AND PROTECTION

- Immediately after placement, protect concrete from premature drying, excessively hot or cold temperatures, and mechanical injury.
- B. Maintain concrete with minimal moisture loss at relatively constant temperature for a period necessary for hydration of cement and hardening of concrete in accordance with ACI 308.
- Cure and protect finished concrete slabs in accordance with ACI 308.

3.05 FIELD QUALITY CONTROL

- Field inspection and testing will be performed in accordance with ACI 301 and under provisions of Section 01010, paragraph 8.0.
- Testing firm will take cylinders, perform slump and air entrainment tests in accordance with ACI 301.
- Provide free access to Work and cooperate with appointed firm.
- Submit proposed concrete mix design to Owner's Representative firm for review 14 days prior to commencement of Work.

E. Testing frequency shall be as specified in Section 01010, paragraph 8, except that one additional test cylinder will be taken during cold weather concreting, cured on job site under same conditions as concrete it represents.

3.06 PATCHING

- Defective Concrete: Concrete not conforming to required lines, details, dimensions, tolerances or specified requirements.
- B. Repair or replacement of defective concrete will be determined by Owner's Representative and performed by the Contractor at no additional cost to the project.
- C. Do not patch, fill, touch-up, repair, or replace exposed concrete except upon express direction of Owner's Representative for each individual area.

END OF SECTION 03300

PART 1. GENERAL

1.01 WORK INCLUDES

 Specifications and guidelines for manufacturing and installing high-density polyethylene embedment liners.

1.02 RELATED SECTIONS

- A. Section 03100 Concrete Formwork.
- B. Section 03300 Cast-in-Place Concrete.

1.03 REFERENCES

- A. American Society for Testing and Materials (ASTM)
 - D 1505 Test Method for Density of Plastics by the Density-Gradient Technique
 - D 1603 Test Method for Carbon Black in Olefin Plastics
 - D 5199 <u>Standard Test Method for Measuring Nominal Thickness of Geotextiles and Geomembranes</u>
 - D 5596 Standard Test Method for Microscopic Evaluation of the Dispersion of Carbon Black in Polyolefin Geosynthetics
 - D 6693 Standard Test Method for Determining Tensile Properties of Nonreinforced Polyethylene and Nonreinforced Flexible Polypropylene Geomembranes
 - D 1204 Standard Test Method for Linear Dimensional Changes of Nongrid Thermoplastic Sheeting or Film at Elevated Temperature
 - D 696 Standard Test Method for Coefficient of Linear Thermal Expansion of Plastics Between -30°C and 30°C With a Vitreous Silica Dilatometer
 - D 746 Standard Test Method for Brittleness Temperature of Plastics and Elastomers by Impact
 - D 570 Standard Test Method for Water Absorption of Plastics
 - E 96 Standard Test Method for Water Vapor Transmission of Material

1.04 SUBMITTALS

A. All work for and in connection with the installation of the lining, field seaming and welding joints shall be completed in strict conformity with all applicable instructions and recommendations of the liner manufacturer. B. Included with the shipment of liner, submit certified test reports that the liner and material are manufactured in accordance with standards specified herein.

1.05 OUALIFICATIONS

- A. The HDPE liner specified in this section shall be furnished by a manufacturer who is fully experienced, reputable and qualified in the manufacturing of the materials. The manufacturer must at least 10 years of manufacturing experience.
- Locking devices must be extruded to the sheet as a one step process.
- C. Liner shall be GSE StudLiner as manufactured by GSE Lining Technology, Inc.
- D. Liner shall be 8 feet in width.
- E. Liner shall demonstrate a minimum pull-out strength of 14,000 psf.

1.06 COORDINATION

Coordinate with placement of formwork, formed openings and other work.

PART 2. PRODUCTS

2.01 ROLL DIMENSIONS

- A. Embedment sheets shall be produced in rolls that are 8.0 ft (2.4 m) in width and a thickness range of 80 mils (2.0 mm) to 200 mils (5.0 mm) in thickness. Roll lengths vary according to thickness.
- B. Locking studs of the same material as that of the liner shall be integrally extruded with the sheet. Stud spacing shall be on approximate 1.25 in (30 mm) centers, such that there are approximately 110 studs per square foot (1200 per square meter).

2.02 MATERIAL PROPERTIES

- A. The material used in the embedment liner and in all welding strips shall be made from 97-98% virgin high density polyethylene and 1.5-3% carbon black or pigmentation for the purpose of an otherwise specified color.
- Plasticizer shall not be added to the resin formulation.

- C. Embedment sheet and welding strips shall be free of holes, pinholes, bubbles, blisters, excessive contamination by foreign matter, and nicks and cuts on roll edges.
- D. The HDPE cap strips shall be made from HDPE, have good impact resistance and have an elongation sufficient to bridge up to 1/4 inch settling cracks.
- Cap strips shall be approximately 4 inches wide or greater and shall be equivalent to that of the liner.
- F. Material shall maintain a repairable state through it's lifecycle by methods approved and recommended by the manufacturer.
- G. Embedment sheets shall have the following physical properties when tested in accordance with Table I.
- H. Raw resin shall have the following properties when tested in accordance with Table 2.

Table 1: Material Properties

| Property | Test Method | | Nomin | al Value | | Testing Frequency |
|---|--|------------------------|------------------------|------------------------|------------------------|---------------------------|
| Thickness, mm (mil) | ASTM D 5199 | 2.00 (80) | 3.00 (120) | 4.00 (160) | 5.00 (200) | Every 5th roll |
| Density, g/cm ³ | ASTM D 1505 | 0.94 | 0.94 | 0.94 | 0.94 | 1/100,000 ft ² |
| Tensile Properties Strength@Yield,lb/in ² (MPa) Elongation @ Break, % | ASTM D 6693 Type IV, Dumbell G.L.= 2.0in. | 2,200 (14.5) 500 | 2,200 (14.5) 500 | 2,200 (14.5) 500 | 2,200 (14.5) 500 | 1/100,000 ft ² |
| Stud Pull-Out Strength ¹ , lb/ft ² (kN/m ²) | | >14,000 (669.89) | >14,000 (669.89) | >14,000 (669.89) | >14,000 (669.89) | 1/ product |
| Carbon Black Content/ Pigment Content, % Black Liner Gray Liner | ASTM D 1603, mod. ASTM D 5630, mod. | 2-3 1.5 – 2.5 | 2-3 1.5 – 2.5 | 2-3 1.5 – 2.5 | 2-3 1.5 – 2.5 | 1/100,000 ft ² |
| Carbon Black Dispersion ² | ASTM D 5596 | Note 2 | Note 2 | Note 2 | Note 2 | 1/100,000 ft ² |
| Notched Constant Tensile Load, hours | ASTM D 5397 | 400 | 400 | 400 | 400 | 1/ formulation |
| Coefficient of Linear Thermal Expansion, per C | ASTM D 696 | 1.20E-04 | 1.20E-04 | 1.20E-04 | 1.20E-04 | I/ product |
| Low Temperature Brittleness, °C | ASTM D 746 | -77 | -77 | -77 | -77 | 1/ product |
| Dimensional Stability, % (each direction) | ASTM D 1204 | ± 1.0 | ± 1.0 | ± 1.0 | ± 1.0 | 1/ product |
| Water Absorption, % | ASTM D 570 | 0.1 | 0.1 | 0.1 | 0.1 | 1/ product |
| Water Vapor Transmission, (g/m²/day) | ASTM E 96 | <0.01 | <0.01 | < 0.01 | <0.01 | 1/ product |

¹Note: Concrete must have a compressive strength of at least 5,000 lb/in¹ (34,500 kPa).
²Note: Dispersion only applies to near spherical agglomerates. 9 of 10 views shall be Category 1 or 2. No more than 1 view for category 3.

Table 2: Raw Material Properties

| Property | Test Method | Value | Testing Frequency |
|---------------------|-----------------------------|-------|-------------------|
| Density, g/cm3 | ASTM D 1505 | 0.932 | 1/ resin lot |
| Melt Flow, g/10 min | ASTM D 1238 (190/2.16) | ≤1.0 | 1/ resin lot |
| OIT, minutes | ASTM D 3895 (1atm/200°C) | 100 | 1/ formulation |

2.03 MATERIAL SUPPLY

- Embedment sheets shall be supplied in roll form, sheets, pre-fabricated tubes or panels.
- Cap strips shall be supplied in 4 inch widths or greater.

PART 3. EXECUTION

3.01 PLACEMENT

- Place, support and secure reinforcement against displacement. Do not deviate from required position. Clean reinforcement of foreign particles or coatings.
- Accommodate placement of formed openings.
- Conform to ACI 318 code for concrete cover over reinforcement.

3.02 FIELD QUALITY CONTROL

A. Contractor shall notify the Owner's Representative at least 24 hrs. in advance of concrete placement. Placement of the Concrete Embedment Liner shall occur in such sequence that the Owner's Representative has sufficient time to inspect the correctness of the placement within the concrete formwork area. The Owner's Representative retains the right to require necessary revisions be made before concrete is placed.

END OF SECTION 03200



Appendix E: Operation & Maintenance Manual for #1 Ash Pond



Coffeen Power Station

Operational Procedure

X-XXX-XXXX--XXX

Operation & Maintenance Manual for #1 Ash Pond

(Bottom Ash Recycle Pond)

Effective Date: xx/xx/xxxx

Reason for Change: New Procedure

Approved By: x Date: xx/xx/xxxx

Responsible Department: Coffeen Power Station, Technical Services Department

John Romang

| This entire document shall be in the field during procedure |
|---|
| performance. |
| The following portions of this procedure shall be in the field |
| during procedure performance: |
| from this procedure shall be in the field during |
| procedure performance. |
| No part of this procedure is required to be in the field during |
| procedure performance |

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1.0 Purpose

1.1 This procedure is intended to ensure the safe and environmentally responsible operation and use of the #1 Ash Pond (Bottom Ash Recycle Pond) at the Coffeen Power Station. The primary purpose of the #1 Ash Pond is for the removal of bottom ash by settling and the recirculation of slag tank water. The pond is used to supply water to the Unit 1 and Unit 2 ash handling systems via the recycle pumps.

2.0 Scope

2.1 This procedure applies to all onsite personnel and the Dam Safety Group staff.

3.0 Responsibilities

- 3.1 Outside Unit Operator Checks the pond level and screens once a shift. Operates the facilities as described in this Operational Procedure. Reports any conditions noted during routine activities to the Shift Supervisor and Chemistry Department. Writes job requests if a problem is identified.
- 3.2 Shift Supervisor (SS) Calls the Chemistry Department when structural concerns or overflow conditions are reported. Make entries into the shift electronic log book (e-log) indicating the concern and actions taken.
- 3.3 Dam Safety Inspector Conducts weekly detailed dam safety inspections and provides a report with findings and recommendations. Make entries in e-log indicating the concern and actions taken.

4.0 Historical Information

- 4.1 The #1 Ash Pond was initially constructed to be a mixed ash deposition pond and was put in service in the mid-1960's. It is located east of the Main Building. It is a 23 acre pond with a maximum outer berm height of 41.5 feet above ground surface level (approximately elevation 637.5'). The pond overflow was located on the north east corner of the pond and discharged into the flume.
- 4.2 The #1 Ash Pond was converted to act as a closed loop system in the late 1970's when the dewatering bins were installed. The mixed ash was removed and deposited into the #2 ash pond during the closure of #2 pond. The #1 Ash Pond berms were modified and an inner berms was added to the pond to aid in dropping out bottom ash solids. Exterior berm elevation is approximately 637.5 feet.

- 4.3 The #1 Ash Pond was equipped with an emergency overflow at the outlet structure. When the pond level reaches approximately 6.5 feet from the top of the berm, it will overflow into the flume. Overflow will be reported to the EPA. In 2011 there was an assessment of the overflow pipe which showed no obstructions or damage.
- 4.4 In 2006, the bottom ash system was modified to directly sluice bottom ash into the pond, bypassing the retired dewatering bins. Bottom Ash is removed from the pond via an outside contractor on an as needed (typically daily) basis.

5.0 Water Supply

All water inlets to the pond are located on the west side of the pond.

The ash sluice lines (from the valve house) discharge to the pond. These lines are used to convey ash from the slag handling system to the #1 Ash Pond. These lines are the southern most of the pond inlets. HPSW system is routed to the pond (valve house sparger valves, floor drains at Unit 1 cyclone level).

The Slag Tank Overflow sump pumps discharge into the pond at the concrete culvert located directly east of the of the lime/soda ash silo. Also in this area, a small stainless line extends thru the concrete. This is the discharge of the sludge pumps at the Waste Treatment System in the Recycle Pump House building.

The recycle pump flow control valves discharge to the pond through a line located at the northwest corner of the pond. Also in the vicinity of this line is the discharge pipe of the recycle pump house sump pumps.

Water from the Unit 1 and Unit 2 oil water separators are typically routed to the pond via the Slag Tank Overflow Pump (STOP) House sumps. Water entering these sumps are floor and roof drains in the plant and the yard area immediately to the north of the main building.

6.0 Operations Requirements

Pond Level - Plant personnel shall monitor the level of the #1 Ash Pond on a daily basis. Pond level is maintained at approximately 1.0' to 1.5' at the water level staff gauge located on the pond side of the screens. The staff gauge has elevation 629.0' as the 0 elevation.

At 2.0' water level (elevation 631.0 feet), the pond overflows resulting in a sampling and analysis requirement for Total Suspended Solids and Oil and Grease with reporting of the results to the IEPA. If the pond is found at or above 2.0' on the pump side staff gauge, contact Chemistry immediately.

Water can be added to the pond from either the Unit 1 or Unit 2 Low Pressure Service Water (LPSW) headers via piping that discharges to the slag tank overflow trench.

Water can be drained from the pond via the water supply pipe to the dewatering bins. Opening this valve drains water from the recycle header which will remove water from the #1 Ash Pond.

Recycle Pump Intake Structure – Suction to the recycle pumps is supplied from the intake structure located at the west end of the north leg of the pond. This is the only water discharge point from the pond. Water level staff gauges are located upstream and downstream of the trash screens for determination of the screen differential. At 0.5′ differential, the screens should be cleaned. Level sensors are also installed upstream and downstream of the screens. Digital displays of the upstream and downstream levels are located along the north side of the catwalk leading out to the screen enclosure. These level sensors will generate a high screen differential alarm in the Control Room DCS. Check screen differential (should clean screens at 6 inches differential.) When the screens become plugged, suction to the recycle pumps is reduced. Call shift supervisor to report if screens needs to be cleaned.

Oil Boom – Plant personnel shall monitor the oil boom that is provided upstream of the intake structure. Check condition of oil booms across pond, at discharge, and across pond inlet. Booms should be replaced when they become oil saturated or damaged. Also check that booms have not come unattached from one another. Write JR to change out booms or to reconnect booms when required.

Emergency Conditions – If a condition arises where there is a possibility of an embankment failure, then the following procedures will be followed:

- 1. Notify the Supervising Engineer Dam Safety immediately.
- 7.0 Dam Safety Requirements
- 7.1 Dam Safety Inspections The plant's impoundment and flood prevention structures shall be inspected and maintained in a manner to ensure safe and environmentally responsible operations. A regular maintenance program shall be performed and shall consist of the following inspection items:

- 1. Earth embankments: Walk the crest, side slopes, and downstream toe of the dam concentrating on surface erosion, seepage, cracks, settlement, slumps, slides, and animal burrows. Frequency of inspection: Weekly.
- 2. Vegetation: Grass should be a thick vigorous growth to stabilize the earth embankment soils and prevent erosion form occurring. There should be NO trees on the earth embankment and none within a minimum of 20 feet of the embankment toe or other structures. Mowing frequency: Semiannually.
- 3. Well Readings: Record level of wells on the crest and toe of the berm. Frequency: Quarterly.
- 4. Special Inspections Special inspections of the levees and ash pond berms shall be performed after earthquakes, floods, water level exceedance in the ponds, or heavy rainfall events. Inspection and report shall be equal to an annual inspection level of detail. Water level in the pond should be noted after a heavy rainfall. Dam Safety staff shall accompany plant personnel on special inspections. Frequency: As required.
- 8.0 Maintenance Log
- 8.1 Dam & Berm Inspector shall enter on e-log under the Dam Safety tab all weekly inspections, any usual occurrences, and maintenance performed.
- 9.0 Contact Numbers

Plant Environmental Supervisor: John Romang / 217-534-7629
Plant Dam & Berm Inspector: Vito Passariello/ 217-534-7664
Plant Control Room: 217-534-7668 / 217-534-7669

Supervising Engineer Dam Safety: Steve Bluemner / 314-554-6298

Dam Safety Staff Contact: Mike Wagstaff / 314-554-6296

10.0 References



Appendix F: Operation and Maintenance Manual, Gypsum Management FacilityOperation (2015)

Operation and Maintenance Manual Coffeen Energy Center Gypsum Management Facility Montgomery County, Illinois

IDNR Permit # DS2014019 Dam Permit # IL50578 & IL50579

Prepared For:

ILLINOIS POWER GENERATING COMPANY
Coffeen Energy Center
134 CIPS Lane
Coffeen, Illinois 62017

Prepared By:

HANSON PROFESSIONAL SERVICES INC. 1525 South Sixth Street Springfield, Illinois 62703

Amended By:

DYNEGY OPERATING COMPANY 1500 Eastport Plaza Drive Collinsville, Illinois 62234

> Original: February 2008 Amended: March 2015

OPERATION AND MAINTENANCE MANUAL COFFEEN ENERGY CENTER GYPSUM MANAGEMENT FACILITY MONTGOMERY COUNTY, ILLINOIS

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SECTION 1.0 GENERAL

This operation and maintenance (O&M) manual outlines objectives, proposed policies, responsibilities, and procedures for Coffeen Energy Center personnel who are responsible for the management of the Coffeen Energy Center Gypsum Management Facility (GMF). The GMF incorporates two reservoirs, the Gypsum Pond and the Recycle Pond, for processing and storing gypsum.

1.1 REASONS FOR DEVELOPMENT AND DISSEMINATION OF THE O&M MANUAL

The State of Illinois Rivers, Lakes and Streams Act, (615 ILCS 5) Paragraph 23a includes the statement "The Department is authorized to carry out inspections of any dam within the State, and to establish standards and issue permits for the safe construction of new dams and the reconstruction, repair, operation and maintenance of all existing dams." (emphasis added).

Part 3702 of Section 17 of the Illinois Administrative Code, Chapter I entitled the "Construction and Maintenance of Dams" details the requirements to obtain a permit for the construction, operation, and maintenance of a dam. Section 3702.40 b) includes the following statements:

- "4) An applicant for a Class I or II dam shall submit an operational plan specifying the method and schedule for the operation of the dam and the routine operating procedures to keep the dam in good working order, including an emergency warning plan." and
- "5) As a condition of each permit, the dam owner shall submit a maintenance plan detailing the procedures and schedules to be followed to maintain the dam and its appurtenances in a reasonable state of repair."

Thus, it is a requirement of all dam owners who have dams which fall under the jurisdiction of the Illinois Department of Natural Resources Office of Water Resources (IDNR-OWR) to operate and maintain them safely.

As a dam owner, Illinois Power Generating Company (IPGC) Coffeen Energy Center is responsible for the safety of the public and for maintaining the structures at the facility for both safety and economy. The overall public interest is served by providing a document to serve as a basis for the safe and economical operation and maintenance of the dam during both emergency and day-to-day conditions.

1.2 GENERAL RESPONSIBILITIES CONCERNING DAMS

IPGC is responsible for the operation and maintenance of the Gypsum Pond Dam and the Recycle Pond Dam. These responsibilities include general maintenance (mowing, removing debris from decants, placing riprap where needed, etc.), operation, inspection and emergency action decisions.

SECTION 2.0 DEFINITIONS

Appurtenant Works - The structures or machinery auxiliary to dams which are built to operate and maintain dams; such as outlet works, spillways, gates, valves, channels, etc.

Boil - A stream of water discharging from the ground surface downstream of the dam carrying with it a volume of soil which is distributed around the hole formed by the discharging water.

Berm - A horizontal step or bench in the sloping profile of an embankment dam.

Breach - A break, gap, or opening (failure) in a dam which releases impoundment water.

Dam - A barrier built for impounding or diverting the flow of water.

Dike (Levee) - An embankment, usually applied to embankments or structures built to protect land from flooding.

Drain, Layer or Blanket - A layer of pervious material in a dam to facilitate the drainage of the embankment including such items as a toe drain, a weephole, and a chimney drain.

Drawdown - The resultant lowering of the water surface level due to the release of water from the impoundment.

Embankment - Fill material, usually rock or earth, placed with sloping sides.

Earthen Dam - Any dam constructed of excavated natural materials.

Emergency Action Plan - A predetermined plan of action to be taken to reduce the potential for property damage and loss of lives.

Failure - An incident resulting in the uncontrolled release of water from the dam.

Freeboard - The vertical distance between a stated water level and the top of the dam.

Gate or Valve - In general, a device in which a leaf or member is moved across the waterway to control or stop the flow.

Groin - The junction of the upstream or downstream face of the dam with the valley wall.

Maintenance - The upkeep, involving labor and materials, necessary for efficient operation of dams and their appurtenant works.

Operation - The administration, management, and performance needed to operate the dam and appurtenant works.

Operation and Maintenance Inspection - Inspections conducted by the dam operator. These inspections are frequent visual "Walk-around" inspections of the dam surface and appurtenant works.

Outlet - An opening through which water can freely discharge for a particular purpose from an impoundment.

Phreatic Surface - The upper surface of saturation in an embankment.

Piping - The progressive development of internal erosion by seepage, appearing downstream as a hole or seam, discharging water that contains soil particles.

Riprap - A layer of large stones, broken rock or precast blocks placed in a random fashion usually on the upstream slope of an embankment dam, on a reservoir shore, or on the sides of a channel as a protection against wave and ice action.

Silt/Sediment - Soil particles and debris in an impoundment.

Slump/Slide Area - A portion of earth embankment which moves downslope, sometimes suddenly, often with cracks developing.

Spillway System - A structure or structures over or through which flows are discharged. If the flow is controlled by gates, it is considered a controlled spillway. If the elevation of the spillway crest is the only control of the flows, it is considered an uncontrolled spillway.

Emergency Spillway - A spillway designed to operate very infrequently, only during exceptionally large floods, usually constructed of materials expected to erode slowly.

Principal Spillway - The main spillway which controls both normal and flood flows and is usually constructed of non-erodable materials.

Auxiliary Spillway - A spillway which works in conjunction with the principal spillway to control flood flows and is usually constructed of non-erodable materials.

Stilling Basin - A basin constructed to dissipate the energy of fast flowing water, such as from a spillway, and to protect the streambed from erosion.

Toe of Embankment - The junction of the face of the dam with the ground surface in the floodplain upstream or downstream of the dam.

SECTION 3.0 INFORMATION ABOUT THE DAMS

3.1 LOCATION

The Gypsum Pond Dam and Recycle Pond Dam are located in the NW 1/4 of Section 11, Township 7 North, Range 3 West of the Third Principal Meridian in Montgomery County, Illinois. More specifically, the dams are located approximately 1.5 miles south of Coffeen, Illinois. A map showing the location of the dams is included in Appendix A.

3.2 DESCRIPTION OF DAM AND APPURTENANCES

The gypsum pond perimeter earthen dam, the gypsum pond "gypsum" dam, and the recycle pond dam will all be regulated in accordance with 17 Illinois Administrative Code (IAC) Part 3702, Construction and Maintenance of Dams. The gypsum pond perimeter earthen dam, which will be lined with a dual high density polyethylene (HDPE) geomembrane system, will have a maximum embankment height of 13 ft and a maximum impounding capacity of 442 acre-ft (measured at the top of earthen dam elevation 632 ft). There will be an additional 123 acre-ft of incised storage. The total volume of gypsum stored within the completed gypsum pond dams will be approximately 2,478 acre-ft.

The dam for the recycle pond, which will be lined with a 60 mil HDPE geomembrane, will have a maximum embankment height of 16 ft and a maximum impounding capacity of 243 acre-ft (measured at the top of dam elevation 629 ft). There will be an additional 99 acre-ft of incised storage.

The gypsum pond will be divided into two sub-cells for the containment of scrubber sludge (gypsum). Discharges to the site will switch back and forth between the two sub-cells so that one sub-cell can be dewatered and raised while the other is in use. There will be two fixed decant pipes constructed in the gypsum stack – one for each sub-cell - which will discharge to stilling wells located adjacent to the perimeter ditches. The control elevation on the decant pipes will be maintained 5.0 ft below the lowest point on the stack cell crest. The decant pipes will enable the cells to be dewatered after storm events so that a minimum of 5.0 ft of freeboard will be maintained in each cell. A minimum of 4.7 ft of freeboard is required above the decant inlet to contain the Probable Maximum Flood (PMF) storm event in addition to peak wind generated waves.

The gypsum pond dam perimeter ditches will be located on the interior sides of the earthen dam. Runoff from the stack will be conveyed through the ditches to a transfer channel which will discharge into the recycle pond. The ditches will be trapezoidal in shape with a 15 ft bottom width, a maximum depth of 9 ft and a longitudinal slope of 0.0005 ft/ft. Side slopes will be 3H:1V. During operation, the ditches will be monitored for erosion. If erosion of the designed ditch geometry occurs, a geogrid will be used for stabilization.

The transfer channel between the gypsum pond dam and the recycle pond have a trapezoidal cross-section with 3H:1V side slopes will be lined with HDPE. The 500 ft long transfer channel will transition from a 32-ft bottom width at an invert elevation of 623.0 ft at the upstream end to a 60-ft bottom width at an invert elevation of 622.0 ft at the downstream end. The transfer channel will be fitted with stop logs capable of raising the discharge control elevation to 625.0 ft. To prevent degradation of the HDPE liner due to flow velocities, the transfer channel and a portion of the recycle pond dam will incorporate an additional sacrificial layer of HDPE.

The emergency spillway for the recycle pond will consist of three 6 ft by 6 ft precast reinforced concrete risers (drop inlets) with a top elevation of 624 ft (5 ft below the top of the dam). The recycle pond's HDPE liner will attach to the exterior sides of each riser. A 4-ft diameter HDPE outlet conduit will be constructed at each riser with an upstream invert of 615.0 ft and a downstream invert of 613.0 ft. Assuming a normal pool elevation of 624 ft (control elevation of the risers), the emergency spillway has been designed to pass the 24-hour PMF storm event with adequate freeboard to prevent overtopping of the recycle pond crest by wind generated waves. The emergency spillway has been provided in the event of accident or catastrophic rainfall only. It is not expected to be activated during the life of the facility. As designed, all discharges from the system will be through the pump house located on the southeast corner of the recycle pond.

3.3 SIZE AND HAZARD CLASSIFICATION

If a worst case failure of the gypsum pond dam were to occur, and the entire volume of the stack is released easterly into Coffeen Lake, the Coffeen Lake reservoir has adequate freeboard to accept this additional volume without overtopping the dam during flood events up to and including the 60 percent PMF. However, the power plant and several residences could potentially be impacted if the gypsum stack dam were to fail in a westerly direction. Considering the regulatory criteria established in Part 3702, the gypsum stack perimeter earthen dam and the gypsum stack "gypsum" dam are classified as intermediate-size Class I (high hazard potential) dams.

A failure of the recycle pond dam would discharge water to Coffeen Lake but it is not anticipated to result in loss of life or any significant economic damage. Breach analyses indicate that a failure of the recycle pond dam during a PMF event would be expected to result in an increase in the Coffeen Lake water surface elevation of not more than ½ inch. Accordingly, the recycle pond dam is classified as a small-size Class III (low hazard potential) dam.

3.4 PURPOSE OF THE DAMS

The dams will be used to dewater, store and dispose of flue gas desulphurization sludge (gypsum) from the Coffeen Power Station (the Plant). Gypsum will be transported to the Gypsum Pond Dam in slurry form (approximately 20 percent solids) and allowed to settle. Clarified process water will then be decanted to the recycle pond and returned to the Plant for reuse via a pipeline.

3.5 PERTINENT DATA

Pertinent data about the dams, appurtenant works, and reservoirs are presented in Table 3-1 and Table 3-2.

Table 3-1 Pertinent Data for the Gypsum Pond Earthen Dam (Based on the Construction of 2 Gypsum Cells)

| Perimeter Ditches | | | Transfer Channel | | |
|-----------------------------------|---------|---------|---------------------------------|--------|---------|
| Bottom Width | 15.00 | feet | Bottom Width | 32.00 | feet |
| Top Width | 73.50 | feet | Top Width | 86.00 | feet |
| Depth | 9.00 | feet | Depth | 9.00 | feet |
| Outer Side Slope | 3:1 | H:V | Upstream Invert | 623.00 | feet |
| Inner Side Slope | 3:1 | H:V | Downstream Invert | 622.00 | feet |
| Upstream Invert | 624.85 | feet | Weir Elevation | 625.00 | feet |
| Downstream Invert | 623.00 | feet | Weir Length (at 2 ft height) | 44.00 | feet |
| Ditch slope | 0.00050 | ft/ft | | | |
| Bank Full Cross-sectional Area | 378.00 | sf | Dam | | |
| Length of Each Ditch (Centerline) | 3710.00 | feet | Top of Dam Elevation | 632 | feet |
| Bank Full Volume of Each Ditch | 32.19 | acre-ft | Reservoir Surface Area | 77.29 | acres |
| Total Ditch length (Centerline) | 7420.00 | feet | Total Watershed Area | 77.29 | acres |
| Total Ditch Bank Full Volume | 64.39 | acre-ft | Dam Length | 7720 | feet |
| | | | Dam Height | 13 | feet |
| | | | | | |
| 1.0 PMF Storm Event | | | 0.5 PMF Storm Event | | |
| Storm Duration | 24 | hours | Storm Duration | 24 | hours |
| Peak Outflow Discharge | 1100.7 | cfs | Peak Outflow Discharge | 541.1 | cfs |
| Total Discharge Volume | 228.83 | acre-ft | Total Discharge Volume | 122.41 | acre-ft |
| Peak WSEL in Perimeter Ditches | 629.89 | feet | Peak WSEL in Perimeter Ditches | 628.23 | feet |
| Freeboard over Max WSEL | 2.11 | feet | Freeboard over Max WSEL | 3.77 | feet |
| Wave Runup/Wind Setup | 2.06 | feet | Wave Runup/Wind Setup | 2.06 | feet |
| Adequate Freeboard? | YES | | Adequate Freeboard? | YES | |
| | | | | | |
| 100-yr Storm Event - Critical Dur | ation | | 100-yr Storm Event - 24 Hour Du | ration | |
| Storm Duration | 12 | hours | Storm Duration | 24 | hours |
| Peak Outflow Discharge | 92.6 | cfs | Peak Outflow Discharge | 62.9 | cfs |
| Total Discharge Volume | 50.91 | acre-ft | Total Discharge Volume | 57.01 | acre-ft |
| Peak WSEL in Perimeter Ditches | 626.07 | feet | Peak WSEL in Perimeter Ditches | 625.84 | feet |
| Freeboard over Max WSEL | 5.93 | feet | Freeboard over Max WSEL | 6.16 | feet |
| Wave Runup/Wind Setup | 2.06 | feet | Wave Runup/Wind Setup | 2.06 | feet |
| Adequate Freeboard? | YES | | Adequate Freeboard? | YES | |
| | | | | | |

Note: The Critical Storm Duration is the duration of the rainfall event which produces the highest reservoir water surface elevation in the Gypsum Stack Perimeter Ditches for the given storm frequency. In each case, the starting normal pool elevation of the Recycle Pond is considered to be at elevation 624 ft.

Table 3-2 Pertinent Data for the Recycle Pond Dam (Based on the Construction of 2 Gypsum Cells)

| Dam | | | 3 Spillways- 6ft x 6ft inlet w/ 4ft d | ia outlet pip | e |
|-------------------------------|--------------------|-------------|--|-------------------|----------|
| Top of Dam Elevation | 629 | feet | Weir Length | 22 | feet |
| Invert of Reservoir Elevation | 605 | feet | Weir Elevation | 624.00 | feet |
| Reservoir Area at Invert | 11.55 | acres | Outlet Conduit Length | 120 | feet |
| Reservoir Area at Top of Dam | 17.07 | acres | Outlet Conduit Diameter (Inside) | 48 | inch |
| Total Reservoir Volume | 341.91 | acre-ft | Upstream Invert | 615 | feet |
| Volume at Elevation 624 ft | 259.60 | acre-ft | Downstream Invert | 614 | feet |
| Total Watershed Area | 94.36 | acres | Outlet Conduit Slope | 0.00833 | |
| Dam Length | 3600 | feet | | | |
| Dam Height | 16 | feet | | | |
| 1.0 PMF Storm Event - Norma | l Pool at El | lev. 624 ft | 1.0 PMF Storm Event - Normal | Pool at Elev | . 609 ft |
| Storm Duration | 24 | hours | Critical Storm Duration | 24 | hours |
| Peak Inflow | 1261.6 | cfs | Peak Inflow | 1261.6 | cfs |
| Peak Outflow | 586.9 | cfs | Peak Outflow | 289.7 | cfs |
| Peak Storage | 315.47 | acre-ft | Peak Storage | 280.65 | acre-ft |
| Peak WSEL (HEC-HMS) | 627.45 | feet | Peak WSEL (HEC-HMS) | 625.34 | feet |
| Freeboard over Peak WSEL | 1.55 | feet | Freeboard over Peak WSEL | 3.66 | feet |
| Wave Runup/Wind Setup | 1.20 | feet | Wave Runup/Wind Setup | 1.20 | feet |
| Adequate Freeboard? | YES | | Water Released from Dam? | YES | |
| 0.5 PMF Storm Event - Norma | | _ | 0.5 PMF Storm Event - Normal | | |
| Storm Duration | 24 | hours | Critical Storm Duration | 24 | hours |
| Peak Inflow | 608.4 | cfs | Peak Inflow | 608.4 | cfs |
| Peak Outflow | 413.6 | cfs | Peak Outflow | 0 | cfs |
| Peak Storage | 286.48 | acre-ft | Peak Storage | 255.83 | acre-ft |
| Peak WSEL (HEC-HMS) | 625.69 | feet | Peak WSEL (HEC-HMS) | 623.75 | feet |
| Freeboard over Peak WSEL | 3.31 | feet | Freeboard over Peak WSEL | 5.25 | feet |
| Wave Runup/Wind Setup | 1.20 YES | feet | Wave Runup/Wind Setup Water Released from Dam? | 1.20 NO | feet |
| Adequate Freeboard? | 163 | | water Released Irolli Dalli? | NO | |
| 100-yr Storm Event - Normal | | ev. 624 ft | 100-yr Storm Event - Normal I | | 619 ft |
| Critical Storm Duration | 12 | hours | Critical Storm Duration | 24 | hours |
| Peak Inflow | 113.2 | cfs | Peak Inflow | 76.6 | cfs |
| Peak Outflow | 95.8 | cfs | Peak Outflow | 0 | cfs |
| Peak Storage | 269.36 | acre-ft | Peak Storage | 258.48 | acre-ft |
| Peak WSEL (HEC-HMS) | 624.63 | feet | Peak WSEL (HEC-HMS) | 623.94 | feet |
| Freeboard over Peak WSEL | 4.37 | feet | Freeboard over Peak WSEL | 5.06 | feet |
| Wave Runup/Wind Setup | 1.20 | feet | Wave Runup/Wind Setup | 1.20 | feet |
| Adequate Freeboard? | YES | 1000 | Water Released from Dam? | NO | 1001 |

Note: The above variation in normal pool elevations for the Recycle Pond is for the purpose of documenting the water surface elevation which must be maintained in the recycle pond in order to prevent the release of water from the GMF for the above described storm events.

SECTION 4.0 OPERATIONS ACTIVITIES

4.1 INTRODUCTION

The operations plan describes the proposed operation of the Coffeen Gypsum Management Facility (GMF) which includes the gypsum pond and the recycle pond.

4.2 SITE OPERATIONS AND PERSONNEL

4.2.1 Site Operations

The GMF will receive gypsum slurry 24 hours per day, seven days per week. Routine facility maintenance and construction activities will generally be conducted during day shift hours. The crest widths for both the gypsum stack earthen dam and the recycle pond dam are 20 ft. In addition, multi-directional ramps are being provided for both structures so that they are readily accessible by inspection, maintenance and gypsum recovery equipment.

The Plant is a restricted access location. Additional fencing around the perimeter of the active sedimentation cells of the gypsum stack and the recycle pond will be erected to prevent unauthorized access to the GMF, which is also under surveillance by security personnel.

4.2.2 Personnel

The proposed GMF will be owned and operated by Ameren Energy Generating Company (Ameren). Corporate offices are located in St. Louis, Missouri. Overall responsibility for the GMF operation lies with Ameren management personnel.

4.3 GYPSUM MANAGEMENT FACILITY STARTUP

The major components of the proposed GMF consist of:

- The gypsum stack dam/impoundment;
- The recycle pond;
- The earthen transfer channel that connects the two structures and through which process water will be decanted from the gypsum stack into the recycle pond; and
- The recycle pond decant and pumphouse through which process water will be returned to the Plant for reuse.

Both the recycle pond and the gypsum stack dam will be constructed before gypsum is placed within the gypsum stack dam/impoundment.

Upon startup, it is likely that the gypsum stack impoundment will have no more than a few feet of water in the bottom to prevent the high density polyethylene (HDPE) geomembrane from moving. The gypsum slurry (approximately 20 percent solids) will be pumped from the

Plant to the gypsum stack via piping. The piping will be HDPE with a suitable pressure rating for the intended hydraulic and static head. The HDPE pipe will discharge the slurry into the impoundment, and gypsum will settle by gravity.

It will take approximately 10 months before the gypsum stack impoundment is filled to elevation 623 ft, the point where process water may begin flowing into the recycle pond via the HDPE-lined earthen channel connecting the two structures. As soon as water begins to fill the recycle pond, it will be pumped back to the Plant for reuse.

4.4 WATER BALANCE

The capacity of the recycle pond has been designed to accommodate all precipitation runoff from the entire gypsum pond/recycle pond area during a 2-week complete maintenance outage at the Coffeen Power Station (the Plant) followed by a 12-week outage of one of the two units. The runoff and excess water accumulated during this time can be stored within the recycle pond without discharging. The design is based on the maximum 3.5 month precipitation that has occurred in the area since 1950. This occurred in April, May, June and half of July, 1957 and consisted of 28.83 inches of rainfall.

The water balance has been carried out for the expected life of the Site. During the first nine or ten months of operation, the water balance is positive, meaning that there is more water entering the gypsum stack/recycle pond system through process water and precipitation than is leaving the system through process water return and evaporation. However, there is 15 ft of freeboard between the pump discharge and the emergency spillway. With proper water-level management, the water surface will remain well below discharge elevation. After this initial startup period, the water balance is negative, meaning that other water sources will need to be continually added to the process water makeup stream to maintain the volume necessary for transport of the gypsum slurry.

The water balance is of particular concern since the entire system is designed to be a closed loop with no discharges. (As previously noted, the recycle pond has been designed with an emergency spillway, but this is only to protect the structures in the event of an unforeseen accident or catastrophic rainfall event.) Table 3.5-2 lists the maximum water surface elevation allowed in the recycle pond in order to prevent the discharge of water for the 100-year storm event and the 0.5 PMF storm event.

4.5 GYPSUM MANAGEMENT FACILITY OPERATION

4.5.1 Routine Operations

Gypsum slurry will initially be discharged at the southwestern corner of the gypsum pond impoundment. Settled gypsum will gradually create a plane of material sloping gently towards the north end of the impoundment. Depending on the slope of the settled gypsum, the discharge pipe may be moved to other corners of the impoundment to evenly distribute the material. Care must be taken during the initial filling period so to ensure that the sand layer covering the ring drains is not disturbed. If necessary, the sand may be armored with larger washed aggregate or

the impoundment may be gradually filled with water to cover the sand prior to the discharge of gypsum slurry into the impoundment.

Once the gypsum plane reaches approximately elevation 627 ft (5 ft below the earthen dam crest), a track excavator or similar piece of equipment will be used to create the first gypsum berm and to form the perimeter ditch. Each gypsum berm will be approximately 10 ft in height and will effectively create a two-compartment impoundment within its perimeter. Gypsum for construction of the gypsum berm will be obtained from the settled material on the inside of the berm, creating an inner ditch. Gypsum slurry will then be discharged alternately into the inner ditch of each compartment. Gypsum will settle out into the inner ditch and clarified process water will flood the compartment to a depth of several feet. This water will be decanted to the perimeter ditch by way of an HDPE decant pipe which will discharge to a stilling well located at the toe of the gypsum stack.

As each compartment fills with settled gypsum, the discharge piping will be moved to the alternate compartment. The compartment, or sub-cell, that is not in service will be allowed to dewater and another gypsum berm will be constructed on top of the previous gypsum berm, effectively raising the gypsum stack another 10 ft. This alternating cycle of gypsum discharge, compartment dewatering and berm construction will continue. Gypsum will be deposited in the stack with an average dry density of approximately 74 lb/ft³. Drawing No. C-10201-25 provides a visual description of this process.

4.5.2 Piezometer Installation and Monitoring

The side slopes of the gypsum pond will be constructed with 3:1 side slopes. After consolidation of the settled gypsum over time, the final slopes should approach 3.75:1. The stability of each gypsum pond slope is <u>critically dependent</u> on the location of the phreatic surface which is anticipated to develop within the stack. Ring drains are intended to lower the phreatic surface so that it is located an adequate distance from the surface of the slope in order to maintain slope stability. In order to monitor the phreatic surface within the stack, piezometers will be installed on each side of the gypsum pond. The piezometers will be installed every 15 vertical feet up the slope (45 horizontal feet based on 3:1 side slopes) and will extend to a depth of at least 15 feet below the anticipated phreatic water surface elevation as shown in Figure 4-1. At the time of installation, each piezometer will be labeled with the "critical elevation" corresponding to the anticipated phreatic surface elevation at that location. The anticipated phreatic surface elevation is the water surface elevation which was used in the slope stability analysis of the gypsum pond. The water level in each piezometer will be read and recorded on a monthly basis. If at any time a reading is recorded higher than "critical elevation" for that specific peizometer, the design engineer must be contacted immediately for evaluation of the reading. Any readings above the "critical elevation" may be indicative of improper ring drain function and/or slope instability which could lead to a failure of the gypsum stack. Therefore, it is critical that the piezometers are installed in accordance with the construction plans and specifications and monitored in accordance with this manual. It may be necessary to install additional subdrainage to maintain the phreatic surface at the desired level within the gypsum stack.

| Figure 4-1 Anticipated Phreatic Surface in Gypsum Pond | ł |
|--|---|
| Refer to figure at the end of the report text. | |

4.6 DAM INSPECTIONS

The inspection program includes two types of dam inspections. The first is regularly conducted by the dam operator and is referred to as an Operation and Maintenance Inspection. The second type of inspection, referred to as the Engineering Inspection, is conducted by a qualified engineer approved by IPGC. All engineering inspection reports must be signed and sealed by an Illinois Registered Professional Engineer.

The dam operator will perform monthly Operation and Maintenance Inspections of the gypsum pond perimeter earthen dam <u>and the gypsum berms and side slopes</u> during the operating life of the structure. During these inspections, the gypsum stack ditches and the transfer channel will also be examined for signs of erosion and liner degradation. The "operating life of the structure" will be considered to cease upon covering of the gypsum with an HDPE/soil cover. Engineering Inspections will be conducted on an annual basis during the operating life of the structure and will continue after covering of the gypsum pond until authorization to abandon the structure is received from IDNR/OWR.

4.6.1 Operation and Maintenance Inspection

Occasional "walk-around" inspections of the dams and appurtenant works are to be made by the dam operator. During these inspections, a checklist of items to be maintained and items to be observed should be recorded. Appendix A provides an example of the Operation and Maintenance Inspection Checklist to be utilized for these inspections. If any of the following items are found to be unusual or are cause for concern, the Shift Supervisor should be notified and the Emergency Action Plan should be immediately consulted for guidance on an appropriate course of action.

Frequency: Operation and maintenance inspections will be performed by the dam operator on a monthly basis and also during and after unusual events such as heavy rainfall or an earthquake.

Inspection Items: During each inspection the following items should be noted in particular.

- 1. Water Level Maximum reservoir levels as a result of heavy rainfall should be recorded.
- 2. Earth Embankment Walk the crest, side slopes and downstream toe of the dam concentrating on surface erosion, seepage, cracks, settlement, slumps, slides, and animal burrows. These are described as follows:
 - Surface Erosion Removal of vegetative cover by water action or pedestrian or vehicle usage forming deep ruts or gullies.
 - Seepage The passage of water through and/or underneath the earth embankment abutment and natural groundline or at the contact between the embankment and

- outlet works. It can be indicated by cattails or other wet environmental vegetation, erosion, channelization, or slumping on the embankment face.
- Cracks Deep cracks usually indicate the movement of the dam and/or the foundation and can be in either the longitudinal (along the length of the dam) or transverse (across the dam) directions. Cracking can be an indicator of the beginning of slumps. Shallow cracks may develop during the summer when the surface soils of the embankment become severely dried and are usually of no concern in regard to the safety of the dam.
- Settlement Settlement is indicated by depressions or low spots and can be signs
 of consolidation of the dam or foundation or the loss of material beneath the
 settlement area.
- Slumps/Slides A slow or sudden movement of the earth embankment slope on either face toward the toe of the dam.
- If seepage indicates the presence of soil particles, or if deep cracks, settlement, slumps, or slides are noticed, a qualified engineer should be contacted immediately for consultation.
- Animal Burrows Animal burrows result in a loss of earth embankment material and can provide seepage paths for water through the embankment.
- 3. Gypsum Embankment Walk the crest, side slopes and downstream toe of the dam concentrating on surface erosion, seepage, cracks, settlement, slumps, slides and animal burrows. The descriptions for these are the same as for earth embankment.
- 4. Vegetation Grass should be a thick vigorous growth to stabilize the earth embankment soils and prevent erosion from occurring. Note the height of the grass; if greater than 1 foot a mowing of the area should be scheduled before the next inspection. There should be NO trees on the earth embankment and NONE within a minimum of 20 feet of the embankment toes or other structures. The gypsum embankment will not be seeded and is not expected to have any vegetation.
- 5. Gypsum Stack piezometers should be inspected for any damage or loss of function. Damaged piezometers must be promptly repaired or replaced since their function is critical to ensuring stability of the gypsum stack.
- 6. The water level in each Gypsum Stack piezometer must be measured and recorded during each monthly inspection. If the water level in any piezometer is above the "critical elevation" as discussed in Section 4.5.2 of this plan, the Ameren Technical Services Superintendent should be notified and the Emergency Action Plan should be immediately consulted for guidance on an appropriate course of action.

- 7. Gypsum Pond LD/LCRS Drains The change in location or amount of flows discharging from the Leak Detection/Leachate Collection Recovery System (LD/LCRS) should be recorded. If a significant change has occurred, a qualified engineer should be contacted for consultation.
- 8. Gypsum Stack Ring Drains The change in location or amount of flows discharging from the Ring Drains should be recorded. If a significant change has occurred, a qualified engineer should be contacted for consultation.
- 9. Gypsum Stack Fixed Decant Check the alignment and supports for the pipe. Record the amount of flows discharging from the pipe and any erosion or scour around the discharge point.
- 10. Gypsum Stack Perimeter Ditch The perimeter ditch should have a consistent prismatic shape for the entire length. Inspect the perimeter ditch for evidence of erosion, sediment deposition and irregularity in channel geometry, especially in the vicinity of siphon, decant or ring drain outfall structures. If irregularities are noted, repairs should be scheduled and completed.
- 11. Drawdown Facilities Check to make sure that the drawdown stop logs in the transfer ditch are undamaged, operating well and allowing for the free flow of water over them. Confirm during inspections the valves are opened and closed at least quarterly.
- 12. Transfer Channel Check for any debris or other obstructions which may block or restrict the free flow of water. Check for any pools or undulation of the floor of the channel.
- 13. Recycle Pond Decant Check for any debris or other obstructions around the Recycle Pond decant which may block or restrict the free flow of water. The emergency dewatering valve should be lubricated. If there is no return water in the pipe, the emergency dewatering valve should be exercised. Record the physical and operating conditions of the system.
- 14. Recycle Pond Drop Inlet Spillways Check for any debris or other obstructions around the inlet crest and at the bottom of the drop inlet which may block or restrict the free flow of water. Check for the development of any rusty areas on the concrete, and seepage, cracking, breaking, or spalling of the concrete. Check for settlement or cracking of the crest. Check for any debris in the pipes which may restrict the flow of water. Check for any tears or leaks in the HDPE liner covering the concrete.
- 15. Recycle Pond Rip Rap Basin Check for any debris or other obstructions in the riprap basin which may block or restrict the free flow of water. Check to make sure that the rip rap is remaining in a uniform position. Freeze/thaw action or flow over the rip rap may tend to lift or fracture, thus requiring replacement or leveling to maintain the necessary level of protection. NO trees or woody vegetation should be growing through the rip rap.

- 16. Fences Check for damage, accumulated debris, operation of gates and locks, and adequacy of locations (this may change with time as people access the area or development occurs in the area).
- 17. Perimeter Check the perimeter of the dams for a distance of at least 100 feet beyond the toe for signs of seepage or boils.
- 18. HDPE Liner Wherever exposed, the HDPE Liner should be inspected for tears, gouges, protrusions under the liner and abrasion.

Records: A log book of activities occurring at the dam is to be kept current by the dam operator. The log book should be reviewed during the Engineering Inspection. This book should contain at the least the following documentation:

- 1. Completed operation and maintenance inspection checklists
- 2. Readings from all piezometers on the Gypsum Stack
- 3. Additional visual observations
- 4. A list of maintenance performed
- 5. A list of any unusual occurrences at the dam
- 6. Copies of the engineering inspection reports

4.6.2 Engineering Inspection

The engineering inspection is to be conducted by a qualified engineer approved by Ameren. The inspection will provide a thorough evaluation of the dam condition and appurtenances. Appendix B is an example of the inspection report form which is to be utilized for these inspections.

Frequency: The Gypsum Pond Dam is a Class I, High Hazard Potential dam and is to be inspected by an Illinois Registered Professional Engineer at least once per year. The Recycle Pond Dam is classified as a Class III, Low Hazard Potential dams and is to be inspected by an Illinois Registered Professional Engineer at least once every five years.

Inspection Items: The engineer will thoroughly inspect all of the items noted in Section 4.6.1 Operation and Maintenance Inspection.

Records: The Dam Inspection Report form from IDNR-OWR "Guidelines and Forms for Inspection of Illinois Dams" (a copy of which is included in Appendix B), will be completed by the inspecting engineer and will be signed and sealed by an Illinois Registered Professional Engineer. This report will document problem areas and deficiencies; recommend remedial actions for problem areas; and establish time requirements for dealing with the problems. The original report will be retained in Dynegy Operating Company (DOC) files, and a copy of the report will be submitted to the Illinois Department of Natural Resources, Office of Water Resources.

4.6.3 Review of Emergency Action Plan

The emergency action plan should be reviewed annually to assure that all contacts, addresses and telephone numbers are current. Changes in the adjacent land use should also be noted and may dictate the need for revisions to the plan. Changes to the plan should be made as appropriate but only with the concurrence of the Montgomery County Emergency Services and Disaster Agency and of the Illinois Department of Natural Resources, Office of Water Resources. Copies of any revisions should also be forwarded to all personnel and known emergency responders that possess previous versions the plan.

SECTION 5.0 MAINTENANCE ACTIVITIES

Timely repairs are a must after problem areas have been identified. The dam operator is to perform the work required to correct items noted in the operation and maintenance inspections and engineering inspections. Such items include repairing erosion of the gypsum slopes, mowing, seeding, tree and brush removal, replacing rip rap, repairing fences and locks, clearing debris, etc. The maintenance activities specified in the following sections are minimum requirements. NOTE: NO alterations or repairs to structural elements should be made without the assistance of the Ameren Chief Dam Safety Engineer and the concurrence of the Illinois Department of Natural Resources, Office of Water Resources.

Debris: Remove all trash, logs and other debris which may obstruct flow into the principal spillway pipes and drop inlets, or block passage from their discharge channels.

Rip Rap: Replenish rip rap as needed to provide adequate protection against erosion.

Vegetation Control

1. Maintain a good grass cover on the embankment by seeding, fertilizing and mulching areas which are refilled, barren, or thinly vegetated. Seeding mixtures used for maintenance reseeding shall result in a cover compatible with adjacent cover. The seeding mixture specified at the time of the dam's construction was IDOT Standard Specifications Class 1A (Salt Tolerant Lawn Mixture) as follows:

| IDOT Class 1A Salt To | olerant Lawn Mixture |
|------------------------------|----------------------|
| Bluegrass | 60 lb/acre |
| Perennial Ryegrass | 20 lb/acre |
| Dawsons Red Fescue | 20 lb/acre |
| Scaldis Hard Fescue | 20 lb/acre |
| Fults Salt Grass | 60 lb/acre |

- 2. Grassed areas such as the embankment and the areas beyond the embankment toes for a distance of at least 20 feet should be mowed at least twice annually or at any time the height of the grass exceeds 1 foot.
- 3. All erosion areas will be filled and compacted, reseeded, fertilized and mulched to establish a thick erosion resistant cover.
- 4. Remove all trees and brush growing on the dam embankment to prevent development of a root system which could provide seepage paths. Herbicides utilized for tree and brush control are discussed in Appendix D.
- 5. Keep the riprap basin clear of weeds, brush, and trees.

6. Clear all brush and trees for a distance of approximately 20 feet beyond the toe of each dam.

Animal Damage: Fill rodent holes and other animal burrows with compacted clayey soil and reseed. If rodents become a nuisance, an effective rodent control program as approved by the Illinois Department of Natural Resources District Wildlife Biologist should be implemented.

Signs: All warning signs shall be maintained (repaired, painted, or replaced) as needed.

Gypsum Slopes: Erosion of the gypsum slopes will be evident with the presence of erosion rills. Erosion rills should be filled with additional gypsum material and graded to conform with the design slope.

Piezometers: All piezometers on the gypsum stack shall be inspected for signs of damage or displacement. Non-functioning piezometers shall immediately be replaced.

APPENDIX A LOCATION MAP

APPENDIX B OPERATION AND MAINTENANCE INSPECTION CHECKLIST

OPERATION AND MAINTENANCE INSPECTION CHECKLIST

| Dam Name (circle one): | Gypsum Pond Dam | Recycle Pond Dam |
|------------------------|-----------------|------------------|
| Date: | Time: | |
| Name of Inspector: | | |
| Reservoir Elevation: | feet | |
| | | |

| <u>ITEM</u> | <u>NO</u> | <u>YES</u> | <u>IF YES</u> |
|---|-----------|------------|--|
| Record Piezometer Readings for Gypsum Stack. Are any readings above the critical level? (see section 4.5.2 of O&M Manual) | | | Contact Manager, Environment & Chemistry and notify Hanson Professional Services |
| Note the condition of the Piezometers on the Gypsum Stack. Any damage? | | | Contact Manager, Environment & Chemistry |
| Deep Surface Cracks | | | Contact Manager, Environment & Chemistry |
| Slump or Slide on the upstream or downstream face | | | Contact Manager, Environment & Chemistry |
| Erosion from runoff, wave action or traffic | | | Repair and stabilize |
| Embankment, abutment or spillway seepage | | | Contact Manager, Environment & Chemistry |
| Seepage or flows of muddy water | | | Contact Manager, Environment & Chemistry |
| Uneven settlement | | | Contact Manager, Environment & Chemistry |
| Trees, brush or burrow holes on the embankment or in the riprap basin | | | Remove trees and brush, fill holes |
| Transfer channel or Spillway pipes blocked | | | Clear immediately |
| Damage to stop logs | | | Repair or replace |
| Damage to HDPE Liner | | | Repair and schedule engineer inspection |
| Settlement or displacement of Gypsum Pond fixed decant pipes or outlets | | | Schedule engineer inspection |
| Discharge from Gypsum Pond LD/LCRS Drains? | | | Record discharge rate for each outlet (time to fill bucket) |
| Discharge from Gypsum Pond Ring Drains? | | | Record discharge rate for each outlet (time to fill bucket) |
| Gypsum Stack Perimeter Ditch erosion | | | Schedule repair |
| Problems with Recycle Pond spillways | | | Contact Manager, Environment & Chemistry |
| Problems with Recycle Pond decant | | | Contact Manager, Environment & Chemistry |
| Height of grass (inches) | | inches | If more than 1 foot, schedule mowing |
| Damage to fencing, gates and locks or other access restriction measures | | | Contact Manager, Environment & Chemistry |
| Confirm drawdown facilities are opened and closed at least quarterly. | | | Contact Manager, Environment & Chemistry |

APPENDIX C ENGINEERING INSPECTION FORMS

Dam Inspection Report

| Name of Dam | Dam Identification Number | | |
|------------------------------------|---------------------------|--|--|
| Permit Number | Class of Dam | | |
| Location NW 1/4 Section 11 | | | |
| Owner | | | |
| Name | Telephone Number (Day) | | |
| Street | Telephone Number (Night) | | |
| | County Montgomery | | |
| City Zip Coo | de | | |
| Type of Dam | | | |
| Type of Spillway | | | |
| | | | |
| Weather When Inspected | | | |
| | | | |
| Pool Elevation When Inspected | | | |
| Tailwater Elevation When Inspected | | | |
| | Inspection Personnel: | | |
| | N. Total | | |
| | Name Title | | |

Professional Engineer's Seal

The Department of Natural Resources is requesting information that is necessary to accomplish the statutory purpose as outlined under the River, Lakes and Streams Act, 615 ILCS 5 (1994 State Bar Edition). Submittal of this information is REQUIRED. Failure to provide the required information could result in the initiation of non-compliance procedures as outlined in Section 702.160 of the "Rules for Construction and Maintenance of Dams". This form has been approved by the State Forms Management Center.

CONDITION CODES

| EC | - | Emergency Condition. A serious dam safety condition exists that needs immediate action. Emergency measures |
|-----------|---|--|
| | | implemented as instructed by Chief Dam Safety Engineer; such as, pool draw down, work stoppage, plant stoppage. |
| <u>NE</u> | = | No evidence of a problem |
| GC | = | Good condition |
| MM | = | Item needing minor maintenance and/or repairs within the year, the safety or integrity of the item is not yet imperiled |
| <u>IM</u> | = | Item needing immediate maintenance to restore or ensure its safety or integrity. Remediation should be completed within 1 month. |
| EC | = | Emergency condition which if not immediately repaired or other appropriate measures taken could lead to failure of the dam |
| <u>OB</u> | = | Condition requires regular observation to ensure that the condition does not become worse |
| <u>NA</u> | = | Not applicable to this dam |
| <u>NI</u> | = | Not inspected - list the reason for non-inspection under deficiencies |
| EC | = | Emergency Condition. A serious dam safety condition exists that needs immediate action. Emergency measures implemented as instructed by Chief Dam Safety Engineer; such as, pool draw down, work stoppage, plant stoppage. |

GYPSUM STACK - EARTH EMBANKMENT

| ITEM | CONDITION | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES & SCHEDULE |
|---|-----------|--------------|--|
| | | | |
| Surface Cracks | | | |
| Vertical and Horizontal Alignment of Crest | | | |
| Unusual movement or Cracking at or Beyond Toe | | | |
| Sloughing or Erosion of Outer Embankment Slopes | | | |
| Upstream Face Slope Protection (HDPE Liner) | | | |
| Seepage | | | |
| Animal Damage | | | |

GYPSUM STACK - EARTH EMBANKMENT

(Continued)

| ITEM | CONDITION | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES & SCHEDULE |
|------------------|-----------|--------------|--|
| Vegetative Cover | | | |
| | | | |
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GYPSUM STACK - GYPSUM EMBANKMENT

| ITEM | CONDITION | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES & SCHEDULE |
|--|-----------|--------------|--|
| | | | |
| Surface Cracks | | | |
| Vertical and Horizontal Alignment of Crest | | | |
| Unusual movement or Cracking at or Beyond Toe | | | |
| Sloughing or Erosion of Outside Embankment Slopes | | | |
| Sloughing or Erosion of Inside Embankment Slopes | | | |
| Seepage | | | |
| Animal Damage | | | |

GYPSUM STACK - GYPSUM EMBANKMENT (Continued)

| ITEM | CONDITION | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES & SCHEDULE |
|---|-----------|--------------|--|
| | | | |
| Condition of Piezometers on Gypsum Stack | | | |
| Piezometer Readings on Gypsum Stack Above Critical Level? | | | |
| | | | |
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<u>GYPSUM STACK – PERIMETER DITCH</u>

| ITEM | CONDITION | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES & SCHEDULE |
|---|-----------|--------------|--|
| Ditch Geometry (15 ft bottom width, 3:1 slopes, 8-9 ft depth) | | | |
| Concrete Apron at ring drain outlets | | | |
| Ring Drain Discharge Pipes | | | |
| Stilling Wells for Fixed Decants | | | |
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TRANSFER CHANNEL - (between gypsum stack and recycle pond)

| Drop Inlet | Structure | X Overflow Spillway Structure | Gated |
|-------------------------|-----------|-------------------------------|--|
| ITEM | CONDITION | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES & SCHEDULE |
| | | | |
| Debris | | | |
| Side Slope Stability | | | |
| HPDE Liner | | | |
| HDPE Liner Welds | | | |
| Stop Logs | | | |
| Differential Settlement | | | |
| | | | |

<u>RECYCLE POND - EMBANKMENT</u>

| ITEM | CONDITION | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES & SCHEDULE |
|---|-----------|--------------|--|
| Surface Cracks | | | |
| Vertical and Horizontal Alignment of Crest | | | |
| Unusual movement or Cracking at or Beyond Toe | | | |
| Sloughing or Erosion of Outer Embankment Slopes | | | |
| Upstream Face Slope Protection (HDPE Liner) | | | |
| Seepage | | | |
| Animal Damage | | | |

<u>RECYCLE POND - EMBANKMENT</u>

(Continued)

| ITEM | CONDITION | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES & SCHEDULE |
|------------------|-----------|--------------|--|
| Vegetative Cover | | | |
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RECYCLE POND - PRINCIPAL SPILLWAY (Left, Looking Downstream)

| X Drop Inlet Structure | | Overflow Spillway Structure | Gated | |
|----------------------------------|-----------|-----------------------------|--|--|
| ITEM | CONDITION | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES & SCHEDULE | |
| | | | | |
| Alignment of Structure Walls | | | | |
| Construction Joints | | | | |
| Differential Settlement | | | | |
| Erosion, Spalling, Cavitation | | | | |
| Joint Separation | | | | |
| Seepage Around or into Conduit | | | | |
| Surface Cracks | | | | |

RECYCLE POND - PRINCIPAL SPILLWAY (Left, Looking Downstream)

(Continued)

| X Drop Inlet | Structure | Overflow Spillway Structure | Gated |
|-------------------|-----------|-----------------------------|--|
| ITEM | CONDITION | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES & SCHEDULE |
| | | | |
| Structural Cracks | | | |
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RECYCLE POND - PRINCIPAL SPILLWAY (Center)

| X Drop Inlet S | Structure | Overflow Spillway Structure | Gated |
|----------------------------------|-----------|-----------------------------|--|
| ITEM | CONDITION | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES & SCHEDULE |
| | | | |
| Alignment of Structure Walls | | | |
| Construction Joints | | | |
| Differential Settlement | | | |
| Erosion, Spalling, Cavitation | | | |
| Joint Separation | | | |
| Seepage Around or into Conduit | | | |
| Surface Cracks | | | |

RECYCLE POND - PRINCIPAL SPILLWAY (Center)

(Continued)

| X Drop Inlet | Structure | Overflow Spillway Structure | Gated |
|-------------------|-----------|-----------------------------|--|
| ITEM | CONDITION | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES & SCHEDULE |
| | | | |
| Structural Cracks | | | |
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RECYCLE POND - PRINCIPAL SPILLWAY (Right, Looking Downstream)

| X Drop Inlet S | Structure | Overflow Spillway Structure | Gated | | |
|----------------------------------|-----------|-----------------------------|--|--|--|
| ITEM | CONDITION | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES & SCHEDULE | | |
| | | | | | |
| Alignment of Structure Walls | | | | | |
| Construction Joints | | | | | |
| Differential Settlement | | | | | |
| Erosion, Spalling, Cavitation | | | | | |
| Joint Separation | | | | | |
| Seepage Around or into Conduit | | | | | |
| Surface Cracks | | | | | |

<u>RECYCLE POND - PRINCIPAL SPILLWAY (Right, Looking Downstream)</u> (Continued)

| X Drop Inlet Structure | | Overflow Spillway Structure | Gated |
|------------------------|-----------|-----------------------------|--|
| ITEM | CONDITION | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES & SCHEDULE |
| | | | |
| Structural Cracks | | | |
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RECYCLE POND - ENERGY DISSIPATOR

| X Principal Spillway | | Outlet Works Type: | FHWA HEC-1 | 4, Riprap Basin | |
|----------------------|-----------|--------------------|------------|--|-------|
| ITEM | CONDITION | DEFICIENCIE: | S | RECOMMENDED REMEDIAL MEASU SCHEDULE | RES & |
| | | | | | |
| Riprap | | | | | |
| Outlet Channel | | | | | |
| Debris | | | | | |
| | | | | | |
| | | | | | |
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RECYCLE POND - DECANT STRUCTURE

| ITEM | CONDITION | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES & SCHEDULE | |
|------------------------------------|-----------|--------------|--|--|
| Alignment | | | | |
| Connection to Bollard | | | | |
| Debris in Inlets | | | | |
| Condition of Pipe | | | | |
| Condition of Liner Beneath Pipe | | | | |
| Connection to Ballast | | | | |
| Connection of Pipe Boot to Liner | | | | |

RECYCLE POND - DECANT STRUCTURE

(continued)

| ITEM | CONDITION | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES & SCHEDULE |
|--------------------------------|-----------|--------------|--|
| Seepage Around or into Conduit | | | |
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<u>RECYCLE POND – WATER LEVEL GAGE STRUCTURE</u>

| ITEM | CONDITION | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES & SCHEDULE |
|------|-----------|--------------|--|
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APPENDIX D HERBICIDES

HERBICIDES

Site personnel should check with the Illinois Department of Natural Resources, Regional Fisheries Biologist and the Regional Wildlife Biologist before using any herbicide. Read the product label prior to use and follow the use directions and precautions accordingly.

On March 1, 1979 the U.S. Environmental Protection Agency (U.S.E.P.A.) halted the use of the herbicide 2, 4, 5-T in parks and recreation areas. The use of silvex (2, 4, 5-TP) around water has also been banned.

The Agronomy Department at the University of Illinois and the Aquatic Biology Section of the Department of Natural Resources, Office of Scientific Research and Analysis indicate that the herbicides containing the 2, 4-D or 2, 4-DP are legal for use in parks and recreation areas and effective for controlling brush and woody growth. Some examples of approved herbicides are:

- 1. Tordon RTU by DOW Chemical. (Can be obtained with blue dye.)
- 2. WEEDONE 170 by Union Carbide
- 3. WEEDONE, 2, 4-DP by Union Carbide
- 4. A 1% to 2% solution of ROUNDUP
- 5. Garlon by DOW Chemical
- 6. Banvel by Sandoz

Your distributor may carry brand name herbicides other than those listed above. Be certain that the product does not contain the ingredients 2, 4, 5-T or 2, 4, 5-TP. An example of an unacceptable product is ESTERON 2, 4, 5 by DOW Chemical.

APPENDIX E CONSTRUCTION DRAWINGS



Appendix G: Photos of 2015 Sloughing Repairs



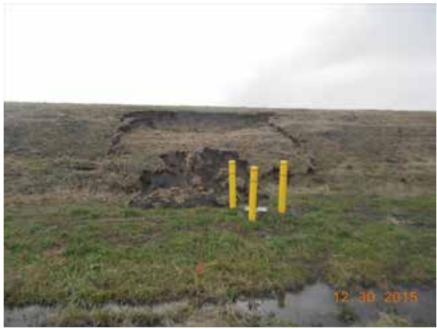


Figure G.1. Photo of 2015 sloughing prior to repairs.



Figure G.2. Photo of 2015 sloughing prior to repairs.

AECOM



Figure G.3. Photo of 2015 sloughing area after repairs.



Figure G.4. Photo of 2015 sloughing area after repairs.

ATTACHMENT C

Coffeen Power Plant - Ash Pond 1's Chemical Constituents

In accordance with 35 I.A.C. 845.230(d)(2)(C), IPGC is submitting available/existing analyses of "the chemical constituents of all waste streams, chemical additives and sorbent materials entering or contained in" the CCR impoundment, Ash Pond 1.

A list of the chemical constituents' analyses contained in the CCR surface impoundment can be found in Appendix A. As determined through antidegradation studies, this list contains chemical constituents found in the surface free liquid and the subsurface free liquids. IPGC is also including a list of chemical additives, sorbent materials and waste streams that were submitted in the facility's NPDES permit applications to IEPA within the past ten years at a minimum and/or listed in the current NPDES permit (IL0001554) in Appendix B.

Appendix A: Chemical Constituents Contained in the Ash Pond

| Pollutant | Units | Surface Free Liquids Average Concentration | | Subsurface Free Liquids Average Concentration | |
|--------------------------|-------|--|-------|--|-------|
| Ammonia | mg/L | < | 0.100 | < | 0.363 |
| Arsenic | mg/L | | 0.002 | | 0.011 |
| Barium | mg/L | | 0.166 | | 0.140 |
| Boron | mg/L | | 2.10 | | 2.55 |
| Cadmium | mg/L | < | 0.001 | < | 0.001 |
| Chloride | mg/L | | 17.4 | | 10.4 |
| Chromium | mg/L | < | 0.004 | < | 0.005 |
| Chromium (hexavalent) | mg/L | < | 0.005 | < | 0.005 |
| Copper | mg/L | | 0.019 | < | 0.003 |
| Cyanide | mg/L | < | 0.005 | < | 0.005 |
| Fluoride | mg/L | | 1.01 | < | 0.500 |
| Iron | mg/L | | 0.270 | | 1.08 |
| Lead | mg/L | < | 0.001 | < | 0.001 |
| Manganese | mg/L | | 0.010 | | 0.035 |
| Mercury | mg/L | < | 0.000 | < | 0.000 |
| Nickel | mg/L | < | 0.005 | < | 0.006 |
| Nitrate | mg/L | < | 0.020 | < | 0.060 |
| Nitrite | mg/L | | | < | 0.100 |
| Nitrogen, Total Kjeldahl | mg/L | < | 1.00 | < | 0.809 |
| Oil and Grease | mg/L | < | 6.02 | < | 5.20 |
| рН | SU | | 7.22 | | 7.03 |
| Phenols | mg/L | < | 0.005 | < | 0.005 |
| Phosphorus | mg/L | | 0.138 | | 0.164 |
| Selenium | mg/L | | 0.001 | | 0.006 |
| Silver | mg/L | < | 0.005 | < | 0.004 |
| Sulfate | mg/L | | 986 | | 1400 |
| TDS | mg/L | | 1156 | | 1850 |
| TSS | mg/L | | 6.56 | | 23.4 |
| Zinc | mg/L | < | 0.006 | < | 0.007 |

^{*}Used https://calstormcompliance.com/ph-averaging-tool

Appendix B: List of Chemical Additives, Waste Streams and Sorbent Materials

Chemical Additives

Surfactant (used 2-drums, one time, for cleaning)

Waste Streams and Sorbent Materials*

Waste Treatment Sump

Slag Tank Overflow Pump House (slag tank overflows, roof drains, de-aerator drain, oil/water separator drains and Unit 1 & 2 Floor & Equip. Drains

Boiler Water Wash

Bottom Ash and Sluice Water

Stormwater from Roof Drains

Service Water Makeup (Coffeen Lake Water)

^{*}No sorbent materials



Bottom Ash SDS Number: 0.0 Revision Date: 03/2018

Safety Data Sheet

Section 1 Identification of the Substance and of the Supplier

1.1 Product Identifier

| Product Name/Identification: | ASTM Bottom Ash |
|------------------------------|---|
| Synonyms: | Ash; Ashes; Ash residues; Ashes, residues, bottom; Bottom ash; Bottom ash residues; Coal Fly Ash; Pozzolan; Waste solids. |
| Formula: | UVCB Substance |

1.2 Relevant Identified Uses of the Substance or Mixture and Uses Advices Against

| Relevant Identified Uses: | Component of wallboard, concrete, roofing material, bricks, cement kiln feed. |
|---------------------------|---|
| Uses Advised Against: | None known. |

1.3 Details of the Supplier of the SDS

| Manufacturer/Supplier: | Dynegy, Inc. |
|-----------------------------|-------------------------------|
| Street Address: | 601 Travis Street, Suite 1400 |
| City, State and Zip Code: | Houston, TX 77002 |
| Customer Service Telephone: | 800-633-4704 |

Preparation Date: 02/23/2018



Bottom Ash SDS Number: 1.0 Revision Date: 03/2018

Section 2

2.1 Classification of the Substance

GHS Classification(s) according to OSHA Hazard Communication Standard (29 CFR 1910.1200):

Hazards Identification

- Eye Irritant, Category 2A
- STOT-SE, Category 3 (Respiratory Irritation)
- Carcinogen, Category 1A
- STOT-RE, Category 1 (Lungs)
- Toxic to Reproduction, Category 2

2.2 Label Elements

| Labelling according to 29 CFR 1910.1200 Appendices A, B and C* | | |
|--|--|--|
| Hazard Pictogram(s): | | |
| Signal word: | DANGER | |
| Hazard Statement(s): | Causes serious eye irritation. May cause respiratory irritation. May cause damage to lungs after repeated/prolonged exposure via inhalation. May cause cancer of the lung. Suspected of damaging fertility or the unborn child. | |
| Precautionary Statement(s): | Obtain special instructions before use. Do not handle until all safety precautions have been read and understood. Avoid breathing dust. Wash thoroughly after handling. Do not eat drink or smoke when using this product. Wear protective gloves/protective clothing/eye protection/face protection. Use outdoors or in a well-ventilated area. If exposed or concerned: Get medical advice/attention. Store in a secure area. Dispose of product in accordance with local/national regulations. | |

^{*} Fly ash and other coal combustion products (CCPs) are UVCB substances (unknown or variable composition or biological). Various CCPs, noted as ashes/ash residuals; Ashes, residues, bottom; Bottom ash; Bottom ash residues; Waste solids, ashes under TSCA are defined as: "The residuum from the burning of a combination of carbonaceous materials. The following elements may be present as oxides: aluminum, calcium, iron, magnesium, nickel, phosphorus, potassium, silicon, sulfur, titanium, and vanadium." Ashes including fly ash and fluidized bed combustion ash are identified by CAS number 68131-74-8. The exact composition of the ash is dependent on the fuel source and flue additives composed of many constituents. The classification of the final substance is dependent on the presence of specific identified oxides as well as other trace elements.

Preparation Date: February 23, 2018



2.3 Other Hazards

Listed Carcinogens:

-Respirable Crystalline Silica

IARC: [Yes] NTP: [Yes] OSHA: [Yes] Other: (ACGIH) [Yes]

Section 3 Composition/Information on Ingredients

| Substance | CAS No. | Percentage (%) | GHS Classification |
|---------------------------------------|-------------------------|----------------|---|
| Crystalline Silica | 14808-60-7 | 20 - 40% | Repeat Dose STOT, Category 1 Carcinogen, Category 1A |
| Silica, crystalline respirable (RCS) | 14808-60-7 | See Footnote 1 | Repeat Dose STOT, Category 1 Carcinogen. Category 1A |
| Aluminosilicates ² | Various, see Footnote 2 | 10 - 60% | Single Exposure STOT, Category 3 |
| Calcium oxide (CaO) | 1305-78-8 | 10 - 30% | Skin Irritant, Category 2 Eye Irritant, Category 1 Single Exposure STOT, Category 3 |
| Iron oxide | 1309-37-1 | 1 - 10% | Not Classified |
| Manganese dioxide (MnO ₂) | 1313-13-9 | <2% | Skin Irritant, Category 2 Eye Irritant, Category 2B |
| Magnesium oxide | 1309-48-4 | 2 - 10% | Not Classified |
| Phosphorus pentoxide (P_2O_5) | 1314-56-3 | ≤2% | Skin Irritant, Category 2 Eye Irritant, Category 2B |
| Sodium oxide | 1313-59-3 | 1 - 10% | Not Classified |
| Potassium oxide (K₂O) | 12136-45-7 | ≤1% | Skin Irritant Category 2 Eye Irritant Category 2B |
| Titanium dioxide (TiO ₂) | 13463-67-7 | <3% | Not Classified |

¹The percentage of respirable crystalline silica has not been determined. Therefore, a GHS classification of Carcinogen 1A has been assigned.

²Aluminosilicates (CAS# 1327-36-2) may be in the form of mullite (CAS# 1302-93-8); aluminosilicate glass; pozzolans (CAS# 71243-67-9); or calcium aluminosilicates such as tricalcium aluminate (C3A), or calcium sulfoaluminate (C4A3S). The form is dependent on the source of the coal and or the process used to create the CCP. Pulverized coal combustion would be more likely to create high levels of pozzolans. Aluminosilicates may have inclusions of calcium, titanium, iron, potassium, phosphorus, magnesium and other metal oxides.



Section 4 First Aid Measures

4.1 Description of First Aid Measures

| Inhalation: | If product is inhaled and irritation of the nose or coughing occurs, remove person to fresh air. Get medical advice/attention if respiratory symptoms persist. |
|---------------|---|
| Skin Contact: | If skin exposure occurs, wash with soap and water. |
| Eye Contact: | If product gets into the eye, rinse copiously with water for several minutes. Remove contact lenses, if present and easy to do. Seek medical attention/advice if irritation occurs or persists. |
| Ingestion: | No specific first aid measures are required. |

4.2 Most Important Health Effects, Both Acute and Delayed

Acute Effects: Direct exposure may cause respiratory irritation, eye irritation and skin irritation. The product dust can dry and irritate the skin and cause dermatitis and can irritate eyes and skin through mechanical abrasion.

Chronic Effects: Chronic exposure may cause lung damage from repeated exposure. Prolonged inhalation of respirable crystalline silica above certain concentrations may cause lung diseases, including silicosis and lung cancer.

4.3 Indication of Any Immediate Medical Attention and Special Treatment Needed

Seek first aid or call a doctor or Poison Control Center if contact with eyes occurs and irritation remains after rinsing. Get medical advice if inhalation occurs and respiratory symptoms persist.



Section 5
Firefighting Measures

5.1 Extinguishing Media

| Suitable Extinguishing Media: | Product is not flammable. Use extinguishing media appropriate for surrounding fire. |
|---------------------------------|---|
| Unsuitable Extinguishing Media: | Not applicable, the product is not flammable. |

5.2 Special Hazards Arising from the Substance or Mixture

| Hazardous Combustion Products: | None known. |
|--------------------------------|-------------|
|--------------------------------|-------------|

5.3 Advice for Firefighters

| · · | As with any fire, wear self-contained breathing apparatus (NIOSH |
|-----------------------------------|--|
| and Precautions for Firefighters: | approved or equivalent) and full protective gear. |

Section 6 Accidental Release Measures

6.1 Personal Precautions, Protective Equipment and Emergency Procedures

| Personal precautions/Protective Equipment: | See Section 8.2.2 Individual Protective Measures. For concentrations exceeding Occupational Exposure Levels (OELs), use a self-contained breathing apparatus (SCBA). |
|--|--|
| Emergency procedures: | Use scooping, water spraying/flushing/misting or ventilated vacuum cleaning systems to clean up spills. Do not use pressurized air. |

6.2 Environmental Precautions

| Environmental precautions: | Prevent contamination of drains or waterways and dispose according to local and national regulations. |
|----------------------------|---|
|----------------------------|---|



6.3 Methods and Material for Containment and Cleaning Up

Methods and materials for

containment and cleaning up:

Do not use brooms or compressed air to clean surfaces. Use dust collection vacuum and extraction systems.

Large spills of dry product should be removed by a vacuum system. Dampened material should be removed by mechanical means and recycled or disposed of according to local and national regulations.

See Sections 8 and 13 for additional information on exposure controls and disposal.

Section 7 Handling and Storage

7.1 Precautions for Safe Handling

Practice good housekeeping. Use adequate exhaust ventilation, dust collection and/or water mist to maintain airborne dust concentrations below permissible exposure limits (note: respirable crystalline silica dust may be in the air without a visible dust cloud).

Do not permit dust to collect on walls, floors, sills, ledges, machinery, or equipment. Maintain and test ventilation and dust collection equipment. In cases of insufficient ventilation, wear a NIOSH approved respirator for silica dust when handling or disposing dust from this product. Avoid contact with skin and eyes. Wash or vacuum clothing that has become dusty. Avoid eating, smoking, or drinking while handling the material.

7.2 Conditions for Safe Storage, Including any Incompatibilities

Minimize dust produced during loading and unloading.



Section 8 Exposure Controls/Personal Protection

8.1 Control Parameters

| OCCUPATIONAL EXPOSURE LIMIT SUBSTANCE | | OSHA PEL TWA (mg/m³) | NIOSH REL TWA (mg/m³) | ACGIH TLV TWA (mg/m³) | CA - OSHA PEL (mg/m³) |
|--|------------|----------------------|-----------------------|-----------------------|--------------------------|
| Calcium oxide | | 5 | 2 | 2 | 2 |
| Particulates Not Otherwise Regulated | Total | 15 | 15 | 10 | 10 |
| | Respirable | 5 | 5 | 3 | 5 |
| Respirable Crystalline Silica | Respirable | 0.05 | 0.05 | 0.025 | 0.05 |
| Manganese dioxide (as manganese compounds) | Total | 5 (Ceiling) | 1 3 (STEL) | 0.1 | 0.2 |
| | Respirable | - | - | 0.02 | - |

8.2 Exposure Controls

8.2.1 Engineering Controls

Provide ventilation to maintain the ambient workplace atmosphere below the occupational exposure limit(s). Use general and local exhaust ventilation and dust collection systems as necessary to minimize exposure.

8.2.2 Personal Protective Equipment (PPE)

| Respiratory protection: | Wear a NIOSH approved particulate respirator if exposure to airborne particulates is unavoidable and where occupational exposure limits may be exceeded. If airborne exposures are anticipated to exceed applicable PELs or TLVs, a self-contained breathing apparatus or airline respirator is recommended. | |
|---------------------------|--|--|
| Eye and face protection: | If eye contact is possible, wear protective glasses with side shields. Avoid contact lenses. | |
| Hand and skin protection: | Wear gloves and protective clothing. Wash hands with soap and water after contact with material. | |



Section 9 Physical and Chemical Properties

9.1 Information on Basic Physical and Chemical Properties

| Property: Value | Property: Value |
|--|--|
| Appearance (physical state, color, etc.): Fine tan/ gray particulate | Upper/lower flammability or explosive limits: Not applicable |
| Odor: Odorless ¹ | Vapor Pressure (Pa): Not applicable |
| Odor threshold: Not applicable | Vapor Density: Not applicable |
| pH (25 °C) (in water): 8 - 11 | Specific gravity or relative density: 2.2 – 2.9 |
| Melting point/freezing point (°C): Not applicable | Water Solubility: Slight |
| Initial boiling point and boiling range (°C): Not applicable | Partition coefficient: n-octane/water: Not determined |
| Flash point (°C): Not determined | Auto ignition temperature (°C): Not applicable |
| Evaporation rate: Not applicable | Decomposition temperature (°C): Not determined |
| Flammability (solid, gas): Not combustible | Viscosity: Not applicable |

The use of urea or aqueous ammonia injected into the flue gas to reduce nitrogen oxides (NOx) emissions may result in the presence of ammonium sulfate or ammonium bisulfate in the ash at less than 0.1%. When ash containing these substances becomes wet under high pH (>9), free ammonia gas may be released resulting in objectionable/nuisance ammonia odor and potential exposure to ammonia gas especially in confined spaces.



Section 10 Stability and Reactivity

| 10.1 Reactivity: | The material is an inert, inorganic material primarily composed of elemental oxides. |
|--|--|
| 10.2 Chemical stability: | The material is stable under normal use conditions. |
| 10.3 Possibility of hazardous reactions: | The material is a relatively stable, inert material; however, when ash containing ammonia becomes wet under high pH (>9), free ammonia gas may be released resulting in an objectionable/nuisance ammonia odor and potential exposure to ammonia gas especially in confined spaces. Polymerization will not occur. |
| 10.4 Conditions to avoid: | Product can become airborne in moderate winds. Dry material should be stored in silos. Materials stored out of doors should be covered or maintained in a damp condition. |
| 10.5 Incompatible materials: | None known. |
| 10. 6 Hazardous decomposition products: | None known. |



Section 11 Toxicological Information

11.1 Information on Toxicological Effects

| Endpoint | Data |
|--------------------------------|--|
| Acute oral toxicity | LD50 > 2000 mg/kg |
| Acute dermal toxicity | LD50 > 2000 mg/kg |
| Acute inhalation toxicity | LD50 > 5.0 mg/L |
| Skin corrosion/irritation | Does not meet the classification criteria but may cause slight skin irritation. Product dust can dry the skin which can result in irritation. |
| Eye damage/irritation | Causes serious eye irritation. Positive scores for conjunctiva irritation and chemosis in 2/3 animals based on average of 24, 48 and 72-hour scores with irritation clearing within 21 days; no corneal or iritis effects observed. |
| Respiratory/skin sensitization | Not a respiratory or dermal sensitizer. |
| Germ cell mutagenicity | Not mutagenic in in-vitro and in-vivo assays with or without metabolic activation. |
| Carcinogenicity | Not available. Respirable crystalline silica has been identified as a carcinogen by OSHA, NTP, ACGIH and IARC. |
| Reproductive toxicity | No developmental toxicity was observed in available animal studies. Reproductive studies on CCPs showed either no reproductive effects, or some effects on male and female reproductive organs and parameters but without a clear dose response. |
| STOT-SE | CCPs when present as a nuisance dust may result in respiratory irritation. |
| STOT-RE | In a 180-day inhalation study with fly ash dust, no effects were observed at the highest dose tested. NOEC = 4.2 mg/m³; it is not possible to assess the level at which toxicologically significant effects may occur. Repeated inhalation exposures to high levels of respirable crystalline silica may result in lung damage (i.e., silicosis). |
| Aspiration Hazard | Not applicable based product form. |



Section 12 Ecological Information

12.1 Toxicity

| Fly Ash (CAS# 68131-74-8) | |
|--------------------------------------|--|
| Toxicity to Fish | LC50 > 100 mg/L |
| Toxicity to Aquatic Invertebrates | Data indicates that the test substance is not toxic to <i>Daphnia magna</i> (EC50 undetermined) |
| Toxicity to Aquatic Algae and Plants | EC50 = 10 mg/L |
| Calcium oxide CAS# 1305-78-8 | |
| Toxicity to Fish | LC50 = 50.6 mg/L The findings were closely related to the pH of the test solutions; therefore, pH is considered to be the main reason for the effects. |
| Toxicity to Aquatic Invertebrates | EC50 = 49.1 mg/L The findings were closely related to the pH of the test solutions; therefore, pH is considered to be the main reason for the effects. |
| Toxicity to Aquatic Algae and Plants | NOEC =48 mg/L @ 72 hours based on Ca(OH) ₂ The initial pH of the test medium was not directly related to the biologically relevant effects. The formation of precipitates is likely the result of the reaction between CO ₂ dissolved in the medium. |

12.2 Persistence and Degradability

Not relevant for inorganic materials.

12.3 Bioaccumulative Potential

This material does not contain any compounds that would bioaccumulate up the food chain.

12.4 Mobility in Soil

No data available.

12.5 Results of PBT and vPvB Assessment

This material does not contain any compounds classified as "persistent, bioaccumulative or toxic" nor as "very persistent/very bioaccumulative".

12.6 Other Adverse Effects

None known.



Section 13 Disposal Considerations

See Sections 7 and 8 above for safe handling and use, including appropriate industrial hygiene practices. Dispose of all waste product and containers in accordance with federal, state and local regulations.

Section 14 Transport Information

| | Shipping Name: | Not Regulated |
|--------------------|----------------|---------------|
| Regulatory entity: | Hazard Class: | Not Regulated |
| U.S. DOT | ID Number: | Not Regulated |
| | Packing Group: | Not Regulated |



Section 15 Regulatory Information

15.1 Safety, Health and Environmental Regulations/Legislation Specific for the Mixture

TSCA Inventory Status

All components are listed on the TSCA Inventory.

California Proposition 65

The following substances are known to the State of California to be carcinogens and/or reproductive toxicants:

- Respirable crystalline silica
- Titanium dioxide
- State Right-to-Know (RTK)

| Component | CAS | MA ^{1,2} | NJ ^{3,4} | PA ⁵ | RI ⁶ |
|--|------------|-------------------|--------------------------|-----------------|-----------------|
| Ammonium bisulfate | 7803-63-6 | No | Yes | No | No |
| Ammonium sulfate | 7783-20-2 | Yes | No | Yes | No |
| Calcium oxide | 1305-78-8 | Yes | Yes | Yes | No |
| Iron oxide | 1309-37-1 | Yes | Yes | Yes | No |
| Magnesium oxide | 1309-48-4 | No | Yes | No | No |
| Phosphorus pentoxide (or | 1314-56-3 | Yes | Yes | Yes | No |
| phosphorus oxide) | | | | | |
| Potassium oxide | 12136-45-7 | No | Yes | No | No |
| Silica-crystalline (SiO ₂), quartz | 14808-60-7 | Yes | Yes | Yes | No |
| Sodium oxide | 1313-59-3 | No | Yes | No | No |
| Titanium dioxide | 13463-67-7 | Yes | Yes | Yes | Yes |

Preparation Date: February 23, 2018

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¹ Massachusetts Department of Public Health, no date
² 189th General Court of The Commonwealth of Massachusetts, no date
³ New Jersey Department of Health and Senior Services, 2010a
⁴ New Jersey Department of Health, 2010b
⁵ Pennsylvania Code, 1986

⁶ Rhode Island Department of Labor and Training, no date



Section 16

Other Information, Including Date of Preparation or Last Revision

16.1 Indication of Changes

Date of preparation or last revision: February 23, 2018

16.2 Abbreviations and Acronyms

ACGIH: American Conference of Industrial Hygienists

CA: California

CAS: Chemical Abstract Services
 CCP: Coal Combustion Product
 CFR: Code of Federal Regulations
 EPA: Environmental Protection Agency

GHS: Globally Harmonized System of Classification and Labelling

IARC: International Agency for Research on Cancer

• LC50: Concentration resulting in the mortality of 50 % of an animal population

• LD50: Dose resulting in the mortality of 50 % of an animal population

MA: MassachusettsNA: Not ApplicableNJ: New Jersey

NOEC: No observed effect concentration

NIOSH: National Institute of Occupational Safety and Health

NOx: Nitrogen oxides

NTP: US National Toxicology ProgramOEL: Occupational Exposure Limit

OSHA: Occupational Safety and Health Administration

PA: Pennsylvania

PBT: Persistent, Toxic and Bioaccumulative

PEL: Permissible exposure limit
 PPE: Personal Protective Equipment
 REL: Recommended exposure limit

RI: Rhode Island

RCS: Respirable Crystalline Silica

• RTK: Right-to-Know

SCBA: Self-contained breathing apparatus

SDS: Safety Data SheetSTEL: Short-term exposure limit

STOT-RE: Specific target organ toxicity-repeated exposure
 STOT-SE: Specific target organ toxicity-single exposure

TLV: Threshold limit value

TSCA: Toxic Substances Control Act
 TWA: Time-weighted average
 UEL: Upper explosive limit

UVCB: Unknown or Variable Composition/Biological

U.S.: United States

Preparation Date: February 23, 2018

U.S. DOT: United States of Department of Transportation



16.3 Other Hazards

| Hazardous Mate | rials | Identification S | yst | em (HMIS) | | | |
|------------------|-------|------------------|-----|----------------------|---|------------------------|--|
| Degree of hazard | =0) b | low, 4 = extreme |) | | | | |
| Health: | 2* | Flammability: | 0 | Physical Hazards: | 0 | Personal protection:** | |

DISCLAIMER:

This SDS has been prepared in accordance with the Hazard Communication Rule 29 CFR 1910.1200. Information herein is based on data considered to be accurate as of date prepared. No warranty or representation, express or implied, is made as to the accuracy or completeness of this data and safety information. No responsibility can be assumed for any damage or injury resulting from abnormal use, failure to adhere to recommended practices, or from any hazards inherent in the nature of the product.

^{*} Chronic Health Effects

^{**} Appropriate personal protection is defined by the activity to be performed. See Section 8 for additional information.

ATTACHMENT D

Memorandum



Date: 25 October 2021

Subject: 35 Ill. Admin. Code Part 845 - Fault Area Location Demonstration for Ash Pond

No.1 at Coffeen Power Plant

Illinois Power Generating Company operates the coal fired Coffeen Power Plant (Plant) located in Montgomery County, Illinois. The Ash Pond No. 1 is an existing surface impoundment storing coal combustion residuals (CCR). The requirements for the Ash Pond No. 1 are found in 35 Ill. Admin. Code (I.A.C.) 845 (Part 845).

This memorandum addresses the requirements of Section 845.320 Fault Areas, which states:

Section 845.320 Fault Areas

- a) Existing and new CCR surface impoundments, and all lateral expansions of CCR surface impoundments must not be located within 60 meters (200 feet) of the outermost damage zone of a fault that has had displacement in Holocene time unless the owner or operator demonstrates that an alternative setback distance of less than 60 meters (200 feet) will prevent damage to the structural integrity of the CCR surface impoundment.
- b) The owner or operator of the CCR surface impoundment must obtain a certification from a qualified professional engineer stating that the demonstration meets the requirements of subsection (a).

Pursuant to Section 845.210(d)(2), for existing CCR surface impoundments, the owner or operator of the CCR surface impoundment may use a previously completed location restriction demonstration required by Section 845.300 (Placement Above the Uppermost Aquifer), Section 845.310 (Wetlands), Section 845.320 (Fault Areas), Section 845.330 (Seismic Impact Zones), and Section 845.340 (Unstable Areas), provided that the previously completed assessments meet the applicable requirements of those Sections.

The previous fault area demonstration was certified by a qualified professional engineer stating that the demonstration meets the requirements of 40 C.F.R. § 257.62. The requirements described in 40 C.F.R. § 257.62 are nearly identical to the requirements contained in I.A.C. Section 845.320. Pursuant to Section 845.210(d)(2), a certification is not required for this demonstration. The previously completed fault area demonstration is included in Attachment D.



HALEY & ALDRICH, INC. 6500 Rockside Road Suite 200 Cleveland, OH 44131 216.739.0555

MEMORANDUM

16 October 2018 File No. 129788

SUBJECT:

Location Restriction Demonstration - Fault Areas

Coffeen Power Station

Ash Pond No. 1 Coffeen, Illinois

Illinois Power Generating Company operates the coal-fired Coffeen Power Station (Plant) located south of Coffeen, Illinois. The Ash Pond No. 1 (Unit) is an existing coal combustion residuals (CCR) surface impoundment. This demonstration addresses the requirements of 40 CFR §257.62 (Fault Areas) of the U.S. Environmental Protection Agency's (EPA) rule entitled Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities. 80 Fed. Reg. 21,302 (Apr. 17, 2015) (promulgating 40 CFR §257.62); 83 Fed. Reg. 36,435 (July 30, 2018) (amending 40 CFR §257.62).

§257.62(a): New CCR landfills, existing and new CCR surface impoundments, and all lateral expansions of CCR units must not be located within 60 meters (200 feet) of the outermost damage zone of a fault that has had displacement in Holocene time unless the owner or operator demonstrates by the dates specified in paragraph (c) of this section that an alternative setback distance of less than 60 meters (200 feet) will prevent damage to the structural integrity of the CCR unit.

A review of available data from the U.S. Geologic Survey, the Illinois State Geological Survey, and other available information was completed for this demonstration. The nearest known mapped faults are the Crown Fault, which is located approximately 31 miles northwest, and the Centralia Fault zone, located approximately 35 miles southeast of the Unit. The timeframe of the most recent activity on these faults is not known. Based on the available published geologic data and information reviewed, there are no active faults or fault damage zones that have had displacement in Holocene time reported or indicated within 200 feet of the Unit.

Coffeen Power Station – Ash Pond No. 1 Location Restriction – Fault Areas 16 October 2018 Page 2

 $\S257.62(b)$: The owner or operator of the CCR unit must obtain a certification from a qualified professional engineer or approval from the Participating State Director or approval from EPA where EPA is the permitting authority stating that the demonstration meets the requirements of paragraph (a) of this section.

I, Steven F. Putrich, being a Registered Professional Engineer in good standing in the State of Illinois, do hereby certify, to the best of my knowledge, information, and belief, that the information contained in this certification has been prepared in accordance with the accepted practice of engineering. I certify, for the above-referenced CCR Unit, that the demonstration that the CCR Unit is not located within 60 meters (200 feet) of the outermost damage zone of a fault that has had a displacement in Holocene time as included in the CCR Rule Location Restrictions Evaluation memorandum dated 12 October 2018 meets the requirements of 40 CFR §257.62(a).

Signed:

Consulting Engineer

Print Name:

Steven F. Putrich

Illinois License No.:

62048779

Title:

Vice President

Company:

Haley & Aldrich, Inc.

Professional Engineer's Seal:





Memorandum



Date: 25 October 2021

Subject: 35 Ill. Admin. Code Part 845 - Placement Above the Uppermost Aquifer Location

Demonstration for Ash Pond No.1 at Coffeen Power Plant

Illinois Power Generating Company operates the coal fired Coffeen Power Plant (Plant) located in Montgomery County, Illinois. The Ash Pond No. 1 is an existing surface impoundment storing coal combustion residuals (CCR). The requirements for the Ash Pond No. 1 are found in 35 Ill. Admin. Code 845, Standards for the Disposal of Coal Combustion Residuals in Surface Impoundments (Part 845).

This memorandum addresses the requirements of Section 845.300 Placement Above the Uppermost Aquifer, which states:

Section 845.300 Placement Above the Uppermost Aquifer

- a) Existing and new CCR surface impoundments, and all lateral expansions of CCR surface impoundments must, be constructed with a base that is located at least 1.52 meters (five feet) above the upper limit of the uppermost aquifer, or must demonstrate that there will not be an intermittent, recurring, or sustained hydraulic connection between any portion of the base of the CCR surface impoundment and the uppermost aquifer due to normal fluctuations in groundwater elevations (including the seasonal high water table).
- b) The owner or operator of the CCR surface impoundment must obtain a certification from a qualified professional engineer stating that the demonstration meets the requirements of subsection (a).

Pursuant to Section 845.210(d)(2), for existing CCR surface impoundments, the owner or operator of the CCR surface impoundment may use a previously completed location restriction demonstration required by Section 845.300 (Placement Above the Uppermost Aquifer), Section 845.310 (Wetlands), Section 845.320 (Fault Areas), Section 845.330 (Seismic Impact Zones), and Section 845.340 (Unstable Areas), provided that the previously completed assessments meet the applicable requirements of those Sections.

The previous upper aquifer demonstration was certified by a qualified professional engineer stating that the demonstration meets the requirements of 40 C.F.R. § 257.60. The requirements described in 40 C.F.R. § 257.60 are nearly identical to the requirements contained in I.A.C. Section 845.300. Pursuant to Section 845.210(d)(2), a certification is not required for this demonstration. The previously completed upper aquifer demonstration is included in Attachment D.



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MEMORANDUM

16 October 2018 File No. 129788

SUBJECT:

Location Restriction Demonstration – Placement Above Uppermost Aquifer

Ash Pond No. 1

Coffeen Power Station

Coffeen, Illinois

Illinois Power Resources Generating, LLC operates the coal-fired Coffeen Power Station (Plant) located near Coffeen, Illinois. The Ash Pond No. 1 (Unit) is an existing coal combustion residuals (CCR) surface impoundment. This demonstration addresses the requirements of 40 CFR §257.60 (*Placement above the uppermost aquifer*) of the U.S. Environmental Protection Agency's (EPA) rule entitled *Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities*. 80 Fed. Reg. 21,302 (Apr. 17, 2015) (promulgating 40 CFR §257.60); 83 Fed. Reg. 36,435 (July 30, 2018) (amending 40 CFR §257.60).

§257.60(a): New CCR landfills, existing and new CCR surface impoundments, and all lateral expansions of CCR units must be constructed with a base that is located no less than 1.52 meters (five feet) above the upper limit of the uppermost aquifer, or must demonstrate that there will not be an intermittent, recurring, or sustained hydraulic connection between any portion of the base of the CCR unit and the uppermost aquifer due to normal fluctuations in groundwater elevations (including the seasonal high water table). The owner or operator must demonstrate by the dates specified in paragraph (c) of this section that the CCR unit meets the minimum requirements for placement above the uppermost aquifer.

Haley & Aldrich reviewed available information provided by Vistra including historic record drawings, and based on review and evaluation of the information provided, the results do not demonstrate compliance with the requirements of 40 CFR §257.60(a).

Coffeen Power Station - Ash Pond No. 1 Location Restriction - Placement Above Uppermost Aquifer 16 October 2018 Page 2

§257.60(b): The owner or operator of the CCR unit must obtain a certification from a qualified professional engineer or approval from the Participating State Director or approval from EPA where EPA is the permitting authority stating that the demonstration meets the requirements of paragraph (a) of this section.

I, Steven F. Putrich, being a Registered Professional Engineer in good standing in the State of Illinois, do hereby certify, to the best of my knowledge, information, and belief, that the information contained in this certification has been prepared in accordance with the accepted practice of engineering. I certify that the above-referenced CCR Unit does not meet the requirements of 40 CFR §257.60(a).

Signed:

Consulting Engineer

Print Name:

Steven F. Putrich

Illinois License No.:

62048779

Title:

Vice President

Company:

Haley & Aldrich, Inc.

Professional Engineer's Seal:





Memorandum



Date: 25 October 2021

Subject: 35 Ill. Admin. Code Part 845 – Seismic Impact Zone Location Demonstration for Ash

Pond No.1 at Coffeen Power Plant

Illinois Power Generating Company operates the coal fired Coffeen Power Plant (Plant) located in Montgomery County, Illinois. The Ash Pond No. 1 is an existing surface impoundment storing coal combustion residuals (CCR). The requirements for the Ash Pond No. 1 are found in 35 Ill. Admin. Code (I.A.C.) 845 (Part 845).

This memorandum addresses the requirements of Section 845.330 Seismic Impact Zone, which states.

Section 845.330 Seismic Impact Zones

- a) Existing and new CCR surface impoundments, and all lateral expansions of CCR surface impoundments must not be located in seismic impact zones unless the owner or operator demonstrates that all structural components including liners, leachate collection and removal systems, and surface water control systems, are designed to resist the maximum horizontal acceleration in lithified earth material for the site.
- b) The owner or operator of the CCR surface impoundment must obtain a certification from a qualified professional engineer stating that the demonstration meets the requirements of subsection (a).

Pursuant to Section 845.210(d)(2), for existing CCR surface impoundments, the owner or operator of the CCR surface impoundment may use a previously completed location restriction demonstration required by Section 845.300 (Placement Above the Uppermost Aquifer), Section 845.310 (Wetlands), Section 845.320 (Fault Areas), Section 845.330 (Seismic Impact Zones), and Section 845.340 (Unstable Areas), provided that the previously completed assessments meet the applicable requirements of those Sections.

The previous seismic impact zone demonstration was certified by a qualified professional engineer stating that the demonstration meets the requirements of 40 C.F.R. § 257.63. The requirements described in 40 C.F.R. § 257.63 are nearly identical to the requirements contained in I.A.C. Section 845.330. Pursuant to Section 845.210(d)(2), a certification is not required for this demonstration. The previously completed seismic impact zone demonstration is included in Attachment D.



HALEY & ALDRICH, INC. 6500 Rockside Road Suite 200 Cleveland, OH 44131 216.739.0555

MEMORANDUM

16 October 2018 File No. 129788

SUBJECT:

Location Restriction Demonstration - Seismic Impact Zone

Coffeen Power Station

Ash Pond No. 1 Coffeen, Illinois

Illinois Power Generating Company operates the coal-fired Coffeen Power Station (Plant) located south of Coffeen, Illinois. The Ash Pond No. 1 (Unit) is an existing coal combustion residuals (CCR) surface impoundment. This demonstration addresses the requirements of 40 CFR §257.63 (Seismic Impact Zones) of the U.S. Environmental Protection Agency's (EPA) rule entitled Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities. 80 Fed. Reg. 21,302 (Apr. 17, 2015) (promulgating 40 CFR §257.63); 83 Fed. Reg. 36,435 (July 30, 2018) (amending 40 CFR §257.63).

§257.63(a): New CCR landfills, existing and new CCR surface impoundments, and all lateral expansions of CCR units must not be located in seismic impact zones unless the owner or operator demonstrates by the dates specified in paragraph (c) of this section that all structural components including liners, leachate collection and removal systems, and surface water control systems, are designed to resist the maximum horizontal acceleration in lithified earth material for the site.

A Seismic Impact Zone is defined in the CCR Rule (40 CFR §257.63) as "an area having a 2% or greater probability that the maximum expected horizontal acceleration, expressed as a percentage of the earth's gravitational pull (g), will exceed 0.10 g in 50 years". The 2014 US Geological Survey Hazard Map raw data for the Coffeen Power Station Ash Pond No. 1 indicates that the maximum expected horizontal acceleration for 2 percent probability of exceedance in 50 years is 0.21g.

The results of our evaluation indicate that the Unit is in compliance with 40 CFR §257.63(a). Although the Unit is located in a seismic impact zone, it satisfies the demonstration requirements of 40 CFR §257.63(a). The AECOM report entitled "CCR Certification Report: Initial Structural Stability Assessment, Initial Safety Factor Assessment, and Initial Inflow Design Flood Control System Plan for the Ash Pond No. 1 at Coffeen Power Station" dated October 2016 (AECOM Report), includes engineering analysis, calculations, and findings that support the requirements of 40 CFR §257.63(a), and provides documentation that those requirements have been evaluated by AECOM for the subject CCR unit.

Coffeen Power Station – Ash Pond No. 1 Location Restriction – Seismic Impact Zone 16 October 2018 Page 2

 $\S 257.63(b)$: The owner or operator of the CCR unit must obtain a certification from a qualified professional engineer or approval from the Participating State Director or approval from EPA where EPA is the permitting authority stating that the demonstration meets the requirements of paragraph (a) of this section.

I, Steven F. Putrich, being a Registered Professional Engineer in good standing in the State of Illinois, do hereby certify, to the best of my knowledge, information, and belief, that the information contained in this certification has been prepared in accordance with the accepted practice of engineering. I certify, that the CCR Unit is located in a seismic impact zone as included in the CCR Rule Location Restrictions memorandum dated 12 October 2018 and satisfies all requirements of 40 CFR §257.63(a).

By providing this certification demonstration statement, we are not stating or inferring that we have verified or certified the details, assumptions, calculations and/or site condition models developed by AECOM in the subject report; those elements of the report are considered the professional opinions and determinations of AECOM.

Signed:

Consulting Engineer

Print Name:

Illinois License No.:

Title:

Company:

Steven F. Putrich

62048779

Vice President

Haley & Aldrich, Inc.

Professional Engineer's Seal:





Memorandum



Date: 25 October 2021

Subject: 35 Ill. Admin. Code Part 845 – Unstable Areas and Floodplains Location Standard

Demonstration for Ash Pond No. 1 at Coffeen Power Plant

Illinois Power Generating Company (IPGC) is the owner of the coal fired Coffeen Power Plant (Plant) located in Montgomery County, approximately 2 miles south of the city of Coffeen, Illinois. The Ash Pond No. 1 is an existing surface impoundment storing coal combustion residuals (CCR). The requirements for the Ash Pond No. 1 are found in 35 Ill. Admin. Code (I.A.C.) 845, Standards for the Disposal of Coal Combustion Residuals in Surface Impoundments (Part 845).

This certification addresses the requirements of Part 845, Section 845.340 Unstable Areas and Floodplains, which states:

<u>Section 845.340 (a):</u> An existing or new CCR surface impoundment, or any lateral expansion of a CCR surface impoundment must not be located in an unstable area unless the owner or operator demonstrates that recognized and generally accepted engineering practices have been incorporated into the design of the CCR surface impoundment to ensure that the integrity of the structural components of the CCR surface impoundment will not be disrupted.

<u>Section 845.340 (b):</u> The owner or operator must consider all the following factors, at a minimum, when determining whether an area is unstable: 1) On-site or local soil conditions, including but not limited to liquefaction, that may result in significant differential settling; 2) On-site or local geologic or geomorphologic features; and 3) On-site or local human-made features or events (both surface and subsurface).

Pursuant to Section 845.210(d)(2), for existing CCR surface impoundments, the owner or operator of the CCR surface impoundment may use a previously completed location restriction demonstration required by Section 845.300 (Placement Above the Uppermost Aquifer), Section 845.310 (Wetlands), Section 845.320 (Fault Areas), Section 845.330 (Seismic Impact Zones), and Section 845.340 (Unstable Areas), provided that the previously completed assessments meet the applicable requirements of those Sections.

The previous unstable area demonstration was certified by a qualified professional engineer stating that the demonstration meets the requirements of 40 C.F.R. § 257.64. The requirements described in 40 C.F.R. § 257.64 are nearly identical to the requirements contained in I.A.C. Section 845.340 (a). Pursuant to Section 845.210(d)(2), a certification is not required for the unstable area demonstration. The previously completed unstable area demonstration meeting the requirements of Section 845.340 (a) is included in Attachment D.

Memorandum (cont'd)



I.A.C. Part 845 – Unstable Areas and Floodplains Certification for Ash Pond No. 1 at Coffeen Power Plant 25 October 2021 Page 2

<u>Section 845.340 (c):</u> An existing or new CCR surface impoundment, or any lateral expansion of a CCR surface impoundment, must not be located in a floodplain unless the owner or operator demonstrates that recognized and generally accepted engineering practices have been incorporated into the design of the CCR surface impoundment to ensure that the CCR surface impoundment will not restrict the flow of the base flood, reduce the temporary water storage capacity of a floodplain, or result in washout of CCR, so as to pose a hazard to human life, wildlife, or land or water resources.

The boundaries of the impoundment were determined by a survey conducted by a professional surveyor licensed in the State of Illinois. The surveyed boundaries were compared to the existing floodplain boundary from the effective FEMA Flood Hazard Boundary Map (FHBM) Number 170992 0009 A, dated January 9, 1981. The location of the Coffeen Ash Pond No. 1 is outside of the FEMA 100-year floodplain, therefore, it was determined that the Coffeen Ash Pond No. 1 is not located within the floodplain.

<u>Section 845.330 (d):</u> The owner or operator of the CCR surface impoundment must obtain a certification from a qualified professional engineer stating that the demonstration meets the requirements of subsections (a) and (c).

Pursuant to Section 845.210(d)(2), for existing CCR surface impoundments, the owner or operator of the CCR surface impoundment may use a previously completed location restriction demonstration required by Section 845.340 (Unstable Areas) and demonstrated in Attachment D. Therefore, a new certification is not included for Section 845.340 (a). Certification for Section 845.340 (c) is included below.

Memorandum (cont'd)



I.A.C. Part 845 – Unstable Areas and Floodplains Certification for Ash Pond No. 1 at Coffeen Power Plant 25 October 2021 Page 3

35 Illinois Administration Code Part 845: Standards for the Disposal of Coal Combustion Residuals in Surface Impoundments Section 845.340 (c): Certification

I, <u>Sarah Espinosa</u>, being a Professional Engineer in good standing in the State of Illinois, do hereby certify, to the best of my knowledge, information, and belief that this floodplain demonstration meets the requirements of 35 Ill. Adm. Code 845.340(c).

| | Sarah Espinosa, P.E. | |
|--------|----------------------|--|
| Printe | d Name | |
| | | |
| | | |





HALEY & ALDRICH, INC. 6500 Rockside Road Suite 200 Cleveland, OH 44131 216.739.0555

MEMORANDUM

16 October 2018 File No. 129788

SUBJECT:

Location Restriction Demonstration – Unstable Areas

Coffeen Power Station

Ash Pond No. 1 Coffeen, Illinois

Illinois Power Generating Company operates the coal-fired Coffeen Power Station (Plant) located south of Coffeen, Illinois. The Ash Pond No. 1 (Unit) is an existing coal combustion residuals (CCR) surface impoundment. This demonstration addresses the requirements of 40 CFR §257.64 (Unstable Areas) of the U.S. Environmental Protection Agency's (EPA) rule entitled Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities. 80 Fed. Reg. 21,302 (Apr. 17, 2015) (promulgating 40 CFR §257.64); 83 Fed. Reg. 36,435 (July 30, 2018) (amending 40 CFR §257.64).

§257.64(a): An existing or new CCR landfill, existing or new CCR surface impoundment, or any lateral expansion of a CCR unit must not be located in an unstable area unless the owner or operator demonstrates by the dates specified in paragraph (d) of this section that recognized and generally accepted good engineering practices have been incorporated into the design of the CCR unit to ensure that the integrity of the structural components of the CCR unit will not be disrupted.

§257.64(b): The owner or operator must consider all of the following factors, at a minimum, when determining whether an area is unstable:

- (1) On-site or local soil conditions that may result in significant differential settling;
- (2) On-site or local geologic or geomorphologic features; and
- (3) On-site or local human-made features or events (both surface and subsurface).

Determination of compliance with §257.64(b)(1) - Conditions associated with the potential for significant differential settlement due to liquefaction were not identified in the area where the Plant is located. A separate report completed by AECOM entitled "CCR Certification Report: Initial Structural Stability Assessment, Initial Safety Factor Assessment, and Initial Inflow Design Flood Control System Plan for the Ash Pond No. 1 at Coffeen Power Station" dated October 2016 concluded that the coarse-grained soils beneath the Unit are not susceptible to liquefaction and soft clays beneath the Unit were susceptible to cyclic softening (strength loss). The post-earthquake stability analysis performed by AECOM to model the stability of the impoundment slopes following an earthquake and soil strength loss produced acceptable factors of safety.

Determination of compliance with §257.64(b)(2) - Based on available United States Geological Survey (USGS) and Illinois State Geological Survey (ISGS) information, karst topography or physiographic features such as sinkholes, vertical shafts, sinking streams, caves, large springs, or blind valleys do not

Coffeen Power Station – Ash Pond No. 1 Location Restriction – Unstable Areas 16 October 2018 Page 2

exist at the Plant. To evaluate the susceptibility of landslides, we reviewed readily available USGS and ISGS data. The USGS data indicates that the Plant is in an area of low landslide incidence and the closest document landslide is more than 10 miles from the site. Accordingly, it is our opinion that the Unit is not located in an area that has high susceptibility to landslides.

Determination of compliance with $\S257.64(b)(3)$ - An abandoned underground coal mine is located below the Unit, however an evaluation by AECOM (2016) concluded that the presence of this underground mine does not negatively affect the stability of the Unit.

§257.64(c): The owner or operator of the CCR unit must obtain a certification from a qualified professional engineer or approval from the Participating State Director or approval from EPA where EPA is the permitting authority stating that the demonstration meets the requirements of paragraph (a) of this section.

I, Steven F. Putrich, being a Registered Professional Engineer in good standing in the State of Illinois, do hereby certify, to the best of my knowledge, information, and belief, that the information contained in this certification has been prepared in accordance with the accepted practice of engineering. I certify, for the above-referenced CCR Unit, that the demonstration indicating the CCR Unit is not located in an unstable area as included in the CCR Rule Location Restrictions Evaluation memorandum dated 12 October 2018 meets the requirements of 40 CFR §257.64(a).

Signed:

Consulting Engineer

Print Name:

Steven F. Putrich

Illinois License No.:

62048779

Title:

Vice President

Company:

Haley & Aldrich, Inc.

Professional Engineer's Seal:





Memorandum



Date: 25 October 2021

Subject: 35 Ill. Admin. Code Part 845 - Wetland Location Demonstration for Ash Pond No.1

at Coffeen Power Plant

Illinois Power Generating Company (IPGC) is the owner of the coal fired Coffeen Power Plant (Plant) located in Montgomery County, approximately 2 miles south of the city of Coffeen, Illinois. The Ash Pond No. 1 is an existing surface impoundment storing coal combustion residuals (CCR). The requirements for the Ash Pond No. 1 are found in 35 Ill. Admin. Code (I.A.C.) 845 (Part 845).

This memorandum addresses the requirements of Section 845.310 Wetlands, which states:

Section 845.310 Wetlands

- a) Existing and new CCR surface impoundments, and all lateral expansions of CCR surface impoundments must not be located in wetlands unless the owner or operator demonstrates [that the requirements listed in 845.310(a)(1) through (5) are met.]
- b) The owner or operator of the CCR surface impoundment must obtain a certification from a qualified professional engineer stating that the demonstration meets the requirements of subsection (a).

Pursuant to Section 845.210(d)(2), for existing CCR surface impoundments, the owner or operator of the CCR surface impoundment may use a previously completed location restriction demonstration required by Section 845.300 (Placement Above the Uppermost Aquifer), Section 845.310 (Wetlands), Section 845.320 (Fault Areas), Section 845.330 (Seismic Impact Zones), and Section 845.340 (Unstable Areas), provided that the previously completed assessments meet the applicable requirements of those Sections.

The previous wetlands demonstration was certified by a qualified professional engineer stating that the demonstration meets the requirements of 40 C.F.R. § 257.61. The requirements described in 40 C.F.R. § 257.61 are nearly identical to the requirements contained in I.A.C. Section 845.310. Pursuant to Section 845.210(d)(2), a certification is not required for this demonstration. The previously completed wetlands demonstration is included in Attachment D.



HALEY & ALDRICH, INC. 6500 Rockside Road Suite 200 Cleveland, OH 44131 216.739.0555

MEMORANDUM

16 October 2018 File No. 129788

SUBJECT:

Location Restriction Demonstration - Wetland Areas

Coffeen Power Station

Ash Pond No. 1 Coffeen, Illinois

Illinois Power Generating Company operates the coal-fired Coffeen Power Station (Plant) located south of Coffeen, Illinois. Ash Pond No. 1 (Unit) is an existing coal combustion residuals (CCR) surface impoundment. This demonstration addresses the requirements of 40 CFR §257.61 (Wetlands) of the U.S. Environmental Protection Agency's (EPA) rule entitled Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities. 80 Fed. Reg. 21,302 (Apr. 17, 2015) (promulgating 40 CFR §257.61); 83 Fed. Reg. 36,435 (July 30, 2018) (amending 40 CFR §257.61.

§257.61(a): New CCR landfills, existing and new CCR surface impoundments, and all lateral expansions of CCR units must not be located in wetlands, as defined in §232.2 of this chapter, unless the owner or operator demonstrates by the dates specified in paragraph (c) of this section that the CCR unit meets the requirements of paragraphs (a)(1) through (5) of this section.

Based on a review of the U.S. Fish and Wildlife Service's National Wetland Inventory mapping, 0.5-meter resolution aerial imagery (2015) and the results of on-site field assessments, the Unit is not located in wetlands as defined by 40 CFR §232.2.

Coffeen Power Station – Ash Pond No. 1 Location Restriction – Wetland Areas 16 October 2018 Page 2

§257.61(b): The owner or operator of the CCR unit must obtain a certification from a qualified professional engineer or approval from the Participating State Director or approval from EPA where EPA is the permitting authority stating that the demonstration meets the requirements of paragraph (a) of this section.

I, Steven F. Putrich, being a Registered Professional Engineer in good standing in the State of Illinois, do hereby certify, to the best of my knowledge, information, and belief, that the information contained in this certification has been prepared in accordance with the accepted practice of engineering. I certify, for the above-referenced CCR Unit, that the CCR Unit is not located in wetlands as included in the CCR Rule Location Restrictions Evaluation memorandum dated 12 October 2018 and, therefore, meets the requirements of 40 CFR §257.61(a).

Signed:

Consulting Engineer

Print Name:

Steven F. Putrich

Illinois License No.:

62048779

Title:

Vice President

Company:

Haley & Aldrich, Inc.

Professional Engineer's Seal





ATTACHMENT E



ATTACHMENT F

Illinois Power Generating Company

COFFEEN POWER PLANT MONTGOMERY COUNTY, ILLINOIS

Emergency Action Plan (EAP)

40 CFR § 257.73(a)(3), 35 Ill. Adm. Code 845.520 Coal Combustion Residual (CCR) Impoundments & Related Facilities

- Gypsum Management Facility (GMF) Pond (NID # IL50579) (IEPA # W1350150004-03)
- GMF Recycle Pond (NID # IL50578) (IEPA # W1350150004-04)
- Ash Pond No. 1 (NID # IL50722) (IEPA # W1350150004-01)
- Ash Pond No. 2 (NID # IL50723) (IEPA # W1350150004-02)

Revision Date: September 16, 2021

Qualified Professional Engineer Certification; Emergency Action Plan for the Coffeen Power Plant GMF Pond, GMF Recycle Pond, Ash Pond 1 and Ash Pond 2

In accordance with 40 C.F.R. § 257.73(a)(3)(iv) and 35 III. Adm. Code 845.520(e), the owner or operator of a CCR unit that is required to prepare a written Emergency Action Plan under 40 C.F.R. § 257.73(a)(3) and 35 III. Adm. Code 845.520(a) must obtain a certification from a qualified professional engineer stating that the written Emergency Action Plan meets the requirements of 40 C.F.R. § 257.73(a) (3) and 35 III. Adm. Code 845.520.

- I, ____Phil Morris_, being a Professional Engineer in good standing in the State of Illinois, do hereby certify, to the best of my knowledge, information, and belief that:
 - 1. the information contained in this Emergency Action Plan was prepared in accordance with the accepted practice of engineering; and
 - this Emergency Action Plan meets the requirements of 40 C.F.R. § 257.73(a)(3) and 35 Ill. Adm. Code 845.520.

Phil Morris

9/27/21

Senior Director, Corporate Environmental

Date

062-058768
REGISTERED
PROFESSIONAL
ENGINEER
9/OF
LINO19

COFFEEN POWER PLANT EMERGENCY ACTION PLAN CCR IMPOUNDMENTS & RELATED FACILITIES

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COFFEEN POWER PLANT EMERGENCY ACTION PLAN CCR IMPOUNDMENTS & RELATED FACILITIES

1 STATEMENT OF PURPOSE

The Coffeen Power Plant (Power Plant) is located near the town of Coffeen in Montgomery County, Illinois. The location of the Power Plant is shown in Figure 1-1. The Power Plant is a coal-fired electricity producing power plant owned and operated by the Illinois Power Generating Company (IPGC), a subsidiary of Dynegy. This Emergency Action Plan (EAP) was prepared in accordance with 40 CFR § 257.73(a)(3) and 35 Ill. Adm. Code 845.520 and covers the following Coal Combustion Residual (CCR) surface impoundments located at the site:

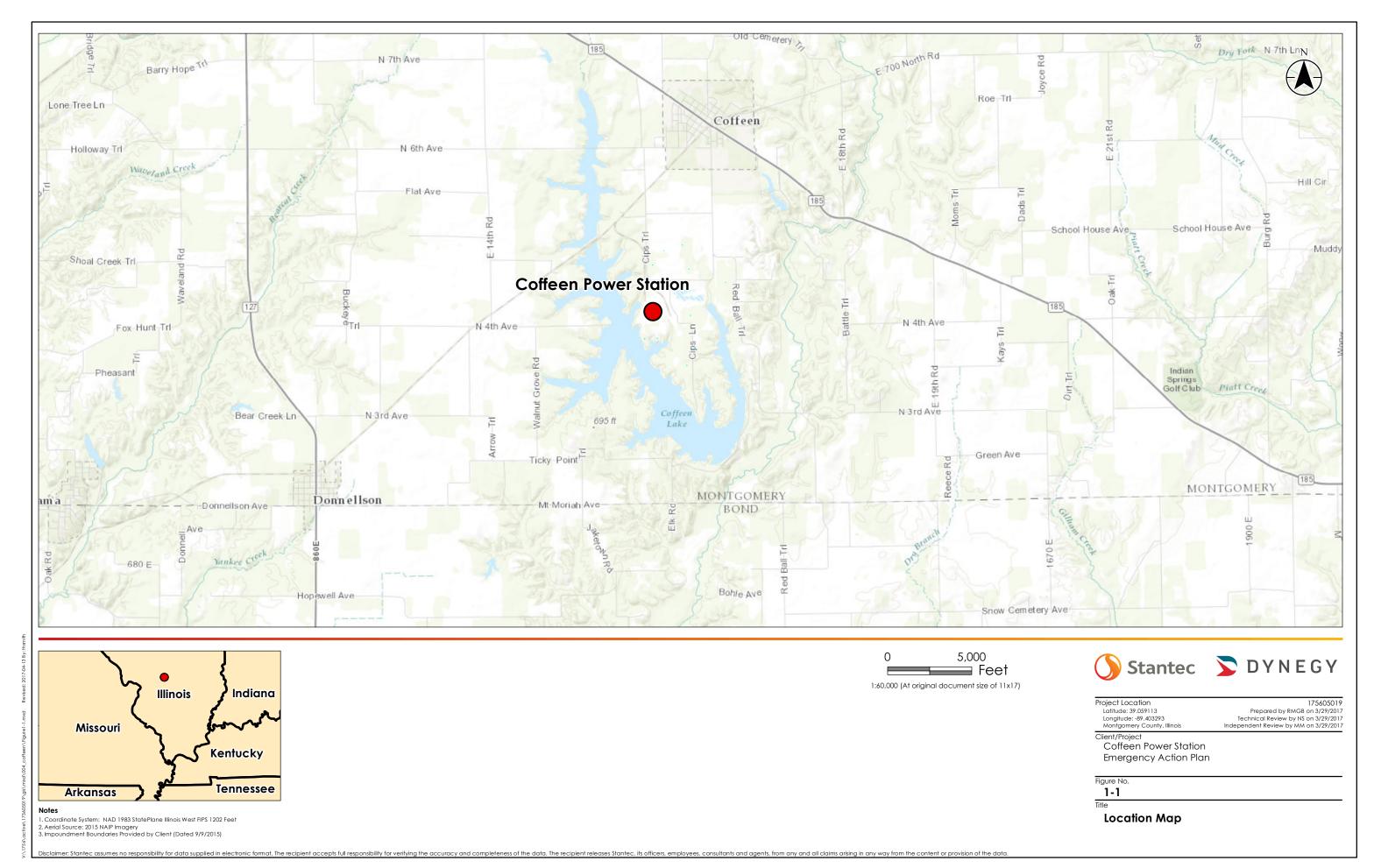
- Gypsum Management Facility (GMF) Pond (NID # IL50579) (IEPA # W1350150004-03)
- GMF Recycle Pond (NID # IL50578) (IEPA # W1350150004-04)
- Ash Pond No. 1 (NID # IL50722) (IEPA # W1350150004-01)
- Ash Pond No. 2 (Capped/Closed) (NID # IL50723) (IEPA # W1350150004-02)

The locations of these impoundments are shown in Figure 1-2. Section 6 of this EAP includes a description of each impoundment.

The purpose of this Emergency Action Plan (EAP) is to:

- Safeguard the lives, as well as to reduce property damage, of citizens living within potential downstream flood inundation areas of CCR impoundments and related facilities at the Coffeen Power Plant.
- Define the events or circumstances involving the CCR impoundments and related facilities at the Coffeen Power Plant that pose a safety hazard or emergency and how to identify those conditions.
- 3. Define responsible persons, their responsibilities, and notification procedures in the event of a safety emergency.
- 4. Provide list of emergency responders.
- 5. Identify emergency actions in the event of a potential or imminent failure of the impoundments.
- 6. Identify the downstream area that would be affected by failure of the impoundments.
- Provide for effective facility surveillance, prompt notification to local Emergency
 Management Agencies, citizen warning and notification responses, and preparation should an
 emergency occur.

Information provided by Illinois Power Generating Company was utilized and relied upon in preparation of this Emergency Action Plan.

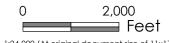






Legend

CCR Surface Impoundment Boundary



1:24,000 (At original document size of 11x17)





Project Location Latitude: 39.059113 Longitude: -89.403293 Montgomery County, Illinois

175605019 Prepared by RMGB on 3/29/2017 Technical Review by NS on 3/29/2017 Independent Review by MM on 3/29/2017

Client/Project
Coffeen Power Station Emergency Action Plan

Figure No.

1-2

CCR Impoundments

Coordinate System: NAD 1983 StatePlane Illinois West FIPS 1202 Feet
 Aerial Source: 2015 NAIP Imagery
 Impoundment Boundaries Provided by Client (Dated 9/9/2015)

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2 COMMUNICATION

To facilitate understanding among everyone involved in implementing this EAP, four response levels are used to identify the condition of an impoundment. These are:

Response Levels:

- <u>Level 0</u>: Normal conditions and routine operations, including surveillance and initial investigation of unusual conditions and effects of storm events.
- <u>Level 1</u>: Potentially hazardous condition exists, requiring investigation and possible corrective action.
- <u>Level 2</u>: Potential failure situation is developing; possible mode of failure is being assessed; corrective measures are underway.
- <u>Level 3</u>: Failure is occurring or is imminent, public protective actions are required.

The 4-Step Incident Response Process is outlined in Figure 2-1. This should be used in conjunction with the Notification Flowchart (Figure 2-2) and EAP Decision Tree (Figure 2-3). Section 4 provides guidance tables for determining Response Levels and a table providing emergency actions to be taken given various situations. Table 2-1 lists contact information for the emergency responders.

Figure 2-1. Summary/Sequence of Tasks 4-Step Incident Response Process

Step 1: Detection, Evaluation, and Response Level Determination

Sequence of Tasks:

- Notify EAP Coordinator, Plant Manager, and Dam Safety Manager of unusual condition detected and confer on next steps needed.
- Conduct technical evaluation of conditions as needed.
- Determine Response Level based on evaluation. (Table 4-1)
- Reset Response Level as revised evaluations warrant.

Step 2: Notification

Sequence of Tasks:

- Notify authorities, designated personnel, and external response partners of change in Response Level, using the Notification Flowchart. (Figure 2-2)
- Re-notify authorities, designated personnel, and external response partners as Response Level is changed.

Step 3: Emergency Actions

Sequence of Tasks:

- Perform emergency actions with goal of saving the impoundment and minimizing impacts to life, property, and environment. (Table 4-3)
- Take continuous actions to include situation assessment, information sharing, remediation, and public safety advisories or warnings, as warranted.
- Revise action plan as changes in conditions warrant.

Step 4: Follow-up

Sequence of Tasks:

- Document conditions and decisions in the Emergency Incident Log.
- Notify authorities, designated personnel, and external response partners that condition is stabilized, limit incident termination declarations to conditions at the site.
- Conduct and document after-action review of incident and response.

Figure 2-2. Notification Flowchart Initial Detector
(Internal) **Initial Detector** (External) 911 Asset Closure Manager **EAP Coordinator** (Environmental Manager) **Determine Response Level Response Level** Dam Safety Manager Level 0 Level 1 Montgomery County ESDA / EMA Coordinator Office: (217) 532-9564 Level 2 Home: (217) 532-6437 Cell: (217) 254-6437 Level 3 **IPGC** Corporate **Affected Parties Local / County Police, Fire & Rescue** Montgomery County 911 Center Director: Greg Nimmo **Onsite Personnel** (217) 532-9564 (OR 911) Montgomery County Sheriff: Jim Vazzi (217) 532-9511 Coffeen Police Department (217) 534-2216 Coffeen Fire Department (217) 534-2410

Coffeen Power Plant, Montgomery County, Illinois

Figure 2-3. EAP Response Process Decision Tree

Note: At any given below, if failure is imminent or actively occurring CALL 911 IMMEDIATELY to notify emergency responders and then continue with process afterwards.

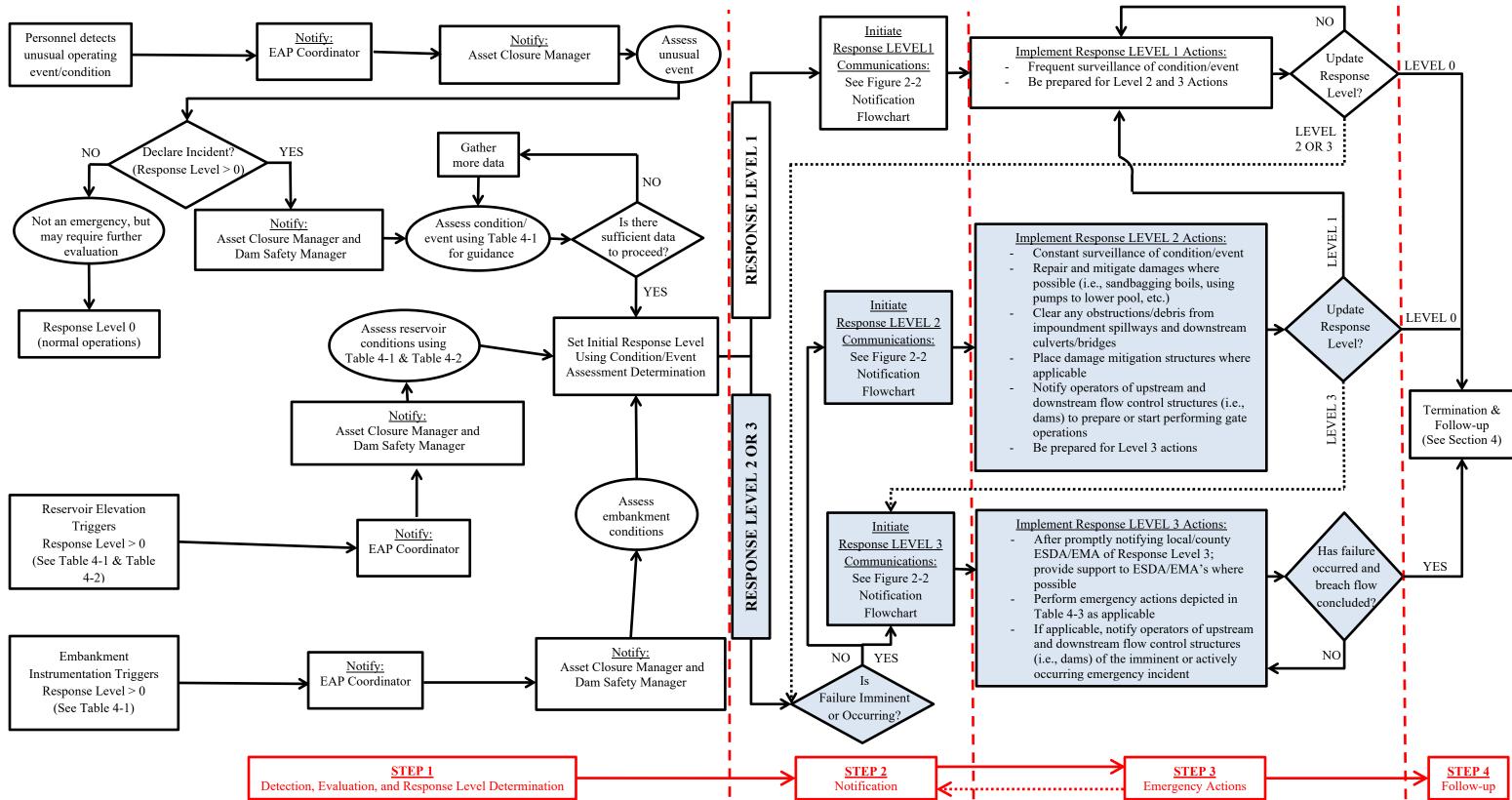


Table 2-1. EAP Emergency Responders

| Position / Entity | Contact Ir | ıformation | | | | |
|---|------------------------------|----------------------|--|--|--|--|
| | Internal Contacts | | | | | |
| Coffeen Power Plant | Pho | ne # | | | | |
| Asset Closure Manager | (903) 5 | 77-5207 | | | | |
| Environmental Manager (EAP Coordinator) | (217) 34 | 41-7319 | | | | |
| Control Room | (217) 53 | 34-7621 | | | | |
| IPGC Corporate Operations | Con | tact | | | | |
| Dam Safety Manager | | (618) 792-8488 | | | | |
| Extern | al Contacts | | | | | |
| Local/County ESDA/EMA, Police, & Fire | Phone # | Alternate Phone # | | | | |
| Montgomery County 911 Emergency Communication Center | 911 | (217) 532-9564 | | | | |
| Montgomery County Sheriff | (217) 532-9511 | | | | | |
| Montgomery County ESDA/EMA Coordinator | (217) 532-9564 | (217) 254-6437 | | | | |
| Coffeen Police Department | (217) 534-2216 | | | | | |
| Coffeen Fire Department | (217) 534-2410 | | | | | |
| Montgomery County Ambulance | (217) 532-9562 | | | | | |
| Montgomery County Engineer | (217) 532-6109 | | | | | |
| State Emergency Management Agencies & Organizations | | | | | | |
| IDNR-OWR Dam Safety Section Manager | (217) 782-4427 | | | | | |
| Coffeen Lake State Fish & Wildlife Area | 7ildlife Area (217) 537-3351 | | | | | |
| Illinois Conservation Police | (309) 338-1017 | | | | | |
| Illinois State Police | (309) 83 | 33-4046 | | | | |

3 EAP ROLES AND RESPONSIBILITIES

Table 3-1 provides a summary of the EAP roles during an emergency event.

Table 3-1. Summary of EAP Roles

| Entity | Role Description |
|--|---|
| IPGC Emergency Response Team (ERT) | ERT: IPGC personnel responsible for EAP implementation, distribution, updates/maintenance, and training activities. The ERT is comprised of the following roles: IPGC Corporate: IPGC corporate entity, committee, team, or position with relevant responsibility for a given generating power plant. Asset Closure Management: Personnel responsible for the management of the closure of the Power Plant. Dam Safety Manager: Personnel that is most knowledgeable about the design and technical operation of facilities at a given power plant. EAP Coordinator: Personnel responsible for implementing the EAP and associated activities. |
| Montgomery County ESDA/EMA | Receive Response Level reports from <u>IPGC Corporate</u> through <u>EAP Coordinator</u>. Coordinate emergency response activities with local/county authorities: police, fire and rescue, etc. Coordinate notification of public as necessary through established channels, which may include doorto-door contact. Coordinate notification activities to affected parties within inundation areas. Evaluate risk to areas beyond the inundation areas, communicate needs to the <u>IPGC Corporate</u> and/or <u>EAP Coordinator</u>, and coordinate aid as appropriate. Responsible for declaring termination of an emergency condition off-site upon receiving notification of an emergency status termination from the <u>IPGC Corporate</u>. If necessary, coordinate with <u>State ESDA/EMA</u>. |
| Local/County Police, Fire & Rescue | Receive alert status reports from the <u>ERT</u> or the Montgomery County <u>ESDA/EMA</u>. If necessary, notify affected parties and general public within inundation areas (see Section 7). Render assistance to Montgomery County <u>ESDA/EMA</u>, as necessary. Render assistance to <u>IPGC Corporate</u> and <u>Power Plant Management</u>, as necessary. |

4 EAP RESPONSE

The 4-Step Incident Response Process is shown in Figure 2-1. The Decision Tree shown in Figure 2-3 provides a flowchart for the various elements of the response process. Upon reaching Step 4 of the response process (termination and follow-up), the EAP Coordinator is responsible for notifying the ESDA/EMA's that the condition of the dam/impoundment has been stabilized. The purpose of this section is to provide specific information that can be used during a response. This information is provided in the following tables:

- Table 4-1 provides guidance for determining the response level.
- Table 4-2 provides impoundment pool level trigger elevations.
- Table 4-3 lists emergency actions to be taken depending on the situation.

Table 4-1. Guidance for Determining the Response Level

| Table 4-1. Guidance for Determining the Response Level | | | | | |
|---|--|----------------|--|--|--|
| Event | Situation | Response Level | | | |
| | Primary spillway flow is not causing active erosion and impoundment water surface elevation is below auxiliary spillway crest elevation (if equipped). | Level 0 | | | |
| | Impoundment water surface elevation is at or above auxiliary spillway crest elevation (if equipped). No active erosion caused by spillway flow. | Level 1 | | | |
| | Spillway flow actively causing minor erosion that is not threatening the control section or dam/impoundment stability. | Level 2 | | | |
| Spillway flow (See Table 4-2 for relevant elevations) | Spillway flow that could result in flooding of people downstream if the reservoir level continues to rise. | Level 2 | | | |
| relevant elevations) | Abnormal operation of the spillway system due to blockage or damage that could lead to flooding. | Level 2 | | | |
| | Spillway flow actively eroding the soil around the spillway that is threatening the control section (e.g., undermining) or dam/impoundment stability. | Level 3 | | | |
| | Spillway flow that is flooding people downstream. | Level 3 | | | |
| Embankment | Impoundment water surface elevation at or below typical normal pool fluctuation elevation. | Level 0 | | | |
| Overtopping | Impoundment water surface elevation above typical high pool fluctuation elevation. | Level 1 | | | |
| (See Table 4-2 for relevant elevations) | Impoundment water surface elevation within 2 feet of the embankment crest elevation | Level 2 | | | |
| | Impoundment water surface elevation at or above embankment crest elevation. | Level 3 | | | |
| | New seepage areas in or near the dam/impoundment with clear flow. | Level 1 | | | |
| Seepage | New seepage areas with cloudy discharge or increasing flow rate. | Level 2 | | | |
| | Heavy seepage with active erosion, muddy flow, and/or sand boils. | Level 3 | | | |
| G: 11 1 | Observation of new sinkhole in impoundment area or on embankment. | Level 2 | | | |
| Sinkholes | Rapidly enlarging sinkhole and/or whirlpool in the impoundment. | Level 3 | | | |
| | New cracks in the embankment greater than ¼ inch wide without seepage. | Level 1 | | | |
| Embankment cracking | Any crack in the embankment with seepage. | Level 2 | | | |
| oracking . | Enlarging cracks with muddy seepage. | Level 3 | | | |

Table 4-1. Guidance for Determining the Response Level

| Event | Situation | Response Level |
|--------------------------------------|--|----------------|
| | Visual signs of movement/slippage of the embankment slope. | Level 1 |
| Embankment movement | Detectable active movement/slippage of the embankment slope or other related effects (tension cracking, bulges/heaves, etc.) that could threaten the integrity of the embankment. | Level 2 |
| | Sudden or rapidly proceeding slides of the embankment slopes. | Level 3 |
| Embankment Monitoring Equipment | Instrumentation readings beyond historic normal. | Level 1 |
| (piezometers, inclinometers, surface | Instrumentation readings indicate the embankment is susceptible to failure. | Level 2 |
| displacement mounts, etc.) | Instrumentation readings indicate embankment is at threshold of failure or is currently failing. | Level 3 |
| | Measurable earthquake felt or reported on or within 100 miles of the impoundment. | Level 1 |
| Earthquake or another event | Earthquake or other event resulting in visible damage to the impoundment or appurtenances. | Level 2 |
| another event | Earthquake or other event resulting in uncontrolled release of water or materials from the impoundment. | Level 3 |
| Security | Verified bomb threat or other physical threat that, if carried out, could result in damage to the impoundment. | Level 2 |
| threat | Detonated bomb or other physical damage that has resulted in damage to the impoundment or appurtenances. | Level 3 |
| | Damage to impoundment or appurtenance with no impact to the functioning of the impoundment. | Level 1 |
| Sabotage/ vandalism | Modification to the impoundment or appurtenances that could adversely impact the functioning of the impoundment. This would include unauthorized operation of spillway facilities. | Level 2 |
| | Damage to impoundment or appurtenances that has resulted in seepage flow. | Level 2 |
| | Damage to impoundment or appurtenances that has resulted in uncontrolled water release. | Level 3 |

Table 4-2. Impoundment Trigger Elevations

| Impoundment | Embankment | Auxiliary Spillway | Normal Pool Fluctuation | |
|------------------|-----------------|--------------------|-------------------------|---------|
| Impoundment | Crest Elevation | Crest Elevation | Typical | High |
| GMF Pond | 632.0 ft. | N/A | 621 ft. | 626 ft. |
| GMF Recycle Pond | 629.0 ft. | 624.1 ft. | 610 ft. | 623 ft. |
| Ash Pond No.1 | 637.5 ft. | 631.0 ft. | 629 ft. | 633 ft. |
| Ash Pond No.2 | 638.0 ft. | N/A | N/A | N/A |

Notes: Elevations are in reference to NAVD88

Table 4-3. Step 3: Emergency Actions

| Condition | Description of Condition | Action to be Taken |
|---|---|---|
| High Water Level/ Large Spillway Release | Not applicable to capped impoundments. See Table 4-1 and Table 4-2 for elevations and triggering water levels associated with the impoundments and spillways covered by this EAP. | Assess cause of increased reservoir stage, especially during fair weather conditions. Determine Response Level. Make proper notifications as outlined in the Figure 2-2 Notification Flowchart. Perform additional tasks as determined through consultation with the ERT. Make notifications if condition worsens such that downstream flooding is imminent. Response Level 0: require enhanced surveillance 3 times per day Response Level 1: contact internal chain of command and external response partners as necessary; inspect impoundment minimum 1 time per hour Response Level 2: contact internal chain of command; notify ESDA/EMA's and notify external response partners. ESDA/EMA's notify affected parties. Response Level 3: contact internal chain of command; notify ESDA/EMA's and notify external response partners. ESDA/EMA's notify affected parties of emergency incident. |
| Seepage | Localized new seepage or boil(s) observed along downstream face / toe of earthen embankment with muddy discharge and increasing but controllable discharge of water. | Measure and record feature dimensions, approximate flow rate, and relative location to existing surface features. Take photos. Document location on a site plan and in inspection notes. Determine Response Level. Make proper notifications as outlined in the Figure 2-2 Notification Flowchart. ERT (with Dam Safety Manager as lead) to determine mitigation actions. The following actions may apply: a) Place a ring of sandbags with a weir at the top towards the natural drainage path to monitor flow rate. If boil becomes too large to sandbag, place a blanket filter over the area using non-woven filter fabric and pea gravel. Attempt to contain flow in such a manner (without performing any excavations) that flow rates can be measured. Stockpile gravel and sand fill for later use, if necessary. b) Inspect the embankment and collect piezometer, water level and seepage flow data daily unless otherwise instructed by the Dam Safety Manager. Record any changes of conditions. Carefully observe embankment for signs of depressions, seepage, sinkholes, cracking or movement. c) Maintain continuous monitoring of feature. Record measured flow rate and any changes of condition, including presence or absence of muddy discharge. Make notifications as outlined in the lower portion of the Notification Flowchart (Figure 2-2) if condition worsens such that failure is imminent. |

Table 4-3. Step 3: Emergency Actions

| Condition | Description of Condition | Action to be Taken |
|---|---|--|
| Sabotage and Miscellaneous Other Issues | Criminal action with significant damage to embankment or structures where significant repairs are required and the integrity of the facility is compromised—condition appears stable with time. | Contact law enforcement authorities and restrict all access (except emergency responders) to impoundment. Restrict traffic on embankment crest to essential emergency operations only. Determine Response Level. Make internal notifications as outlined in the upper portion of the Notification Flowchart (Figure 2-2). In conjunction with the Dam Safety Manager, assess extent of damage and visually inspect entire embankment and ancillary structures for additional less obvious damage. Based on inspection results, confirm if extent of damage to various components of the impoundment warrants a revised Response Level and additional notifications. Perform additional tasks as directed by the ERT. Make notifications if conditions worsen. |
| Embankment Deformation | Cracks: New longitudinal (along the embankment) or transverse (across the embankment) cracks more than 6 inches deep or more than 3 inches wide or increasing with time. New concave cracks on or near the embankment crest associated with slope movement. | Measure and record feature dimensions, approximate flow rate, and relative location to existing surface features. Take photos. Document location on a site plan and in inspection notes. Restrict traffic on embankment crest to essential emergency operations only. Determine Response Level. Make notifications as outlined in the Figure 2-2 Notification Flowchart. ERT (with Dam Safety Manager as lead) to determine mitigation actions. The following actions may apply: Place buttress fill against base of slope immediately below surface feature. Stockpile additional fill. Place sandbags as necessary around crack area to divert any storm water runoff from flowing into crack(s). As directed by the Dam Safety Manager, additional inspection and monitoring of the dam may be required. Items may include: inspect the dam on a schedule determined by the Dam Safety Manager; collect piezometer and water level data; and record any changes of condition. Carefully observe dam for signs of depressions, seepage, sinkholes, cracking or movement. Make notifications as outlined in the Figure 2-2 Notification Flowchart if conditions worsen such that failure is imminent. |
| | Slides / Erosion: Deep slide / erosion (greater than 2 feet deep) on the embankment that may also extend beyond the embankment toe but does not encroach onto the embankment crest and appears stable with time. | Measure and record feature dimensions, approximate flow rate, and relative location to existing surface features. Take photos. Document location on a site plan and in inspection report. Restrict traffic on embankment crest to essential emergency operations only. Determine the Response Level. Make notifications as outlined in the Figure 2-2 Notification Flowchart. ERT (with Dam Safety Manager as lead) to determine mitigation actions. Additional actions may include the following items. a) Place sandbags as necessary around slide area to divert any storm water runoff from flowing into slide(s). b) Increase inspections of the dam; collect piezometer and water level data; and record any changes of condition. During inspections, carefully observe dam for signs of depressions, seepage, sinkholes, cracking or movement. Make notifications as outlined in the Figure 2-2 Notification Flowchart if conditions worsen such that failure is imminent. |

Table 4-3. Step 3: Emergency Actions

| Condition | Description of Condition | Action to be Taken |
|--------------------------------|---|---|
| Embankment Deformation (cont.) | Sinkholes: Small depression observed on the embankment or within 50 feet of the embankment toe that is less than 5 feet deep and 30 feet wide or which is increasing with time. | Slowly open drain gates to lower pool elevation. Measure and record feature dimensions, approximate flow rate, and relative location to existing surface features. Take photos. Document location on a site plan and in inspection notes. Restrict traffic on embankment crest to essential emergency operations only. Determine Response Level. Make notifications as outlined in the Figure 2-2 Notification Flowchart. ERT (with Dam Safety Manager as lead) to determine mitigation actions. Additional actions may include the following items: a) Backfill the depression with relatively clean earth fill (free of organic materials) generally even with surrounding grade and slightly mounded (6 to 12 inches higher) in the center in order to shed storm water away from the depression. Stockpile additional fill. b) Increase inspections of the dam; collect piezometer and water level data daily unless otherwise instructed by Dam Safety Manager; and record any changes of condition. Carefully observe dam for signs of depressions, seepage, sinkholes, cracking or movement. Make notifications as outlined in the Figure 2-2 Notification Flowchart if conditions worsen such that failure is imminent. |
| Gate Malfunction or Failure | Sluice gate damaged structurally (sabotage, debris, etc.) with uncontrolled release of water at a constant volume. Condition appears stable. | Close any other gates, if open. Determine Response Level. Make notifications as outlined in the Figure 2-2 Notification Flowchart. Obtain instructions from the Dam Safety Manager to determine if there are other methods to stop or slow down the flow of water. If conditions worsen such that failure is imminent, make notifications as outlined in the lower portion of the Figure 2-2 Notification Flowchart. |

5 PREPAREDNESS

The intent of this section is to provide information that will be utilized during a response. Established emergency supplies and locations, suppliers, and equipment are provided in Table 5-1. Supplier contact information is listed in Table 5-2.

A coordination meeting shall be conducted annually between representatives of the Illinois Power Generating Company and local emergency responders. This meeting may be in the form of a face-to-face meeting, tabletop exercise, or additional training regarding the EAP.

Table 5-1. Emergency Supplies and Equipment

| Flashlights Yes Contact EAP Coordinator for location(s). Generator Yes Contact EAP Coordinator for location(s). Contact Grand Rental Station for additional generators (see Table 5-2). Extension Cords Yes Contact EAP Coordinator for location(s). Fire extinguishers Yes Contact EAP Coordinator for location(s). Floodlights Yes Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Backhoe Yes Backhoe/tractor and 650 John Deere Track hoe available. Contact EAP Coordinator for location(s). Dozer Yes D7 & D10 Crawler Tractors and two rubber-tired dozers (844B & 834B). Contact EAP Coordinator for location(s). Large Equipment Rental (excavating equipment, large earth moving, etc.) Pump and Hoses Yes Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Contact United Rental (excavating equipment, large earth moving, etc.) Pump and Hoses Yes Contact EAP Coordinator for location(s). Contact The Curry Companies or Rain for Rent for high-capacity portable pumps (see Table 5-2). Sandbags Yes Contact EAP Coordinator for location(s). Contact The Curry Companies or Rain for Rent for high-capacity portable pumps (see Table 5-2). Contact EAP Coordinator for location(s). Contact Great Western Bag Co. for additional sandbags (see Table 5-2). Contact EAP Coordinator for location(s). Contact Great Western Bag Co. for additional sandbags (see Table 5-2). Contact EAP Coordinator for location(s). Contact Isted suppliers in Table 5-20 for gavel, sand, and riprap fill as necessary. Contact EAP Coordinator for location(s). Contact Vandalia Ready Mix and/or Greenville Ready Mix for additional concrete (see Table 5-2). Geotextile Filter Fabric Yes Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Should be maintained in close proximity to any features that might require immediate access. Personal Flotation Devices Yes Contact EAP Coordinator for location(s). | Item | On-site (Yes/No/Occasionally) | Remarks |
|--|---|----------------------------------|--|
| Extension Cords Yes Contact EAP Coordinator for location(s). Fire extinguishers Yes Contact EAP Coordinator for location(s). Floodlights Yes Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Contact Grand Rental Station for additional emergency lighting (see Table 5-2). Backhoe Yes Backhoe Yes Backhoe/tractor and 650 John Deere Track hoe available. Contact EAP Coordinator for location(s). Dozer Yes D7 & D10 Crawler Tractors and two rubber-tired dozers (844B & 834B). Contact EAP Coordinator for location(s). Dump Truck Yes Contact EAP Coordinator for location(s). Contact EAP Coordinator for availability and location(s). Contact United Rental (excavating equipment, large earth moving, etc.) Pump and Hoses Yes Contact EAP Coordinator for location(s). Contact The Curry Companies or Rain for Rent for high-capacity portable pumps (see Table 5-2). Sandbags Yes Contact EAP Coordinator for location(s). Contact The Curry Companies or Rain for Rent for high-capacity portable pumps (see Table 5-2). Fill (Stone, aggregate, sand) Yes Contact EAP Coordinator for location(s). Contact United sudditional sandbags (see Table 5-2). Contact EAP Coordinator for location(s). Contact United See Table 5-2 for gravel, sand, and riprap fill as necessary. Contact EAP Coordinator for location(s). Contact United See Table 5-2 for gravel, sand, and riprap fill as necessary. Two rolls of 10-ounce, non-woven filter fabric available. Contact EAP Coordinator for location(s). Plastic Sheeting Yes Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). | Flashlights | Yes | Contact EAP Coordinator for location(s). |
| Fire extinguishers Yes Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Contact Grand Rental Station for additional emergency lighting (see Table 5-2). Backhoe Yes Backhoe/tractor and 650 John Deere Track hoe available. Contact EAP Coordinator for location(s). Dozer Yes D7 & D10 Crawler Tractors and two rubber-tired dozers (844B & 834B). Contact EAP Coordinator for location(s). Dump Truck Yes Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Contact EAP Coordinator for availability and location(s). Contact United Rental (excavating equipment, large earth moving, etc.) Pump and Hoses Yes Contact EAP Coordinator for availability and location(s). Contact United Rentals (see Table 5-2) and/or other nearby large equipment rental providers for additional large equipment as necessary. Contact EAP Coordinator for location(s). Contact The Curry Companies or Rain for Rent for high-capacity portable pumps (see Table 5-2). Sandbags Yes Contact EAP Coordinator for location(s). Contact Great Western Bag Co. for additional sandbags (see Table 5-2). Fill (Stone, aggregate, sand) Yes Contact EAP Coordinator for location(s). Contact listed suppliers in Table 5-2 for gravel, sand, and riprap fill as necessary. Concrete/grout Yes Contact EAP Coordinator for location(s). Contact Vandalia Ready Mix and/or Greenville Ready Mix for additional concrete (see Table 5-2). Two rolls of 10-ounce, non-woven filter fabric available. Contact EAP Coordinator for location(s). Plastic Sheeting Yes Contact EAP Coordinator for location(s). Should be maintained in close proximity to any features that might require immediate access. | Generator | Yes | |
| Floodlights Yes Contact EAP Coordinator for location(s). Contact Grand Rental Station for additional emergency lighting (see Table 5-2). Backhoe Yes Backhoe/tractor and 650 John Deere Track hoe available. Contact EAP Coordinator for location(s). Dozer Yes D7 & D10 Crawler Tractors and two rubber-tired dozers (844B & 834B). Contact EAP Coordinator for location(s). Dump Truck Yes Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Contact EAP Coordinator for availability and location(s). Contact United Rentals (see Table 5-2) and/or other nearby large equipment rental providers for additional large equipment as necessary. Pump and Hoses Yes Contact EAP Coordinator for location(s). Contact The Curry Companies or Rain for Rent for high-capacity portable pumps (see Table 5-2). Sandbags Yes Contact EAP Coordinator for location(s). Contact Great Western Bag Co. for additional sandbags (see Table 5-2). Fill (Stone, aggregate, sand) Yes Contact EAP Coordinator for location(s). Contact Great Western Bag Co. for additional sandbags (see Table 5-2). Concrete/grout Yes Contact EAP Coordinator for location(s). Contact listed suppliers in Table 5-2 for gravel, sand, and riprap fill as necessary. Concrete/grout Yes Contact EAP Coordinator for location(s). Contact Vandalia Ready Mix and/or Greenville Ready Mix for additional concrete (see Table 5-2). Two rolls of 10-ounce, non-woven filter fabric available. Contact EAP Coordinator for location(s). Plastic Sheeting Yes Contact EAP Coordinator for location(s). Should be maintained in close proximity to any features that might require immediate access. | Extension Cords | Yes | Contact EAP Coordinator for location(s). |
| Backhoe Yes Backhoe/tractor and 650 John Deere Track hoe available. Contact EAP Coordinator for location(s). Dozer Yes D7 & D10 Crawler Tractors and two rubber-tired dozers (844B & 834B). Contact EAP Coordinator for location(s). Dump Truck Yes Contact EAP Coordinator for location(s). Large Equipment Rental (excavating equipment, large earth moving, etc.) Pump and Hoses Yes Contact EAP Coordinator for location(s). Contact United Rentals (see Table 5-2) and/or other nearby large equipment rental providers for additional large equipment as necessary. Pump and Hoses Yes Contact EAP Coordinator for location(s). Contact The Curry Companies or Rain for Rent for high-capacity portable pumps (see Table 5-2). Sandbags Yes Contact EAP Coordinator for location(s). Contact Great Western Bag Co. for additional sandbags (see Table 5-2). Fill (Stone, aggregate, sand) Yes Contact EAP Coordinator for location(s). Contact listed suppliers in Table 5-2 for gravel, sand, and riprap fill as necessary. Concrete/grout Yes Contact EAP Coordinator for location(s). Contact Vandalia Ready Mix and/or Greenville Ready Mix for additional concrete (see Table 5-2). Geotextile Filter Fabric Yes Contact EAP Coordinator for location(s). Plastic Sheeting Yes Contact EAP Coordinator for location(s). | Fire extinguishers | Yes | Contact EAP Coordinator for location(s). |
| Dozer Yes Coordinator for location(s). Dozer Yes D10 Crawler Tractors and two rubber-tired dozers (844B & 834B). Dump Truck Yes Contact EAP Coordinator for location(s). Large Equipment Rental (excavating equipment, large earth moving, etc.) Pump and Hoses Yes Contact EAP Coordinator for availability and location(s). Contact United Rentals (see Table 5-2) and/or other nearby large equipment rental providers for additional large equipment as necessary. Contact EAP Coordinator for location(s). Contact The Curry Companies or Rain for Rent for high-capacity portable pumps (see Table 5-2). Sandbags Yes Contact EAP Coordinator for location(s). Contact Great Western Bag Co. for additional sandbags (see Table 5-2). Fill (Stone, aggregate, sand) Yes Contact EAP Coordinator for location(s). Contact listed suppliers in Table 5-2 for gravel, sand, and riprap fill as necessary. Concrete/grout Yes Contact EAP Coordinator for location(s). Contact Vandalia Ready Mix and/or Greenville Ready Mix for additional concrete (see Table 5-2). Geotextile Filter Fabric Yes Two rolls of 10-ounce, non-woven filter fabric available. Contact EAP Coordinator for location(s). Plastic Sheeting Yes Contact EAP Coordinator for location(s). Should be maintained in close proximity to any features that might require immediate access. | Floodlights | Yes | |
| Dump Truck Yes Contact EAP Coordinator for location(s). Dump Truck Yes Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Contact EAP Coordinator for availability and location(s). Contact United Rentals (see Table 5-2) and/or other nearby large equipment rental providers for additional large equipment as necessary. Pump and Hoses Yes Contact EAP Coordinator for location(s). Contact The Curry Companies or Rain for Rent for high-capacity portable pumps (see Table 5-2). Sandbags Yes Contact EAP Coordinator for location(s). Contact Great Western Bag Co. for additional sandbags (see Table 5-2). Fill (Stone, aggregate, sand) Yes Contact EAP Coordinator for location(s). Contact listed suppliers in Table 5-2 for gravel, sand, and riprap fill as necessary. Concrete/grout Yes Contact EAP Coordinator for location(s). Contact Vandalia Ready Mix and/or Greenville Ready Mix for additional concrete (see Table 5-2). Two rolls of 10-ounce, non-woven filter fabric available. Contact EAP Coordinator for location(s). Plastic Sheeting Yes Contact EAP Coordinator for location(s). | Backhoe | Yes | |
| Large Equipment Rental (excavating equipment, large earth moving, etc.) Pump and Hoses Yes Contact EAP Coordinator for availability and location(s). Contact United Rentals (see Table 5-2) and/or other nearby large equipment rental providers for additional large equipment as necessary. Pump and Hoses Yes Contact EAP Coordinator for location(s). Contact The Curry Companies or Rain for Rent for high-capacity portable pumps (see Table 5-2). Sandbags Yes Contact EAP Coordinator for location(s). Contact Great Western Bag Co. for additional sandbags (see Table 5-2). Contact EAP Coordinator for location(s). Contact listed suppliers in Table 5-2 for gravel, sand, and riprap fill as necessary. Concrete/grout Yes Contact EAP Coordinator for location(s). Contact Vandalia Ready Mix and/or Greenville Ready Mix for additional concrete (see Table 5-2). Two rolls of 10-ounce, non-woven filter fabric available. Contact EAP Coordinator for location(s). Plastic Sheeting Yes Contact EAP Coordinator for location(s). Should be maintained in close proximity to any features that might require immediate access. | Dozer | Yes | |
| Rental (excavating equipment, large earth moving, etc.) Pump and Hoses Yes Contact EAP Coordinator for location(s). Contact United Rentals (see Table 5-2) and/or other nearby large equipment rental providers for additional large equipment as necessary. Yes Contact EAP Coordinator for location(s). Contact The Curry Companies or Rain for Rent for high-capacity portable pumps (see Table 5-2). Sandbags Yes Contact EAP Coordinator for location(s). Contact Great Western Bag Co. for additional sandbags (see Table 5-2). Fill (Stone, aggregate, sand) Yes Contact EAP Coordinator for location(s). Contact listed suppliers in Table 5-2 for gravel, sand, and riprap fill as necessary. Contact EAP Coordinator for location(s). Contact Vandalia Ready Mix and/or Greenville Ready Mix for additional concrete (see Table 5-2). Two rolls of 10-ounce, non-woven filter fabric available. Contact EAP Coordinator for location(s). Plastic Sheeting Yes Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Should be maintained in close proximity to any features that might require immediate access. | Dump Truck | Yes | Contact EAP Coordinator for location(s). |
| Rain for Rent for high-capacity portable pumps (see Table 5-2). Sandbags Yes Contact EAP Coordinator for location(s). Contact Great Western Bag Co. for additional sandbags (see Table 5-2). Fill (Stone, aggregate, sand) Yes Contact EAP Coordinator for location(s). Contact listed suppliers in Table 5-2 for gravel, sand, and riprap fill as necessary. Concrete/grout Yes Contact EAP Coordinator for location(s). Contact Vandalia Ready Mix and/or Greenville Ready Mix for additional concrete (see Table 5-2). Two rolls of 10-ounce, non-woven filter fabric available. Contact EAP Coordinator for location(s). Plastic Sheeting Yes Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Should be maintained in close proximity to any features that might require immediate access. | Rental (excavating equipment, large earth | Occasionally | Rentals (see Table 5-2) and/or other nearby large equipment rental providers |
| Additional sandbags (see Table 5-2). Fill (Stone, aggregate, sand) Yes Contact EAP Coordinator for location(s). Contact listed suppliers in Table 5-2 for gravel, sand, and riprap fill as necessary. Concrete/grout Yes Contact EAP Coordinator for location(s). Contact Vandalia Ready Mix and/or Greenville Ready Mix for additional concrete (see Table 5-2). Two rolls of 10-ounce, non-woven filter fabric available. Contact EAP Coordinator for location(s). Plastic Sheeting Yes Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Should be maintained in close proximity to any features that might require immediate access. | Pump and Hoses | Yes | |
| (Stone, aggregate, sand) Concrete/grout Yes Contact EAP Coordinator for location(s). Contact Vandalia Ready Mix and/or Greenville Ready Mix for additional concrete (see Table 5-2). Two rolls of 10-ounce, non-woven filter fabric available. Contact EAP Coordinator for location(s). Plastic Sheeting Yes Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Should be maintained in close proximity to any features that might require immediate access. | Sandbags | Yes | |
| Concrete/grout Yes and/or Greenville Ready Mix for additional concrete (see Table 5-2). Two rolls of 10-ounce, non-woven filter fabric available. Contact EAP Coordinator for location(s). Plastic Sheeting Yes Contact EAP Coordinator for location(s). Contact EAP Coordinator for location(s). Should be maintained in close proximity to any features that might require immediate access. | | Yes | |
| Coordinator for location(s). Plastic Sheeting Yes Contact EAP Coordinator for location(s). Rope Yes Contact EAP Coordinator for location(s). Should be maintained in close proximity to any features that might require immediate access. | Concrete/grout | Yes | |
| Rope Yes Contact EAP Coordinator for location(s). Should be maintained in close proximity to any features that might require immediate access. | Geotextile Filter Fabric | Yes | |
| proximity to any features that might require immediate access. | Plastic Sheeting | Yes | Contact EAP Coordinator for location(s). |
| Personal Flotation Devices Yes Contact EAP Coordinator for location(s). | Rope | Yes | |
| | Personal Flotation Devices | Yes | Contact EAP Coordinator for location(s). |

Table 5-2. Supplier Addresses

| | Table 5-2. Supplier Addre | | |
|---|---|----------------------------|---|
| Supply/Rental Item(s) | Supplier Contact Information | Distance from Site (miles) | Address |
| Sandbags | Great Western Bag Co. (314) 421-0498 (days) (314) 993-5287 (nights/weekends) | 66 | 1416 N. Broadway St. Louis, MO |
| Gravel, Sand, & Riprap | Fuller Brothers Ready Mix (217) 532-2422 | 11 | 935 Ash Street Hillsboro, IL |
| Gravel, Sand, & Riprap | Vandalia Sand and Gravel (618) 283-4029 | 20 | Route 140 Vandalia, IL |
| Gravel, Sand, & Riprap | Central Illinois Materials (618) 283-3259 | 20 | RR 2 Vandalia, IL |
| Gravel, Sand, Riprap & High- Capacity Portable Pumps | The Curry Companies Brian Fenton: (217) 854-3101 | 40 | 21149 Route 4 Carlinville, IL |
| High-Capacity Portable Pumps | Rain for Rent Mark ByBee: (618) 931-0901 | 60 | 3711 Horseshoe Lake Road Granite City, IL |
| High-Capacity Portable Pumps | Linden and Company (800) 383-4811 | 145 | 800 W. Deerbrook Peoria, IL 61615 |
| High-Capacity Portable Pumps | Heartland Pumps (618) 985-5110 | 120 | 1800 Supply Road, Suite A Carterville, IL 62918 |
| Emergency Lighting, 5,000 to 8,500watt Generators, Concrete Mixers, Compact Excavators, Skid Steers, Portable Pumps, & Plate Compactors | Grand Rental Station Fairview Heights, IL (618) 277-7750 (866) 645-0218 (after hours) | 60 | 5612 N. Illinois Street Fairview Heights, IL |
| Emergency Lighting, 4,000watt Generators, Concrete Mixers, Tractor Backhoes/Loaders, Compact Excavators, Skid Steers, Portable Pumps, & Compactors (Plate & Vibratory) | Grand Rental Station Litchfield, IL (217) 324-4000 (866) 645-0218 (after hours) | 20 | 1105 West Weir Street Litchfield, IL 62056 |
| Concrete (Ready Mix Concrete Supplier) | Vandalia Ready Mix (618) 283-1600 | 20 | 1021 Janette Drive Vandalia, IL 62471 |
| Concrete (Ready Mix Concrete Supplier) | Greenville Ready Mix (618) 664-1340 | 17 | 1311 S. 4 th Street Greeneville, IL 62246 |
| Large Earthmoving Equipment (25,000 to 50,000 lb. Track hoe Excavators & 3.0 to 3.4 CY Wheel Loaders) | <u>United Rentals</u> (618) 345-6050 | 60 | 5076 Mid America Court Collinsville, IL 62234 |

6 FACILITY/IMPOUNDMENT DESCRIPTION

The impoundments included in this EAP are described as follows and illustrated in Figure 1-2. Table 6-1 contains additional geometric details for each impoundment.

The Coffeen Power Plant is located in Montgomery County, Illinois approximately 1.5 miles south of Coffeen, Illinois. The plant is located on the east bank of Coffeen Lake, which is an impoundment created by Coffeen Lake Dam.

The GMF Pond is located northeast of power plant and north of the GMF Recycle Pond. The GMF Pond consists of a single pond formed by an earthen embankment around its perimeter. The earthen embankment crest elevation is currently 13-feet above grade; however, its final design has a crest elevation 100-feet above grade. The final design was used in the breach analysis and corresponding inundation map because the final design is more conservative than existing conditions (larger volume, greater dam height, etc.). The GMF Pond is used to dewater, store and dispose of gypsum from the Power Plant's flue gas desulphurization system. The GMF Pond discharges via a HDPE lined transfer channel into the GMF Recycle Pond. The transfer channel has a trapezoidal cross section with 3H:1V side slopes, a bottom width of 32 feet, a depth of 9-feet, and is 500-feet long.

The GMF Recycle Pond is located northeast of the power plant and south of the GMF Pond. The GMF Recycle Pond consists of a single pond formed by an earthen embankment around its perimeter. The pond is used to dewater, store and dispose of gypsum. It also is used to retain stormwater discharge from the GMF Pond transfer channel. The pool level is controlled by a recycle pump system that is located at the southeast corner. There is an emergency spillway located at the northeast corner that discharges into a creek that runs along the east side of the pond and discharges into the eastern cove of Coffeen Lake (Eastern Cove).

Ash Pond No. 1 is located east of the power plant and consists of a single pond formed by earthen embankments around the perimeter. The pool level is controlled by a recycle pump system that is located at the northwest corner. The emergency spillway consists of a pipe that connects to the top of the recycle pump intake pipe. The emergency spillway discharges into the cooling water discharge channel to the north which feeds into the eastern cove of Coffeen Lake. The stored material settled in the bottom of the pond consists of primarily bottom ash and boiler slag.

Ash Pond No. 2 is located east of the power plant, north of Ash Pond No. 1 and west of the Cooling Water Pond. Ash Pond No. 2 was closed by leaving CCR in place and constructing a final cover system. The boundaries of these impoundments encompass a total area of approximately 60 acres.

Table 6-1. Power Plant Impoundment Characteristics

| Feature/Parameter | GMF Pond | GMF Recycle Pond | Ash Pond No.1 | Ash Pond No.2 |
|---|---------------------|---|---|--|
| Maximum Embankment Height | 13.0 feet | 20.0 feet | 41.5 feet | 28.0 feet |
| Length of Dam | 5,060 feet | 3,600 feet | 4,300 feet | 6,400 feet |
| Crest Width | 20 feet | 20 feet | N/A | N/A |
| Crest Elevation | 632.0 feet | 629.0 feet | 637.5 feet | 638.0 feet |
| Reservoir Area at Top of Dam | 37.6 acres | 17.0 acres | N/A | N/A |
| Storage Capacity at Top of Dam | 442 acre-feet | 324 acre-feet | N/A | N/A |
| Primary Spillway Type | Trapezoidal Channel | Recycle Pump | Recycle Pump (48" dia. steel intake pipe) | Stormwater let- down structures are now the spillways |
| Primary Spillway Crest Elevation | 623.0 feet | 610.0 feet | N/A | N/A |
| Storage Capacity at Primary Spillway Elevation | 1,150 acre-feet | 49.7 acre-feet | N/A | N/A |
| Reservoir Area at Normal Water Surface Elevation | 27.0 acres | 10.4 acres | N/A | N/A |
| Auxiliary Spillway Type | None | (3x) 6'x6' conc. risers to (3x) 4'dia. HDPE pipes | N/A | N/A |
| Auxiliary Spillway Crest Elevation | N/A | 624.1 feet | N/A | N/A |

Notes: Elevations are in reference to NAVD88

7 BREACH INUNDATION MAPS AND POTENTIAL IMPACTS

Inundation maps for GMF Pond, GMF Recycle Pond, Ash Pond No.1, and Ash Pond No.2 potential breach scenarios are provided in the following pages. It is the Montgomery County ESDA/EMA's responsibility to keep a current list of affected parties/properties to contact in the case of emergencies that result in Response Level 2 or 3. This list should encompass all properties within and adjacent to the probable inundation extents shown in the provided inundation maps.

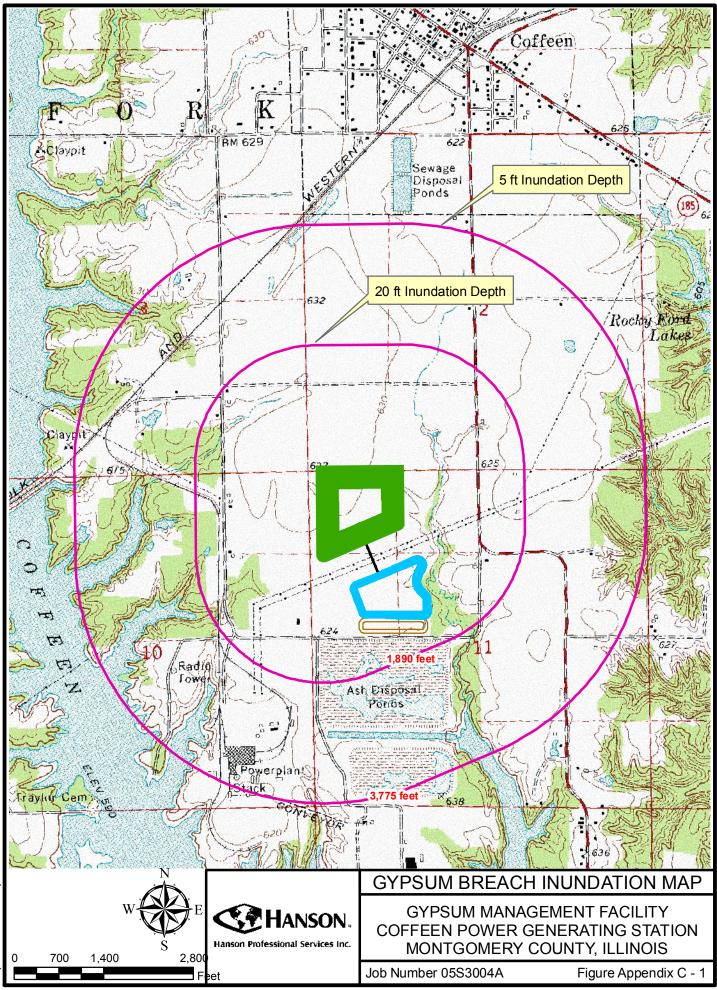
The methodology used to identify probable inundation extents for potential breach scenarios varied as a function of the impoundment size, location, surrounding topography, and surrounding structures/facilities/waterbodies.

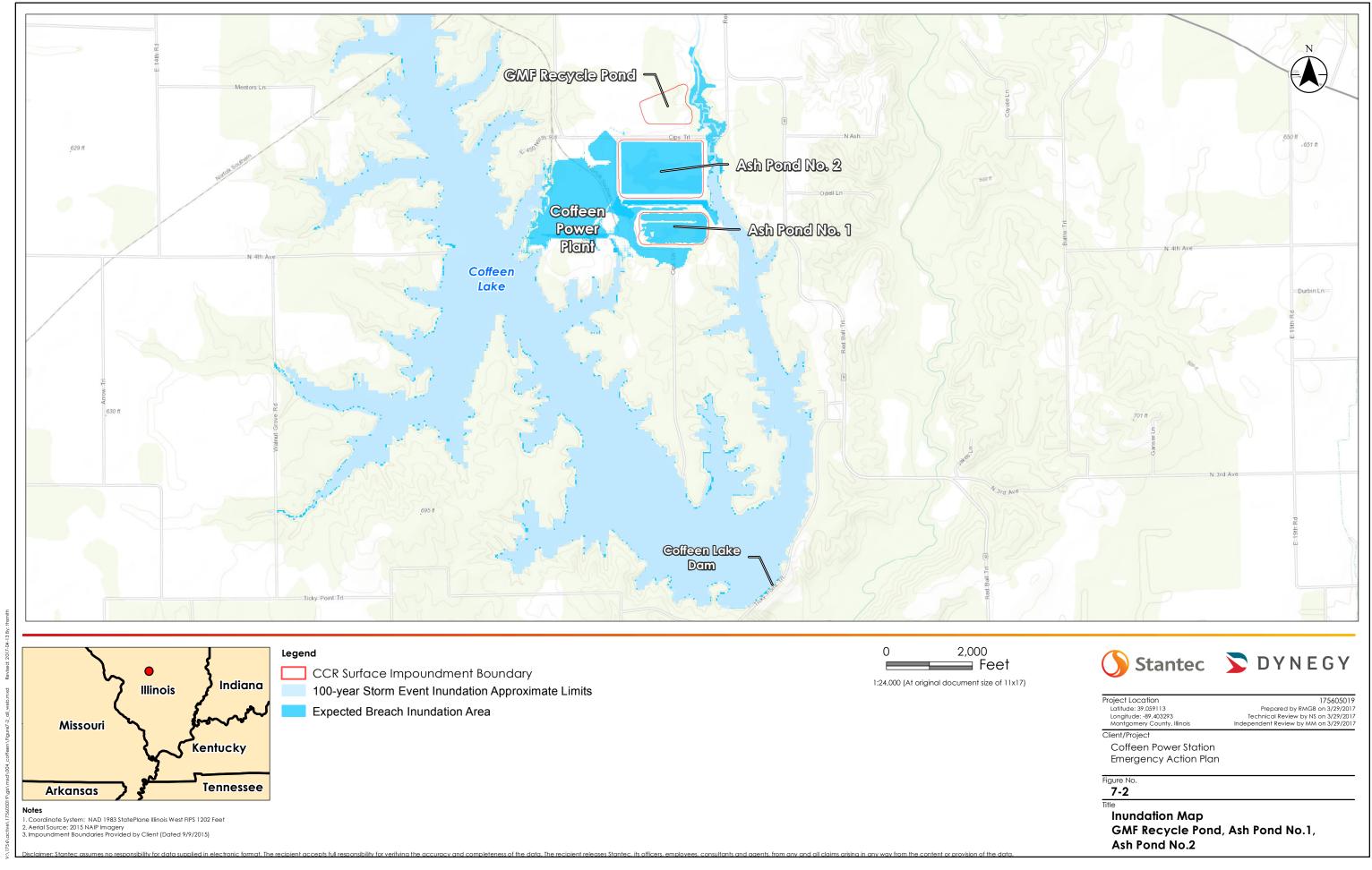
The GMF Pond inundation map was developed by Hanson Professional Services Inc. (2007) using final design conditions (100-feet tall and 2,478 acre-feet of stored volume) and an approximate method of computing the inundation limits of gypsum slurry by computing a runout distance on a constant slope. It was assumed that a breach of the earthen perimeter embankment would cause saturated gypsum material to liquefy and release towards downstream areas in a semi-circular pattern. This breach scenario was simulated at multiple locations along the earthen perimeter dike and the corresponding results were used to create the inundation map shown as Figure 7-1.

The GMF Recycle Pond breach analysis consisted of a Probable Maximum Precipitation (PMP) failure scenario at the eastern embankment. The resultant breach discharges were modeled downstream using 1D and 2D capabilities of HEC-RAS. The approximate inundation area is illustrated in the inundation map shown as Figure 7-2.

The Ash Pond No. 1 breach analysis consisted of PMP failure scenarios of the embankment near the northwest and northeast corners of the pond. The breach discharges were modeled downstream using 1D and 2D capabilities of HEC-RAS. The approximate inundation area is illustrated in the inundation map shown as Figure 7-2.

The Ash Pond No. 2 breach analysis consisted of a failure scenario where the stored volume liquefies and breaches the embankment near the southwest corner of the pond. The breach discharge was modeled downstream using 2D capabilities of HEC-RAS. The approximate inundation area is illustrated in the inundation map shown as Figure 7-2.





ATTACHMENT G

CCR Fugitive Dust Control Plan

for Coffeen Power Plant

Prepared for:

Illinois Power Generating Company

Coffeen Power Plant 134 Cips Lane Coffeen, IL 62017

Prepared by:

Burns & McDonnell Kansas City, Missouri

Amendment 1

October 2021

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1 Introduction

This Coal Combustion Residuals (CCR) fugitive dust control plan has been prepared for the retired Coffeen Power Plant, located in Montgomery County, Illinois. This plan addresses the air criteria in 40 C.F.R. § 257.80 of the United States Environmental Protection Agency's CCR rule, which requires the owner or operator of a CCR unit to "adopt measures that will effectively minimize CCR from becoming airborne at the facility" and to "prepare and operate in accordance with a CCR fugitive dust control plan." The plan also addresses the air criteria in 35 I.A.C. 845.500 of the Illinois Environmental Protection Agency's CCR rule, which contains similar requirements to the federal CCR rule.

1.1 Facility Information

- Facility Name: Coffeen Power Plant (Retired)
- Facility Address: 134 Cips Lane, Coffeen, IL 62017
- Owner/Operator: Illinois Power Generating Company

1.2 Certification

The owner or operator must obtain a certification from a qualified professional engineer that the initial CCR fugitive dust control plan, or any subsequent amendment of it, meets the requirements of 40 C.F.R. § 257.80 and 35 I.A.C. 845.500. See 40 C.F.R. § 257.80(b)(7); 35 I.A.C. 845.500(b)(7).

I certify under penalty of law that, to the best of my knowledge, this plan meets the requirements of 40 C.F.R. § 257.80 and 35 I.A.C. 845.500. This certification is based on my review of the document and conditions at the site and on my inquiry of the person or persons who managed the preparation of this document.

John R. Hesemann
Printed Name of Qualified Professional Engineer

1062-058523

| Signature of Qualified Professional Engineer and Date

| O62.058523 - Illinois - Expires 11/30/2021 | Registration Number and State

| O62.058523 - Illinois - Expires 11/30/2021 | Registration Number and State

2 CCR Fugitive Dust Control Measures and Appropriateness

CCR fugitive dust has the potential to become airborne at the facility during periods of CCR management in the CCR units, CCR handling and CCR transport. Areas at the facility that have the potential for airborne CCR fugitive dust are CCR surface impoundments, a CCR landfill, CCR handling equipment and CCR transport in trucks. This section identifies and describes the control measures selected and adopted by the facility to minimize CCR from becoming airborne at the facility and explains how the selected measures are applicable and appropriate for site conditions. The control measures may be adjusted or modified based on observed effectiveness of minimizing CCR from becoming airborne and weather conditions.

2.1 Management of CCR in the CCR Units

The facility manages CCR in surface impoundments and a landfill located at the facility. Table 2-1 below identifies CCR fugitive dust control measures that have been selected for use by the facility during CCR management in the CCR units, including placement of CCR into the CCR units, and explains how the selected measures are applicable and appropriate for site conditions. The facility will use the identified measures during CCR management in the CCR units to minimize CCR from becoming airborne at the facility.

| CCR Activity | CCR Fugitive Dust Control Measure | Applicability and Appropriateness of Control Measure |
|---|--|---|
| | Condition CCR to be emplaced in the landfill before emplacement. | Conditioning CCR placed in the landfill allows CCR to bind together and thus minimizes the potential for CCR fugitive dust generation when CCR is managed in the landfill. The added moisture content will prevent wind dispersal of the CCR but will not result in free liquids. Use of conditioned CCR also achieves at least equivalent performance to conventional daily cover in terms of preventing wind entrainment. |
| Management of CCR in the facility's CCR units | Wet management of CCR bottom ash and flue gas desulfurization materials in CCR surface impoundments. | Wet management of CCR minimizes the potential for CCR fugitive dust generation. |
| | Water areas of exposed CCR in CCR units, as necessary. | Water will be applied to areas of exposed CCR to maintain moisture content to minimize the potential for CCR fugitive dust generation in excessively dry or windy conditions. |
| | Naturally occurring grass vegetation in areas of exposed CCR in CCR surface impoundments. | Vegetation provides a wind screen and/or cover and reduces wind entrainment of CCR. |
| | Reduce or halt operations during high wind events, as necessary. | Reducing or halting operations during high wind events minimizes the potential for CCR fugitive dust generation. |

Table 2-1. Control Measures for CCR Management in CCR Units

2.2 Handling of CCR

Bottom ash may be periodically removed from the CCR surface impoundments and remains sufficiently wet during and after handling activities, including dewatering, associated with transfer of the CCR. Table 2-2 below identifies CCR fugitive dust control measures that have been selected for use by the facility during handling of CCR and explains how the selected measures are applicable and appropriate for site conditions. The facility will use the identified measures when handling CCR to minimize CCR from becoming airborne at the facility.

| CCR Activity | CCR Fugitive Dust Control Measure | Applicability and Appropriateness of Control Measure |
|--------------------|--|--|
| | CCR bottom ash removed from CCR surface impoundments and loaded into trucks for transport remains conditioned during handling. | Conditioned CCR allows CCR to bind together and thus minimizes the potential for CCR fugitive dust generation when CCR is handled. |
| Handling of CCR at | CCR fly ash to be emplaced in the landfill is conditioned before emplacement. | Conditioning allows CCR to bind together and thus minimizes the potential for CCR fugitive dust generation. |
| the facility | Condition CCR materials to be transported offsite before they are loaded into trucks, as necessary. | Conditioning allows CCR to bind together and thus minimizes the potential for CCR fugitive dust generation while loading CCR into trucks and during transport. |
| | Reduce or halt operations during high wind events, as necessary. | Reducing or halting operations during high wind events minimizes the potential for CCR fugitive dust generation. |

Table 2-2. Control Measures for Handling CCR

2.2.1 Conditioning of CCR Prior to Emplacement in CCR Landfill

Conditioned CCR is CCR that has been wetted with water or an appropriate chemical dust suppressant. Water or a chemical dust suppressant is added to raise the moisture content of the CCR to prevent wind dispersal but will not result in free liquids. Conditioning allows for the CCR to bind together, which minimizes the potential for CCR fugitive dust.

CCR generated offsite that is authorized for placement in the facility's landfill, is conditioned in a pug mill or otherwise conditioned prior to emplacement into the facility's landfill. Therefore, all CCR that is added to the facility's landfill is emplaced in the landfill as conditioned CCR.

2.3 Transportation of CCR

CCR is transported via truck at the facility using a combination of paved and unpaved facility roads. Table 2-3 below identifies CCR fugitive dust control measures that have been selected for use by the facility during transport of CCR. The facility will use the identified measures when transporting CCR to minimize CCR from becoming airborne at the facility.

| CCR Activity | CCR Fugitive Dust Control Measure | Applicability and Appropriateness of Control Measure |
|---------------------------------------|---|---|
| | Condition CCR to be emplaced in the landfill before emplacement. | Conditioning CCR increases moisture content of the CCR and minimizes the potential for CCR fugitive dust generation during CCR transport (and emplacement in the landfill). |
| | Condition CCR materials to be transported offsite before they are loaded into trucks, as necessary. | Conditioning allows CCR to bind together and thus minimizes the potential for CCR fugitive dust generation while loading CCR into trucks and during transport. |
| | Cover or enclose trucks used to transport CCR fly ash. | Covering or enclosing trucks transporting CCR on facility roads minimizes the potential for CCR fugitive dust generation from the CCR transport trucks. |
| | Limit the speed of vehicles to no more than 15 mph on facility roads. | Limiting the speed of vehicles traveling on facility roads minimizes the potential for CCR fugitive dust generation from the CCR transport trucks. |
| Transportation of CCR at the facility | Cover or enclose trucks used to transport CCR other than fly ash, as necessary. | Covering or enclosing trucks transporting CCR on facility roads minimizes the potential for CCR fugitive dust generation from the CCR transport trucks. |
| | Sweep or rinse CCR off of the outside of the trucks transporting CCR, as necessary. | Removing CCR present on the outside of the truck minimizes the potential for movement of the truck or wind to cause CCR fugitive dust to become airborne. |
| | Remove CCR, as necessary, deposited on facility road surfaces during transport. | Removing CCR deposited on facility road surfaces as a result of transport minimizes the potential for CCR fugitive dust generation from vehicle traffic. |
| | Condition CCR haul roads, including landfill roads, with water or dust suppressant as necessary. | Watering CCR haul roads, as well as landfill roads, minimizes the potential for dust generation to occur as a result of CCR hauling traffic and heavy equipment use. |
| | Reduce or halt operations during high wind events, as necessary. | Reducing or halting operations during high wind events minimizes the potential for CCR fugitive dust generation. |

Table 2-3. Control Measures for Transportation of CCR

3 Procedures for Periodic Assessment of Effectiveness of the Plan

The facility conducts inspections associated with CCR fugitive dust control. The facility also uses the procedures identified in section 5 of this plan to log every citizen complaint involving CCR fugitive dust events at the facility. These inspections and the investigations of citizen complaints will be used to periodically assess the effectiveness of the CCR fugitive dust control plan per 40 C.F.R. § 257.80(b)(4) and 35 I.A.C. 845.500(b)(3).

The facility routinely performs inspections to verify the effectiveness of the CCR fugitive dust control measures used at the facility. Inspections are conducted during daylight working hours and include observing for the presence of CCR fugitive dust emissions from vehicles transporting CCR on facility roads, CCR handling and CCR management activities, including CCR placement in CCR units. Inspection records include information such as the name of the person conducting the inspection, the date and time of the inspection, the results of the inspection, and any corrective action taken.

When a CCR fugitive dust event is observed or a citizen complaint involving a CCR fugitive dust event at the facility is received, current CCR management practices will be reviewed to see that the selected control measures are being properly implemented. If the control measures are not being properly implemented, relevant operating personnel will be notified and, as warranted, retrained in the proper implementation of CCR fugitive dust control measures. If appropriate, use of revised and/or additional control measures will be evaluated. As warranted, revised and/or additional control measures found to be applicable and appropriate to control CCR fugitive dust emissions will be incorporated into an amended CCR fugitive dust control plan.

The plan also will be reassessed in the event of material changes in site conditions potentially resulting in CCR fugitive dust becoming airborne at the facility.

Coffeen

4 Recordkeeping, Notification, Internet Site

The written CCR fugitive dust control plan, any amendment of the written plan, and the annual CCR fugitive dust control report required by 40 C.F.R. § 257.80(c) and 35 I.A.C. 845.500(c) will be placed in the facility's written operating record and posted to the company's CCR website in accordance with 40 C.F.R. § 257.105(g), § 257.107(g), and 845.800(d)(7), (14) and 845.810(e). Notification of the availability of the CCR fugitive dust control plan, any amendment of the plan, and the annual CCR fugitive dust control report will be provided to IEPA in accordance with 40 C.F.R. § 257.106(g). Any amendment of the fugitive dust control plan will be submitted to IEPA in accordance with 845.500(b)(5).

Additionally, pursuant to 845.500(b)(6), this fugitive dust control plan is being placed in facility's operating record and posted to the company's CCR website prior to the submission of any permits for the Coffeen Power Plant.

5 Procedures to Log Citizen Complaints

In the event the owner or operator of the facility receives a citizen complaint involving a CCR fugitive dust event at the facility, relevant information about the complaint will be logged. Information that will be recorded includes, as applicable:

- Date/Time the complaint is received
- Date/Time and duration of the CCR fugitive dust event
- Description of the nature of the CCR fugitive dust event
- Name of the citizen entering the complaint
- Address & phone number of citizen entering the complaint
- Name of the personnel who took the complaint
- All actions taken to assess and resolve the complaint

All citizen complaints involving CCR fugitive dust events at the facility will be investigated promptly. As deemed appropriate or necessary, corrective measures will be taken and a follow-up response will be provided to the complainant.

Pursuant to 35 I.A.C. 845.500(b)(2), quarterly reports will be submitted to IEPA no later than 14 days from the end of the quarter for all complaints received in that quarter. At a minimum, the quarterly report will include the date of the complaint, the date of the incident, the name and contact information of the complainant (if given), and all actions taken to assess and resolve the complaint.

6 Amendments

The written CCR fugitive dust control plan may be amended at any time provided the revised plan is placed in the facility's operating record as required by 40 C.F.R. § 257.105(g)(1) and 845.500(b)(6). Any amendment of the fugitive dust control plan will be submitted to IEPA in accordance with 845.500(b)(5). The written CCR fugitive dust control plan must be amended whenever there is a change in conditions that would substantially affect the written plan in effect.

| Amendment Number and Date | Pages or Section | Description of Amendment | Professional Engineer Certifying Plan |
|---------------------------------|------------------|---|---|
| Version 0 October 2015 | | Initial Plan | Wendy M. Pennington |
| Amendment 1 October 2021 | Various | Administrative changes and adjustments to site condition controls as appropriate. | John R. Hesemann |
| | | | |
| | | | |
| | | | |
| | | | |
| | | | |
| | | | |

Table 6-1. CCR Fugitive Dust Control Plan Amendments

ATTACHMENT H

Intended for

Illinois Power Generating Company

Date

October 25, 2021

Project No.

1940100806-002

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT

ASH POND NO. 1 COFFEEN POWER PLANT COFFEEN, ILLINOIS

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT ASH POND NO. 1

Project Name Coffeen Power Plant Ash Pond No. 1

Project No. **1940100806-002**

Recipient Illinois Power Generating Company

Document Type Hydrogeologic Site Characterization Report

Revision FINAL

Date October 25, 2021

Ramboll

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| Appendix F | Hydraulic Conductivity Test Data |
| Appendix G | FEMA Flood Hazard Map |

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ACRONYMS AND ABBREVIATIONS

°F degrees Fahrenheit

§ Section

35 I.A.C. Title 35 of the Illinois Administrative Code 40 C.F.R. Title 40 of the Code of Federal Regulations

AP1 Ash Pond No. 1
AP2 Ash Pond No. 2
bgs below ground surface
CCR coal combustion residuals
CCR Rule 40 C.F.R. § 257 Subpart D
cm/s centimeters per second
CPP Coffeen Power Plant

DA deep aquifer

DCU deep confining unit

ESRI Environmental Systems Research Institute, Inc.

FEMA Federal Emergency Management Agency

ft/day feet per day ft/ft feet per foot

g horizontal acceleration

GMF GSP Gypsum Management Facility Gypsum Stack Pond

GMF RP Gypsum Management Facility Recycle Pond

GMP Groundwater Monitoring Plan
GMZ Groundwater Management Zone
GWPS Groundwater Protection Standard
Hanson Hanson Professional Services, Inc.

HCR Hydrogeologic Site Characterization Report

HDPE high-density polyethylene

HELP Hydrologic Evaluation of Landfill Performance

HUC Hydrologic Unit Code

ID identification

IDNR Illinois Department of Nature Resources
IEPA Illinois Environmental Protection Agency

ILWATER Illinois Water and Related Wells
IPGC Illinois Power Generating Company
ISAS Illinois State Archaeological Survey
ISGS Illinois State Geological Survey

LCU lower confining unit

LF Landfill

mg/L milligrams per liter msl above mean sea level

NAVD88 North American Vertical Datum of 1988 NGVD29 National Geodetic Vertical Datum of 1929

NID National Inventory of Dams

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NPDES National Pollutant Discharge Elimination System

No. number

NRT Natural Resource Technology, Inc.

NRT/OBG NRT, an OBG Company

Part 845 Standards for the Disposal of Coal Combustion Residuals in Surface

Impoundments: 35 I.A.C. § 845

pcf pounds per cubic foot pCi/L picoCuries per liter

PMP potential migration pathways

Ramboll Americas Engineering Solutions, Inc.

SI Surface Impoundments

Site Area near AP1

SSURGO Soil Survey Geographic Database

SU Standard Units

TDS total dissolved solids UCU upper confining unit

USEPA United States Environmental Protection Agency

USFWS United States Fish and Wildlife Service

USGS United States Geological Survey

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EXECUTIVE SUMMARY

This Hydrogeologic Site Characterization Report (HCR) for the Coffeen Ash Pond Number (No.) 1 (AP1) expands upon the hydrogeology and groundwater quality data presented in previous hydrogeologic investigation reports prepared for the Coffeen Power Plant (CPP) (Natural Resource Technology [NRT], 2017; Hanson Professional Services, Inc. [Hanson], 2009; Hanson, 2016). This report has been assembled to satisfy the information and analysis requirements of Title 35 of the Illinois Administrative Code (35 I.A.C.) Section (§) 845.620 as summarized in **Table ES-1**. The conceptual site model includes hydrogeologic and groundwater quality data specific to AP1, which has been collected from 2015 to 2021. AP1 is part of the CPP, which is two miles south of the city of Coffeen, Illinois and about eight miles southeast of the city of Hillsboro, Illinois.

The CPP operated as a coal-fired power plant from 1964 until November 2019 and has five coal combustion residuals (CCR) management units. The CCR unit that is the subject of this report is AP1 (Vistra Identification [ID] No. 101, Illinois Environmental Protection Agency [IEPA] ID No. W1350150004-01, and National Inventory of Dams [NID] No. IL50722). Coffeen AP1 is a 23-acre, unlined surface impoundment (SI) used to manage CCR and non-CCR waste streams at the CPP. Its total storage capacity is approximately 300 acre-feet.

CPP is located between the two lobes of Coffeen Lake (**Figure 1-1**), which was formed in 1963 by damming the McDavid Branch of the East Fork of Shoal Creek. Coffeen Lake encompasses approximately 1,100 acres and was created to provide a source of cooling water for the CPP. Coffeen Lake borders the CPP to the west, east, and south, and agricultural land is located to the north. Historically coal mines were operated at depth below the site. Mine shafts, processing facilities and historic coal storage was located south of AP1.

Unlithified material present above the bedrock in the vicinity of the CPP was categorized into hydrostratigraphic units for this HCR. In addition to the CCR, the hydrostratigraphic units occur in the following order (from surface downward) and include:

- **Upper Confining Unit (UCU):** Composed of the Roxana and Peoria Silts (Loess Unit) and the upper clayey portion of the Hagarstown member which are classified as silts to clayey silts and gravelly clay below the surficial soil. The UCU has been eroded east of AP1, near the Unnamed Tributary.
- **Uppermost Aquifer:** The uppermost aquifer is the Hagarstown Member which is classified as primarily sandy to gravelly silts and clays with thin beds of sands. Similar to the Loess Unit, the Hagarstown is absent in some locations near the Unnamed Tributary.
- Lower Confining Unit (LCU): Comprised of the Vandalia Member, Mulberry Grove Member, and Smithboro Member. These units include a sandy to silty till with thin, discontinuous sand lenses, a discontinuous and limited extent sandy silt which has infilled prior erosional features, and silty to clayey diamicton, respectively.
- **Deep Aquifer (DA):** Sand and sandy silt/clay units of the Yarmouth Soil, which include accretionary deposits of fine sediment and organic materials, typically less than five feet thick and discontinuous across the CPP.
- **Deep Confining Unit (DCU):** Comprised of the Banner Formation generally clays, silts, and sands. The Lierle Clay Member is the upper layer of the Banner Formation which was encountered at the CPP.

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Bedrock of the Bond Formation which consists of limestone and calcareous clays and shale, was not encountered in the borings advanced at the CPP.

Flow of groundwater from central portions of the CPP to Coffeen Lake or the Unnamed Tributary through the uppermost aquifer are the primary pathways for contaminant migration. Groundwater elevations are primarily controlled by surface topography, geologic unit topography, and water levels within Coffeen Lake and the Unnamed Tributary. A groundwater divide trending north-south is observed running through the approximate center of the CPP. Phreatic surfaces or water elevations within the SIs are generally consistent and have not been observed to fluctuate with groundwater elevations, indicating limited hydraulic connection with the SIs.

35 I.A.C. § 845 parameters were monitored in the uppermost aquifer monitoring wells at AP1 as part of the Title 40 of the Code of Federal Regulations (40 C.F.R.) § 257 and IEPA groundwater monitoring programs from 2015 to 2021. These data were supplemented with installation and sampling of additional wells installed in 2021. The results indicate the following parameters were detected at concentrations/measurements greater than (or less than for pH) the applicable 35 I.A.C. § 845.600 groundwater protection standards (GWPSs) and are considered potential exceedances:

- Arsenic in downgradient uppermost aquifer wells G302, G303, and G304/G307. Arsenic was also detected in upgradient uppermost aquifer well G306.
- Boron in downgradient uppermost aquifer wells G301, G302, G303, G304/G307, G305, G308, G311, and G313. Boron was also detected in upgradient uppermost aquifer well G306.
- Cadmium in downgradient uppermost aquifer well G304/G307.
- Chromium in downgradient uppermost aquifer well G304/G307.
- Cobalt in downgradient uppermost aquifer wells G301, G302, G303, G304/G307, and G305; and in downgradient LCU well G314. Cobalt was also detected in upgradient uppermost aquifer well G306.
- Lead in downgradient uppermost aquifer wells G301, G302, G303, G304/G307 and G305; and in downgradient LCU well G316. Lead was also detected in upgradient uppermost aquifer well G306.
- Lithium in downgradient uppermost aquifer wells G303 and G304/G307.
- pH (lower limit) in downgradient uppermost aquifer wells G301 and G312.
- Radium 226 and 228 combined in downgradient LCU well G316.
- Sulfate in downgradient uppermost aquifer wells G301, G302, G303, G304/G307, G305, G308, G309, G310, G311, G312, G313, G315, and G317; in downgradient LCU wells G307D, G314, and G316; and in downgradient DA well G314D. Sulfate was also detected at concentrations greater than the GWPS in upgradient uppermost aquifer well G306.
- Total dissolved solids (TDS) in downgradient uppermost aquifer wells G301, G302, G303, G304/G307, G305, G308, G309, G310, G311, G312, G313, G315, and G317; in downgradient LCU wells G307D, G314, and G316; and in downgradient DA well G314D. Sulfate was also detected at concentrations greater than the GWPS in upgradient uppermost aquifer well G306.

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Groundwater monitoring results were compared to the applicable 35 I.A.C. § 845.600 GWPSs to determine potential exceedances. Potential exceedances include results reported during the background groundwater monitoring or prior period that are greater than the GWPS. The results are considered potential exceedances because the results were compared directly to the standard and did not include an evaluation of background groundwater quality or utilize the statistical methodologies proposed in the groundwater monitoring plan (GMP) provided in the Operating Permit application. Exceedances will be determined following IEPA approval of the GMP.

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TABLE ES-1. PART 845 REQUIREMENTS CHECKLIST

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Part 845 Reference Individual Part 845 Components Reviewed for Completeness | | Location of Information in HCR |
|---|---|--|
| 845.620(b) | The hydrogeologic site characterization shall include but not be limited to the following: | |
| 845.620(b)(1) | Geologic well logs/boring logs; | Table 3-1 Figure 3-1 Appendix C |
| 845.620(b)(2) | Climatic aspects of the site, including seasonal and temporal fluctuations in groundwater flow; | Sections 3.2.4 & 3.3.1 Table 3-3 Figures 3-2 through 3-5 |
| 845.620(b)(3) | Identification of nearby surface water bodies and drinking water intakes; | Sections 3.3.2 & 5.2 Appendix B |
| 845.620(b)(4) | Identification of nearby pumping wells and associated uses of the groundwater; | Section 5.1 Appendix B |
| 845.620(b)(5) | Identification of nearby dedicated nature preserves; | Section 5.3 Appendix B |
| 845.620(b)(6) | Geologic setting; | Sections 2.4 & 2.5 Figures 2-2 through 2-4 |
| 845.620(b)(7) | Structural characteristics; | Section 2.4.3 Figure 2-5 |
| 845.620(b)(8) | Geologic cross-sections; | Figure 2-7 |
| 845.620(b)(9) | Soil characteristics; | Section 2.3 Figure 2-2 Tables 2-1 & 2-4 |
| 845.620(b)(10) | Identification of confining layers; | Sections 3.2.1 |



TABLE ES-1. PART 845 REQUIREMENTS CHECKLIST

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Part 845 Reference | Individual Part 845 Components Reviewed for Completeness | Location of Information in HCR |
|--------------------|--|---|
| 845.620(b)(11) | Identification of potential migration pathways; | Section 3.2.1 & 3.2.3 |
| 845.620(b)(12) | Groundwater quality data; | Section 4.2 Table 4-1 |
| 845.620(b)(13) | Vertical and horizontal extent of the geologic layers to a minimum depth of 100 feet below land surface, including lithology and stratigraphy; | Section 2.8 Figures 2-7 & 2-8 Appendix C |
| 845.620(b)(14) | A map displaying any known underground mines beneath a CCR surface impoundment; | Section 2.7 Appendix B |
| 845.620(b)(15) | Chemical and physical properties of the geologic layers to a minimum depth of 100 feet below land surface; | Section 2.8 Tables 2-1, 2-2, & 2-4 Appendices D & F |
| 845.620(b)(16) | Hydraulic characteristics of the geologic layers identified as migration pathways and geologic layers that limit migration, including: | Sections 3.2.4.1, 3.2.5, & 3.2.6 Tables 3-2 to 3-4 Appendices D & F |
| 845.620(b)(16)(A) | water table depth; | Section 3.2.4 Figures 3-3 & 3-4 Appendix E |
| 845.620(b)(16)(B) | hydraulic conductivities; | Sections 3.2.5 Tables 2-1 & 3-3 Appendices D & F |
| 845.620(b)(16)(C) | effective and total porosities; | Section 2.5.1 Table 2-1 |



TABLE ES-1. PART 845 REQUIREMENTS CHECKLIST

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Part 845 Reference | Location of Information in HCR | | |
|--------------------|---|---|--|
| 845.620(b)(16)(D) | direction and velocity of groundwater flow; and | Section 3.2.4 to 3.2.6 Tables 3-2 & 3-4 Figures 3-3 & 3-4 | |
| 845.620(b)(16)(E) | map of the potentiometric surface; | Figures 3-3 & 3-4 | |
| 845.620(b)(17) | Groundwater classification pursuant to 35 I.A.C. § 620; and | Section 3.2.7 | |

[O: LDC 06/15/21, U: LDC 08/19/21; C: EJT 08/19/21; U:KLT 8/24/21, C: LDC 09/17/21]

Notes:

-- = reference to main regulation

35 I.A.C. § 620 = Title 35 of the Illinois Administrative Code, Part 620

HCR = Hydrogeologic Site Characterization Report



1. INTRODUCTION

1.1 Overview

In accordance with requirements of the Standards for the Disposal of Coal Combustion Residuals in Surface Impoundments: 35 I.A.C. § 845 (Part 845) (IEPA, 2021), Ramboll Americas Engineering Solutions, Inc. (Ramboll) has prepared this HCR on behalf of CPP (**Figure 1-1**), operated by Illinois Power Generating Company (IPGC). This report will apply specifically to the CCR Unit referred to as AP1. However, information gathered to evaluate other CCR units on site regarding geology, hydrogeology, and groundwater quality is included, where appropriate. AP1 is an unlined impoundment that covers an area of approximately 23 acres, has berms up to 41 feet above the surrounding land surface, and a volume of 300 acre-feet. This HCR includes Part 845 content requirements specific to 35 I.A.C. § 845.620(b) (Hydrogeologic Site Characterization) for AP1 at CPP.

1.2 Part 845 Description

Under Part 845 (IEPA, April 15, 2021), the IEPA has developed a rule of general applicability for CCR SIs at power generating facilities. Part 845 contains comprehensive rules for the design, construction, operation, corrective action, closure, and post closure care of SIs containing CCR. CCR is commonly referred to as coal ash, and CCR SIs are commonly referred to as coal ash ponds. This rule includes GWPSs applicable to each CCR SI at the waste boundary and requires each owner or operator to monitor groundwater. IEPA's rule includes a permitting program as well as all federal standards for CCR SIs promulgated by the United States Environmental Protection Agency (USEPA). In addition, the rules include procedures for public participation, closure alternatives analyses, and closure prioritization, and provides access to records via public website. The rules also include financial assurance requirements for CCR SIs.

1.3 Previous Investigations and Reports

Numerous hydrogeologic investigations have been performed concerning the CCR Units located at the CPP. The information presented in this HCR includes data collected in support of the monitoring well network established for development of the GMP and supplements comprehensive data collection and evaluations from prior hydrogeologic investigation reports (recent to oldest), including, but not limited to, the following:

- NRT, January 24, 2017. Hydrogeologic Site Characterization Report, Ash Pond 2, Coffeen Power Station, Coffeen, Illinois.
 Summarizes the results of numerous hydrogeologic investigations that have been performed at the Site, including recent data collected to comply with 40 C.F.R. § 257 Subpart D (CCR Rule) as well as comprehensive data collection and evaluations from prior hydrogeologic investigation reports.
- NRT, January 24, 2017. Groundwater Management Zone Application, Coffeen Ash Pond No. 2, Coffeen Power Station, Coffeen, Illinois.
 Establishes a three-dimensional Groundwater Management Zone (GMZ) containing groundwater being managed to mitigate a potential release of CCR constituents from Ash Pond No. 2 (AP2).
- NRT, January 24, 2017. Groundwater Monitoring Plan. Coffeen Power Station, Coffeen, Illinois.

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The plan describes the groundwater monitoring and reporting to be completed in support of the Closure Plan for AP2.

• NRT, January 24, 2017. Hydrostatic Modeling Report. Coffeen Power Station, Coffeen, Illinois.

Utilized the Hydrologic Evaluation of Landfill Performance (HELP) model to predict percolation from AP2 and to evaluate AP2 hydrostatic conditions in response to the proposed cover system as described in the Revised 30% Closure Design Package.

• NRT, January 24, 2017. Groundwater Modeling Report. Coffeen Power Station, Coffeen, Illinois.

Included simulations of the site hydrology, the extent of CCR leachate impacts on groundwater and the effect of pond closure on groundwater quality.

• Hanson, April 16, 2016. Corrective Action Plan.

A plan to remediate groundwater exceedances around AP2 and other units. Proposed plan includes reduction in leachate within AP2, enhanced cover system on AP2, and a GMZ.

• AECOM, April 2016. Revised 30% Closure Design Package for Coffeen Power Station Ash Pond No. 2.

A 30% design package for closure of AP2 including the design basis and summary in addition to preliminary construction costs and schedule.

• Hanson, April 2016. Uppermost Aquifer Considerations.

A discussion of the construction of the gypsum pond and relation to the uppermost aquifer in the vicinity of the site.

• Hanson, 2015. G153 Assessment.

Evaluation of manganese, sulfate, and TDS concentrations that were identified at concentrations greater than Class I Groundwater Standards at well G153, which concluded that elevated concentrations were also found upgradient of the Storm Water Runoff Pond and intrawell standards should be utilized.

• Hanson, July 2011. Hydrogeologic Report.

Supports permit applications for the Gypsum Management Facility Gypsum Stack Pond (GMF GSP) and Gypsum Management Facility Recycle Pond (GMF RP).

In conjunction with this report, a GMP is being prepared for AP1.

1.4 Site Location and Background

The CPP is located in Montgomery County, in central Illinois, within Section 11 Township 7 North and Range 7 East. The CPP is approximately two miles south of the city of Coffeen and about eight miles southeast of the city of Hillsboro, Illinois (**Figure 1-1**). AP1 is located between the two lobes of Coffeen Lake (identified as "Coffeen Lake" and "Unnamed Tributary" on **Figures 1-1 and 1-2**) to the west, east, and south, and is bordered by agricultural land to the north. The approximately 1,100-acre Coffeen Lake was built by damming the McDavid Branch of the East Fork of Shoal Creek in 1963 for use as an artificial cooling lake for the CPP. Historically, several coal mines were operated at depth in the vicinity of the CPP as well as a US Minerals processing facility located to the north. **Figure 1-2** is a site map showing the location of AP1 (Part 845 regulated CCR Unit and subject of this HCR), AP2, GMF RP, GMF GSP, and Landfill (LF). The area near AP1 will hereinafter be referred to as the Site.

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1.5 Site History and CCR Units

The CPP was a coal-fired electrical generating plant that began operation in 1964. The plant initially burned bituminous coal from Illinois and CCR from the coal fired units was disposed of in AP1. AP2 was also utilized in the early 1970's and AP1 was reconstructed in 1978. Both of these units were used until the mid-1980's, beginning in 2010 CCR material was placed in the LF and GMF Units.

Ash Pond No. 1 (AP1): This SI (also known as the Bottom Ash/ Recycle Pond) is a reclaimed ash pond that was reconstructed utilizing the existing earthen berms with reinforcement, as provided by Water Pollution Control Permit 1978-EA-389 issued by the Agency on May 26, 1978. AP1 (existing unlined SI) covers an area of approximately 23 acres, has berms up to 41 feet above the surrounding land surface, and a volume of 300 acre-feet. It primarily received bottom ash and low volume wastes from floor drains in the main power block building. Several years ago, air heater wash and boiler chemical cleaning wastes were directed to AP1, but this practice was discontinued. The bottom ash was periodically removed for beneficial uses by a third-party contractor. Sluicing of waste to AP1 ceased prior to November 4, 2019.

Ash Pond No. 2 (AP2): AP2 is a closed (IEPA approved) SI with a surface area of approximately 60 acres and berms 47 feet higher than the surrounding land surface. AP2 was originally removed from service and capped in the mid 1980's. A clay and soil cap was placed on the surface of the pond with contouring and drainage provided to direct storm water to four engineered revetment down drain structures. Prior to capping, this pond was identified as Outfall 004 in the facility National Pollutant Discharge Elimination System (NPDES) operating permit, IL0000108. Additional closure activities include the construction of a geomembrane cover system that began in July 2019 and was completed on November 17, 2020. The construction was completed in accordance with the Closure and Post Closure Care Plan approved by the IEPA on January 30, 2018.

GMF Gypsum Stack Pond (GMF GSP): The 77-acre GMF GSP received blowdown from the air emission scrubbers and was put into operation in 2010. Construction of the GMF GSP was in accordance with Water Pollution Control Permit 2008-EA-4661 and features a composite 60-mil high-density polyethylene (HDPE) liner with 3 feet of recompacted soil with a hydraulic conductivity of 1×10^{-7} centimeters per second (cm/s) with internal piping and drains to collect contact water. Construction of the unit required excavation to approximately 603 feet and installation of a groundwater underdrain system to eliminate inward pressure on the liner prior to placement of CCR. The GMF GSP underdrain was actively pumped during construction but is no longer actively pumped. IPGC ceased receipt of waste to the GMF GSP prior to April 11, 2021.

GMF Recycle Pond (GMF RP): The 17-acre GMF RP received blowdown from the air emission scrubbers and was put into operation in 2010. Construction of the GMF RP was in accordance with Water Pollution Control Permit 2008-EA-4661 and features a composite 60-mil HDPE liner with 3 feet of recompacted soil with a hydraulic conductivity of 1×10^{-7} cm/s with internal piping and drains to collect contact water. Construction of the unit required excavation to approximately 601 feet and installation of a groundwater underdrain system to eliminate inward pressure on the liner prior to placement of CCR. The GMF RP underdrain is a passive, gravity drained system. IPGC ceased receipt of waste to the GMF RP prior to April 11, 2021.

Landfill (LF): Fly ash was managed in a permitted composite lined landfill constructed in 2010. The LF has an active groundwater underdrain system that is currently being pumped.

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Additionally, the ash landfill leachate collection system is restricted by rule to no more than one foot of leachate on the composite liner. An IEPA groundwater monitoring program is in effect for the GMF (under Bureau of Water) and Ash Landfill (under Bureau of Land).

The approximate dates of construction of each successive stage of the CCR Units at the CPP are summarized in **Table A** below (AECOM, 2016).

Table A. History of Construction

| Date | Event |
|-----------|---|
| 1964 | Construction of AP1 (formerly identified as the Bottom Ash Recycle Pond) |
| 1971 | Construction of AP2 |
| 1978-1979 | Installation of internal embankment and new recycle intake structure in AP1 and abandonment of existing outfall structure |
| 1984-1985 | Closure of AP2 by installing a clay cover |
| 2000 | Installation of a sheet pile wall to facilitate construction of drainage flume along the northeast corner of AP1 |
| 2006 | Bottom ash system modified in AP1 |
| 2008-2010 | Construction of the GMF GSP and the GMF RP |
| 2009 | Installation of well dewatering system in AP2 |
| 2015 | Notice of intent to close AP2 |
| 2015 | Closure plans for AP1, AP2, GMF GSP, GMF RP, and LF submitted to IEPA |
| 2018 | IEPA approved Closure and Post-Closure Care Plan for AP2 |
| 2020 | Completion of closure of AP2 with geomembrane cover system |

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2. REGIONAL AND LOCAL GEOLOGY

2.1 Topography

The CPP and embankments surrounding AP1 are located at an elevation of approximately 636 feet North American Vertical Datum of 1988 (NAVD88) with the surrounding areas having low topographic relief, generally at an elevation of around 615 to 620 feet NAVD88 (**Figure 2-1**). East and south of AP1, towards the Unnamed Tributary and Coffeen Lake, the elevation decreases to less than 590 feet NAVD88.

Topographic maps drawn prior to construction (1947) indicate the areas of the CPP were generally from 600 to 640 feet above mean sea level (msl), with elevations at AP1 generally from 600 to 620 feet msl (**Appendix A**). A minor drainage feature was present in the northeast corner of AP1 with an approximate base from 595 to 600 feet msl, although the extent appears to be limited.

2.2 Regional Geomorphology

The CPP is located in the central portion of the Springfield Plain of the Till Plains section, the largest physiographic division in Illinois, covering approximately four-fifths of the state. It is characterized by level to undulatory till plains with a few morainic ridges in a late youthful stage of erosion. The Springfield Plain includes the level to gently undulating portion of the Illinoian drift-sheet in central and south-central Illinois (Leighton et al., 1948; Zuehls et al., 1984). Distinguishing features include flatness and shallow drainage features. Moraines in this region are low and broad. Drainage systems are well developed, and the valleys tend to be shallow, broadly alluviated, and terraced (Leighton et al., 1948). Streams in the western portion of the Springfield Plain primarily flow westward, ultimately into the Mississippi River, while streams in the eastern portion flow eastward ultimately into the Wabash River.

2.3 Soils

Surficial soils at the CPP and vicinity are shown on **Figure 2-2** and based on Montgomery County soil survey data available in the Soil Survey Geographic Database (SSURGO) by the United States Department of Agriculture's Natural Resources Conservation Service provided by Environmental Systems Research Institute, Inc.'s (ESRI's) web hosted layer. Former soils underlying the CPP, not including the Fill and CCR within the limits of AP1 are identified as: Orthents (loamy, undulating) along the boundary, and in the immediate vicinity, of AP1; Ava silt loam (2 to 5 percent slopes), Bunkham silty clay loam (5 to 10 percent slopes, severely eroded), and Hickory silt loam (18 to 35 percent slopes) to the southeast between the unit and the Unnamed Tributary; and Cowden-Piasa silt loams, 0 to 2 percent slopes) near background monitoring well G281.

2.4 Regional Geology

2.4.1 Unlithified Deposits

Pleistocene deposits of unlithified glacial diamictons, lacustrine/alluvial deposits, and windblown loess overlie Pennsylvanian-age bedrock throughout central Illinois. The most extensive glacial deposits are those from the Illinoian Stage which cover much of the state and are present at the CPP. Windblown (aeolian) deposits, the Peoria and Roxana Silts, cover the glacial deposits over a

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majority of the state. These units are fine-grained deposits blown from river valleys by prevailing winds (Hansel and Johnson, 1996).

Surficial deposits, as reported and mapped on a regional scale by the Illinois State Geological Survey (ISGS), are the Vandalia Member (**Figure 2-3**), although the Hagarstown Member has been identified in the vicinity of the CPP. The general sequence of unlithified Quaternary deposits, depicted on **Figure 2-4**, from ground surface down is:

- **Loess Unit:** The loess unit is comprised of the Peoria and Roxana Silts. The Peoria Silt is generally classified and described as light yellow-tan to gray, fine sandy silt. The Roxana Silt is predominately silt-sized material but can be sandier in localized areas and the base of this unit is often colluvium of silt, and sand (Hansel and Johnson, 1996).
- Glasford Formation: Till members present in the surrounding area include (youngest to oldest): the Hagarstown Member, the Vandalia Member, the Mulberry Grove Member, and the Smithboro Member. The Hagarstown Member is bounded at the top by the Sangamon Soil. The Vandalia Member is described as a sandy till with thin lenticular bodies of silt, sand, and gravel. It is calcareous, except where weathered, generally gray, and moderately compact. The member consists of gravelly till, poorly sorted gravel, well sorted gravel, and sand. The Mulberry Grove Member is intermittent at the CPP and is described as a calcareous gray silt and fine sand containing some fossil mollusks. The Smithboro Member is described as a gray, compact, silty till. The Smithboro is bounded below by the Yarmouth Soil (Willman and Frey, 1970).
- **Banner Formation:** Composed primarily of glacial tills and intercalated outwash of sand, gravel, and silt. Members differentiated in western Illinois include the Yarmouth Soil and the Lierle Clay (Hanson, 2009).

2.4.2 Bedrock

Unlithified deposits at the CPP and surrounding areas, described in **Section 2.4.1**, are underlain by rocks belonging to the Pennsylvanian Bond Formation (Kolata, 2005). Detailed descriptions of the Pennsylvanian strata of Illinois were published by Willman et al. (1975). The Bond Formation includes all strata from the base of the Shoal Creek Limestone Member or the LaSalle Limestone Member to the top of the Millersville Limestone Member or the Livingstone Limestone Member. It is overlain by the Mattoon Formation and underlain by the Modesto Formation. It varies from less than 150 feet thick in eastern Illinois to over 300 feet thick in southeastern Illinois, averaging about 250 feet. The Bond Formation is characterized by a high percentage of limestone and calcareous clays and shales. The Bond and Modesto Formations of the McLeansboro Group also contain multiple thin (typically less than 2 feet) intermittent coal beds. The upper formation of the Kewanee Group is the Carbondale Formation which contains multiple coal beds, including the Herrin (No. 6) Coal, of varying thicknesses (up to 7 feet) (ISGS, 2020). It is bound by thick limestone members (up to 50 feet), the thickest and purest limestones in the Pennsylvanian System of Illinois. Gray shales constitute the greatest part of the formation, although thick channel sandstones are developed locally.

The elevation of the bedrock surface in the area ranges from 450 to 500 feet msl. The bedrock surface slopes gently towards the west into a minor bedrock valley that runs north-south (Herzog et al., 1994). Well logs indicate that the lithology of the uppermost bedrock is predominantly shale (Zeizel, 1959).

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2.4.3 Structure

The major geologic structural features around Illinois are shown on **Figure 2-5**. There are no major structural features in Montgomery County. The nearest major structural feature to CPP is the Louden Anticline, which is north-south trending and located approximately 25 miles east of the CPP. Smaller-scale structural features within Montgomery County include the Hillsboro North and Hillsboro South Domes, which are located approximately 15 miles north of the CPP. The Crown Fault, which is a left-lateral fault, and the Girard Fault, which is a northeast dipping normal fault, are located approximately 31 miles northwest of the CPP.

Located south of the CPP in Bond County are the Ayers and Woburn Anticlines and the Greenville Dome. The Ayers Anticline is located approximately 10 miles south of the CPP and trends east-west. The Woburn Anticline is located approximately 10 miles southeast of the CPP and trends north-south. The Greenville Dome is located approximately 15 miles south of the CPP (Nelson, 1995). A review of the available data from the United States Geological Survey (USGS, 2010), ISGS, and other available structural information was completed by Haley & Aldrich, Inc., (2018) for the Location Restriction Demonstration to address the requirements of 40 C.F.R. § 257.62 (Fault Areas). The review found that the nearest known mapped fault is the Crown Fault referenced above, which is located approximately 31 miles northwest of the CPP, and the Centralia Fault zone, located approximately 35 miles southeast of the CPP. The timeframe of the most recent activity on these fault zones is unknown. There are no known active faults or fault damage zones that have had displacement in Holocene time reported or indicated within 200 feet of AP1 (**Figure 2-5**).

2.4.4 Seismic Setting

The nearest areas of present-day fault related, seismic activity are the Northern Illinois Seismic Source Zone, the Wabash Valley Fault Zone near southwestern Indiana, and the New Madrid Fault Zone along the Ohio and Mississippi River Valleys in southeastern Illinois. No recent earthquake epicenters are located in Montgomery County. A magnitude 3.80 earthquake occurred approximately 15 miles south of CPP in Bond County in 1981 and a magnitude 3.60 earthquake occurred approximately 20 miles southeast of CPP in Fayette County in 1990.

35 I.A.C. § 845.330 requires that existing and new CCR SIs and lateral expansions of existing SIs must not be located in seismic impact areas, unless owners or operators demonstrate that the SI is designed to resist the maximum horizontal acceleration (g) in lithified earth material. This requirement is identical to that in 40 C.F.R. § 257.63. The definition of a seismic impact zone is "areas having a 2 percent or greater probability that the maximum expected horizontal acceleration, expressed as a percentage of the earth's gravitation pull, will exceed 0.10 g in 50 years." Although AP1 is located within a seismic impact zone, it satisfies the demonstration requirements of 35 I.A.C. § 845.330. The AECOM report titled "CCR Certification Report: Initial Structural Stability Assessment, Initial Safety Factor Assessment, and Initial Flow Design Control System Plan for the Ash Pond No. 1 at Coffeen Power Station", dated October 2016, includes engineering analysis, calculations, and findings that support the requirements of 40 C.F.R. § 257.63 (Haley & Aldrich, Inc., 2018), and, by extension, 35 I.A.C. § 845.330.

2.4.5 Mining Activities

Several coal mines, both strip and underground types, previously operated in Montgomery County, Illinois. A survey to identify historic mining activities was conducted for a 1,000-meter

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radius around the Site. Based on records obtained from ISGS, two mines were identified within a 1,000-meter radius of AP1. A map showing the extent of historic mines is provided in **Appendix B**.

In the southeast portion of the Site is the Hillsboro Mine (ISGS Mine No. 871), which was operated as a room and pillar panel mine. Operations began in 1964 under the Truax-Traer Coal Company. The mine was purchased by the Consolidation Coal Company in 1971 and production ceased in 1983. An approximately 5- to 7-foot-thick seam of Herrin Coal was mined at approximately 500 feet below ground surface (bgs) (ISGS, 2019). The mine showed indications of small-scale faulting, roof stability issues and floor heaving. AP1 directly overlies the Hillsboro Mine. Mine shafts, processing facilities and some historic coal storage associated with these historic mines was located south of AP1 (**Appendix B**).

To the north/northwest is the Clover Leaf No. 4 Mine (ISGS Mine No. 442), which was operated as a room and pillar panel mine. Operations began in 1906 under the Clover Leaf Mining Company. Production discontinued in 1924 under Clover Leaf Coal Company ownership. An approximately 6- to 8-foot-thick seam of Herrin Coal was mined at approximately 510 feet bgs (ISGS, 2019). AP1 does not overlie the Clover Leaf No. 4 Mine, nor does it fall within the buffer zone of the mine.

2.5 Site Geology

The Quaternary deposits in the vicinity of the CPP consist mainly of diamictons and interbedded outwash deposits that were deposited during Illinoian and Pre-Illinoian glaciations. The CPP geology summarized below is from a combination of the Coffeen Hydrogeologic Monitoring Plan (NRT, an OBG Company [NRT/OBG], 2017) and a field investigation performed in 2021 to collect additional data for the discussion of vertical and horizontal lithology, stratigraphy, chemical properties, and physical properties of geologic layers to a minimum of 100 feet bgs as specified in 35 I.A.C. § 845.620(b). Field investigation locations are shown on **Figure 2-6** and cross-sections are included in **Figure 2-7**. Soil boring logs and well construction logs are provided in **Appendix C**. Samples for geotechnical analysis were collected from interpreted geologic units and composited to obtain a representative sample of the entire geologic unit prior to submittal (**Table 2-1**). The unconsolidated deposits and bedrock which occur at the CPP include the following units (beginning at the ground surface):

- **Fill and CCR Unit:** CCR consisting of bottom ash and other non-CCR waste is present within AP1 and non-CCR fill material consisting of silty clay, sandy lean clay, or lean clay with sand, with trace amounts of fine gravel comprises the berms surrounding AP1.
- **Loess Unit**: Clays and silts, including undifferentiated Roxana Silt and Peoria Silt with thicknesses ranging from 1 to 16 feet, where present at the CPP.
- **Hagarstown Member**: The Hagarstown Member (consisting of gravelly clay till and sandy materials in contact with the Vandalia Member (also referred to as Hagarstown Beds) has been separated into two units for this discussion: the first unit, consisting of the gravelly clay till and the second unit consisting of sandy material overlying the Vandalia Member. The Upper Hagarstown Member is up to 6 feet thick, while the sandy portions, where present, are generally less than 3 feet thick, although thicknesses up to 7 feet have been observed north of the LF.
- Vandalia Member: Sandy, silt, or clay till that is generally greater than 15 feet thick.

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- **Mulberry Grove Member**: Gray silt and sandy silt/clay unit found between the Vandalia Till and the Smithboro Till. Generally thin and not laterally continuous across the CPP.
- **Smithboro Member**: Thick, gray compacted silty clay diamicton.
- **Yarmouth Soil**: Sand and sandy silt/clay, which include accretionary deposits of fine sediment and organic materials, typically less than 5 feet thick and not laterally continuous.
- **Lierle Clay Member:** Clay and silt with some sand which is the upper portion of the Banner Formation. No borings advanced on site penetrated the full thickness of the Lierle Clay.

Soil boring logs and well construction logs are provided in **Appendix C**.

2.5.1 Fill and CCR

CCR (bottom ash) and other non-CCR wastes are present within AP1. CCR sample locations are shown on **Figure 2-6.** The elevation at the top of the fill layer estimated from the topographic surface (**Figure 2-1**) within the limits of AP1 is from approximately 629 to 637 feet NAVD88.

CCR thickness extends approximately 18 feet deep as measured in XPW02 and consists mostly of bottom ash (approximately 90 percent sand sized particles). Average ash thickness in AP1 is approximately 10 feet. AP1 overlies the Loess Unit described in **Section 2.5.2**; however, former drainage features in localized areas eroded through the loess and clay such that the ash fill may be in contact with the sandy portion of the Hagarstown Member (**Section 2.5.3**). The elevation of the bottom of ash is lowest in the eastern portion of the pond and extends to an elevation of approximately 595 to 600 feet (**Appendix A**).

The geotechnical testing results are summarized in **Table 2-1** and the geotechnical laboratory report is included in **Appendix D**. Geotechnical testing results from the CCR material encountered at XPW02 and composited for analysis indicated the following:

- Moisture content is 12.5 percent.
- Calculated porosity is 31.7 percent.
- Dry density is 110.8 pounds per cubic foot (pcf).
- Specific gravity is 2.60.
- Particle size distribution is 0 percent gravel, 90 percent sand, 10 percent fines.
- Vertical hydraulic conductivity was 8.8 x 10⁻⁵ cm/s.

Solids samples collected from XPW01 and XPW02 were also collected for chemical analysis. The results of solids samples collected from within AP1 are summarized in **Table 2-2.** Additionally, leachate wells XPW01 and XPW02 were sampled in 2021. The results of leachate samples collected from within AP1 are summarized in **Table 2-3**.

2.5.2 Loess Unit

The Loess Unit is the uppermost unlithified unit identified at the CPP. This unit is comprised of the combined Roxana and Peoria Silt and extends from beneath the topsoil, derived from the loess, to the top of the Hagarstown Member. The loess has been classified as silt or clayey silt, with minor amounts of sand. The Loess Unit is generally considered unsaturated, and the uppermost aquifer is recharged by precipitation that percolates through this unit.

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The top of the Loess Unit was typically encountered from approximately 606 to 628 feet NAVD88. Loess Unit thickness ranges from 0 feet (absent) to 16 feet. Construction of the LF, GMF GSP, and GMF RP required the excavation and removal of this layer within the unit footprints. The Loess Unit is typically thickest to the north, and is absent near historic drainage features to the south.

During the 2021 investigation of AP1, the Loess Unit was typically encountered from 1 to 4 feet bgs, at elevations of approximately 605 to 625 feet NAVD88, and was generally 8 to 14 feet thick, where present near AP1. CCR borings XPW01 and XPW02 encountered the Loess Unit at approximately 13 and 18 feet bgs, at an elevation of approximately 619 feet NAVD88 at both locations. The Loess Unit was absent in borings G314, G314D, and G316, advanced along the eastern lobe of Coffeen Lake and located near the Unnamed Tributary.

The geotechnical testing results are summarized in **Table 2-1** and geotechnical laboratory report is included in **Appendix D**. Geotechnical testing results from the Loess Unit indicated the following:

- Average moisture content is 18.6 percent and ranges from 16.5 to 21.6 percent.
- Average calculated porosity is 31.2 percent and ranges from 29.8 to 33.5 percent.
- Average dry density is 109.9 pounds per cubic foot (pcf) and ranges from 105.0 to 115.7 pcf.
- Average specific gravity is 2.61 and ranges from 2.59 to 2.64.
- Particle size distribution is 0 percent gravel, 33 to 35 percent sand, and 65 to 67 percent fines (37 to 41 percent silt and 28 to 35 percent clay).

Soil samples collected from the Loess Unit were also submitted to an analytical laboratory for chemical analysis. The results of this chemical analysis are summarized in **Table 2-4**.

2.5.3 Hagarstown Member

The Hagarstown Member (also referred to as Hagarstown Beds) exhibits two units: the first unit consisting of the gravelly clay till and the second consisting of sandy material overlying the Vandalia Member. The clay till portion had varying thicknesses ranging from approximately 2 to 6 feet as observed adjacent to, south, and west of the Pond. This unit underlies 95 percent of AP1, and the clayey portion is up to 6 feet thick. The thickness of the sandy portion of the Hagarstown is generally 1 to 2 feet thick. The composition of the sandy portion of the Hagarstown unit varies across the CPP and has been classified as gravelly till, poorly sorted gravel, well sorted gravel, sand, and silty sand. Based on the historic topographic map (Appendix A), the Hagarstown Member is not present in former drainage features (i.e., the northeast corner of AP1).

During construction of the LF, GMF GSP, and the GMF RP, the Loess Unit and the Hagarstown Member were excavated to facilitate construction and eliminate groundwater flow into excavations. The excavations were backfilled with structural fill and an underdrain system was installed to mitigate inward hydraulic pressure and potential liner uplift damage before the CCR units were filled. The LF underdrain system remains but is no longer actively pumped. The GMF GSP underdrain system has not been actively pumped since construction was completed. The GMF RP gravity underdrain remains in place.

Where present the sandy portion of the Hagarstown is generally 2 to 4 feet thick. The composition of the sandy portion of the Hagarstown unit varies across the CPP and has been

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classified as gravelly till, poorly sorted gravel, well sorted gravel, sand, and silty sand. The elevation of the top of the Hagarstown generally declines as the unit approaches Coffeen Lake or other topographic drainage features.

During the 2021 investigation, the sandy portion of the Hagarstown Member near AP1 was generally encountered from 9 to 34 feet bgs, at elevations of approximately 603 to 611 feet NAVD88, and was generally 1 to 5 feet thick, where present (**Figure 2-7**).

The geotechnical testing results are summarized in **Table 2-1** and the geotechnical laboratory report is included in **Appendix D**. Geotechnical testing results from the Hagarstown Member indicated the following:

- Average moisture content is 14.3 percent and ranges from 11.4 to 19.2 percent.
- Average calculated porosity is 24.6 percent and ranges from 24.2 to 25.1 percent.
- Average dry density is 125.1 pcf and ranges from 123.4 to 126.8 pcf.
- Average specific gravity is 2.64 and ranges from 2.59 to 2.68.
- Particle size distribution is 0 to 14 percent gravel, 28 to 79 percent sand, and 7 to 72 percent fines (7 to 52 percent silt and 0 to 26 percent clay).

Soil samples collected from the Hagarstown Member were also submitted to an analytical laboratory for chemical analysis. The results of this chemical analysis are summarized in **Table 2-4**.

2.5.4 Vandalia Member

The Vandalia (Till) Member is a sandy/silty till with thin, discontinuous lenses of silt, sand, and gravel. The Vandalia Member was encountered in all borings advanced at the CPP. The Vandalia Member typically ranged in thickness from 11.7 feet in the northern portion of the CPP, to 31.0 feet between the GMF GSP and the GMF RP. Similar to the observed top elevation of the Hagarstown Member, the top of the Vandalia Member declines in elevation near Coffeen Lake and topographic drainage features. This unit is relatively thick throughout the CPP, with an average thickness of over 15 feet (Hanson, 2009).

During the 2021 investigation, the Vandalia Member was encountered from 1.5 to 34 feet bgs, at elevations of approximately 598 to 608 feet NAVD88, where present.

The geotechnical testing results are summarized in **Table 2-1** and the geotechnical laboratory report is included in **Appendix D**. Geotechnical testing results from the Vandalia Member indicated the following:

- Average moisture content is 12.7 percent and ranges from 8.7 to 16.2 percent.
- Average calculated porosity is 23.3 percent and ranges from 18.9 to 27.6 percent.
- Average dry density is 122.2 pcf and ranges from 115.7 to 131.6 pcf.
- Average specific gravity is 2.59 and ranges from 2.56 to 2.61.
- Particle size distribution is 0 percent gravel, 26 to 44 percent sand, 56 to 74 percent fines.

Soil samples collected from the Vandalia Member were also submitted to an analytical laboratory for chemical analysis. The results of this chemical analysis are summarized in **Table 2-4**.

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2.5.5 Mulberry Grove Member

The Mulberry Grove (Silt) Member typically consists of a thin, lenticular unit of gray sandy silt (Willman et al., 1975). It represents the interval between the retreat of the glacier that deposited the Smithboro Member and the advance of the glacier that deposited the Vandalia Member. At the CPP, the Mulberry Grove Member is represented by pockets (generally less than 2 feet thick) of gray sandy silt. This unit was absent in many borings through the central portion of the CPP from south to north. Where sampled, the Mulberry Grove Member ranged in thickness from 0.5 to 4.9 feet near the GMF GSP (Hanson, 2009). During the 2021 investigation, the Mulberry Grove Silt was not encountered in the borings near AP1. These silts appear to be deposited in depressions found in the surface of the underlying Smithboro Member.

2.5.6 Smithboro Member

The Smithboro (Till) Member is described as a gray, compact, silty, clayey diamicton. The Smithboro Member ranges in thickness from 6.7 to 21.2 feet northwest of the landfill.

The geotechnical testing results are summarized in **Table 2-1** and the geotechnical laboratory report is included in **Appendix D**. Geotechnical testing results from the Smithboro Member indicated the following:

- Average moisture content is 15.5 percent and ranges from 15.0 to 16.6 percent.
- Calculated porosity of the G311D sample is 28.5 percent and 29 percent for G314D.
- Average dry density is 115.9 pcf and ranges from 114.2 to 118.8 pcf.
- Average specific gravity is 2.58 and ranges from 2.56 to 2.61.
- Particle size distribution of the samples collected from G311D and G314D is 0 percent gravel, 26-28 percent sand, 72-74 percent fines.

Soil samples collected from the Smithboro Member were also submitted to an analytical laboratory for chemical analysis. The results of this chemical analysis are summarized in **Table 2-4**.

2.5.7 Yarmouth Soil

The Yarmouth Soil is described as the weathered zone on the Kansan drift, but in some places, it consists of accretionary deposits of fine sediment and organic material that accumulated in poorly drained areas on the surface of the Kansan deposits. Historical borings in the northern portion of the CPP which encountered the Yarmouth were summarized previously by Hanson (2009) as ranging in thickness from 0 feet (absent) to 5.1 feet.

During the 2021 investigation, the Yarmouth Soil was encountered from 46 to 55 feet bgs, at an elevation from approximately 565 to 577 feet NAVD88, and was 1 to 3 feet thick, where present. The measured thickness was consistent with previous investigations.

The geotechnical testing results are summarized in **Table 2-1** and the geotechnical laboratory report is included in **Appendix D**. Geotechnical testing results from the Yarmouth Soil indicated the following:

• Moisture content of the G314D sample is 14.9 percent.

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- No samples were analyzed for dry density. Therefore, average porosity was not calculated for the Yarmouth Soil. Based on material type encountered in the borings, the effective porosity is expected to range from 10 to 28 percent (Fetter, 2001).
- Specific gravity of the G314D sample is 2.61.
- Particle size distribution of the G314D sample is 0 percent gravel, 84 percent sand, 16 percent silt, and 0 percent clay.

Soil samples collected from the Yarmouth Soil were also submitted to an analytical laboratory for chemical analysis. The results of this chemical analysis are summarized in **Table 2-4**.

2.5.8 Lierle Clay Member/ Banner Formation

The Lierle Clay Member is the uppermost member of the Kansan Stage Banner Formation. It is described as an accretion-gley with clay, silt, and some sand. It was encountered by Hanson (2009) in all but a few borings on site. During the 2021 investigation, borings G307D, G311D, and G314D encountered the Lierle Clay at approximately 47 to 57 feet bgs, at approximate elevations from 564 to 575 feet NAVD88. No borings penetrated the full thickness of the Banner Formation near AP1.

The geotechnical testing results are summarized in **Table 2-1** and the geotechnical laboratory report is included in **Appendix D**. Geotechnical testing results from the Lierle Clay Member indicated the following:

- Average moisture content is 14 percent and ranges from 8.7 to 18.9 percent, typically decreasing with depth.
- Average calculated porosity is 27.6 percent and ranges from 19.2 to 33.2 percent.
- Average dry density is 118.8 pcf and ranges from 108.0 to 134.6 pcf.
- Average specific gravity is 2.64 and ranges from 2.58 to 2.73.
- Particle size distribution is 0 percent gravel, 16 to 24 percent sand, and 76 to 84 percent fines.

Soil samples collected from the Lierle Clay were also submitted to an analytical laboratory for chemical analysis. The results of this chemical analysis are summarized in **Table 2-4**.

2.5.9 Bedrock

Pennsylvanian-age Bond Formation bedrock was not encountered in any borings advanced at the CPP, so site-specific information is not available.

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3. REGIONAL AND LOCAL HYDROGEOLOGY

3.1 Regional Hydrogeology

The water table conforms more or less to the topographic features of the land surface. Recharge occurs in the uplands and flows towards drainage features. Moderate thicknesses of unconsolidated materials fill shallow valleys or are present on the uplands bordering the main valleys. These materials contain thin and discontinuous deposits of sand and gravel. Potable water in Montgomery County is primarily serviced by the Hillsboro and Litchfield Water Departments. Surface water of Lake Glenn Shoals and Old Hillsboro Lake serves Hillsboro, Illinois, and the surrounding communities (e.g., Coffeen) (Hillsboro, 2021). Groundwater for domestic and farm supplies is obtained locally in this area from wells drilled in sand and gravel, but in some places good water-yielding deposits are absent and water from the unconsolidated material is obtainable only with large-diameter dug wells (Selkregg et al., 1957).

3.2 Site Hydrogeology

Over 100 monitoring wells have been installed since 2006 to monitor groundwater conditions around the five CCR units at the CPP for both State and Federal programs. Two monitoring wells were installed in 2010 near AP1. From 2015 to 2017, five additional wells and piezometers were installed around AP1 to meet requirements of the CCR Rule. In 2021, thirteen additional wells were installed around AP1 to provide information to meet requirements of Part 845. A summary of the current monitoring well networks, and construction details, is included in **Table 3-1** and locations shown on **Figure 3-1**. This section discusses the recently (2021) collected information, focusing on the existing well network and monitoring wells installed after 2015 around AP1, as well as appropriate historical data from wells installed prior to 2015.

3.2.1 Hydrostratigraphic Units

Six hydrostratigraphic units have been identified at the CPP based on stratigraphic relationships and common hydrogeologic characteristics, and are summarized as follows:

- **CCR**: This unit is composed of CCR, consisting primarily of bottom ash. This also includes earthen fill deposits of predominantly silt and clay materials from on-site excavations that were used to construct berms and roads surrounding the various impoundments across the CPP.
- **UCU**: Consists of the Loess Unit and the upper clayey portion of the Hagarstown Member which has generally lower vertical permeability and generally greater than 60 percent fines (**Table 2-1**). This Unit was encountered across most of the CPP, with the exception of the eastern edges of AP1 near the Unnamed Tributary where the unit was eroded following deposition or locations where it has been excavated for construction.
- **Uppermost Aquifer**: This unit consists primarily of sand and sandy silts and clays at the base of the Hagarstown Member and, in some locations, the uppermost weathered sandy clay portion of the Vandalia Member. This unit is absent in several locations due to weathering and in others due to excavation during construction of the CCR Unit. The hydraulic characteristics of the Hagarstown Member indicate the unit has a moderate hydraulic conductivity.
- **LCU**: This unit is composed of the sandy clay till of the Vandalia Member, the silt of the Mulberry Grove Formation, and the compacted clay till of the Smithboro Member. The unit

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underlies the uppermost aquifer and was encountered in all boring locations on the CPP. Results from laboratory tests completed for vertical hydraulic conductivity indicate the Vandalia Member has a very low vertical hydraulic conductivity.

- **DA**: This unit consists primarily of sandy silt and sands of the Yarmouth Soil, which are thin (less than 5 feet) and discontinuous across the CPP.
- **DCU**: This unit underlies the DA and is composed of the Banner Formation, of which the thick Lierle Clay is the first encountered unit. No boring penetrated the full thickness of this formation.

3.2.2 Uppermost Aquifer

The base of the Hagarstown Member is identified as the uppermost aquifer on Site. The sandy clay and sand of the uppermost aquifer is confined except where site excavations and ravines extend through the Loess Unit into the Hagarstown Member. The top of the uppermost aquifer was evaluated with respect to the location restrictions in 2018 (Haley & Aldrich, Inc., 2018) and provided in **Figure 3-2**. The top of the uppermost aquifer is separated from overlying CCR material by the low permeability Loess and Hagarstown Member Till (**Figure 2-7**). The base of the uppermost aquifer is the top of the LCU which is comprised of the low permeability Vandalia Member, Mulberry Grove Member, and Smithboro Till.

3.2.3 Potential Migration Pathways

Potential migration pathways (PMPs) were interpreted using the lithologic composition and hydrogeologic properties (hydraulic conductivity, hydraulic position with respect to the unit) of the screened materials. In addition to the physical properties, the analytical results from the baseline groundwater monitoring performed in wells screened in the confining units and DA were used to identify PMPs. The uppermost aquifer is the first occurrence of groundwater and therefore the PMPs identified are in geologic units located below the uppermost aquifer. Monitoring wells G307D, G311D, G314, and G316 are considered LCU PMP monitoring locations and G314D is considered a DA PMP monitoring location. Wells G307D, G311D, G314, and G316 evaluate the potential for migration of impacts through the LCU where the uppermost aquifer is absent.

3.2.4 Water Table Elevation and Groundwater Flow Direction

Porewater monitoring wells XPW01 and XPW02 were installed during the 2021 investigation to collect porewater samples and water elevations within AP1, and staff gauge XSG-01 was installed to monitor pond water levels in AP1. The phreatic surface in AP1 showed minimal variation, with elevations from approximately 629 to 630 feet NAVD88 (**Appendix E**).

No monitoring wells were installed in the UCU during 2021 investigation activities and no wells have historically been installed across solely the UCU because it is not present or is unsaturated in portions of the CPP.

During the 2021 Part 845 investigation, groundwater elevations in the uppermost aquifer ranged from approximately 591 to 625 feet NAVD88 across the CPP (**Appendix E**). Groundwater elevations were typically highest towards the northern extent of the CPP, near the GMF GSP and GMF RP, except monitoring well G307 south of AP1, which consistently had the highest groundwater elevation. Groundwater elevations were lowest near the Unnamed Tributary and east of AP1 towards Coffeen Lake. Groundwater elevations in the vicinity of AP1 were typically from 591 to 621 feet NAVD88, with the exception of G307 as noted above, which was typically

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around 624 feet NAVD88 (**Figures 3-3 and 3-4**). No seasonal variation has been observed in the uppermost aquifer monitoring wells, and any seasonal responses may be muted by the proximity and hydraulic connection to Coffeen Lake.

Overall groundwater flow within the uppermost aquifer is divided towards the two lobes of Coffeen Lake. The groundwater divide runs approximately through the center of the CPP, with groundwater east of the divide flowing east to southeast towards the Unnamed Tributary or the eastern lobe and groundwater west of the divide flowing west to southwest towards the western lobe. Groundwater flows north to northeast across AP1 (**Figures 3-3 and 3-4** and **Appendix E**) toward the former discharge structure and Unnamed Tributary. Although elevations vary seasonally, the groundwater flow direction in the uppermost aquifer is consistent and likely controlled by the proximity and hydraulic connection to Coffeen Lake.

Monitoring wells G206D, G275D, and G314D are screened across the DA. Groundwater elevation within the DA typically ranges from 567 to 590 feet NAVD88. G314D is nearest AP1 and typically has groundwater elevations ranging from about 567 to 573 feet NAVD88. Groundwater contour maps are not generated for the DA; however, groundwater flow within the DA is expected to generally follow subsurface topography for the unit.

3.2.4.1 Vertical Hydraulic Gradient

Vertical hydraulic gradients were calculated using available groundwater elevation data from March through July 2021, and from historic readings from 2017 to 2019, at nested well locations within the uppermost aquifer, LCU, and DA. Vertical hydraulic gradients for AP1 are presented in **Table 3-2**. Vertical hydraulic gradients for other nested well locations at the CPP are included in **Appendix E**. The results of the vertical hydraulic gradient calculations between hydrostratigraphic units are summarized below:

- Uppermost aquifer to Upper LCU (Vandalia Member)
 - In 2021, vertical gradients in well nest G405/T408, located north of AP2, were consistently downward, with an average vertical gradient of 0.03 feet per foot (ft/ft).
 From 2017 to 2020, vertical gradients in well nest G405/T408 varied between upward and downward, with an average (downward) vertical gradient of 0.04 ft/ft.
 - In 2021, vertical gradients in well nest G406/T409, located south of AP2 / northwest of AP1, were consistently upward, with an average vertical gradient of -0.18 ft/ft. From 2017 to 2020, vertical gradients in well nest G406/T409 varied between upward and downward, with an average (downward) vertical gradient of 0.02 ft/ft.
- Uppermost aquifer to Lower LCU (Smithboro Member)
 - During 2021, vertical gradients at well nest G307/G307D, located south of AP1, were downward, with an average vertical gradient of 0.05 ft/ft. In well nest G311/G311D gradients were consistently strongly downward, with an average vertical gradient of 0.93 ft/ft.
- Upper LCU (Vandalia Member) to Lower LCU (Smithboro Member)
 - In 2021, vertical gradients at well nest T408/G45D, located north of AP2, were consistently downward with an average vertical gradient of 0.20 ft/ft. The direction is consistent with measurements from 2017 to 2020 although less than the average downward gradient measured (2.02 ft/ft).

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 In 2021, vertical gradients at well nest T409/G46D, located near the southwest corner of AP2 / northwest of AP1, were downward with an average vertical gradient of 0.25 ft/ft.
 This direction is consistent with measurements from 2017 to 2020, although less than the average downward vertical gradient measured (1.28 ft/ft).

LCU to DA

 During 2021, vertical gradients in well nest G314/G314D, located east of AP1, were consistently strongly downward, with an average vertical gradient of 1.32 ft/ft.

Vertical hydraulic gradients indicate there is consistently downward migration of groundwater in most areas of the CPP, with the exception being northwest of AP1, where consistent upward gradients were measured between the upper LCU and UA in 2021.

3.2.4.2 Impact of Existing Ponds and Ash Saturation

Groundwater surface does not appear to be affected by water levels in AP1. Changes in pond elevations in 2021 are minimal, and do not result in, or vary with, corresponding changes in groundwater elevations. Comparisons of the base of ash elevations at XPW01 and XPW02 and the top of the uppermost aquifer elevations at nearby wells (G304, G307, and G307D) indicate that at least 8 to 10 feet of the UCU is present and limits hydraulic connection between the aquifer and the SI.

In the northeast corner of AP1, the historic land surface contours suggest CCR may have been placed at elevations as low as 595 to 600 feet, while nearby wells (G312, G313, G314) indicate the top of the uppermost aguifer ranges from 599 to 604 feet NAVD88.

3.2.4.3 Impact of Coffeen Lake on Groundwater Flow

Groundwater contour maps prepared from elevation data measured in monitoring wells indicate groundwater elevations can be variable, but flow directions are generally consistent. Groundwater generally flows from the center of the CPP west towards Coffeen Lake, and east towards the Unnamed Tributary, the eastern lobe of Coffeen Lake, and the discharge flume, resulting in a groundwater divide (high) running through the middle of the CPP.

Construction of the LF, GMF GSP, and GMF RP required removal of the Hagarstown Member, in effect removing the aquifer beneath the footprint of these units (Hanson, 2016). It is uncertain whether these constructed units significantly limit lateral groundwater flow, either by creating no flow zones or by capturing groundwater via their dewatering (NRT, 2017).

3.2.5 Hydraulic Conductivities

3.2.5.1 Field Hydraulic Conductivities

Field hydraulic conductivity tests were performed by Hanson in 2021 as part of characterization efforts to complete Part 845 requirements. Individual field hydraulic conductivity test results conducted at the AP1 are summarized in **Table 3-3** and the field hydraulic conductivity data is included in **Appendix F**. The results of the tests are summarized as follows:

• **Uppermost aquifer:** Hydraulic conductivities near AP1 ranged from 2.6×10^{-4} to 9.1×10^{-3} cm/s. Tests had a geometric mean of 2.0×10^{-3} cm/s. This is generally consistent with, although higher than, tests conducted prior to 2017 as part of CCR Rule characterization efforts that

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indicated hydraulic conductivities varied from 1.7×10^{-5} to 2.1×10^{-3} cm/s with a geometric mean of 2.9×10^{-4} cm/s (NRT, 2017).

- **LCU:** Hydraulic conductivities ranged from 1.2 x 10⁻⁴ to 2.3 x 10⁻³ cm/s. Tests had a geometric mean of 5.0 x 10⁻⁴ cm/s. Monitoring wells with the highest hydraulic conductivities were located near the GMF RP and wells with the lowest hydraulic conductivities were located near AP1. Prior to 2017, field hydraulic conductivity tests completed in the LCU for monitoring well and temporary piezometers (G45D, G46D, T408, and T409) indicate horizontal conductivities from 4.0 x 10⁻⁸ to 3.4 x 10⁻⁵ cm/s. The elevated hydraulic conductivity values (10⁻⁴ to 10⁻³ cm/s) in LCU wells are likely not representative of the primary LCU lithology, but instead reflect the isolated and discontinuous sandy lenses in which the wells are screened (NRT, 2017).
- **DA:** Geometric mean hydraulic conductivity at DA well G314D, near AP1, was 8.7×10^{-5} cm/s and was slightly lower than tests completed in the northern portion of the CPP in 2009 that resulted in hydraulic conductivity values ranging from 1.3×10^{-4} to 1.7×10^{-3} cm/s, with a geometric mean of 4.4×10^{-4} cm/s (NRT, 2017).
- No monitoring wells are screened only within the DCU, and no field hydraulic conductivity tests were conducted for the DCU.

3.2.5.2 Laboratory Hydraulic Conductivities

Falling head permeability tests (ASTM D5084 Method F) were performed in the laboratory on nine samples collected primarily from CCR and confining units at the CPP during the 2021 investigations. Samples collected from locations near AP1 are shown on **Figure 2-6** The geotechnical laboratory report is provided in **Appendix D**. The results are summarized in **Table 2-1** and discussed below.

• **CCR:** One geotechnical sample of CCR (ash) was collected at XPW02 and the vertical hydraulic conductivity is 8.8×10^{-5} cm/s.

• UCU:

- Vertical hydraulic conductivities of samples collected from G307D and G311D near AP1 are 4.8×10^{-8} and 2.9×10^{-8} cm/s, respectively. These values are consistent with historically reported values.
- Geotechnical tests conducted prior to 2017 indicated UCU vertical hydraulic conductivity values ranging from 1.3×10^{-8} to 5.0×10^{-7} cm/s, with a geometric mean of 1.0×10^{-7} cm/s (NRT, 2017).
- **Uppermost Aquifer:** One geotechnical sample of uppermost aquifer material was collected from G275D, near the GMF RP, with a vertical hydraulic conductivity of 1.6 x 10⁻⁴ cm/s. No uppermost aquifer samples collected near AP1 were analyzed for vertical hydraulic conductivity.

• LCU:

Three samples collected from G307D, G311D, and G314D, near AP1, have vertical hydraulic conductivities ranging from 5.5×10^{-8} to 3.7×10^{-7} cm/s, with a geometric mean of 1.8×10^{-7} cm/s. Vertical hydraulic conductivities from 2021 are consistent with those observed historically.

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- Intermittently present within the LCU is the Mulberry Grove Member. Historic vertical hydraulic conductivities of the Mulberry Grove Member were measured as 1.6 x 10^{-6} and 1.9×10^{-6} cm/s.
- Historic laboratory tests reported LCU hydraulic conductivity values ranging from 6.8×10^{-9} to 4.5×10^{-6} cm/s, with a geometric mean of 3.0×10^{-8} cm/s (NRT, 2017).
- DA: No laboratory vertical hydraulic conductivity tests were completed during 2021 on DA materials.
- **DCU**: No laboratory vertical hydraulic conductivity tests were completed during 2021 on DCU materials. Historic vertical hydraulic conductivity tests were performed on samples collected north and west of the GMF GSP. Vertical hydraulic conductivities of 6.8×10^{-9} and 4.5×10^{-6} cm/s were reported (NRT, 2017).

3.2.6 Horizontal Groundwater Gradients and Flow Velocity

Horizontal gradient and flow velocities are calculated using the flow path from G308 to G301. Horizontal gradients range from 0.004 to 0.005 ft/ft, equating to a minimum flow velocity of 0.19 feet/day (ft/day) and a maximum flow velocity of 0.24 ft/day. Average calculated flow velocity across AP1 is 0.22 ft/day (**Table 3-4**).

Horizontal gradient and flow velocities were also calculated using the flow path from G315 to G312. Horizontal gradients are from 0.009 to 0.012 ft/ft, equating to a minimum flow velocity of 0.71 ft/day and a maximum flow velocity of 0.95 ft/day. Average calculated flow velocity across AP1 is 0.91 ft/day (**Table 3-4**).

3.2.7 Groundwater Classification

Per 35 I.A.C. § 620.210, groundwater within the uppermost aquifer at AP1 meets the definition of a Class I - Potable Resource Groundwater based on the following criteria:

- Groundwater in the uppermost aquifer is located 10 feet or more below the land surface and
- Within a geologic material which is capable of a hydraulic conductivity of 1 x 10⁻⁴ cm/s or greater using a slug test (**Table 3-3**).

3.3 Surface Water Hydrology

3.3.1 Climate

Average climatic data was obtained from the National Oceanic and Atmospheric Administration National Centers for Environmental Information Climate Data Online. The data was recorded between 2001 and May 2021 from Hillsboro, Illinois, which is located approximately eight miles northwest of CPP. The data includes monthly maximum and monthly minimum daily temperatures (degrees Fahrenheit [°F]) and average rainfall for each month calculated from daily values collected over the 20-year period. The data is summarized in **Table B** below.

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Table B: Average Monthly Temperature Extremes and Precipitation for Hillsboro, IL

| | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | Annual |
|--------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|--------|
| Maximum Temperature (°F) | 38.4 | 42.8 | 54.8 | 67.2 | 77.2 | 86.1 | 88.4 | 86.0 | 82.3 | 69.5 | 54.2 | 44.9 | 66.3 |
| Minimum Temperature (°F) | 22.3 | 24.5 | 34.9 | 44.3 | 55.4 | 64.2 | 67.2 | 64.7 | 58.6 | 46.6 | 34.5 | 28.3 | 45.8 |
| Precipitation (inches) | 1.94 | 2.14 | 2.78 | 5.72 | 4.18 | 4.64 | 3.71 | 3.37 | 2.77 | 3.29 | 2.88 | 2.95 | 40.4 |

https://www.ncei.noaa.gov/orders/cdo/2651630.csv

3.3.2 Surface Waters

The primary surface water body in the area, Coffeen Lake, is comprised of two lobes (identified as "Coffeen Lake" and "Unnamed Tributary" on **Figure 1-2**). The main body of Coffeen Lake is immediately adjacent to CPP on the west and south and the Unnamed Tributary borders CPP to the east.

In 1963, a 75-foot-high earthen dam was built across the McDavid Branch of East Fork Shoal Creek, creating Coffeen Lake for use as an artificial cooling lake for CPP. Coffeen Lake covers approximately 1,100 acres. The lake is part of the Shoal Creek Watershed (Hydrologic Unit Code [HUC] 07140203), which encompasses approximately 916 square miles. The average depth of Coffeen Lake is approximately 19 feet and the maximum depth is approximately 59 feet (Illinois Department of Nature Resources [IDNR], 2014). The average elevation of Coffeen Lake is approximately 591 feet NAVD88.

A USGS stream gage (USGS 05593900) for East Fork Shoal Creek near Coffeen, Illinois (latitude 39.1347 degrees north, longitude 89.3525 degrees west) is located approximately 6.5 miles northeast (upstream) of CPP. The gage datum elevation is 574.76 feet National Geodetic Vertical Datum of 1929 (NGVD29) (574.39 feet NAVD88). Daily gage heights for the period of January 1, 2018 through March 30, 2021 are shown below in **Figure A** (USGS, 2021). The gage height of approximately 2 feet, representing approximate baseflow, occurs at an elevation of about 576.39 feet NAVD88.

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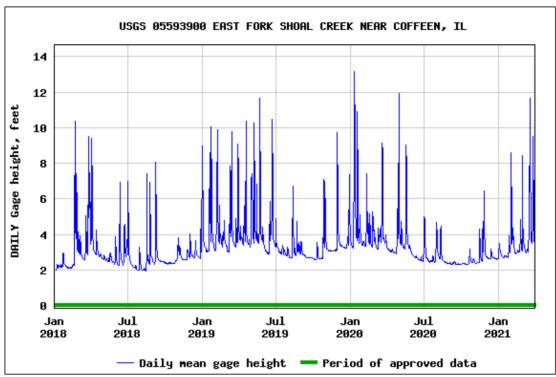


Figure A. Daily Gage Height of East Fork Shoal Creek (USGS 05593900)

Historically, Coffeen Lake received water discharge from both CPP and the Hillsboro Mine in additional to natural precipitation and drainage from East Fork Shoal Creek. At present, Coffeen Lake receives discharge from CPP under NPDES Permit No. IL 0000108. Additionally, an emergency spillway, located at the northeast corner of the GMF RP, discharges to the Unnamed Tributary, east of the CPP.

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4. GROUNDWATER QUALITY

4.1 Summary of Groundwater Monitoring Activities

In 2015, additional well installation and groundwater sampling was initiated to meet the requirements of 40 C.F.R. § 257. Groundwater samples were collected, and totals analyses were completed for Appendix III and Appendix IV parameters. In 2021, additional wells were installed to comply with Part 845; wells were sampled for the parameters listed in 35 I.A.C. § 845.600. A review and summary of data from both the 40 C.F.R. § 257 and Part 845 monitoring programs is included in the evaluation of groundwater quality at the Site.

4.1.1 40 C.F.R. § 257 Program Monitoring and Well Network

The 40 C.F.R. § 257 monitoring well network consists of six monitoring wells screened in the uppermost aquifer, including two background monitoring wells (G281 and G306) and four compliance wells (G301, G302, G303, and G307). Monitoring well G304, originally in the 40 C.F.R. § 257 monitoring well network, was abandoned and replaced by G307. The boring logs, well construction forms, and other related monitoring well forms for the 40 C.F.R. § 257 monitoring well network are included in **Appendix C** of this HCR. The well locations are shown on **Figure 3-1**.

40 C.F.R. § 257 monitoring well network groundwater samples are collected and analyzed for the laboratory parameters from Appendix III and Appendix IV of 40 C.F.R. § 257 as summarized in **Table C** below.

Table C. 40 C.F.R. § 257 Groundwater Monitoring Program Parameters

| Field Parameters ¹ | | | | | | |
|-------------------------------|-------------------------|----------|------------|--|--|--|
| Groundwater Elevation | рН | | | | | |
| Appendix III Paramete | ers (Total, except TDS) | | | | | |
| Boron | Chloride | Sulfate | | | | |
| Calcium | TDS | Fluoride | | | | |
| Appendix IV Paramete | rs (Total) | | | | | |
| Antimony | Beryllium | Cobalt | Molybdenum | | | |
| Arsenic | Cadmium | Lead | Selenium | | | |
| Barium | Chromium | Lithium | Thallium | | | |
| Radium 226 and 228 combined | | | | | | |

¹ Dissolved oxygen, temperature, specific conductance, and oxidation/reduction potential, and turbidity were recorded during sample collection.

4.1.2 Part 845 Well Installation and Groundwater Monitoring

In 2021, thirteen additional monitoring wells (G307D, G308, G309, G310, G311, G311D, G312, G313, G314, G314D, G315, G316, and G317), two CCR source sample collection points (XPW01 and XPW02), and three staff gauges (SG02, SG03, and XSG01) were installed around Coffeen AP1 to assess the vertical and horizontal lithology, stratigraphy, chemical properties, and physical properties of geologic layers to a minimum of 100 feet bgs as specified in 35 I.A.C. § 845.620(b). The boring logs, well construction forms, and other related monitoring well forms for the monitoring well network are included in **Appendix C** of this HCR.

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Prospective Part 845 monitoring wells were sampled for eight rounds from February to August 2021 and the results were assessed for selection of the AP1 Part 845 monitoring well network presented in the GMP. Samples were collected from the new monitoring points and analyzed for 35 I.A.C. § 845.600 parameters summarized in **Table D** below. Part 845 groundwater monitoring results are discussed below in **Section 4.2**.

Table D. Part 845 Groundwater Monitoring Program Parameters

| Field Parameters ¹ | | | |
|-------------------------------|-----------------------|-----------|------------|
| pH | Groundwater Elevation | Turbidity | |
| Metals (Total) | | | |
| Antimony | Boron | Cobalt | Molybdenum |
| Arsenic | Cadmium | Lead | Selenium |
| Barium | Calcium | Lithium | Thallium |
| Beryllium | Chromium | Mercury | |
| Inorganics (Total) | | | |
| Fluoride | Sulfate | Chloride | TDS |
| Other (Total) | | | |
| Radium 226 and 228 | combined | | |

¹ Dissolved oxygen, temperature, specific conductance, and oxidation/reduction potential were recorded during sample collection.

4.2 Groundwater Monitoring Results and Analysis

Groundwater data collected from the AP1 40 C.F.R. § 257 network monitoring wells from 2015 to 2021 were supplemented with sampling of additional locations in 2021 and evaluated with respect to standards included in 35 I.A.C. § 845.600(a)(1). This data set was selected because it includes parameters (total metals) consistent with the parameter list in 35 I.A.C. § 845.600(a)(1). Based on this data set there were no concentrations of antimony, barium, calcium, chloride, fluoride, mercury, molybdenum, selenium, or thallium greater than the GWPSs. Results indicate that the parameters discussed in the following sections were detected at concentrations greater than the applicable 35 I.A.C. § 845.600(a)(1) standards and are considered potential exceedances^[1]. A summary of groundwater analytical data is provided in **Table 4-1**. Field parameters are included in **Table 4-2** and groundwater elevations are provided in **Appendix E**.

4.2.1 Arsenic

Arsenic was detected at concentrations greater than the GWPS (0.01 milligrams per liter [mg/L]) in three downgradient uppermost aquifer wells (G302, G303, and G304/G307). Arsenic was also detected at concentrations greater than the GWPS in background uppermost aquifer well (G306).

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^[1] Potential exceedances include results reported during the eight rounds of baseline groundwater monitoring that are greater than the applicable 35 I.A.C. § 845.600(a)(1) standards. The results are considered potential exceedances because they were compared directly to the standard and did not include an evaluation of background groundwater quality or apply the statistical methodologies proposed in the Groundwater Monitoring Plan (GMP). For simplicity, "GWPS" will be used hereafter in discussing potential exceedances. Exceedances will be determined following IEPA approval of the GMP.

Arsenic concentrations in these downgradient uppermost aquifer wells ranged from non-detect (at a reporting limit of 0.001 mg/L) to 0.041 mg/L. Arsenic concentrations in the background uppermost aquifer well noted above ranged from non-detect to 0.02 mg/L. Arsenic was not detected during 2021 groundwater monitoring events.

No LCU or DA monitoring wells had concentrations greater than the arsenic GWPS.

4.2.2 Boron

Boron is a primary indicator parameter for CCR leachate impacts on groundwater quality. Boron has been detected consistently at concentrations greater than the GWPS (2 mg/L) at eight downgradient uppermost aquifer wells (G301, G302, G303, G304/G307, G305, G308, G311, and G313) and infrequently at two downgradient uppermost aquifer wells (G309 and G312). Boron was also frequently detected at concentrations greater than the GWPS at background uppermost aquifer monitoring well G306. Boron concentrations observed at the downgradient uppermost aquifer wells listed above ranged from 0.28 to 3.5 mg/L, excluding one event at G309 where the boron concentration was 7.5 mg/L. Boron concentrations in the background uppermost aquifer well ranged from 2.3 to 3.5 mg/L.

No LCU or DA monitoring wells had concentrations greater than the boron GWPS.

4.2.3 Cadmium

Cadmium was detected at concentrations greater than the GWPS (0.005 mg/L) during two events in one downgradient uppermost aquifer well (G304/G307). Cadmium concentrations in G304/G307 ranged from non-detect (at a reporting limit of 0.001 mg/L) to 0.027 mg/L. Cadmium was not detected at concentrations greater than the GWPS during 2021.

No LCU or DA monitoring wells had concentrations greater than the cadmium GWPS.

4.2.4 Chromium

Chromium was detected at concentrations greater than the GWPS (0.1 mg/L) during one event in May 2017 in one downgradient uppermost aquifer well (G304/G307). Chromium concentration in G304/G307 ranged from non-detect (at a reporting limit of 0.004 mg/L) to 0.11 mg/L.

No LCU or DA monitoring wells had concentrations greater than the chromium GWPS.

4.2.5 Cobalt

Cobalt has been frequently detected at concentrations greater than the GWPS (0.006 mg/L) at one downgradient uppermost aquifer well (G304/G307) and occasionally at four downgradient uppermost aquifer wells (G301, G302, G303, and G305). Cobalt has also been detected at concentrations greater than the GWPS often at one background uppermost aquifer well (G306). Cobalt concentrations of the downgradient wells listed above ranged from non-detect (at a reporting limit of 0.002 mg/L) to 0.034 mg/L. Cobalt concentrations in the background well noted above ranged from non-detect to 0.02 mg/L.

Cobalt has been frequently detected at concentrations greater than the GWPS (0.006 mg/L) at one downgradient LCU well (G314). Cobalt concentrations at G314 range from non-detect (at a reporting limit of 0.002 mg/L) to 0.011 mg/L.

No DA monitoring wells had concentrations greater than the cobalt GWPS.

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4.2.6 Lead

Lead has been detected at concentrations greater than the GWPS (0.0075 mg/L) often at one downgradient uppermost aquifer well (G304/G307) and occasionally at three downgradient uppermost aquifer wells (G301, G302, and G305). Lead has also been detected at concentrations greater than the GWPS often at one background uppermost aquifer well (G306). Lead concentrations in these downgradient uppermost aquifer wells ranged from non-detect (at a reporting limit of 0.001 mg/L) to 0.068 mg/L. Lead concentrations in the background uppermost aquifer well noted above ranged from non-detect to 0.028 mg/L.

Lead was detected at concentrations greater than the GWPS in downgradient LCU well G316 during the July 2021 event. Concentrations at G316 ranged from non-detect (at a reporting limit of 0.001 mg/L) to 0.014 mg/L.

No DA monitoring wells had concentrations greater than the lead GWPS.

4.2.7 Lithium

Lithium has been detected consistently at concentrations greater than the GWPS (0.04 mg/L) at one downgradient uppermost aquifer well (G303) and once at one downgradient uppermost aquifer well (G304/G307). Lithium concentrations observed at the downgradient wells listed above ranged from 0.01 to 0.1 mg/L.

No LCU or DA monitoring wells had concentrations greater than the lithium GWPS.

4.2.8 pH

Intermittently, pH has been detected at measurements less than the lower GWPS (6.5 Standard Units [SU]) in two downgradient uppermost aquifer wells (G301 and G312). Measurements of pH have ranged from 6.3 to 7.1 SU at these wells.

None of the uppermost aquifer wells had measurements greater than the upper pH GWPS.

No LCU or DA monitoring wells had measurements less than the lower pH GWPS or greater than the upper pH GWPS.

4.2.9 Radium 226 and 228 Combined

Radium 226 and 228 combined was detected at concentrations greater than the GWPS (5 picoCuries per liter [pCi/L]) in downgradient LCU well G316 during one event in May 2021. Radium 226 and 228 combined concentrations at G316 range from 0.196 to 17.5 mg/L.

No uppermost aquifer wells had concentrations greater than the radium 226 and 228 combined GWPS.

No DA monitoring wells had concentrations greater than the radium 226 and 228 combined ${\sf GWPS}$.

4.2.10 Sulfate

Sulfate is also a primary indicator parameter of CCR leachate impacts on groundwater quality. Sulfate was consistently detected at concentrations greater than the GWPS (400 mg/L) in twelve downgradient uppermost aquifer wells (G301, G302, G303, G304/G307, G308, G309, G310,

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G311, G312, G313, G315, and G317) and intermittently in one downgradient uppermost aquifer well (G305). Sulfate was also detected at concentrations greater than the GWPS during one event in May 2017 at background uppermost aquifer monitoring well G306. Sulfate concentrations of the downgradient uppermost aquifer wells listed above ranged from 260 to 1,300 mg/L. Sulfate concentrations at background uppermost aquifer well G306 ranged from 5.9 to 700 mg/L.

Sulfate was frequently detected at concentrations greater than the GWPS at three downgradient LCU wells (G307D, G314, and G316). Sulfate concentrations of the downgradient LCU wells ranged from 330 to 2,400 mg/L.

Sulfate was often detected at concentrations greater than the GWPS at downgradient DA well G314D. Sulfate concentrations at G314D range from 820 to 1,100 mg/L.

4.2.11 Total Dissolved Solids

TDS was consistently detected at concentrations greater than the GWPS (1,200 mg/L) in ten downgradient uppermost aquifer wells (G303, G304/G307, G308, G309, G310, G311, G312, G313, G315, and G317) and intermittently in three downgradient uppermost aquifer wells (G301, G302, and G305). TDS concentrations of these downgradient uppermost aquifer wells ranged from 780 to 2,000 mg/L.

TDS was consistently detected at concentrations greater than the GWPS at one downgradient LCU well (G314) and frequently detected at concentrations greater than the GWPS at two downgradient LCU wells (G307D and G316). TDS concentrations of the downgradient LCU wells ranged from 1,100 to 4,000 mg/L.

TDS was occasionally detected at concentrations greater than the GWPS at downgradient DA well G314D. TDS concentrations at G314D ranged from 1,600 to 2,400 mg/L.

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5. EVALUATION OF POTENTIAL RECEPTORS

5.1 Water Well Survey

A water well survey was conducted for a 1,000-meter radius around. Based on State of Illinois records obtained from the ISGS Illinois Water and Related Wells (ILWATER) Map¹ there are twelve water wells located within 1,000 meters of AP1. These included four monitoring wells and eight farm/domestic wells. A map of wells in the vicinity of AP1 is presented in **Appendix B**.

5.2 Surface Water

A search was performed utilizing the United States Fish and Wildlife Service (USFWS) Wetlands Mapper² and the USGS National Map ³ for surface water bodies within 1,000 meters of AP1. The predominant surface water body in the region is Coffeen Lake and associated tributaries. Coffeen Lake consists of two lobes which are located approximately 1,300 feet west, 3,700 feet south, and 150 feet east and downgradient from AP1. A USGS stream gage (USGS 05593900) for the East Fork Shoal River near Coffeen, Illinois is located 6.5 miles north and east (upstream) of CPP.

Additional surface waters indicated in the USFWS Wetland Mapper and USGS National Map include several man-made freshwater ponds ranging from 0.2 to 4.8 and two emergent wetlands, one 0.2 acres and northeast and one 1.6 acres and east of AP1. A map of wetlands and surface waters in the vicinity of AP1 is presented in **Appendix B**.

The USGS National Map places CPP within the Shoal Creek watershed (HUC 07140203), which is part of the Middle Kaskaskia River Watershed.

A Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map for Montgomery County, Illinois (Map No. 170992 0009 A, effective: January 9, 1981) is available in **Appendix G**. AP1 does not occur within the special flood hazard zones identified on the 1981 FEMA map. The flood hazard areas shown on the map are defined as those areas subject to inundation by the 1 percent annual chance flood (*i.e.*, 100-year flood), also known as the base flood, that has a 1 percent chance of being equaled or exceeded in any given year.

5.3 Nature Preserves, Historic Sites, Endangered/Threatened Species

A comprehensive search of the IDNR Natural Heritage Database⁴ for natural areas and protected areas within 1,000 meters of the AP1 was performed. No natural or protected areas within the IDNR database were identified within 1,000 meters of the AP1. A list of sites identified at the county level is found in **Appendix B**.

The IDNR Natural Heritage Database Threatened and Endangered Species by County⁵ lists eleven threatened and endangered species as located within Montgomery County, including

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¹ ISGS ILWATER Map:

 $[\]frac{\text{https://prairieresearch.maps.arcgis.com/apps/webappviewer/index.html?} id = e06b64ae0c814ef3a4e43a191cb57f87$

² USFWS Wetlands Mapper: https://www.fws.gov/wetlands/data/mapper.html

³ USGS National Map: https://apps.nationalmap.gov/viewer/

⁴ IDNR Natural Heritage Database:

https://www2.illinois.gov/dnr/conservation/NaturalHeritage/Pages/NaturalHeritageDatabase.aspx

⁵ Illinois Threatened and Endangered Species by County: https://www2.illinois.gov/dnr/ESPB/Documents/ET_by_County.pdf

six endangered and five threatened species. Habitats for endangered or threatened species are identified at the county level only.

Additionally, a search of the IDNR Historic Preservation Division⁶ database for historic sites in the vicinity of the Site yielded six results at the county level located within Montgomery County. Four of these sites were identified from the Illinois Natural Areas Inventory and two were identified from the Illinois Nature Preserves list. None of these sites fall within 1,000 meters of AP1. The Illinois State Archaeological Survey (ISAS)⁷ databases that do not require credentials to access were also searched and yielded no results within 1,000 meters of AP1.

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 $^{^{6}\ \} IDNR\ Historic\ Preservation\ Division:\ \underline{https://www2.illinois.gov/dnrhistoric/Pages/default.aspx}$

⁷ ISAS: https://www.isas.illinois.edu/

6. CONCLUSIONS

Based on extensive site investigation and monitoring, AP1 has been characterized and a detailed site conceptual model has been developed. Results of these hydrogeologic studies were summarized and updated to include geologic, hydrogeologic, and groundwater quality data collected with a focus on AP1 (Part 845 regulated CCR Unit and subject of this HCR).

Results of these hydrogeologic studies were reintroduced in this HCR and updated to include geologic, hydrogeologic, and groundwater quality data collected with a focus on AP1 (Part 845 regulated CCR Unit and subject of this HCR). The data were summarized and evaluated for changes in groundwater conditions since the previous investigations; available groundwater quality data for AP1 collected from 2015 to present was compared to the Part 845 Standards.

The results of the hydrogeologic and groundwater quality evaluation are:

- There are eight principal unlithified units above the bedrock in the vicinity of AP1, these include the following in descending order:
 - CCR: CCR consisting of fly ash and bottom ash is present within AP1 and non-CCR fill
 material consisting of silt, clay, and sand comprises the berms surrounding AP1.
 - Loess Unit: Clays and silts, including undifferentiated Roxana Silt and Peoria Silt with thicknesses ranging from 1 to 16 feet, where present.
 - Hagarstown Member: The Hagarstown Member (consisting of gravelly clay till and sandy materials in contact with the Vandalia Member (also referred to as Hagarstown Beds) which has been subdivided into two units: the first unit consists of the gravelly clay till, and the second unit consists of sandy material overlying the Vandalia Member. The Upper Hagarstown Member is up to 6 feet thick, while the sandy portions, where present, are generally less than 3 feet thick.
 - Vandalia Member: Sandy, silt till, or clay till that is generally greater than 15 feet thick.
 - Mulberry Grove Member: Gray silt and sandy silt/clay unit found between the Vandalia
 Till and the Smithboro Till. Generally thin and not laterally continuous across the Site.
 - **Smithboro Member**: Thick, gray compacted silty clay diamicton.
 - Yarmouth Soil: Sand and sandy silt/clay, which include accretionary deposits of fine sediment and organic materials, typically less than 5 feet thick and not laterally continuous.
 - Lierle Clay Member: Clay and silt with some sand which is the upper portion of the Banner Formation. No borings advanced on site penetrated the full thickness of the Lierle Clay.
 - Bedrock: Was not encountered in any deep borings advanced at AP1.
- Unlithified materials, described above, in the vicinity of the CPP were categorized into hydrostratigraphic units for this HCR. In addition to the CCR Unit, the hydrostratigraphic units occur in the following order (from surface downward) and include:

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- UCU: Composed of the Loess Unit and clayey portions of the Hagarstown Formation
 which are classified as silts to clayey silts and gravelly clay below the surficial soil. The
 UCU has been eroded east of AP1, near the Unnamed Tributary.
- Uppermost Aquifer: The uppermost aquifer is the Hagarstown Member which is classified as primarily sandy to gravelly silts and clays with thin beds of sands. Similar to the Loess Unit, the Hagarstown is also absent in some locations near the Unnamed Tributary.
- LCU: Comprised of the Vandalia Member, Mulberry Grove Member, and Smithboro Member. These units include a sandy to silty till with thin, discontinuous sand lenses, a discontinuous and limited extent sandy silt which has infilled prior erosional features, and silty to clayey diamicton, respectively.
- DA: Sand and sandy silt/clay units of the Yarmouth Soil, which include accretionary deposits of fine sediment and organic materials, typically less than 5 feet thick and discontinuous across the Site.
- DCU: Comprised of the Banner Formation, generally consists of clays, silts, and sands.
 The Lierle Clay Member is the upper layer of the Banner Formation which was encountered at the Site.
- The elevations of water within AP1 are greater than the surrounding areas; however, approximately 8 to 10 feet of UCU is present beneath AP1 and water elevation within AP1 does not vary coincidentally with surrounding groundwater elevations. Based on historic topographic maps, ash may have been placed as low as 595 to 600 feet NAVD88 in the northeast corner of AP1. Groundwater elevations may be above the base of ash in this area.
- Groundwater flow within the uppermost aquifer is divided towards the two lobes of Coffeen
 Lake. The groundwater divide runs approximately through the center of the CPP property,
 with groundwater east of the divide flowing east to southeast towards the Unnamed Tributary
 or the eastern lobe and groundwater west of the divide flowing west to southwest towards the
 western lobe. Groundwater flows north to northeast across AP1.
- Vertical gradients measured near the site indicate downward flow from the uppermost aquifer
 to the LCU and DA. The LCU in locations without the uppermost aquifer and the DA have been
 identified as PMPs due to the presence of downward gradients and also the relatively higher
 hydraulic conductivities measured in the DA.
- Historically coal mines were operated at depth below the Site. Mine shafts, processing facilities and historic coal storage associated with these mines were located south of AP1.
- As determined by the detailed geologic information provided for AP1, and the hydrogeologic and groundwater quality data, groundwater within the uppermost aquifer at the AP1 is classified as Class I - Potable Resource Groundwater.
- Potential exceedances of 35 I.A.C. § 845.600 GWPSs were detected in monitoring wells downgradient of AP1 in the various hydrostratigraphic units as follows:
 - Arsenic in downgradient uppermost aquifer wells G302, G303, and G304/G307. Arsenic was also detected in upgradient uppermost aquifer well G306.

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- Boron in downgradient uppermost aquifer wells G301, G302, G303, G304/G307, G305, G308, G311, and G313. Boron was also detected in upgradient uppermost aquifer well G306.
- Cadmium in downgradient uppermost aquifer well G304/G307.
- Chromium in downgradient uppermost aguifer well G304/G307.
- Cobalt in downgradient uppermost aquifer wells G301, G302, G303, G304/G307, and G305; and in downgradient LCU well G314. Cobalt was also detected in upgradient uppermost aquifer well G306.
- Lead in downgradient uppermost aquifer wells G301, G302, G303, G304/G307 and G305;
 and in downgradient LCU well G316. Lead was also detected in upgradient uppermost aquifer well G306.
- Lithium in downgradient uppermost aquifer wells G303 and G304/G307.
- pH (lower limit) in downgradient uppermost aquifer wells G301 and G312.
- Radium 226 and 228 combined in downgradient LCU well G316.
- Sulfate in downgradient uppermost aquifer wells G301, G302, G303, G304/G307, G305, G308, G309, G310, G311, G312, G313, G315, and G317; in downgradient LCU wells G307D, G314, and G316; and in downgradient DA well G314D. Sulfate was also detected at concentrations greater than the GWPS in upgradient uppermost aquifer well G306.
- TDS in downgradient uppermost aquifer wells G301, G302, G303, G304/G307, G305, G308, G309, G310, G311, G312, G313, G315, and G317; in downgradient LCU wells G307D, G314, and G316; and in downgradient DA well G314D. Sulfate was also detected at concentrations greater than the GWPS in upgradient uppermost aquifer well G306.

Groundwater results are considered potential exceedances because they were compared directly to the standard and did not include an evaluation of background groundwater quality or apply the statistical methodologies proposed in the GMP.

This HCR satisfies Part 845 content requirements specific to 35 I.A.C. § 845.620(b) (Hydrogeologic Site Characterization) for AP1 at the CPP.

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TABLES

TABLE 2-1. GEOTECHNICAL DATA SUMMARY

| Sample ID | Field Location ID | Top of Sample (ft bgs) | Bottom of Sample (ft bgs) | Moisture Content (%) | Dry Density (pcf) | Specific Gravity | Calculated Porosity ¹ (%) | Vertical Hydraulic Conductivity (cm/s) | LL | PL | PI | uscs | Gravel (%) | Sand (%) | Fines (%) |
|------------------|----------------------|------------------------------|---------------------------------|----------------------------|----------------------|---------------------|--------------------------------------|---|----|----------|----|-------|--|-------------|--|
| Loess Unit | | | | | | | | | | | | | | | |
| G307D/Comp 1 | G307D | 4 | 12.8 | 19.4 | 107.5 | 2.59 | 33.5 | | 33 | 16 | 17 | CL | 0 | 33 | 67 |
| G307D, ST5 | G307D | 8 | 10 | 21.6 | 105.0 | | | 4.8E-08 | | | | CL/CH | | | |
| G311D/Comp 1 | G311D | 4 | 22 ** | 16.5 | 115.7 | 2.64 | 29.8 | | 31 | 13 | 18 | CL | 0 | 35 | 65 |
| G311D, ST4 | G311D | 6 | 8 | 19.0 | 107.5 | | | 2.9E-08 | | | | CL | | | |
| G314D/Comp 1 | G314D | 4.2 | 17 | 16.5 | 113.6 | 2.61 | 30.2 | | 29 | 14 | 15 | CL | 0 | 34 | 66 |
| Hagarstown Membe | er | | | | | | | | | | | | | | |
| G307D/Comp 2 | G307D | 12.8 | 14 | 19.2 | | 2.59 | | | NP | NP | NP | SW | 14 | 79 | 7 |
| G311D/Comp 2 | G311D | 12 | 14 | 11.4 | 126.8 | 2.68 | 24.2 | | 18 | 13 | 5 | SM | 0 | 65 | 35 |
| G314D/Comp 2 | G314D | 17.3 | 21.6 | 12.2 | 123.4 | 2.64 | 25.1 | | 29 | 14 | 15 | CL | 0 | 28 | 72 |
| Vandalia Member | | | | | | | | | | | | | | | |
| G307D/Comp 3 | G307D | 18 | 34.9 | 8.7 | 131.6 | 2.60 | 18.9 | | 19 | 13 | 6 | SP-SM | 0 | 44 | 56 |
| G311D/Comp 3 | G311D | 18 ** | 42 | 11.4 | 124.8 | 2.61 | 23.4 | | 30 | 15 | 15 | CL | 0 | 28 | 72 |
| G311D, ST14 | G311D | 28 | 30 | 16.2 | 116.7 | | | 5.5E-08 | | | | CL | | | |
| G314D/Comp 3 | G314D | 21.8 | 45.5 | 14.6 | 115.7 | 2.56 | 27.6 | | 31 | 15 | 16 | CL | 0 | 26 | 74 |
| Smithboro Member | | | | | | | | | | | | | | | |
| G307D/Comp 4 | G307D | 40 | 54 | 15.6 | 115.7 | 2.61 | 29.0 | | 30 | 15 | 15 | CL | 0 | 28 | 72 |
| G307D, ST22 | G307D | 42 | 44 | 15.0 | 118.8 | | | 3.7E-07 | | | | CL | | | |
| G311D/Comp 4 | G311D | 44 | 52 | 15.5 | 114.2 | 2.56 | 28.5 | | 30 | 16 | 14 | CL | 0 | 26 | 74 |
| G314D, ST18 | G314D | 37 | 39 | 16.6 | 115.0 | | | 3.0E-07 | | | | CL | | | |
| Yarmouth Soil | | | _ | | | | _ | | | 1 | 1 | | | | |
| G314D/Comp 4 | G314D | 46 | 47 | 14.9 | | 2.61 | | | | | | SP-SM | 0 | 84 | 16 |
| Lierle Clay | | | | | | | _ | | | 1 | 1 | | | | |
| G307D/Comp 5 | G307D | 54 | 60 | 8.7 | 134.6 | 2.67 | 19.2 | | 47 | 18 | 29 | CL | 0 | 20 | 80 |
| G311D/Comp 5 | G311D | 52 | 60 | 18.9 | 108.0 | 2.59 | 33.2 | | 37 | 17 | 20 | CL | 0 | 19 | 81 |
| G314D/Comp 5 | G314D | 47.8 | 52 | 17.5 | 109.6 | 2.58 | 31.9 | | 43 | 18 | 25 | CL | 0 | 24 | 76 |
| G314D/Comp 6 | G314D | 52.2 | 62.9 | 13.6 | 120.2 | 2.64 | 27.0 | | 37 | 18 | 19 | CL | 0 | 19 | 81 |
| Banner Formation | | | _ | | | | _ | | | 1 | 1 | | <u>, </u> | | <u>, </u> |
| G314D/Comp 7 | G314D | 73.9 | 82.5 | 14.0 | 120.3 | 2.64 | 27.0 | | 29 | 19 | 10 | CL | 0 | 16 | 84 |
| G314D/Comp 8 | G314D | 93.5 | 100.3 | 8.5 | 123.6 | 2.73 | 27.4 | | 35 | 19 | 16 | CL | 0 | 16 | 84 |

TABLE 2-1. GEOTECHNICAL DATA SUMMARY

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Sample ID | Field Location ID | Top of Sample (ft bgs) | Bottom of Sample (ft bgs) | Moisture Content (%) | Dry Density (pcf) | Specific Gravity | Calculated Porosity ¹ (%) | Vertical Hydraulic Conductivity (cm/s) | LL | PL | ΡI | USCS | Gravel (%) | Sand (%) | Fines (%) |
|------------|----------------------|------------------------------|---------------------------------|----------------------------|----------------------|---------------------|--|---|----|----|----|------------|---------------|-------------|--------------|
| CCR | | | | | | | | | | | | | | | |
| XPW02 Bulk | XPW02 | 0 | 17.7 | 12.5 | 110.8 | 2.60 | 31.7 | 8.8E-05 | - | | | Bottom Ash | 0 | 90 | 10 |

[O:KLT, QC: FPO][U: FPO, QC:KLT 8/9/21][U:KLT 8/13/21, C:EDP 8/30/21]

Notes:

¹ Porosity calculated as relationship of bulk density (p_b) to particle density (p_d) $(n = 100[1-(p_b/p_d)])$

-- = not analyzed

% = Percent

** = not all sampled in the noted interval were included in this composite sample

bgs = below ground surface

cm/s = centimeters per second

ft = foot/feet

LL = Liquid limit

NP = Non Plastic

pcf = pounds per cubic foot

PI = Plasticity Index

PL = Plastic Limit

USCS = Unified Soil Classification System

CH = Fat Clay

CL = Lean Clay

ML = Silt

SC = Clayey Sand

SM = Silty Sand

SP-SM = Poorly Graded-Sand with Silt

TABLE 2-2. ASH ANALYTICAL RESULTS

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Sample Location | Sample Depth (ft BGS) | Sample Date | Antimony (mg/kg) | Arsenic (mg/kg) | Barium (mg/kg) | Beryllium (mg/kg) | Boron (mg/kg) | Cadmium (mg/kg) | Chloride (mg/kg) | Chromium (mg/kg) | Cobalt (mg/kg) | Fluoride (mg/kg) | Lead (mg/kg) | Lithium (mg/kg) | Mercury (mg/kg) | Molybdenum (mg/kg) | Selenium (mg/kg) | Sulfate (mg/kg) | Thallium (mg/kg) |
|--------------------|-----------------------------|----------------|---------------------|--------------------|-------------------|----------------------|------------------|--------------------|---------------------|---------------------|-------------------|---------------------|-----------------|--------------------|--------------------|-----------------------|---------------------|--------------------|---------------------|
| XPW01 | 0-8 | 02/08/2021 | <2.7 | 6.9 | 710 | 1.9 | 110 | 0.96 | <10 | 41 | 4.8 | <2.5 | 4.7 | 18 | <0.18 | 7 | 7.5 | 450 | <0.91 |
| XPW02 | 0-8 | 02/08/2021 | <2.8 | <0.93 | 850 | 1.6 | 70 | <0.93 | <10 | 24 | 4.3 | <2.5 | 1.3 | 20 | <0.19 | 2.5 | <0.93 | 85 | <0.93 |

Notes:

< = concentration is less than the concentration shown, which corresponds to the reporting limit for the method.</p>
BGS = below ground surface

ft = feet

mg/kg = milligrams per kilogram

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TABLE 2-3. POREWATER ANALYTICAL RESULTS

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Sample Location | Sample Date | Antimony, total (mg/L) | Arsenic, total (mg/L) | Barium, total (mg/L) | Beryllium, total (mg/L) | Boron, total (mg/L) | Cadmium, total (mg/L) | Calcium, total (mg/L) | Chloride, total (mg/L) | Chromium, total (mg/L) | Cobalt, total (mg/L) | Fluoride, total (mg/L) | Lead, total (mg/L) | Lithium, total (mg/L) | Mercury, total (mg/L) | Molybdenum, total (mg/L) | pH (field) (SU) | Radium 226 and 228 combined (pCi/L) | Selenium, total (mg/L) | Sulfate, total (mg/L) | Thallium, total (mg/L) |
|--------------------|----------------|------------------------------|-----------------------------|----------------------------|-------------------------------|---------------------------|-----------------------------|-----------------------------|------------------------------|------------------------------|----------------------------|------------------------------|--------------------------|-----------------------------|-----------------------------|--------------------------------|-----------------------|---|------------------------------|-----------------------------|------------------------------|
| XPW01 | 03/30/2021 | <0.003 | 0.002 | 0.043 | <0.001 | 2.4 | <0.001 | 280 | 13 | <0.004 | <0.002 | 0.791 | <0.001 | 0.037 | <0.0002 | 0.082 | 8.0 | 0 | <0.001 | 820 | <0.001 |
| XPW01 | 04/22/2021 | <0.003 | 0.0011 | 0.035 | <0.001 | 2.4 | <0.001 | 270 | 17 | <0.004 | <0.002 | 0.396 | <0.001 | 0.039 | <0.0002 | 0.078 | 7.8 | 0.0477 | <0.001 | 860 | <0.001 |
| XPW01 | 05/05/2021 | <0.003 | 0.0017 | 0.033 | <0.001 | 2.5 | <0.001 | 290 | 17 | <0.004 | <0.002 | 0.77 | <0.001 | 0.032 | <0.0002 | 0.078 | 8.0 | 0.169 | <0.001 | 850 | <0.001 |
| XPW01 | 05/18/2021 | <0.003 | 0.0017 | 0.032 | <0.001 | 2.5 | <0.001 | 270 | 15 | <0.004 | <0.002 | 0.846 | <0.001 | 0.035 | <0.0002 | 0.079 | 8.0 | 0.447 | <0.001 | 820 | <0.001 |
| XPW01 | 06/14/2021 | | | | | | | | | | | | | | | | | 0.21 | | | |
| XPW01 | 06/28/2021 | | | | | | | | | | | | | | | | | 1.15 | | | |
| XPW01 | 07/27/2021 | <0.003 | 0.0014 | 0.031 | <0.001 | 2.9 | <0.001 | 250 | 13 | <0.004 | <0.002 | 0.799 | <0.001 | 0.038 | <0.0002 | 0.062 | 8.1 | | <0.001 | 740 | <0.001 |
| XPW02 | 03/30/2021 | <0.003 | 0.0034 | 0.11 | <0.001 | 2.4 | <0.001 | 210 | 17 | <0.004 | <0.002 | 0.551 | <0.001 | 0.057 | <0.0002 | 0.024 | 7.9 | 0.0969 | 0.0013 | 570 | <0.001 |
| XPW02 | 04/22/2021 | <0.003 | 0.0017 | 0.089 | <0.001 | 2.2 | <0.001 | 220 | 17 | <0.004 | <0.002 | <0.25 | <0.001 | 0.06 | <0.0002 | 0.024 | 8.0 | 0.203 | <0.001 | 620 | <0.001 |
| XPW02 | 05/05/2021 | <0.003 | 0.0035 | 0.11 | <0.001 | 2.4 | <0.001 | 230 | 17 | <0.004 | <0.002 | 0.56 | <0.001 | 0.059 | <0.0002 | 0.02 | 7.9 | 0.0971 | <0.001 | 610 | <0.001 |
| XPW02 | 05/19/2021 | <0.003 | 0.0023 | 0.089 | <0.001 | 2.4 | <0.001 | 220 | 1.5 | <0.004 | <0.002 | <0.25 | <0.001 | 0.066 | <0.0002 | 0.016 | 8.1 | 0.387 | <0.001 | 650 | <0.001 |
| XPW02 | 06/14/2021 | | | | | | | | | | | | | | | | | 0.593 | | | |
| XPW02 | 06/28/2021 | | | | | | | | | | | | | | | | | 1.29 | | | |
| XPW02 | 07/27/2021 | <0.003 | 0.002 | 0.083 | <0.001 | 2.4 | <0.001 | 210 | 14 | <0.004 | <0.002 | 0.643 | <0.001 | 0.061 | <0.0002 | 0.025 | 8.2 | | <0.001 | 600 | <0.001 |

Field readings are reported with as many significant figures as provided by analytical laboratory.

-- = data not available

< = concentration is less than the concentration shown, which corresponds to the reporting limit for the method.</p>

mg/L = milligrams per liter pCi/L = picocuries per liter

SU = standard units

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TABLE 2-4. SOIL ANALYTICAL RESULTS

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Sample Location | Geologic Unit | Sample Depth (ft BGS) | Sample Date | Antimony (mg/kg) | Arsenic (mg/kg) | Barium (mg/kg) | Beryllium (mg/kg) | Boron (mg/kg) | Cadmium (mg/kg) | Chloride (mg/kg) | Chromium (mg/kg) | Cobalt (mg/kg) | Fluoride (mg/kg) | Lead (mg/kg) | Lithium (mg/kg) | Mercury (mg/kg) | Molybdenum (mg/kg) | Selenium (mg/kg) | Sulfate (mg/kg) | Thallium (mg/kg) |
|--------------------|---|--------------------------------|----------------|---------------------|--------------------|-------------------|----------------------|------------------|--------------------|---------------------|---------------------|-------------------|---------------------|-----------------|--------------------|--------------------|-----------------------|---------------------|--------------------|---------------------|
| G307D | Loess Unit/Hagarstown Member | 4-12.8 | 02/09/2021 | <2.6 | 7.5 | 150 | <0.86 | <8.6 | 1.2 | <10 | 9.5 | 25 | 3.1 | 15 | <4.3 | <0.17 | 1.3 | <0.86 | 220 | <0.86 |
| G307D | Hagarstown Member | 12.8-14 | 02/09/2021 | <2 | 1.7 | 10 | <0.66 | <6.6 | <0.66 | 19 | 3.8 | 1.4 | <2.5 | 3.3 | <3.3 | <0.13 | <0.66 | <0.66 | 170 | <0.66 |
| G307D | Vandalia Till Member | 18-34.9 | 02/09/2021 | <2.6 | 2.9 | 20 | <0.87 | <8.7 | <0.87 | <10 | 8.5 | 4.5 | <2.5 | 5.9 | 10 | <0.17 | <0.87 | <0.87 | 30 | <0.87 |
| G307D | Smithboro Till Member | 40-54 | 02/09/2021 | <2.8 | 5.7 | 93 | <0.93 | <9.3 | <0.93 | <10 | 10 | 7.1 | 4.2 | 7.7 | 7.1 | <0.19 | 1.4 | <0.93 | <10 | <0.93 |
| G307D | Lierle Clay | 54-60 | 02/09/2021 | <2.4 | 4.2 | 110 | <0.79 | <7.9 | <0.79 | <10 | 8.5 | 6 | 6.8 | 7.2 | 6.8 | <0.16 | <0.79 | <0.79 | <10 | <0.79 |
| G311D | Loess Unit/Hagarstown Member/Vandlia Till Member | 4-22 | 02/05/2021 | <3 | 3.2 | 57 | <1 | <10 | <1 | <1 | 10 | 3.1 | <0.25 | 8.1 | <5 | <0.2 | <1 | <1 | 2.3 | <1 |
| G311D | Hagarstown Member | 12-14 | 02/05/2021 | <3.2 | 3.5 | 44 | <1.1 | <11 | <1.1 | <1 | 8 | 4 | <0.25 | 5.4 | 6.4 | <0.21 | 1.2 | <1.1 | <1 | <1.1 |
| G311D | Vandalia Till Member | 18-42 | 02/05/2021 | <3 | 2.8 | 69 | <1 | <10 | <1 | <1 | 10 | 5 | <0.25 | 6.9 | 8.4 | <0.2 | 1.2 | <1 | <1 | <1 |
| G311D | Smithboro Till Member | 44-52 | 02/05/2021 | <2.8 | 3.2 | 90 | <0.95 | <9.5 | <0.95 | <1 | 12 | 5.9 | <0.25 | 8.7 | 10 | <0.19 | 1.3 | <0.95 | <1 | <0.95 |
| G314D | Soil/Vandalia Till Member | 4.2-17 | 02/10/2021 | <2.8 | 1.3 | 63 | <0.93 | <9.3 | <0.93 | <10 | 8.7 | <1.9 | <2.5 | 5.5 | <4.6 | <0.19 | <0.93 | <0.93 | 76 | <0.93 |
| G314D | Vandalia Till Member | 17.3- 21.6 | 02/11/2021 | <3 | 2.7 | 27 | <1 | <10 | <1 | <10 | 9.9 | 5.2 | <2.5 | 7.3 | 9.1 | <0.2 | 1.2 | <1 | 210 | <1 |
| G314D | Vandalia Till Member/Smithboro Till Member | 21.8- 45.5 | 02/11/2021 | <2.4 | 3.8 | 140 | <0.8 | <8 | <0.8 | <10 | 25 | 10 | 3.1 | 11 | 28 | <0.16 | <0.8 | 0.98 | <10 | <0.8 |

< = concentration is less than the concentration shown, which corresponds to the reporting limit for the method.
BGS = below ground surface
ft = foot or feet
mg/kg = milligrams per kilogram</pre>

generated 10/05/2021, 2:17:38 PM CDT



| Well Number | HSU | Date Constructed | Top of PVC Elevation (ft) | Measuring Point Elevation (ft) | Measuring Point Description | Ground Elevation (ft) | Screen Top Depth (ft BGS) | Screen Bottom Depth (ft BGS) | Screen Top Elevation (ft) | Screen Bottom Elevation (ft) | Well Depth (ft BGS) | Bottom of Boring Elevation (ft) | Screen Length (ft) | Screen Diameter (inches) | Latitude (Decimal Degrees) | Longitude (Decimal Degrees) |
|----------------|-----|---------------------|---------------------------------|---|-----------------------------------|-----------------------------|------------------------------------|---------------------------------------|---------------------------------|---------------------------------------|---------------------------|--|--------------------------|--------------------------------|----------------------------------|-----------------------------------|
| G045D | LCU | 08/17/2016 | 623.81 | 623.81 | Top of PVC | 620.94 | 31.88 | 41.52 | 589.06 | 579.42 | 41.92 | 578.90 | 9.6 | 2 | 39.064349 | -89.396281 |
| G046D | LCU | 08/19/2017 | 625.24 | 625.24 | Top of PVC | 621.91 | 41.61 | 51.26 | 580.30 | 570.65 | 51.65 | 569.90 | 9.7 | 2 | 39.060305 | -89.398524 |
| G101 | UA | 02/02/2010 | | 627.60 | Top of Disk | 625.27 | 15.68 | 20.32 | 609.59 | 604.95 | 20.89 | 603.40 | 4.6 | 2 | 39.071386 | -89.400107 |
| G102 | UA | 04/28/2006 | | 629.04 | Top of Disk | 626.18 | 12.02 | 16.78 | 614.16 | 609.40 | 17.15 | 609.00 | 4.8 | 2 | 39.071387 | -89.398991 |
| G103 | UA | 02/15/2010 | | 633.80 | Top of Disk | 627.94 | 15.88 | 20.67 | 612.06 | 607.27 | 21.09 | 606.90 | 4.8 | 2 | 39.070412 | -89.399107 |
| G104 | UA | 02/15/2010 | | 632.94 | Top of Disk | 627.96 | 14.91 | 19.61 | 613.05 | 608.35 | 20.08 | 605.80 | 4.7 | 2 | 39.069451 | -89.399104 |
| G105 | UA | 02/16/2010 | | 632.08 | Top of Disk | 626.86 | 16.11 | 20.90 | 610.75 | 605.96 | 21.37 | 604.40 | 4.8 | 2 | 39.068491 | -89.3991 |
| G106 | UA | 02/16/2010 | | 631.15 | Top of Disk | 625.96 | 14.37 | 18.96 | 611.59 | 607.00 | 19.44 | 605.50 | 4.6 | 2 | 39.06753 | -89.399097 |
| G107 | UA | 02/17/2010 | 630.22 | 630.22 | Top of Disk | 628.20 | 13.87 | 18.50 | 614.33 | 609.70 | 19.00 | 607.50 | 4.6 | 2 | 39.067106 | -89.399646 |
| G108 | UA | 02/12/2010 | | 630.22 | Top of Disk | 625.58 | 16.82 | 21.50 | 608.76 | 604.08 | 22.00 | 603.60 | 4.7 | 2 | 39.066984 | -89.400035 |
| G109 | UA | 02/11/2010 | | 629.76 | Top of Disk | 624.79 | 15.39 | 19.93 | 609.40 | 604.86 | 20.50 | 604.30 | 4.5 | 2 | 39.067045 | -89.400423 |
| G110 | UA | 02/11/2010 | | 629.65 | Top of Disk | 624.81 | 15.05 | 19.59 | 609.76 | 605.22 | 20.16 | 604.70 | 4.5 | 2 | 39.067172 | -89.400704 |
| G111 | UA | 02/11/2010 | | 629.90 | Top of Disk | 625.28 | 14.61 | 19.15 | 610.67 | 606.13 | 19.72 | 605.60 | 4.5 | 2 | 39.067292 | -89.40097 |
| G119 | UA | 02/09/2010 | | 631.55 | Top of Disk | 626.57 | 17.29 | 21.83 | 609.28 | 604.74 | 22.38 | 604.20 | 4.5 | 2 | 39.068986 | -89.401213 |
| G120 | UA | 02/08/2010 | | 631.87 | Top of Disk | 627.21 | 15.10 | 19.62 | 612.11 | 607.59 | 20.21 | 605.10 | 4.5 | 2 | 39.069479 | -89.401214 |
| G121 | UA | 02/04/2010 | | 632.83 | Top of Disk | 627.94 | 16.79 | 21.47 | 611.15 | 606.47 | 21.95 | 603.80 | 4.7 | 2 | 39.069781 | -89.401216 |
| G122 | UA | 02/04/2010 | | 632.69 | Top of Disk | 628.05 | 16.51 | 21.05 | 611.54 | 607.00 | 21.66 | 606.20 | 4.5 | 2 | 39.070098 | -89.401218 |
| G123 | UA | 02/04/2010 | | 632.96 | Top of Disk | 628.12 | 20.94 | 25.46 | 607.18 | 602.66 | 26.07 | 602.10 | 4.5 | 2 | 39.070399 | -89.401219 |
| G124 | UA | 02/03/2010 | | 633.39 | Top of Disk | 628.70 | 15.98 | 20.51 | 612.72 | 608.19 | 21.06 | 606.70 | 4.5 | 2 | 39.070715 | -89.40122 |
| G125 | UA | 02/03/2010 | | 633.51 | Top of Disk | 628.85 | 17.03 | 21.56 | 611.82 | 607.29 | 22.04 | 606.80 | 4.5 | 2 | 39.071003 | -89.401221 |
| G126 | UA | 02/10/2010 | | 625.39 | Top of Disk | 622.96 | 12.89 | 17.43 | 610.07 | 605.53 | 18.00 | 605.00 | 4.5 | 2 | 39.067304 | -89.401274 |
| G151 | UA | 12/19/2011 | | 625.93 | Top of Disk | 622.82 | 15.34 | 19.84 | 607.48 | 602.98 | 20.46 | 602.40 | 4.5 | 2 | 39.0672 | -89.40159 |
| G152 | UA | 12/20/2011 | | 626.52 | Top of Disk | 623.06 | 13.59 | 18.09 | 609.47 | 604.97 | 18.57 | 604.50 | 4.5 | 2 | 39.066275 | -89.401289 |



| Well Number | HSU | Date Constructed | Top of PVC Elevation (ft) | Measuring Point Elevation (ft) | Measuring Point Description | Ground Elevation (ft) | Screen Top Depth (ft BGS) | Screen Bottom Depth (ft BGS) | Screen Top Elevation (ft) | Screen Bottom Elevation (ft) | Well Depth (ft BGS) | Bottom of Boring Elevation (ft) | Screen Length (ft) | Screen Diameter (inches) | Latitude (Decimal Degrees) | Longitude (Decimal Degrees) |
|----------------|-----|---------------------|---------------------------------|---|-----------------------------------|-----------------------------|------------------------------------|---------------------------------------|---------------------------------|---------------------------------------|---------------------------|--|--------------------------|--------------------------------|----------------------------------|-----------------------------------|
| G153 | UA | 12/15/2011 | 626.35 | 626.40 | Top of Disk | 623.23 | 15.90 | 20.34 | 607.33 | 602.89 | 20.80 | 602.50 | 4.4 | 2 | 39.065857 | -89.402567 |
| G154 | UA | 12/16/2011 | | 626.35 | Top of Disk | 623.52 | 14.26 | 18.76 | 609.26 | 604.76 | 19.10 | 603.50 | 4.5 | 2 | 39.067089 | -89.403574 |
| G155 | UA | 12/19/2011 | | 625.86 | Top of Disk | 622.89 | 15.09 | 19.58 | 607.80 | 603.31 | 23.23 | 599.70 | 4.5 | 2 | 39.067493 | -89.402659 |
| G200 | UA | 02/25/2008 | | 625.94 | Top of Disk | 623.27 | 12.19 | 16.98 | 611.08 | 606.29 | 17.36 | 605.30 | 4.8 | 2 | 39.075139 | -89.395009 |
| G201 | UA | 02/25/2008 | 627.15 | 627.15 | Top of Riser | 624.19 | 13.01 | 17.80 | 611.18 | 606.39 | 18.15 | 606.00 | 4.8 | 2 | 39.075141 | -89.397829 |
| G205 | UA | 02/21/2008 | | 624.34 | Top of Disk | 622.10 | 10.04 | 14.53 | 612.06 | 607.57 | 15.07 | 606.10 | 4.5 | 2 | 39.068596 | -89.394147 |
| G206 | UA | 10/14/2010 | | 632.82 | Top of Disk | 630.53 | 17.51 | 21.92 | 613.02 | 608.61 | 22.42 | 606.50 | 4.4 | 2 | 39.067399 | -89.398548 |
| G206D | DA | 01/25/2021 | 634.14 | 634.14 | Top of PVC | 631.41 | 49.20 | 59.00 | 582.21 | 572.41 | 59.39 | 571.41 | 9.8 | 2 | 39.067428 | -89.398493 |
| G207 | UA | 10/08/2010 | | 633.21 | Top of Disk | 630.61 | 18.24 | 22.77 | 612.37 | 607.84 | 23.30 | 606.60 | 4.5 | 2 | 39.067568 | -89.397952 |
| G208 | UA | 10/07/2010 | | 633.16 | Top of Disk | 630.57 | 17.53 | 22.06 | 613.04 | 608.51 | 22.60 | 606.60 | 4.5 | 2 | 39.067743 | -89.397402 |
| G209 | UA | 10/07/2010 | | 632.91 | Top of Disk | 630.57 | 17.74 | 22.28 | 612.83 | 608.29 | 22.81 | 606.60 | 4.5 | 2 | 39.067923 | -89.39685 |
| G210 | UA | 10/06/2010 | | 632.99 | Top of Disk | 630.48 | 19.39 | 23.93 | 611.09 | 606.55 | 24.46 | 605.50 | 4.5 | 2 | 39.068088 | -89.396322 |
| G211 | UA | 10/11/2010 | | 632.64 | Top of Disk | 630.31 | 17.34 | 21.88 | 612.97 | 608.43 | 22.41 | 606.30 | 4.5 | 2 | 39.068263 | -89.395792 |
| G212 | UA | 10/11/2010 | | 632.89 | Top of Disk | 630.59 | 16.74 | 21.29 | 613.85 | 609.30 | 21.81 | 606.60 | 4.6 | 2 | 39.06843 | -89.395318 |
| G213 | UA | 10/12/2010 | | 632.81 | Top of Disk | 630.34 | 16.75 | 21.29 | 613.59 | 609.05 | 21.82 | 606.30 | 4.5 | 2 | 39.068585 | -89.394822 |
| G214 | UA | 10/14/2010 | | 632.85 | Top of Disk | 630.39 | 17.75 | 22.14 | 612.64 | 608.25 | 22.65 | 606.40 | 4.4 | 2 | 39.068919 | -89.393982 |
| G215 | UA | 10/13/2010 | | 633.06 | Top of Disk | 630.48 | 19.41 | 23.80 | 611.07 | 606.68 | 24.31 | 606.20 | 4.4 | 2 | 39.069309 | -89.39394 |
| G216 | UA | 10/13/2010 | | 632.76 | Top of Disk | 630.28 | 20.04 | 24.42 | 610.24 | 605.86 | 24.93 | 604.30 | 4.4 | 2 | 39.069765 | -89.393946 |
| G217 | UA | 10/12/2010 | | 633.10 | Top of Disk | 630.67 | 20.49 | 24.88 | 610.18 | 605.79 | 25.38 | 604.70 | 4.4 | 2 | 39.07034 | -89.393959 |
| G218 | UA | 10/12/2010 | | 633.11 | Top of Disk | 630.64 | 20.33 | 24.77 | 610.31 | 605.87 | 25.27 | 604.60 | 4.4 | 2 | 39.070876 | -89.393956 |
| G270 | UA | 02/26/2008 | | 625.86 | Top of Disk | 623.73 | 13.13 | 17.92 | 610.60 | 605.81 | 18.27 | 605.50 | 4.8 | 2 | 39.066564 | -89.397403 |
| G271 | UA | 09/10/2009 | | 625.57 | Top of Disk | 622.89 | 9.96 | 14.31 | 612.93 | 608.58 | 14.79 | 606.90 | 4.4 | 2 | 39.065007 | -89.395587 |
| G272 | UA | 09/10/2009 | | 623.81 | Top of Disk | 620.72 | 9.11 | 13.98 | 611.61 | 606.74 | 14.32 | 606.40 | 4.9 | 2 | 39.064989 | -89.394785 |



| Well Number | HSU | Date Constructed | Top of PVC Elevation (ft) | Measuring Point Elevation (ft) | Measuring Point Description | Ground Elevation (ft) | Screen Top Depth (ft BGS) | Screen Bottom Depth (ft BGS) | Screen Top Elevation (ft) | Screen Bottom Elevation (ft) | Well Depth (ft BGS) | Bottom of Boring Elevation (ft) | Screen Length (ft) | Screen Diameter (inches) | Latitude (Decimal Degrees) | Longitude (Decimal Degrees) |
|----------------|-----|---------------------|---------------------------------|---|-----------------------------------|-----------------------------|------------------------------------|---------------------------------------|---------------------------------|---------------------------------------|---------------------------|--|--------------------------|--------------------------------|----------------------------------|-----------------------------------|
| G273 | UA | 09/10/2009 | | 623.02 | Top of Disk | 620.17 | 9.08 | 14.56 | 611.09 | 605.61 | 15.10 | 604.20 | 5.5 | 2 | 39.064985 | -89.393973 |
| G274 | UA | 09/16/2009 | | 624.04 | Top of Disk | 621.67 | 12.90 | 17.67 | 608.77 | 604.00 | 18.06 | 603.60 | 4.8 | 2 | 39.064991 | -89.393198 |
| G275 | UA | 09/16/2009 | | 618.26 | Top of Disk | 616.14 | 8.22 | 12.62 | 607.92 | 603.52 | 13.19 | 603.00 | 4.4 | 2 | 39.065151 | -89.392561 |
| G275D | DA | 01/14/2021 | 620.31 | 620.31 | Top of PVC | 617.52 | 49.76 | 59.55 | 567.76 | 557.97 | 59.89 | 517.80 | 9.8 | 2 | 39.065121 | -89.392595 |
| G276 | UA | 09/16/2009 | | 632.00 | Top of Disk | 629.14 | 22.41 | 27.22 | 606.73 | 601.92 | 27.65 | 601.10 | 4.8 | 2 | 39.065534 | -89.392617 |
| G277 | UA | 09/14/2009 | | 623.08 | Top of Disk | 620.79 | 14.29 | 18.77 | 606.50 | 602.02 | 19.24 | 600.80 | 4.5 | 2 | 39.065927 | -89.392572 |
| G278 | UA | 09/11/2009 | 631.19 | 631.17 | Top of Disk | 628.85 | 18.93 | 23.70 | 609.92 | 605.15 | 24.06 | 604.80 | 4.8 | 2 | 39.066737 | -89.393161 |
| G279 | UA | 09/10/2009 | | 632.04 | Top of Disk | 629.19 | 22.40 | 26.79 | 606.79 | 602.40 | 27.30 | 601.20 | 4.4 | 2 | 39.067156 | -89.392998 |
| G280 | UA | 02/26/2008 | 625.35 | 625.35 | Top of Riser | 623.11 | 12.79 | 17.63 | 610.32 | 605.48 | 17.98 | 605.10 | 4.8 | 2 | 39.067216 | -89.394992 |
| G281 | UA | 09/08/2015 | | 626.36 | Top of Disk | 623.82 | 15.51 | 20.16 | 608.31 | 603.66 | 20.30 | 603.50 | 4.7 | 2 | 39.065405 | -89.399322 |
| G283 | LCU | 01/14/2021 | 610.75 | 610.75 | Top of PVC | 608.30 | 8.39 | 18.17 | 599.91 | 590.13 | 18.36 | 589.90 | 9.8 | 2 | 39.064645 | -89.392119 |
| G284 | UA | 02/03/2021 | 618.42 | 618.42 | Top of PVC | 615.33 | 8.08 | 12.85 | 607.25 | 602.48 | 13.23 | 601.30 | 4.8 | 2 | 39.065487 | -89.390631 |
| G285 | LCU | 01/25/2021 | 613.52 | 613.52 | Top of PVC | 610.54 | 13.68 | 23.45 | 596.86 | 587.09 | 23.83 | 584.50 | 9.8 | 2 | 39.066513 | -89.391474 |
| G286 | UA | 01/18/2021 | 613.13 | 613.13 | Top of PVC | 609.97 | 3.37 | 8.16 | 606.60 | 601.81 | 8.50 | 600.00 | 4.8 | 2 | 39.067277 | -89.391883 |
| G287 | UA | 01/20/2021 | 617.45 | 617.45 | Top of PVC | 614.34 | 5.43 | 10.25 | 608.91 | 604.09 | 10.59 | 602.50 | 4.8 | 2 | 39.068297 | -89.392388 |
| G288 | UA | 01/19/2021 | 620.07 | 620.07 | Top of PVC | 617.08 | 7.59 | 12.26 | 609.49 | 604.82 | 12.75 | 603.10 | 4.7 | 2 | 39.067834 | -89.390082 |
| G301 | UA | 09/04/2015 | | 622.65 | Top of Disk | 620.88 | 11.31 | 15.96 | 608.96 | 604.31 | 16.21 | 604.10 | 4.7 | 2 | 39.05951 | -89.395415 |
| G302 | UA | 09/04/2015 | | 620.04 | Top of Disk | 618.52 | 13.21 | 17.86 | 604.74 | 600.09 | 18.39 | 599.60 | 4.7 | 2 | 39.059544 | -89.393192 |
| G303 | UA | 08/26/2010 | | 622.02 | Top of Disk | 619.33 | 10.00 | 20.00 | 609.07 | 599.07 | 20.40 | 598.70 | 10 | 2 | 39.057144 | -89.391721 |
| G304 | UA | 08/26/2010 | | 626.72 | Top of Disk | 623.32 | 10.00 | 20.00 | 613.32 | 603.32 | 20.40 | 602.90 | 10 | 2 | 39.057205 | -89.395663 |
| G305 | UA | 05/03/2016 | 625.67 | 625.67 | Top of PVC | 623.23 | 13.44 | 18.27 | 609.10 | 604.27 | 18.50 | 604.10 | 4.8 | 2 | 39.056558 | -89.396798 |
| G306 | UA | 05/03/2016 | 625.91 | 625.91 | Top of PVC | 623.57 | 13.07 | 17.68 | 609.77 | 605.16 | 17.90 | 604.80 | 4.6 | 2 | 39.056494 | -89.393556 |
| G307 | UA | 07/27/2016 | 624.60 | 624.60 | Top of PVC | 624.73 | 12.96 | 17.80 | 609.12 | 604.28 | 18.22 | 603.90 | 4.8 | 2 | 39.057214 | -89.395545 |



| Well Number | HSU | Date Constructed | Top of PVC Elevation (ft) | Measuring Point Elevation (ft) | Measuring Point Description | Ground Elevation (ft) | Screen Top Depth (ft BGS) | Screen Bottom Depth (ft BGS) | Screen Top Elevation (ft) | Screen Bottom Elevation (ft) | Well Depth (ft BGS) | Bottom of Boring Elevation (ft) | Screen Length (ft) | Screen Diameter (inches) | Latitude (Decimal Degrees) | Longitude (Decimal Degrees) |
|----------------|-----|---------------------|---------------------------------|---|-----------------------------------|-----------------------------|------------------------------------|---------------------------------------|---------------------------------|---------------------------------------|---------------------------|--|--------------------------|--------------------------------|----------------------------------|-----------------------------------|
| G307D | LCU | 01/19/2021 | 624.88 | 624.88 | Top of PVC | 622.51 | 48.98 | 58.75 | 573.53 | 563.76 | 59.60 | 562.50 | 9.8 | 2 | 39.05721 | -89.39552 |
| G308 | UA | 01/18/2021 | 624.59 | 624.59 | Top of PVC | 621.59 | 10.10 | 14.89 | 611.49 | 606.70 | 15.24 | 605.80 | 4.8 | 2 | 39.057379 | -89.397134 |
| G309 | UA | 01/21/2021 | 625.88 | 625.88 | Top of PVC | 622.77 | 12.97 | 17.75 | 609.80 | 605.02 | 18.10 | 604.70 | 4.8 | 2 | 39.058508 | -89.397243 |
| G310 | UA | 02/09/2021 | 622.87 | 622.87 | Top of PVC | 619.89 | 10.24 | 15.03 | 609.65 | 604.86 | 15.38 | 604.00 | 4.8 | 2 | 39.059532 | -89.396907 |
| G311 | UA | 01/13/2021 | 621.04 | 621.04 | Top of PVC | 618.32 | 9.27 | 14.04 | 609.05 | 604.28 | 14.40 | 603.90 | 4.8 | 2 | 39.059513 | -89.394363 |
| G311D | LCU | 01/12/2021 | 621.24 | 621.24 | Top of PVC | 618.39 | 50.16 | 60.10 | 568.23 | 558.29 | 60.58 | 557.80 | 9.9 | 2 | 39.059513 | -89.394312 |
| G312 | UA | 01/15/2021 | 619.78 | 619.78 | Top of PVC | 616.92 | 9.79 | 14.58 | 607.13 | 602.34 | 14.93 | 601.70 | 4.8 | 2 | 39.059558 | -89.391983 |
| G313 | UA | 02/05/2021 | 614.30 | 614.30 | Top of PVC | 611.51 | 6.30 | 11.11 | 605.21 | 600.40 | 11.46 | 599.50 | 4.8 | 2 | 39.058773 | -89.391124 |
| G314 | LCU | 02/05/2021 | 613.88 | 613.88 | Top of PVC | 611.11 | 14.56 | 19.58 | 596.55 | 591.53 | 20.02 | 591.10 | 5 | 2 | 39.05782 | -89.390964 |
| G314D | DA | 02/04/2021 | 613.70 | 613.70 | Top of PVC | 610.87 | 39.34 | 49.11 | 571.53 | 561.76 | 49.47 | 510.60 | 9.8 | 2 | 39.057852 | -89.390958 |
| G315 | UA | 01/14/2021 | 623.52 | 623.52 | Top of PVC | 620.94 | 9.69 | 14.48 | 611.25 | 606.46 | 14.85 | 605.00 | 4.8 | 2 | 39.057165 | -89.393667 |
| G316 | LCU | 02/26/2021 | 602.59 | 602.59 | Top of PVC | 599.64 | 10.02 | 14.82 | 589.62 | 584.82 | 15.16 | 583.90 | 4.8 | 2 | 39.057847 | -89.389698 |
| G317 | UA | 02/12/2021 | 641.93 | 641.93 | Top of PVC | 638.85 | 30.14 | 34.93 | 608.71 | 603.92 | 35.28 | 602.90 | 4.8 | 2 | 39.056727 | -89.390148 |
| G401 | UA | 09/14/2015 | | 625.57 | Top of Disk | 623.03 | 14.36 | 18.79 | 608.67 | 604.24 | 19.29 | 603.70 | 4.4 | 2 | 39.060259 | -89.395295 |
| G402 | UA | 08/27/2010 | | 613.37 | Top of Disk | 610.36 | 10.00 | 20.00 | 600.36 | 590.36 | 20.40 | 590.00 | 10 | 2 | 39.060207 | -89.391712 |
| G403 | UA | 09/11/2015 | | 626.47 | Top of Disk | 623.81 | 13.11 | 17.78 | 610.70 | 606.03 | 18.15 | 605.70 | 4.7 | 2 | 39.063167 | -89.398779 |
| G404 | UA | 05/01/2007 | | 615.67 | Top of Disk | 613.57 | 6.42 | 11.17 | 607.15 | 602.40 | 11.62 | 601.60 | 4.8 | 2 | 39.064329 | -89.392493 |
| G405 | UA | 05/01/2007 | | 623.63 | Top of Disk | 621.40 | 9.01 | 13.76 | 612.39 | 607.64 | 14.21 | 607.20 | 4.8 | 2 | 39.064345 | -89.396234 |
| G406 | UA | 08/19/2016 | 625.36 | 625.36 | Top of PVC | 621.86 | 13.56 | 18.37 | 608.30 | 603.49 | 18.75 | 603.10 | 4.8 | 2 | 39.060309 | -89.398508 |
| G407 | UA | 08/16/2016 | 621.32 | 621.32 | Top of PVC | 618.35 | 13.78 | 18.61 | 604.57 | 599.74 | 19.04 | 598.40 | 4.8 | 2 | 39.061574 | -89.402004 |
| G410 | UA | 02/23/2018 | | 619.79 | Top of Disk | 617.21 | 8.89 | 13.68 | 608.32 | 603.53 | 14.09 | 603.10 | 4.8 | 2 | 39.061572 | -89.403763 |
| G411 | UA | 02/22/2018 | | 623.25 | Top of Disk | 620.49 | 11.21 | 16.07 | 609.28 | 604.42 | 16.47 | 604.00 | 4.9 | 2 | 39.063979 | -89.404033 |
| MW01D | DA | 05/03/2006 | 609.02 | 609.02 | Top of PVC | 607.08 | 33.29 | 38.05 | 573.79 | 569.03 | 38.41 | 567.10 | 4.8 | 2 | 39.067068 | -89.402747 |



| Well Number | HSU | Date Constructed | Top of PVC Elevation (ft) | Measuring Point Elevation (ft) | Measuring Point Description | Ground Elevation (ft) | Screen Top Depth (ft BGS) | Screen Bottom Depth (ft BGS) | Screen Top Elevation (ft) | Screen Bottom Elevation (ft) | Well Depth (ft BGS) | Bottom of Boring Elevation (ft) | Screen Length (ft) | Screen Diameter (inches) | Latitude (Decimal Degrees) | Longitude (Decimal Degrees) |
|----------------|-----|---------------------|---------------------------------|---|-----------------------------------|-----------------------------|------------------------------------|---------------------------------------|---------------------------------|---------------------------------------|---------------------------|--|--------------------------|--------------------------------|----------------------------------|-----------------------------------|
| MW02S | UA | 05/05/2006 | 627.12 | 627.12 | Top of PVC | 624.16 | 10.34 | 15.12 | 613.82 | 609.04 | 15.51 | 608.70 | 4.8 | 2 | 39.071017 | -89.403648 |
| MW02D | LCU | 05/05/2006 | 626.99 | 626.99 | Top of PVC | 624.14 | 22.03 | 26.83 | 602.11 | 597.31 | 27.22 | 596.90 | 4.8 | 2 | 39.071031 | -89.403649 |
| MW03D | DA | 04/27/2006 | 629.01 | 629.01 | Top of PVC | 625.86 | 52.29 | 57.06 | 573.57 | 568.80 | 57.40 | 567.90 | 4.8 | 2 | 39.071386 | -89.398976 |
| MW04S | UA | 05/11/2006 | 625.89 | 625.89 | Top of PVC | 622.63 | 9.83 | 14.26 | 612.80 | 608.37 | 14.77 | 607.90 | 4.4 | 2 | 39.075356 | -89.399232 |
| MW05S | UA | 05/17/2006 | 625.95 | 625.95 | Top of PVC | 622.65 | 12.66 | 17.41 | 609.99 | 605.24 | 17.71 | 604.90 | 4.8 | 2 | 39.075866 | -89.40333 |
| MW05D | DA | 05/17/2006 | 625.91 | 625.91 | Top of PVC | 622.65 | 45.57 | 50.33 | 577.08 | 572.32 | 50.72 | 568.70 | 4.8 | 2 | 39.075863 | -89.403313 |
| MW06S | UA | 05/04/2006 | 626.15 | 626.15 | Top of PVC | 623.37 | 11.04 | 15.62 | 612.33 | 607.75 | 16.08 | 607.30 | 4.6 | 2 | 39.078189 | -89.403644 |
| MW07S | UA | 05/09/2006 | 627.60 | 627.60 | Top of PVC | 624.90 | 9.91 | 13.79 | 614.99 | 611.11 | 14.39 | 610.50 | 3.9 | 2 | 39.0786 | -89.399383 |
| MW08S | UA | 05/10/2006 | 628.01 | 628.01 | Top of PVC | 625.09 | 11.51 | 16.00 | 613.58 | 609.09 | 16.60 | 608.00 | 4.5 | 2 | 39.080234 | -89.399079 |
| MW09S | UA | 05/03/2006 | 627.62 | 627.62 | Top of PVC | 624.70 | 11.21 | 15.62 | 613.49 | 609.08 | 16.20 | 608.50 | 4.4 | 2 | 39.079954 | -89.394899 |
| MW09D | LCU | 05/03/2006 | 627.61 | 627.61 | Top of PVC | 624.68 | 45.81 | 50.57 | 578.87 | 574.11 | 51.00 | 570.70 | 4.8 | 2 | 39.07994 | -89.394899 |
| MW10S | UA | 05/02/2006 | 624.45 | 624.45 | Top of PVC | 621.43 | 11.28 | 15.76 | 610.15 | 605.67 | 16.30 | 605.10 | 4.5 | 2 | 39.07601 | -89.394068 |
| MW10D | LCU | 05/01/2006 | 624.47 | 624.47 | Top of PVC | 621.33 | 41.74 | 46.57 | 579.59 | 574.76 | 47.02 | 572.60 | 4.8 | 2 | 39.075995 | -89.39407 |
| MW11S | UA | 04/28/2006 | 625.27 | 625.27 | Top of PVC | 622.04 | 8.89 | 13.63 | 613.15 | 608.41 | 14.08 | 608.00 | 4.7 | 2 | 39.071888 | -89.393913 |
| MW11D | LCU | 04/28/2006 | 625.52 | 625.52 | Top of PVC | 622.19 | 28.31 | 33.04 | 593.88 | 589.15 | 33.50 | 585.90 | 4.7 | 2 | 39.071888 | -89.393894 |
| MW12S | UA | 05/10/2006 | 625.31 | 625.31 | Top of PVC | 622.24 | 10.61 | 15.18 | 611.63 | 607.06 | 15.61 | 606.60 | 4.6 | 2 | 39.068514 | -89.394199 |
| MW12D | DA | 05/10/2006 | 625.21 | 625.21 | Top of PVC | 622.24 | 42.46 | 46.99 | 579.78 | 575.25 | 47.47 | 572.20 | 4.5 | 2 | 39.068501 | -89.394199 |
| MW13S | UA | 05/09/2006 | 625.96 | 625.96 | Top of PVC | 622.80 | 11.43 | 16.23 | 611.37 | 606.57 | 16.62 | 606.20 | 4.8 | 2 | 39.066297 | -89.40118 |
| MW13D | DA | 05/09/2006 | 625.86 | 625.86 | Top of PVC | 622.85 | 49.81 | 54.60 | 573.04 | 568.25 | 55.00 | 567.90 | 4.8 | 2 | 39.066293 | -89.401163 |
| MW14S | UA | 05/02/2006 | 626.88 | 626.88 | Top of PVC | 624.62 | 12.26 | 17.02 | 612.36 | 607.60 | 17.38 | 607.20 | 4.8 | 2 | 39.069153 | -89.400442 |
| MW15S | UA | 04/25/2006 | 626.66 | 626.66 | Top of PVC | 623.83 | 14.41 | 19.16 | 609.42 | 604.67 | 19.62 | 604.20 | 4.8 | 2 | 39.069772 | -89.397088 |
| MW15D | LCU | 04/25/2006 | 626.44 | 626.44 | Top of PVC | 623.83 | 33.68 | 38.45 | 590.15 | 585.38 | 38.80 | 585.00 | 4.8 | 2 | 39.06977 | -89.397073 |
| MW16S | UA | 04/25/2006 | 629.47 | 629.47 | Top of PVC | 626.32 | 14.59 | 19.41 | 611.73 | 606.91 | 19.76 | 606.40 | 4.8 | 2 | 39.073571 | -89.397006 |



| Well Number | HSU | Date Constructed | Top of PVC Elevation (ft) | Measuring Point Elevation (ft) | Measuring Point Description | Ground Elevation (ft) | Screen Top Depth (ft BGS) | Screen Bottom Depth (ft BGS) | Screen Top Elevation (ft) | Screen Bottom Elevation (ft) | Well Depth (ft BGS) | Bottom of Boring Elevation (ft) | Screen Length (ft) | Screen Diameter (inches) | Latitude (Decimal Degrees) | Longitude (Decimal Degrees) |
|----------------|-----|---------------------|---------------------------------|---|-----------------------------------|-----------------------------|------------------------------------|---------------------------------------|---------------------------------|---------------------------------------|---------------------------|--|--------------------------|--------------------------------|----------------------------------|-----------------------------------|
| MW16D | DA | 04/25/2006 | 629.38 | 629.38 | Top of PVC | 626.37 | 45.90 | 50.34 | 580.47 | 576.03 | 50.78 | 575.40 | 4.4 | 2 | 39.073571 | -89.397036 |
| MW17S | UA | 05/04/2006 | 630.56 | 630.56 | Top of PVC | 627.28 | 14.02 | 23.56 | 613.26 | 603.72 | 24.11 | 603.20 | 9.5 | 2 | 39.07715 | -89.396978 |
| MW17D | DA | 05/04/2006 | 630.29 | 630.29 | Top of PVC | 627.47 | 48.82 | 53.32 | 578.65 | 574.15 | 53.87 | 573.60 | 4.5 | 2 | 39.077151 | -89.396958 |
| MW18S | UA | 05/11/2006 | 628.66 | 628.66 | Top of PVC | 625.69 | 11.31 | 15.79 | 614.38 | 609.90 | 16.40 | 609.30 | 4.5 | 2 | 39.077033 | -89.401698 |
| MW20S | UA | 05/01/2007 | 622.90 | 622.90 | Top of PVC | 620.26 | 8.41 | 13.22 | 611.85 | 607.04 | 13.67 | 604.30 | 4.8 | 2 | 39.064968 | -89.394322 |
| R104 | UA | 10/08/2010 | | 632.84 | Top of Disk | 629.03 | 14.59 | 19.32 | 614.44 | 609.71 | 19.85 | 609.20 | 4.7 | 2 | 39.069474 | -89.399109 |
| R201 | UA | 10/08/2010 | | 626.34 | Top of Disk | 624.02 | 14.59 | 19.32 | 609.43 | 604.70 | 19.85 | 604.20 | 4.7 | 2 | 39.075142 | -89.397855 |
| R205 | UA | 03/20/2017 | | 624.52 | Top of Disk | 621.91 | 11.32 | 16.01 | 610.59 | 605.90 | 16.42 | 605.50 | 4.7 | 2 | 39.068593 | -89.394164 |
| T127 | UA | 02/10/2010 | | 630.96 | Top of Disk | 625.53 | 17.53 | 22.07 | 608.00 | 603.46 | 22.64 | 602.90 | 4.5 | 2 | 39.068119 | -89.40121 |
| T128 | UA | 02/09/2010 | 631.03 | 630.93 | Top of Disk | 626.27 | 16.53 | 21.04 | 609.74 | 605.23 | 21.64 | 602.20 | 4.5 | 2 | 39.068532 | -89.401211 |
| T202 | UA | 10/15/2010 | | 628.63 | Top of Disk | 626.22 | 12.27 | 16.65 | 613.95 | 609.57 | 17.21 | 608.20 | 4.4 | 2 | 39.071776 | -89.397705 |
| T408 | LCU | 08/17/2016 | 624.08 | 624.08 | Top of PVC | 621.09 | 20.66 | 25.49 | 600.43 | 595.60 | 25.92 | 595.20 | 4.8 | 2 | 39.064353 | -89.396307 |
| T409 | LCU | 08/19/2016 | 625.01 | 625.01 | Top of PVC | 621.85 | 21.79 | 26.59 | 600.06 | 595.26 | 26.99 | 594.90 | 4.8 | 2 | 39.0603 | -89.398538 |
| TA31 | UA | 10/28/2014 | 626.55 | 626.55 | Top of PVC | 623.89 | 15.09 | 19.57 | 608.80 | 604.32 | 20.19 | 603.70 | 4.5 | 2 | 39.071368 | -89.401366 |
| TA32 | UA | 10/27/2014 | 621.42 | 621.42 | Top of PVC | 618.93 | 11.31 | 15.68 | 607.62 | 603.25 | 16.47 | 602.50 | 4.4 | 2 | 39.074093 | -89.402223 |
| TA33 | UA | 06/02/2015 | 625.27 | 625.27 | Top of PVC | 622.51 | 12.23 | 16.89 | 610.28 | 605.62 | 17.44 | 605.10 | 4.7 | 2 | 39.071556 | -89.403506 |
| TA34 | UA | 06/03/2015 | 626.52 | 626.52 | Top of PVC | 624.10 | 10.92 | 15.41 | 613.18 | 608.69 | 16.10 | 608.00 | 4.5 | 2 | 39.069631 | -89.402759 |
| TR32 | UA | 07/02/2021 | 621.68 | 621.68 | Top of PVC | 619.28 | 11.00 | 15.68 | 608.28 | 603.60 | 16.17 | 603.11 | 4.68 | 2 | 39.074064 | -89.397758 |
| XPW01 | CCR | 01/14/2021 | 634.57 | 634.57 | Top of PVC | 631.85 | 8.21 | 12.98 | 623.64 | 618.87 | 13.36 | 617.90 | 4.8 | 2 | 39.057878 | -89.396196 |
| XPW02 | CCR | 02/08/2021 | 639.69 | 639.69 | Top of PVC | 636.64 | 8.05 | 17.85 | 628.59 | 618.79 | 18.20 | 618.40 | 9.8 | 2 | 39.058828 | -89.395267 |
| XSG-01 | CCR | | 635.52 | 635.52 | staff gauge | 635.52 | | | | | | | | | 39.059128 | -89.396727 |
| SG-02 | SW | | | 605.87 | Top of Prot Casing | 605.87 | | | | | | | | | 39.059695 | -89.391429 |
| SG-03 | SW | | | 594.94 | Top of Prot Casing | 594.94 | | | | | | | | | 39.059092 | -89.390342 |



TABLE 3-1. MONITORING WELL LOCATIONS AND CONSTRUCTION DETAILS

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| N | Well lumber | HSU | Date Constructed | Top of PVC Elevation (ft) | Measuring Point Elevation (ft) | Measuring Point Description | Ground Elevation (ft) | Screen Top Depth (ft BGS) | Screen Bottom Depth (ft BGS) | Screen Top Elevation (ft) | Screen Bottom Elevation (ft) | Well Depth (ft BGS) | Bottom of Boring Elevation (ft) | Screen Length (ft) | Screen Diameter (inches) | Latitude (Decimal Degrees) | Longitude (Decimal Degrees) | |
|---|----------------|-----|---------------------|---------------------------------|---|-----------------------------------|-----------------------------|------------------------------------|---------------------------------------|---------------------------------|---------------------------------------|---------------------------|--|--------------------------|--------------------------------|----------------------------------|-----------------------------------|--|
| | SG-04 | SW | | | 599.52 | Top of Prot Casing | 599.52 | | | | | | | | | 39.064146 | -89.390504 | |

Notes:

All elevation data are presented relative to the North American Vertical Datum 1988 (NAVD88), GEOID 12A

-- = data not available
BGS = below ground surface
CCR = Coal Combustion Residual

DA = deep aquifer

ft = foot or feet

HSU = Hydrostratigraphic Unit LCU = lower confining unit PVC = polyvinyl chloride SW = surface water

UA = uppermost aquifer

generated 10/05/2021, 2:17:49 PM CDT



TABLE 3-2. VERTICAL HYDRAULIC GRADIENTS

| Date | G405 Groundwater Elevation (ft NAVD88) UA | T408 Groundwater Elevation (ft NAVD88) LCU (upper) | Head Change (ft) | Distance Change ¹ (ft) | Vertical H Gradie (dh/ | ent ² |
|------------|---|--|------------------------|---|------------------------------|------------------|
| 2/4/2017 | 618.47 | 619.46 | -0.99 | 12.00 | -0.08 | up |
| 5/13/2017 | 618.74 | 619.00 | -0.26 | 12.00 | -0.02 | up |
| 7/8/2017 | 618.54 | 619.12 | -0.58 | 12.00 | -0.05 | up |
| 10/21/2017 | 614.47 | 614.81 | -0.34 | 12.00 | -0.03 | up |
| 5/8/2018 | 618.94 | 615.82 | 3.12 | 12.00 | 0.26 | down |
| 8/2/2018 | 617.55 | 614.45 | 3.10 | 12.00 | 0.26 | down |
| 10/23/2018 | 616.40 | 616.30 | 0.10 | 12.00 | 0.01 | down |
| 1/15/2019 | 616.81 | 617.01 | -0.20 | 12.00 | -0.02 | up |
| 8/5/2019 | 617.72 | 617.15 | 0.57 | 12.00 | 0.05 | down |
| 1/20/2020 | 619.28 | 619.13 | 0.15 | 12.00 | 0.01 | down |
| 8/10/2020 | 617.62 | 617.38 | 0.24 | 12.00 | 0.02 | down |
| 1/20/2021 | 617.12 | 616.85 | 0.27 | 12.00 | 0.02 | down |
| 4/20/2021 | 617.13 | 616.65 | 0.48 | 12.00 | 0.04 | down |
| 7/26/2021 | 617.37 | 617.21 | 0.16 | down | | |
| | | | Middle | G405D | 610.0 | |
| | | | Middle | n T408 | 598.0 | |

| Date | G406 Groundwater Elevation (ft NAVD88) UA | T409 Groundwater Elevation (ft NAVD88) LCU (upper) | Head Change (ft) | Distance Change ¹ (ft) | Vertical Hydraulic Gradient ² (dh/dl) | | | |
|------------|---|--|------------------------|---|--|-------|-------|----|
| 2/4/2017 | 617.52 | 615.93 | 1.59 | 8.23 | 0.19 | down | | |
| 5/13/2017 | 616.20 | 616.75 | -0.55 | 8.23 | -0.07 | up | | |
| 7/8/2017 | 616.29 | 617.05 | -0.76 | 8.23 | -0.09 | up | | |
| 10/21/2017 | 611.27 | 612.16 | -0.89 | 8.23 | -0.11 | up | | |
| 5/8/2018 | 615.47 | 616.02 | -0.55 | 8.23 | -0.07 | up | | |
| 8/2/2018 | 615.75 | 615.25 | 0.50 | 8.23 | 0.06 | down | | |
| 10/23/2018 | 614.11 | 613.96 | 0.15 | 8.23 | 0.02 | down | | |
| 1/15/2019 | 615.36 | 614.78 | 0.58 | 8.23 | 0.07 | down | | |
| 8/5/2019 | 616.50 | 615.10 | 1.40 | 8.23 | 0.17 | down | | |
| 1/20/2020 | 617.48 | 617.16 | 0.32 | 8.23 | 0.04 | down | | |
| 8/10/2020 | 615.54 | 615.43 | 0.11 | 8.23 | 0.01 | down | | |
| 1/20/2021 | 612.97 | | | 614.41 | 12.97 614.41 -1.44 | 8.23 | -0.17 | up |
| 4/20/2021 | 613.78 | 615.33 | -1.55 | 8.23 | -0.19 | up | | |
| 7/26/2021 | 614.20 | 615.72 | -1.52 | 8.23 | -0.18 | up | | |
| | | | | of screen elevation | n G406 | 605.9 | | |
| | | | Middle | of screen elevation | n T409 | 597.7 | | |

TABLE 3-2. VERTICAL HYDRAULIC GRADIENTS

| Date | T408 Groundwater Elevation (ft NAVD88) LCU (upper) | G45D Groundwater Elevation (ft NAVD88) LCU (lower) | Head Change (ft) | Distance Change ¹ (ft) | Vertical H Gradie (dh/ | ent ² | | | |
|------------|--|--|------------------------|---|------------------------------|------------------|--|--|--|
| 2/4/2017 | 619.46 | 587.71 | 31.75 | 13.78 | 2.30 | down | | | |
| 5/13/2017 | 619.00 | 586.19 | 32.81 | 13.78 | 2.38 | down | | | |
| 7/8/2017 | 619.12 | 586.29 | 32.83 | 2.38 | down | | | | |
| 10/21/2017 | 614.81 | 584.69 | 30.12 | | | | | | |
| 5/8/2018 | 615.82 | 587.56 | 28.26 | 13.78 | 2.05 | down | | | |
| 8/2/2018 | 614.45 | 585.81 | 28.64 | 13.78 | 2.08 | down | | | |
| 10/23/2018 | 616.30 | 584.60 | 31.70 | 13.78 | 2.30 | down | | | |
| 1/15/2019 | 617.01 | 586.96 | 30.05 | 13.78 | 2.18 | down | | | |
| 8/5/2019 | 617.15 | 588.04 | 29.11 | 13.78 | 2.11 | down | | | |
| 8/10/2020 | 617.38 | 614.21 | 3.17 | 13.78 | 0.23 | down | | | |
| 1/20/2021 | 616.85 | 614.60 | 2.25 | 13.78 | 0.16 | down | | | |
| 4/20/2021 | 616.65 | 614.32 | 2.33 | 0.17 | down | | | | |
| 7/26/2021 | 617.21 | 613.58 | 3.63 | 0.26 | down | | | | |
| | _ | _ | Middle | n T408 | 598.0 | | | | |
| | | | Middle | 584.2 | | | | | |

| Date | T409 Groundwater Elevation (ft NAVD88) LCU (upper) | G46D Groundwater Elevation (ft NAVD88) LCU (lower) | Head Change (ft) | Distance Change ¹ (ft) | Vertical F Gradi (dh <i>i</i> | ent ² |
|------------|--|--|------------------------|---|-------------------------------------|------------------|
| 2/4/2017 | 615.93 | 586.06 | 29.87 | 22.19 | 1.35 | down |
| 5/13/2017 | 616.75 | 584.87 | 31.88 | 22.19 | 1.44 | down |
| 7/8/2017 | 617.05 | 585.22 | 31.83 | 22.19 | 1.43 | down |
| 5/8/2018 | 616.02 | 585.86 | 30.16 | 22.19 | 1.36 | down |
| 8/2/2018 | 615.25 | 583.95 | 31.30 | 22.19 | 1.41 | down |
| 10/23/2018 | 613.96 | 582.05 | 31.91 | 22.19 | 1.44 | down |
| 1/15/2019 | 614.78 | 583.17 | 31.61 | 22.19 | 1.42 | down |
| 8/5/2019 | 615.10 | 583.68 | 31.42 | 22.19 | 1.42 | down |
| 8/10/2020 | 615.43 | 609.00 | 6.43 | 22.19 | 0.29 | down |
| 1/20/2021 | 614.41 | 610.49 | 3.92 | 22.19 | 0.18 | down |
| 4/20/2021 | 615.33 | 611.06 | 4.27 | 22.19 | 0.19 | down |
| 7/26/2021 | 615.72 | 607.21 | 8.51 | down | | |
| | | | Middle | of screen elevation | n T409 | 597.7 |
| | | | Middle | of screen elevatio | n G46D | 575.5 |

TABLE 3-2. VERTICAL HYDRAULIC GRADIENTS

| Date | G307 Groundwater Elevation (ft NAVD88) UA | G307D Groundwater Elevation (ft NAVD88) LCU (lower) | Head Change (ft) | Distance Change ¹ (ft) | Vertical H Gradie (dh/ | ent ² |
|-----------|---|---|------------------------|---|------------------------------|------------------|
| 4/20/2021 | 624.50 | 622.48 | 2.02 | 38.06 | 0.05 | down |
| 5/17/2021 | 624.45 | 622.44 | 2.01 | 38.06 | 0.05 | down |
| 7/12/2021 | 624.45 | 622.59 | 1.86 | 38.06 | 0.05 | down |
| _ | _ | | Middle | of screen elevation | n G307 | 606.7 |
| | | | Middle | G307D | 568.6 | |

| Date | G311 Groundwater Elevation (ft NAVD88) UA | G311D Groundwater Elevation (ft NAVD88) LCU (lower) | Head Change (ft) | Distance Change ¹ (ft) | Vertical I Gradi (dh. | ient ² |
|-----------|---|---|------------------------|---|-----------------------------|-------------------|
| 3/29/2021 | 616.54 | 575.42 | 41.12 | 43.41 | 0.95 | down |
| 4/22/2021 | 613.68 | 575.74 | 37.94 | 0.87 | down | |
| 5/3/2021 | 614.01 | 573.09 | 40.92 | down | | |
| 5/17/2021 | 613.86 | 572.40 | 41.46 | 43.41 | 0.96 | down |
| 6/9/2021 | 613.13 | 573.85 | 39.28 | 43.41 | 0.90 | down |
| 6/15/2021 | 612.78 | 575.25 | 37.53 | 43.41 | 0.86 | down |
| 6/23/2021 | 612.45 | 571.74 | 40.71 | 43.41 | 0.94 | down |
| 7/12/2021 | 613.75 | 571.63 | 42.12 | 43.41 | 0.97 | down |
| 7/26/2021 | 613.05 | 569.74 | 43.31 | down | | |
| | _ | _ | Middle | 606.7 | | |
| | | | Middle | 563.3 | | |

TABLE 3-2. VERTICAL HYDRAULIC GRADIENTS

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Date | G314 Groundwater Elevation (ft NAVD88) LCU (upper) | G314D Groundwater Elevation (ft NAVD88) DA (PMP) | Head Change (ft) | Distance Change ¹ (ft) | Vertical H Gradie (dh/ | ent ² |
|-----------|--|--|------------------------|---|------------------------------|------------------|
| 3/29/2021 | 596.40 | 572.75 | 23.65 | 29.76 | 0.79 | down |
| 4/20/2021 | 603.16 | 571.76 | 31.40 | down | | |
| 5/3/2021 | 604.66 | 568.77 | 35.89 | 27.40 | 1.31 | down |
| 5/17/2021 | 605.61 | 566.84 | 38.77 | 27.40 | 1.42 | down |
| 6/9/2021 | 607.54 | 567.45 | 40.09 | 27.40 | 1.46 | down |
| 6/14/2021 | 608.16 | 568.60 | 39.56 | 27.40 | 1.44 | down |
| 6/23/2021 | 605.19 | 566.77 | 38.42 | 27.40 | 1.40 | down |
| 7/12/2021 | 605.32 | 566.88 | 38.44 | 27.40 | 1.40 | down |
| 7/26/2021 | 606.66 | 566.65 | 40.01 | down | | |
| | | | Middle | of screen elevation | n G314 | 594.0 |
| | | | Middle o | G314D | 566.6 | |

[O: KLT 6/4/21, C:YMD 6/7/21; U:KLT 8/25/21, C:EDP 8/31/21]

Notes:

DA = deep aquifer

dh = head change

dl = distance change

ft = foot/feet

LCU (lower) = lower confining unit (Smithboro)

LCU (upper) = lower confining unit (Vandalia)

NAVD88 = North American Vertical Datum of 1988

PMP = potential migration pathway

UA = uppermost aquifer

¹ Distance change was calculated using the midpoint of the piezometer screen and water table surface. If the water table surface was above the top of the monitoring well screen, then distance change was calculated using the midpoint of both screens.

 $^{^{2}}$ Vertical gradients between ± 0.0015 are considered flat, and typically have less than 0.02 foot difference in groundwater elevation between wells.

^{- - =} no data collected on date / no vertical gradient calculated

TABLE 3-3. FIELD HYDRAULIC CONDUCTIVITIES

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT **COFFEEN POWER PLANT** ASH POND NO. 1 COFFEEN, ILLINOIS

| Well ID | Gradient Position | Bottom of Screen Elevation (ft NAVD88) | Screen Length ¹ (ft) | Field Identified Screened Material | Slug Type | Analysis Method | Falling Head (Slug In) Hydraulic Conductivity (cm/s) | Rising Head (Slug Out) Hydraulic Conductivity (cm/s) | Minimum Hydraulic Conductivity (cm/s) | Maximum Hydraulic Conductivity (cm/s) | Hydraulic Conductivity Geometric Mean (cm/s) |
|-----------|----------------------|--|------------------------------------|---------------------------------------|-----------|--------------------------|--|--|--|--|---|
| Uppermost | t Aquifer | | | | | | | | | | |
| G301 | D | 604.31 | 4.65 | (ML)s | solid | Kansas Geological Survey | 1.1E-03 | 1.2E-03 | | | |
| G303 | D | 599.07 | 10 | CL | solid | Kansas Geological Survey | 2.8E-04 | 2.6E-04 | | | |
| G308 | D | 606.70 | 4.79 | s(ML), s(CL), (CL)s | solid | Kansas Geological Survey | 5.5E-03 | 1.6E-03 | | | |
| G309 | D | 605.02 | 4.78 | SP, s(CL), (ML)s | solid | Kansas Geological Survey | 9.1E-03 | 8.8E-04 | | | |
| G310 | D | 604.86 | 4.79 | SM, s(ML) | solid | Kansas Geological Survey | 7.5E-03 | 5.9E-03 | 2.6E-04 | 9.1E-03 | 2.0E-03 |
| G311 | D | 604.28 | 4.77 | s(ML), s(CL) | solid | Bouwer-Rice | 1.5E-03 | | | | |
| G312 | D | 602.34 | 4.79 | s(ML), s(CL) | solid | Kansas Geological Survey | 1.1E-03 | 1.1E-03 | | | |
| G313 | D | 600.40 | 4.81 | SP, s(ML), (CL)s | solid | Kansas Geological Survey | 2.7E-03 | 3.5E-03 | | | |
| G315 | D | 606.46 | 4.79 | s(CL) | solid | Kansas Geological Survey | 6.6E-03 | 5.8E-03 | | | |
| Lower Con | fining Unit | | | | | | | | | | |
| G307D | D | 563.76 | 9.77 | (CL)s | solid | Kansas Geological Survey | 3.2E-04 | 1.2E-04 | | | |
| G311D | D | 558.29 | 9.94 | CL | solid | Kansas Geological Survey | 3.8E-04 | 2.1E-04 | 1.2E-04 | 2.3E-03 | 5.0E-04 |
| G316 | D | 584.82 | 4.80 | | | Kansas Geological Survey | 2.3E-03 | 2.3E-03 | | | |
| Deep Aqui | fer (PMP) | | | | | | • | | | | |
| G314D | D | 561.76 | 9.77 | SP, s(CL) | solid | Bouwer-Rice | 3.3E-04 | 2.3E-05 | 2.3E-05 | 3.3E-04 | 8.7E-05 |
| | | | | | | | | | | [O: KLT 07/0 | 9/21; C:EDP 8/31/21] |

1. All wells are constructed from 2 inch PVC with 0.01 inch slotted screens.

- - = Test not analyzed/performed

cm/s = centimeters per second

D = downgradient

ft = foot/feet

NAVD88 = North American Vertical Datum of 1988

PMP= potential migration pathway

PVC = polyvinyl chloride

USCS = Unified Soil Classification System
CL = Lean Clay
s(CL) = Sandy Lean Clay
(CL)s = Lean Clay with Sand
s(ML) = Sandy Silt
(ML)s = Silt with Sand
SP = Poorly-Graded Sand



TABLE 3-4. HORIZONTAL HYDRAULIC GRADIENTS AND GROUNDWATER FLOW VELOCITIES

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

 $V = K i / n_e$ V = Groundwater Velocity

K = Hydraulic Conductivity ¹ i = hydraulic gradient $n_e = Effective Porosity$ ²

Across Ash Pond No. 1 (G308 to G301)

Distance between Wells (ft): 920
Hydraulic Conductivity (ft/day): 6.80

Effective Porosity (%): 14 Assumes: Silt and Clay

| Date | G308 Elevation (ft NAVD88) | G301 Elevation (ft NAVD88) | Change in Elevation (ft) | Horizontal Gradient (ft/ft) | Velocity (ft/day) |
|-----------------|-------------------------------|-------------------------------|--------------------------------|-----------------------------------|----------------------|
| 4/20/21-4/21/21 | 620.15 | 616.05 | 4.10 | 0.004 | 0.22 |
| 5/3/2021 | 620.04 | 616.12 | 3.92 | 0.004 | 0.21 |
| 5/17/2021 | 619.93 | 615.99 | 3.94 | 0.004 | 0.22 |
| 6/9/2021 | 619.17 | 615.63 | 3.54 | 0.004 | 0.19 |
| 6/23/2021 | 618.54 | 615.02 | 3.52 | 0.004 | 0.19 |
| 7/12/2021 | 620.22 | 615.79 | 4.43 | 0.005 | 0.24 |
| 7/26/2021 | 619.68 | 615.31 | 4.37 | 0.005 | 0.24 |
| | | | Average | 0.004 | 0.22 |

Across Ash Pond No. 1 (G315 to G312)

Distance between Wells (ft): 995 Hydraulic Conductivity (ft/day): 10.48

Effective Porosity (%): 14 Assumes: Silt and Clay

| =11000110101010101010101010101010101010 | | | | , | |
|---|-------------------------------|-------------------------------|--------------------------------|-----------------------------------|----------------------|
| Date | G315 Elevation (ft NAVD88) | G312 Elevation (ft NAVD88) | Change in Elevation (ft) | Horizontal Gradient (ft/ft) | Velocity (ft/day) |
| 3/29/2021 | 621.24 | 612.19 | 9.05 | 0.009 | 0.71 |
| 4/20/2021 | 621.05 | 609.11 | 11.94 | 0.012 | 0.93 |
| 5/3/2021 | 621.13 | 609.47 | 11.66 | 0.012 | 0.91 |
| 5/17/2021 | 621.14 | 609.27 | 11.87 | 0.012 | 0.93 |
| 6/9/2021 | 620.24 | 608.31 | 11.93 | 0.012 | 0.93 |
| 6/15/2021 | 619.70 | 607.64 | 12.06 | 0.012 | 0.94 |
| 6/23/2021 | 619.17 | 606.99 | 12.18 | 0.012 | 0.95 |
| 7/12/2021 | 620.91 | 608.70 | 12.21 | 0.012 | 0.95 |
| 7/26/2021 | 620.42 | 608.56 | 11.86 | 0.012 | 0.93 |
| | | | Average | 0.012 | 0.91 |

[O:KLT 9/16/21, C: LDC 09/17/21]

TABLE 3-4. HORIZONTAL HYDRAULIC GRADIENTS AND GROUNDWATER FLOW VELOCITIES

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

Notes:

- ¹ Hydraulic conductivity values used above are average of the individual wells used in each velocity calculation as derived from slug tests completed in February and March 2021 by Ramboll.
- ² Effective porosity used in these calculations was derived from an average between estimated values of 0.20 for silt materials, 0.267 for gravel, 0.07 for clay, and 0.28 for sand from *Morris, D.A. and A.I. Johnson, 1967.* Summary of hydrologic and physical properties of rock and soil materials as analyzed by the Hydrologic Laboratory of the U.S. Geological Survey, U.S. Geological Survey Water-Supply Paper 1839-D, 42p. and Heath, R.C., 1983. Basic ground-water hydrology, U.S. Geological Survey Water-Supply Paper 2220, 86p. Effective porosity may be as high as maximum total porosity (50%) calculated in Table 2-1.

-- = not calculated % = percent ft = foot/feet ft/day = feet per day ft/ft = feet per foot NAVD88 = North American Vertical Datum of 1988 NI = not installed NM = not measured

| Location | Sample Date | Antimony, total (mg/L) | Arsenic, total (mg/L) | Barium, total (mg/L) | Beryllium, total (mg/L) | Boron, total (mg/L) | Cadmium, total (mg/L) | Calcium, total (mg/L) | Chloride, total (mg/L) | Chromium, total (mg/L) | Cobalt, total (mg/L) | Fluoride, total (mg/L) | Lead, total (mg/L) | Lithium, total (mg/L) | Mercury, total (mg/L) | Molybdenum, total (mg/L) | pH (field) (SU) | Radium 226 and 228 combined (pCi/L) | Selenium, total (mg/L) | Sulfate, total (mg/L) | Thallium, total (mg/L) | Total Dissolved Solids (mg/L) |
|-----------|----------------|------------------------------|-----------------------------|----------------------------|-------------------------------|---------------------------|-----------------------------|-----------------------------|------------------------------|------------------------------|----------------------------|------------------------------|--------------------------|-----------------------------|-----------------------------|--------------------------------|-----------------------|--|------------------------------|-----------------------------|------------------------------|--|
| 35 I.A.C. | Lower | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6.5 | 0 | 0 | 0 | 0 | 0 |
| 845.600 | Upper | 0.006 | 0.010 | 2.0 | 0.004 | 2 | 0.005 | | 200 | 0.1 | 0.006 | 4.0 | 0.0075 | 0.04 | 0.002 | 0.1 | 9.0 | 5 | 0.05 | 400 | 0.002 | 1200 |
| G281 | 11/20/2015 | <0.003 | 0.0043 | 0.14 | <0.001 | <0.01 | <0.001 | 150 | 74 | 0.011 | 0.0056 | 0.349 | 0.0063 | 0.013 | <0.0002 | 0.0015 | 7.0 | 1.12 | <0.001 | 300 | <0.001 | 820 |
| G281 | 02/11/2016 | <0.003 | <0.001 | 0.067 | <0.001 | 0.01 | <0.001 | 120 | 55 | <0.004 | <0.002 | 0.411 | <0.001 | <0.01 | <0.0002 | <0.001 | 7.1 | 0.622 | <0.001 | 340 | <0.001 | 740 |
| G281 | 05/10/2016 | <0.003 | <0.001 | 0.072 | <0.001 | <0.01 | <0.001 | 130 | 72 | <0.004 | <0.002 | 0.405 | <0.001 | <0.01 | <0.0002 | <0.001 | 7.0 | 0.218 | <0.001 | 370 | <0.001 | 740 |
| G281 | 08/01/2016 | <0.003 | <0.001 | 0.078 | <0.001 | 0.012 | <0.001 | 140 | 70 | <0.004 | <0.002 | 0.368 | 0.0011 | <0.01 | <0.0002 | <0.001 | 7.0 | 1.49 | <0.001 | 310 | <0.001 | 780 |
| G281 | 11/16/2016 | <0.003 | 0.001 | 0.081 | <0.001 | 0.022 | <0.001 | 110 | 68 | <0.004 | <0.002 | 0.263 | 0.0013 | <0.01 | <0.0002 | <0.001 | 6.9 | 0.94 | <0.001 | 310 | <0.001 | 840 |
| G281 | 02/10/2017 | <0.003 | <0.001 | 0.08 | <0.001 | <0.01 | <0.001 | 120 | 67 | <0.004 | <0.002 | 0.27 | <0.001 | <0.01 | <0.0002 | <0.001 | 6.7 | 1.63 | <0.001 | 310 | <0.001 | 840 |
| G281 | 05/16/2017 | <0.003 | <0.001 | 0.081 | <0.001 | <0.01 | <0.001 | 130 | 68 | <0.004 | <0.002 | 0.308 | <0.001 | <0.01 | <0.0002 | <0.001 | 6.9 | 0.437 | <0.001 | 330 | <0.001 | 840 |
| G281 | 07/12/2017 | <0.003 | 0.001 | 0.087 | <0.001 | <0.01 | <0.001 | 130 | 75 | <0.004 | <0.002 | 0.273 | 0.0013 | <0.01 | <0.0002 | <0.001 | 7.0 | 0.36 | <0.001 | 300 | <0.001 | 760 |
| G281 | 10/25/2017 | | | | | 0.012 | | 110 | 64 | | | 0.351 | | | | | 7.0 | | | 300 | | 800 |
| G281 | 05/11/2018 | <0.003 | <0.001 | 0.081 | <0.001 | <0.01 | <0.001 | 120 | 69 | <0.004 | 0.0023 | 0.268 | 0.0017 | <0.01 | <0.0002 | <0.001 | 7.1 | | <0.001 | 310 | <0.001 | 840 |
| G281 | 05/30/2018 | | | | | | | | | | | | | | | | | 0.742 | | | | |
| G281 | 08/03/2018 | | 0.0029 | 0.1 | | 0.013 | <0.001 | 130 | 66 | 0.0059 | 0.0036 | 0.364 | 0.003 | <0.01 | | <0.001 | 7.0 | 1.05 | | 280 | | 840 |
| G281 | 01/23/2019 | <0.003 | <0.001 | 0.072 | <0.001 | 0.013 | <0.001 | 130 | 85 | <0.004 | <0.002 | 0.299 | <0.001 | <0.01 | <0.0002 | <0.001 | 7.0 | 0.333 | <0.001 | 380 | <0.001 | 880 |
| G281 | 08/13/2019 | | 0.0015 | 0.091 | <0.001 | <0.01 | <0.001 | 140 | 72 | 0.0048 | <0.002 | 0.546 | 0.0016 | 0.014 | | <0.001 | 6.9 | 0.879 | <0.001 | 310 | | 900 |
| G281 | 01/24/2020 | <0.003 | <0.001 | 0.07 | <0.001 | 0.011 | <0.001 | 140 | 75 | <0.004 | <0.002 | 0.317 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.3 | 0 | <0.001 | 300 | <0.001 | 880 |
| G281 | 08/12/2020 | | <0.001 | 0.057 | <0.001 | 0.037 | <0.001 | 130 | 81 | <0.004 | <0.002 | 0.324 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.9 | 0.304 | <0.001 | 260 | | 700 |
| G281 | 01/29/2021 | <0.003 | <0.001 | 0.064 | <0.001 | <0.01 | <0.001 | 130 | 100 | <0.004 | <0.002 | 0.314 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.1 | 0.397 | <0.001 | 260 | <0.001 | 870 |
| G281 | 03/31/2021 | <0.003 | <0.001 | 0.066 | <0.001 | 0.11 | <0.001 | 130 | 90 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.0 | 0.159 | <0.001 | 280 | <0.001 | 830 |
| G281 | 04/21/2021 | <0.003 | <0.001 | 0.061 | <0.001 | <0.01 | <0.001 | 130 | 120 | <0.004 | <0.002 | 0.317 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.9 | 0.0358 | <0.001 | 250 | <0.001 | 1000 |
| G281 | 05/05/2021 | <0.003 | <0.001 | 0.065 | <0.001 | 0.015 | <0.001 | 130 | 86 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.1 | 0 | <0.001 | 260 | <0.001 | 820 |
| G281 | 05/17/2021 | <0.003 | 0.0018 | 0.086 | <0.001 | 0.043 | <0.001 | 130 | 85 | 0.0049 | 0.0026 | 0.362 | 0.002 | <0.02 | <0.0002 | <0.001 | 7.1 | 0.199 | <0.001 | 280 | <0.001 | 870 |
| G281 | 06/14/2021 | <0.003 | <0.001 | 0.06 | <0.001 | <0.01 | <0.001 | 140 | 76 | <0.004 | <0.002 | 0.379 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.1 | 1.22 | <0.001 | 260 | <0.001 | 930 |



| Location | Sample Date | Antimony, total (mg/L) | Arsenic, total (mg/L) | Barium, total (mg/L) | Beryllium, total (mg/L) | Boron, total (mg/L) | Cadmium, total (mg/L) | Calcium, total (mg/L) | Chloride, total (mg/L) | Chromium, total (mg/L) | Cobalt, total (mg/L) | Fluoride, total (mg/L) | Lead, total (mg/L) | Lithium, total (mg/L) | Mercury, total (mg/L) | Molybdenum, total (mg/L) | pH (field) (SU) | Radium 226 and 228 combined (pCi/L) | Selenium, total (mg/L) | Sulfate, total (mg/L) | Thallium, total (mg/L) | Total Dissolved Solids (mg/L) |
|-----------|----------------|------------------------------|-----------------------------|----------------------------|-------------------------------|---------------------------|-----------------------------|-----------------------------|------------------------------|------------------------------|----------------------------|------------------------------|--------------------------|-----------------------------|-----------------------------|--------------------------------|-----------------------|--|------------------------------|-----------------------------|------------------------------|--|
| 35 I.A.C. | Lower | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6.5 | 0 | 0 | 0 | 0 | 0 |
| 845.600 | Upper | 0.006 | 0.010 | 2.0 | 0.004 | 2 | 0.005 | | 200 | 0.1 | 0.006 | 4.0 | 0.0075 | 0.04 | 0.002 | 0.1 | 9.0 | 5 | 0.05 | 400 | 0.002 | 1200 |
| G281 | 06/28/2021 | <0.003 | <0.001 | 0.062 | <0.001 | 0.036 | <0.001 | 130 | 86 | <0.004 | <0.002 | 0.277 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.2 | 0.106 | <0.001 | 280 | <0.001 | 830 |
| G281 | 07/12/2021 | <0.003 | <0.001 | 0.061 | <0.001 | <0.01 | <0.001 | 130 | 73 | <0.004 | <0.002 | 0.334 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.2 | 0.601 | <0.001 | 260 | <0.001 | 910 |
| G281 | 07/27/2021 | <0.003 | <0.001 | 0.061 | <0.001 | <0.01 | <0.001 | 120 | 73 | <0.004 | <0.002 | 0.352 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.1 | | <0.001 | 270 | 0.001 | 880 |
| G301 | 11/20/2015 | <0.003 | 0.0026 | 0.079 | <0.001 | 2.3 | <0.001 | 140 | 33 | 0.0071 | 0.0053 | 0.31 | 0.0038 | 0.015 | <0.0002 | <0.001 | 6.9 | 1.07 | <0.001 | 700 | <0.001 | 1200 |
| G301 | 02/23/2016 | <0.003 | <0.001 | 0.041 | <0.001 | 2.4 | <0.001 | 140 | 25 | 0.0045 | 0.0028 | 0.324 | 0.0011 | <0.01 | <0.0002 | <0.001 | 6.6 | 0.399 | <0.001 | 740 | <0.001 | 1000 |
| G301 | 05/20/2016 | <0.003 | <0.001 | 0.031 | <0.001 | 2.6 | <0.001 | 130 | 24 | <0.004 | 0.0028 | 0.404 | <0.001 | <0.01 | <0.0002 | <0.001 | 6.4 | 0.202 | <0.001 | 710 | <0.001 | 1100 |
| G301 | 08/15/2016 | <0.003 | <0.001 | 0.032 | <0.001 | 2.9 | <0.001 | 140 | 24 | <0.004 | 0.0022 | 0.296 | <0.001 | 0.011 | <0.0002 | <0.001 | 6.8 | 1.03 | <0.001 | 740 | <0.001 | 1200 |
| G301 | 11/17/2016 | <0.003 | <0.001 | 0.036 | <0.001 | 2.4 | 0.0011 | 120 | 25 | <0.004 | 0.0024 | <0.25 | 0.0017 | <0.01 | <0.0002 | <0.001 | 6.9 | 0.604 | <0.001 | 800 | <0.001 | 1400 |
| G301 | 02/16/2017 | <0.003 | 0.0017 | 0.063 | <0.001 | 2.4 | <0.001 | 150 | 23 | 0.0064 | 0.0044 | <0.25 | 0.0028 | 0.01 | <0.0002 | <0.001 | 7.0 | 0.994 | <0.001 | 790 | <0.001 | 1200 |
| G301 | 05/17/2017 | <0.003 | <0.001 | 0.029 | <0.001 | 2.1 | <0.001 | 120 | 21 | <0.004 | 0.0022 | <0.25 | 0.0013 | <0.01 | <0.0002 | <0.001 | 7.1 | 2.16 | <0.001 | 650 | <0.001 | 1100 |
| G301 | 07/12/2017 | <0.003 | 0.0021 | 0.058 | <0.001 | 2.3 | <0.001 | 120 | 23 | 0.0075 | 0.0031 | <0.25 | 0.0038 | 0.011 | 0.001 | <0.001 | 6.8 | 0.674 | <0.001 | 760 | <0.001 | 1100 |
| G301 | 10/26/2017 | | | | | 2.3 | | 110 | 22 | | | 0.28 | | | | | 6.8 | | | 680 | - | 1100 |
| G301 | 05/11/2018 | <0.003 | 0.0016 | 0.06 | <0.001 | 2.1 | <0.001 | 130 | 22 | 0.0081 | 0.0042 | 0.302 | 0.0047 | 0.011 | <0.0002 | <0.001 | 6.9 | | <0.001 | 810 | <0.001 | 1200 |
| G301 | 05/30/2018 | | | | | | | | | | | - | | | | | | 1.54 | | | - | |
| G301 | 08/03/2018 | | 0.0035 | 0.084 | | 2.4 | <0.001 | 150 | 20 | 0.014 | 0.0051 | 0.31 | 0.0058 | 0.012 | | <0.001 | 6.9 | 1.28 | | 860 | - | 1200 |
| G301 | 01/23/2019 | <0.003 | 0.0045 | 0.11 | <0.001 | 2.1 | <0.001 | 170 | 21 | 0.017 | 0.0084 | 0.272 | 0.0086 | <0.01 | <0.0002 | <0.001 | 7.0 | 0.943 | <0.001 | 850 | <0.001 | 1500 |
| G301 | 08/19/2019 | | <0.001 | 0.02 | <0.001 | 2 | <0.001 | 110 | 12 | <0.004 | <0.002 | 0.351 | <0.001 | 0.014 | | <0.001 | 6.9 | 1.6 | <0.001 | 570 | | 950 |
| G301 | 01/23/2020 | <0.003 | 0.0012 | 0.034 | <0.001 | 2.1 | <0.001 | 160 | 16 | 0.0044 | 0.0032 | <0.25 | 0.0015 | <0.02 | <0.0002 | <0.001 | 6.7 | 0.391 | <0.001 | 820 | <0.001 | 1400 |
| G301 | 08/11/2020 | | <0.001 | 0.016 | <0.001 | 2.1 | <0.001 | 150 | 14 | <0.004 | <0.002 | 0.263 | <0.001 | <0.02 | | <0.001 | 6.6 | 0.781 | <0.001 | 750 | | 1200 |
| G301 | 01/27/2021 | <0.003 | <0.001 | 0.017 | <0.001 | 2 | <0.001 | 160 | 17 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.6 | 1.02 | <0.001 | 650 | <0.001 | 1300 |
| G302 | 11/20/2015 | <0.003 | 0.0098 | 0.067 | <0.001 | 2 | <0.001 | 180 | 22 | 0.0044 | 0.004 | 0.267 | 0.0024 | 0.032 | <0.0002 | 0.002 | 6.9 | 0.672 | <0.001 | 480 | <0.001 | 1200 |
| G302 | 02/23/2016 | <0.003 | 0.0014 | 0.029 | <0.001 | 2.1 | <0.001 | 170 | 21 | <0.004 | 0.0022 | 0.288 | <0.001 | 0.018 | <0.0002 | 0.0015 | 6.8 | 0.532 | <0.001 | 530 | <0.001 | 1000 |



| Location | Sample Date | Antimony, total (mg/L) | Arsenic, total (mg/L) | Barium, total (mg/L) | Beryllium, total (mg/L) | Boron, total (mg/L) | Cadmium, total (mg/L) | Calcium, total (mg/L) | Chloride, total (mg/L) | Chromium, total (mg/L) | Cobalt, total (mg/L) | Fluoride, total (mg/L) | Lead, total (mg/L) | Lithium, total (mg/L) | Mercury, total (mg/L) | Molybdenum, total (mg/L) | pH (field) (SU) | Radium 226 and 228 combined (pCi/L) | Selenium, total (mg/L) | Sulfate, total (mg/L) | Thallium, total (mg/L) | Total Dissolved Solids (mg/L) |
|-----------|----------------|------------------------------|-----------------------------|----------------------------|-------------------------------|---------------------------|-----------------------------|-----------------------------|------------------------------|------------------------------|----------------------------|------------------------------|--------------------------|-----------------------------|-----------------------------|--------------------------------|-----------------------|--|------------------------------|-----------------------------|------------------------------|--|
| 35 I.A.C. | Lower | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6.5 | 0 | 0 | 0 | 0 | 0 |
| 845.600 | Upper | 0.006 | 0.010 | 2.0 | 0.004 | 2 | 0.005 | | 200 | 0.1 | 0.006 | 4.0 | 0.0075 | 0.04 | 0.002 | 0.1 | 9.0 | 5 | 0.05 | 400 | 0.002 | 1200 |
| G302 | 05/20/2016 | <0.003 | 0.0018 | 0.024 | <0.001 | 2.5 | <0.001 | 140 | 12 | <0.004 | <0.002 | 0.39 | <0.001 | 0.013 | <0.0002 | 0.0014 | 6.8 | 0.681 | <0.001 | 440 | <0.001 | 1000 |
| G302 | 08/15/2016 | <0.003 | 0.0015 | 0.028 | <0.001 | 1.9 | <0.001 | 130 | 9.7 | <0.004 | 0.002 | 0.304 | 0.0011 | 0.022 | 0.00052 | <0.001 | 7.0 | 0.876 | <0.001 | 360 | <0.001 | 910 |
| G302 | 11/17/2016 | <0.003 | 0.0035 | 0.037 | <0.001 | 1.9 | <0.001 | 140 | 14 | <0.004 | 0.0025 | <0.25 | <0.001 | 0.023 | <0.0002 | 0.0011 | 7.1 | 0.309 | <0.001 | 450 | <0.001 | 1100 |
| G302 | 02/16/2017 | <0.003 | 0.0036 | 0.03 | <0.001 | 1.4 | <0.001 | 160 | 14 | <0.004 | <0.002 | 0.29 | <0.001 | 0.026 | <0.0002 | 0.001 | 7.1 | 0.976 | <0.001 | 430 | <0.001 | 1100 |
| G302 | 05/17/2017 | <0.003 | <0.001 | 0.02 | <0.001 | 1.1 | <0.001 | 130 | 6.5 | <0.004 | 0.0024 | <0.25 | <0.001 | 0.013 | <0.0002 | <0.001 | 7.0 | 0.848 | <0.001 | 330 | <0.001 | 820 |
| G302 | 07/12/2017 | <0.003 | 0.0072 | 0.06 | <0.001 | 2 | <0.001 | 160 | 14 | 0.0075 | 0.0045 | 0.388 | 0.0035 | 0.031 | <0.0002 | 0.0019 | 7.0 | 1.55 | <0.001 | 460 | <0.001 | 1000 |
| G302 | 10/26/2017 | | | | | 1.1 | | 180 | 8.3 | | | 0.319 | | | | | 7.1 | | | 320 | | 840 |
| G302 | 05/11/2018 | <0.003 | 0.0053 | 0.039 | <0.001 | 2.1 | <0.001 | 170 | 17 | <0.004 | 0.0034 | 0.329 | 0.0018 | 0.022 | <0.0002 | 0.0024 | 7.1 | | <0.001 | 510 | <0.001 | 1100 |
| G302 | 05/30/2018 | | | | | | | | | | | | | | | | | 3.76 | | | | |
| G302 | 08/03/2018 | | 0.0051 | 0.054 | | 2.3 | <0.001 | 180 | 17 | 0.0074 | 0.0046 | 0.3 | 0.0041 | 0.02 | | 0.0016 | 7.0 | 0.458 | | 500 | | 1200 |
| G302 | 01/23/2019 | <0.003 | 0.013 | 0.095 | <0.001 | 1.9 | <0.001 | 210 | 20 | 0.019 | 0.0084 | 0.267 | 0.011 | 0.028 | <0.0002 | 0.0029 | 7.0 | 1.29 | 0.0011 | 500 | <0.001 | 1400 |
| G302 | 08/19/2019 | | <0.001 | 0.028 | <0.001 | 1.8 | <0.001 | 120 | 5.9 | <0.004 | 0.0056 | 0.381 | <0.001 | 0.02 | | <0.001 | 7.0 | 1.89 | <0.001 | 280 | | 800 |
| G302 | 01/23/2020 | <0.003 | 0.0038 | 0.045 | <0.001 | 1.7 | <0.001 | 150 | 14 | 0.0073 | 0.0028 | <0.25 | 0.003 | 0.023 | <0.0002 | 0.0012 | 7.1 | 0.0859 | <0.001 | 350 | <0.001 | 960 |
| G302 | 08/11/2020 | | 0.001 | 0.022 | <0.001 | 1.2 | <0.001 | 140 | 5.9 | <0.004 | <0.002 | 0.28 | <0.001 | <0.02 | | <0.001 | 6.9 | 0.652 | <0.001 | 260 | | 780 |
| G302 | 01/27/2021 | <0.003 | <0.001 | 0.027 | <0.001 | 1.2 | <0.001 | 180 | 22 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.6 | 0.129 | <0.001 | 430 | <0.001 | 1100 |
| G303 | 11/20/2015 | <0.003 | 0.013 | 0.046 | <0.001 | 1.5 | <0.001 | 170 | 32 | 0.01 | 0.0065 | <0.25 | 0.0053 | 0.062 | <0.0002 | 0.0033 | 6.9 | 0.631 | <0.001 | 860 | <0.001 | 1700 |
| G303 | 02/23/2016 | <0.003 | 0.0023 | 0.014 | <0.001 | 2.5 | <0.001 | 170 | 32 | <0.004 | <0.002 | 0.329 | <0.001 | 0.031 | <0.0002 | 0.0017 | 7.0 | 0.472 | <0.001 | 700 | <0.001 | 1400 |
| G303 | 05/20/2016 | <0.003 | 0.0039 | 0.016 | <0.001 | 2.4 | <0.001 | 160 | 29 | <0.004 | 0.0028 | 0.342 | <0.001 | 0.024 | <0.0002 | 0.0019 | 6.9 | 0.432 | <0.001 | 700 | <0.001 | 1400 |
| G303 | 08/15/2016 | <0.003 | 0.0074 | 0.016 | <0.001 | 1.8 | <0.001 | 170 | 30 | <0.004 | 0.0041 | 0.257 | <0.001 | 0.076 | 0.0009 | 0.0019 | 6.9 | 0.65 | <0.001 | 830 | <0.001 | 1600 |
| G303 | 11/17/2016 | <0.003 | 0.0065 | 0.016 | <0.001 | 1.6 | <0.001 | 180 | 30 | <0.004 | 0.0032 | <0.25 | <0.001 | 0.064 | <0.0002 | 0.0024 | 6.9 | 0.421 | <0.001 | 870 | <0.001 | 1900 |
| G303 | 02/19/2017 | <0.003 | 0.018 | 0.016 | <0.001 | 1.7 | <0.001 | 170 | 28 | <0.004 | 0.0027 | 0.3 | <0.001 | 0.066 | <0.0002 | 0.0024 | 6.9 | 1.62 | <0.001 | 860 | <0.001 | 1700 |
| G303 | 05/17/2017 | <0.003 | 0.0092 | 0.017 | <0.001 | 1.4 | <0.001 | 210 | 28 | <0.004 | 0.0033 | 0.277 | <0.001 | 0.06 | 0.00067 | 0.0027 | 7.1 | 0.659 | <0.001 | 780 | <0.001 | 1900 |



| Location | Sample Date | Antimony, total (mg/L) | Arsenic, total (mg/L) | Barium, total (mg/L) | Beryllium, total (mg/L) | Boron, total (mg/L) | Cadmium, total (mg/L) | Calcium, total (mg/L) | Chloride, total (mg/L) | Chromium, total (mg/L) | Cobalt, total (mg/L) | Fluoride, total (mg/L) | Lead, total (mg/L) | Lithium, total (mg/L) | Mercury, total (mg/L) | Molybdenum, total (mg/L) | pH (field) (SU) | Radium 226 and 228 combined (pCi/L) | Selenium, total (mg/L) | Sulfate, total (mg/L) | Thallium, total (mg/L) | Total Dissolved Solids (mg/L) |
|-----------|----------------|------------------------------|-----------------------------|----------------------------|-------------------------------|---------------------------|-----------------------------|-----------------------------|------------------------------|------------------------------|----------------------------|------------------------------|--------------------------|-----------------------------|-----------------------------|--------------------------------|-----------------------|--|------------------------------|-----------------------------|------------------------------|--|
| 35 I.A.C. | Lower | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6.5 | 0 | 0 | 0 | 0 | 0 |
| 845.600 | Upper | 0.006 | 0.010 | 2.0 | 0.004 | 2 | 0.005 | | 200 | 0.1 | 0.006 | 4.0 | 0.0075 | 0.04 | 0.002 | 0.1 | 9.0 | 5 | 0.05 | 400 | 0.002 | 1200 |
| G303 | 07/13/2017 | <0.003 | 0.008 | 0.016 | <0.001 | 1.7 | <0.001 | 170 | 31 | <0.004 | 0.0053 | 0.277 | <0.001 | 0.051 | <0.0002 | 0.0018 | 7.0 | 1.68 | <0.001 | 860 | <0.001 | 1500 |
| G303 | 10/26/2017 | | | | | 2.5 | | 130 | 28 | | | 0.311 | | | | | 7.0 | | | 600 | | 1300 |
| G303 | 05/14/2018 | <0.003 | 0.0064 | 0.018 | < 0.001 | 1.5 | < 0.001 | 170 | 30 | <0.004 | 0.0032 | 0.279 | <0.001 | 0.05 | <0.0002 | 0.0024 | 7.0 | | <0.001 | 780 | <0.001 | 1500 |
| G303 | 05/30/2018 | | | | | | | | | | | | | | | | | 2.2 | | | | |
| G303 | 08/03/2018 | | 0.0044 | 0.019 | | 1.6 | <0.001 | 200 | 28 | <0.004 | 0.0031 | 0.275 | <0.001 | 0.041 | | 0.002 | 7.0 | 0.216 | | 780 | | 1600 |
| G303 | 01/23/2019 | <0.003 | 0.0031 | 0.015 | <0.001 | 1.8 | <0.001 | 190 | 30 | <0.004 | <0.002 | 0.3 | <0.001 | 0.033 | <0.0002 | 0.0022 | 7.0 | 0.884 | <0.001 | 760 | <0.001 | 1800 |
| G303 | 08/19/2019 | | 0.0036 | 0.016 | <0.001 | 1.8 | <0.001 | 190 | 32 | <0.004 | 0.0024 | 0.334 | <0.001 | 0.058 | | 0.0021 | 7.0 | 1.14 | <0.001 | 730 | | 1700 |
| G303 | 01/23/2020 | <0.003 | 0.0012 | 0.015 | <0.001 | 2.3 | <0.001 | 160 | 29 | <0.004 | <0.002 | 0.256 | <0.001 | 0.028 | <0.0002 | 0.0016 | 7.0 | 0.6 | <0.001 | 690 | <0.001 | 1200 |
| G303 | 08/11/2020 | | 0.0041 | 0.033 | <0.001 | 1.7 | <0.001 | 210 | 24 | 0.0043 | 0.0056 | 0.294 | 0.0037 | 0.041 | | 0.0023 | 6.9 | 1.37 | <0.001 | 790 | | 1700 |
| G303 | 01/26/2021 | <0.003 | <0.001 | 0.013 | <0.001 | 2 | <0.001 | 170 | 32 | <0.004 | <0.002 | <0.25 | <0.001 | 0.033 | <0.0002 | 0.0016 | 6.8 | 0.355 | <0.001 | 730 | <0.001 | 1600 |
| G304 | 11/20/2015 | <0.003 | 0.0078 | 0.06 | <0.001 | 2.3 | <0.001 | 170 | 27 | 0.0065 | 0.014 | 0.354 | 0.0035 | 0.014 | <0.0002 | 0.0023 | 7.1 | 1.93 | <0.001 | 1000 | <0.001 | 1500 |
| G304 | 02/23/2016 | <0.003 | 0.0016 | 0.029 | <0.001 | 2.4 | <0.001 | 220 | 27 | <0.004 | 0.0033 | 0.414 | 0.0012 | 0.012 | 0.00023 | 0.0012 | 7.1 | 0.611 | <0.001 | 1100 | <0.001 | 1400 |
| G304 | 05/20/2016 | <0.003 | 0.0023 | 0.032 | <0.001 | 2.6 | <0.001 | 200 | 27 | 0.0049 | 0.0047 | 0.476 | 0.0017 | <0.01 | <0.0002 | 0.0017 | 7.1 | 0.22 | <0.001 | 1000 | <0.001 | 1300 |
| G305 | 05/19/2016 | <0.003 | 0.0071 | 0.093 | <0.001 | 2.6 | <0.001 | 180 | 27 | 0.026 | 0.0088 | 0.531 | 0.023 | 0.02 | <0.0002 | 0.0024 | 7.1 | 0.723 | <0.001 | 890 | <0.001 | 1300 |
| G305 | 07/01/2016 | <0.003 | <0.001 | 0.043 | <0.001 | 2.5 | <0.001 | 190 | 28 | 0.0057 | <0.002 | 0.424 | 0.0028 | 0.014 | <0.0002 | 0.0013 | 7.2 | 0.767 | <0.001 | 900 | <0.001 | 1500 |
| G305 | 08/16/2016 | <0.003 | <0.001 | 0.035 | <0.001 | 2.4 | <0.001 | 150 | 27 | <0.004 | <0.002 | 0.425 | 0.0016 | 0.014 | <0.0002 | <0.001 | 7.3 | 1.26 | <0.001 | 930 | <0.001 | 1400 |
| G305 | 09/29/2016 | <0.003 | <0.001 | 0.036 | <0.001 | 2.7 | <0.001 | 190 | 30 | <0.004 | <0.002 | 0.503 | 0.0011 | <0.01 | <0.0002 | <0.001 | 6.9 | 0.691 | <0.001 | 890 | <0.001 | 1400 |
| G305 | 11/17/2016 | <0.003 | 0.0013 | 0.039 | <0.001 | 1.8 | <0.001 | 100 | 60 | <0.004 | <0.002 | 0.546 | 0.003 | <0.01 | <0.0002 | 0.0035 | 7.1 | 0.344 | <0.001 | 710 | <0.001 | 1400 |
| G306 | 05/19/2016 | <0.003 | 0.0041 | 0.088 | <0.001 | 2.3 | <0.001 | 130 | 14 | 0.012 | 0.0064 | 0.426 | 0.0049 | 0.011 | <0.0002 | 0.0019 | 6.7 | 0.778 | <0.001 | 350 | <0.001 | 720 |
| G306 | 07/01/2016 | <0.003 | <0.001 | 0.061 | <0.001 | 2.7 | <0.001 | 130 | 8.9 | <0.004 | 0.0043 | 0.344 | <0.001 | <0.01 | <0.0002 | 0.0016 | 6.5 | 0.545 | <0.001 | 330 | <0.001 | 720 |
| G306 | 08/16/2016 | <0.003 | <0.001 | 0.062 | <0.001 | 2.4 | <0.001 | 110 | 7.2 | <0.004 | 0.0025 | 0.308 | <0.001 | <0.01 | <0.0002 | 0.0012 | 6.9 | 0.885 | <0.001 | 320 | <0.001 | 680 |
| G306 | 09/29/2016 | <0.003 | <0.001 | 0.059 | <0.001 | 2.6 | <0.001 | 120 | 6.8 | <0.004 | 0.0025 | 0.326 | <0.001 | <0.01 | <0.0002 | <0.001 | 6.6 | 0.818 | 0.0011 | 320 | <0.001 | 660 |



| Location | Sample Date | Antimony, total (mg/L) | Arsenic, total (mg/L) | Barium, total (mg/L) | Beryllium, total (mg/L) | Boron, total (mg/L) | Cadmium, total (mg/L) | Calcium, total (mg/L) | Chloride, total (mg/L) | Chromium, total (mg/L) | Cobalt, total (mg/L) | Fluoride, total (mg/L) | Lead, total (mg/L) | Lithium, total (mg/L) | Mercury, total (mg/L) | Molybdenum, total (mg/L) | pH (field) (SU) | Radium 226 and 228 combined (pCi/L) | Selenium, total (mg/L) | Sulfate, total (mg/L) | Thallium, total (mg/L) | Total Dissolved Solids (mg/L) |
|-----------|----------------|------------------------------|-----------------------------|----------------------------|-------------------------------|---------------------------|-----------------------------|-----------------------------|------------------------------|------------------------------|----------------------------|------------------------------|--------------------------|-----------------------------|-----------------------------|--------------------------------|-----------------------|--|------------------------------|-----------------------------|------------------------------|--|
| 35 I.A.C. | Lower | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6.5 | 0 | 0 | 0 | 0 | 0 |
| 845.600 | Upper | 0.006 | 0.010 | 2.0 | 0.004 | 2 | 0.005 | | 200 | 0.1 | 0.006 | 4.0 | 0.0075 | 0.04 | 0.002 | 0.1 | 9.0 | 5 | 0.05 | 400 | 0.002 | 1200 |
| G306 | 11/16/2016 | <0.003 | <0.001 | 0.076 | <0.001 | 2.7 | <0.001 | 120 | 6.6 | <0.004 | <0.002 | <0.25 | <0.001 | <0.01 | <0.0002 | 0.0018 | 7.0 | 0.143 | <0.001 | 330 | <0.001 | 820 |
| G306 | 02/19/2017 | <0.003 | <0.001 | 0.059 | <0.001 | 2.7 | <0.001 | 130 | 6.2 | <0.004 | <0.002 | 0.263 | <0.001 | <0.01 | <0.0002 | 0.0017 | 7.0 | 0.864 | <0.001 | 5.9 | <0.001 | 820 |
| G306 | 05/17/2017 | <0.003 | <0.001 | 0.066 | <0.001 | 2.5 | <0.001 | 150 | 5.5 | <0.004 | <0.002 | 0.304 | <0.001 | <0.01 | <0.0002 | 0.0016 | 7.1 | 1.39 | <0.001 | 700 | <0.001 | 800 |
| G306 | 07/13/2017 | <0.003 | <0.001 | 0.085 | <0.001 | 2.9 | <0.001 | 130 | 8.3 | <0.004 | <0.002 | 0.326 | <0.001 | <0.01 | <0.0002 | 0.0019 | 7.0 | 0.76 | <0.001 | 340 | <0.001 | 720 |
| G306 | 10/27/2017 | | | | | 3.1 | | 120 | 4.7 | | | 0.332 | | | | | 6.9 | | | 350 | | 720 |
| G306 | 05/14/2018 | <0.003 | <0.001 | 0.06 | <0.001 | 2.8 | <0.001 | 130 | 3.9 | <0.004 | <0.002 | 0.319 | <0.001 | 0.01 | <0.0002 | 0.0013 | 6.9 | | <0.001 | 320 | <0.001 | 720 |
| G306 | 05/30/2018 | | | | | | | | | | | | | | | | | 1.31 | | | | |
| G306 | 08/03/2018 | | 0.0093 | 0.17 | | 2.7 | <0.001 | 160 | 3.7 | 0.035 | 0.0094 | 0.313 | 0.012 | 0.02 | | 0.0026 | 7.0 | 0.454 | | 290 | | 820 |
| G306 | 01/23/2019 | <0.003 | 0.02 | 0.28 | 0.0013 | 2.4 | <0.001 | 170 | 4.1 | 0.071 | 0.02 | 0.269 | 0.028 | 0.036 | <0.0002 | 0.0037 | 7.0 | 2.61 | 0.0028 | 250 | <0.001 | 900 |
| G306 | 08/19/2019 | | 0.0025 | 0.088 | <0.001 | 2.5 | <0.001 | 160 | 4.4 | 0.013 | 0.0024 | 0.413 | 0.0031 | 0.015 | | 0.0016 | 7.0 | 0.533 | <0.001 | 260 | | 780 |
| G306 | 01/21/2020 | <0.003 | 0.006 | 0.089 | <0.001 | 3.5 | <0.001 | 150 | 2.5 | 0.019 | 0.0062 | <0.25 | 0.0067 | <0.02 | <0.0002 | 0.0015 | 7.0 | 0.576 | 0.0016 | 260 | <0.001 | 830 |
| G306 | 08/11/2020 | | <0.001 | 0.039 | <0.001 | 2.6 | <0.001 | 140 | 1.5 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | | <0.001 | 6.9 | 0.145 | <0.001 | 250 | | 700 |
| G306 | 01/26/2021 | <0.003 | <0.001 | 0.03 | <0.001 | 2.4 | <0.001 | 110 | 2.1 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.8 | 0.876 | 0.0012 | 240 | <0.001 | 700 |
| G306 | 03/29/2021 | <0.003 | <0.001 | 0.039 | <0.001 | 2.5 | <0.001 | 120 | 1.6 | 0.0042 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.7 | 0.351 | 0.0012 | 260 | <0.001 | 690 |
| G306 | 04/21/2021 | <0.003 | <0.001 | 0.04 | <0.001 | 2.6 | <0.001 | 130 | 2 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.8 | 0.173 | 0.0012 | 240 | <0.001 | 830 |
| G306 | 05/05/2021 | <0.003 | <0.001 | 0.039 | <0.001 | 2.9 | <0.001 | 130 | <1 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.0011 | 6.8 | 0.0696 | 0.0015 | 240 | <0.001 | 670 |
| G306 | 05/18/2021 | <0.003 | 0.0011 | 0.04 | <0.001 | 2.9 | <0.001 | 140 | 1.1 | <0.004 | <0.002 | 0.382 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.9 | 0.115 | <0.001 | 250 | <0.001 | 680 |
| G306 | 06/15/2021 | <0.003 | 0.001 | 0.035 | <0.001 | 3.2 | <0.001 | 140 | 1.5 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.8 | 0.0641 | <0.001 | 250 | <0.001 | 670 |
| G306 | 06/28/2021 | <0.003 | <0.001 | 0.042 | <0.001 | 2.5 | <0.001 | 140 | 2.4 | <0.004 | <0.002 | 0.321 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.0 | 1.28 | <0.001 | 210 | <0.001 | 700 |
| G306 | 07/14/2021 | <0.003 | <0.001 | 0.03 | <0.001 | 2.9 | <0.001 | 110 | <1 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.8 | 0.186 | <0.001 | 230 | <0.001 | 730 |
| G306 | 07/27/2021 | <0.003 | <0.001 | 0.033 | <0.001 | 3.1 | <0.001 | 110 | <1 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | 0.0013 | <0.001 | 6.8 | | <0.001 | 220 | <0.001 | 650 |
| G307 | 08/16/2016 | <0.003 | <0.001 | 0.031 | <0.001 | 2.1 | <0.001 | 210 | 26 | <0.004 | 0.0029 | 0.37 | <0.001 | 0.012 | 0.00042 | 0.0013 | 7.0 | 0.588 | <0.001 | 1000 | <0.001 | 1500 |



| Location | Sample Date | Antimony, total (mg/L) | Arsenic, total (mg/L) | Barium, total (mg/L) | Beryllium, total (mg/L) | Boron, total (mg/L) | Cadmium, total (mg/L) | Calcium, total (mg/L) | Chloride, total (mg/L) | Chromium, total (mg/L) | Cobalt, total (mg/L) | Fluoride, total (mg/L) | Lead, total (mg/L) | Lithium, total (mg/L) | Mercury, total (mg/L) | Molybdenum, total (mg/L) | pH (field) (SU) | Radium 226 and 228 combined (pCi/L) | Selenium, total (mg/L) | Sulfate, total (mg/L) | Thallium, total (mg/L) | Total Dissolved Solids (mg/L) |
|-----------|----------------|------------------------------|-----------------------------|----------------------------|-------------------------------|---------------------------|-----------------------------|-----------------------------|------------------------------|------------------------------|----------------------------|------------------------------|--------------------------|-----------------------------|-----------------------------|--------------------------------|-----------------------|--|------------------------------|-----------------------------|------------------------------|--|
| 35 I.A.C. | Lower | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6.5 | 0 | 0 | 0 | 0 | 0 |
| 845.600 | Upper | 0.006 | 0.010 | 2.0 | 0.004 | 2 | 0.005 | | 200 | 0.1 | 0.006 | 4.0 | 0.0075 | 0.04 | 0.002 | 0.1 | 9.0 | 5 | 0.05 | 400 | 0.002 | 1200 |
| G307 | 09/29/2016 | <0.003 | <0.001 | 0.029 | <0.001 | 2.2 | <0.001 | 250 | 26 | <0.004 | 0.0034 | 0.416 | <0.001 | <0.01 | <0.0002 | 0.0011 | 6.9 | 0.767 | <0.001 | 1000 | <0.001 | 1300 |
| G307 | 11/16/2016 | <0.003 | <0.001 | 0.034 | <0.001 | 2.1 | <0.001 | 190 | 24 | <0.004 | 0.0038 | 0.263 | 0.0012 | 0.011 | <0.0002 | 0.0019 | 6.9 | 0.529 | <0.001 | 1000 | <0.001 | 1600 |
| G307 | 02/19/2017 | <0.003 | <0.001 | 0.033 | <0.001 | 2 | <0.001 | 200 | 22 | <0.004 | 0.0039 | 0.323 | <0.001 | 0.011 | <0.0002 | 0.0013 | 7.0 | 1.88 | <0.001 | 1100 | <0.001 | 1500 |
| G307 | 05/17/2017 | <0.003 | 0.041 | 0.38 | 0.0029 | 1.8 | 0.0013 | 400 | 19 | 0.11 | 0.034 | 0.364 | 0.068 | 0.1 | <0.0002 | 0.0054 | 7.2 | 0.907 | 0.0038 | 940 | <0.001 | 1500 |
| G307 | 07/13/2017 | <0.003 | 0.012 | 0.13 | <0.001 | 2.2 | 0.0011 | 220 | 21 | 0.031 | 0.012 | 0.495 | 0.02 | 0.028 | <0.0002 | 0.0024 | 7.0 | 0.676 | 0.0014 | 1300 | <0.001 | 1300 |
| G307 | 10/27/2017 | | | | | 2.1 | | 230 | 18 | | | 0.411 | | | | | 7.0 | | | 980 | | 1400 |
| G307 | 05/14/2018 | <0.003 | 0.0037 | 0.071 | <0.001 | 2.2 | 0.0015 | 220 | 17 | 0.013 | 0.0059 | 0.389 | 0.007 | 0.02 | <0.0002 | 0.0021 | 7.0 | | <0.001 | 1100 | <0.001 | 1400 |
| G307 | 05/30/2018 | | | | | | | | | | | | | | | | | 0.813 | | | | |
| G307 | 08/03/2018 | | 0.0064 | 0.1 | | 2 | 0.0034 | 270 | 17 | 0.025 | 0.0078 | 0.391 | 0.013 | 0.02 | | 0.0022 | 7.0 | 0.0687 | | 1100 | | 1500 |
| G307 | 08/19/2019 | | 0.0049 | 0.11 | <0.001 | 2.1 | 0.027 | 280 | 18 | 0.025 | 0.0072 | 1.37 | 0.01 | 0.03 | | 0.002 | 7.0 | 1.06 | 0.0012 | 1100 | | 1600 |
| G307 | 02/26/2020 | <0.003 | <0.001 | 0.033 | <0.001 | 2.1 | 0.009 | 250 | 18 | 0.004 | 0.0031 | 0.264 | 0.0014 | <0.02 | <0.0002 | 0.0014 | 7.0 | 0.885 | <0.001 | 1000 | <0.001 | 1500 |
| G307 | 05/06/2020 | | | | | | | | | | 0.0026 | | | | | | 7.3 | | | | | |
| G307 | 08/11/2020 | | <0.001 | 0.021 | <0.001 | 2.1 | <0.001 | 230 | 15 | <0.004 | 0.0024 | 0.414 | <0.001 | <0.02 | | 0.0013 | 7.3 | 0.593 | <0.001 | 910 | | 1200 |
| G307 | 01/27/2021 | <0.003 | <0.001 | 0.02 | <0.001 | 1.9 | <0.001 | 200 | 14 | <0.004 | 0.0024 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.0012 | 7.4 | 0.616 | <0.001 | 850 | <0.001 | 1400 |
| G307D | 03/29/2021 | <0.003 | 0.001 | 0.044 | <0.001 | 1.4 | <0.001 | 170 | 34 | <0.004 | <0.002 | 0.435 | <0.001 | <0.02 | <0.0002 | 0.012 | 7.3 | 0.454 | <0.001 | 820 | <0.001 | 1400 |
| G307D | 04/21/2021 | <0.003 | <0.001 | 0.04 | <0.001 | 1.4 | <0.001 | 180 | | <0.004 | <0.002 | | <0.001 | <0.02 | <0.0002 | 0.012 | 7.2 | 0.568 | <0.001 | | <0.001 | |
| G307D | 05/04/2021 | <0.003 | 0.0012 | 0.037 | <0.001 | 1.4 | <0.001 | 180 | 29 | <0.004 | <0.002 | 0.612 | <0.001 | <0.02 | <0.0002 | 0.011 | 7.3 | 0.213 | <0.001 | 850 | <0.001 | 1300 |
| G307D | 05/18/2021 | <0.003 | 0.002 | 0.035 | <0.001 | 1.4 | <0.001 | 180 | 28 | <0.004 | <0.002 | 0.652 | <0.001 | <0.02 | <0.0002 | 0.011 | 7.3 | 0.139 | <0.001 | 840 | <0.001 | 1500 |
| G307D | 06/15/2021 | | | | | | | | | | | | | | | | | 0.138 | | | | |
| G307D | 06/28/2021 | | | | | | | | | | | | | | | | | 0.733 | | | | |
| G307D | 07/27/2021 | <0.003 | <0.001 | 0.032 | <0.001 | 1.7 | <0.001 | 160 | 22 | <0.004 | <0.002 | 0.716 | <0.001 | <0.02 | 0.00031 | 0.0082 | 7.2 | | <0.001 | 790 | <0.001 | 1400 |
| G308 | 03/29/2021 | <0.003 | <0.001 | 0.024 | <0.001 | 2.4 | <0.001 | 210 | 17 | <0.004 | <0.002 | 0.621 | <0.001 | <0.02 | <0.0002 | 0.0014 | 7.3 | 0.213 | <0.001 | 1100 | <0.001 | 1900 |



| Location | Sample Date | Antimony, total (mg/L) | Arsenic, total (mg/L) | Barium, total (mg/L) | Beryllium, total (mg/L) | Boron, total (mg/L) | Cadmium, total (mg/L) | Calcium, total (mg/L) | Chloride, total (mg/L) | Chromium, total (mg/L) | Cobalt, total (mg/L) | Fluoride, total (mg/L) | Lead, total (mg/L) | Lithium, total (mg/L) | Mercury, total (mg/L) | Molybdenum, total (mg/L) | pH (field) (SU) | Radium 226 and 228 combined (pCi/L) | Selenium, total (mg/L) | Sulfate, total (mg/L) | Thallium, total (mg/L) | Total Dissolved Solids (mg/L) |
|-----------|----------------|------------------------------|-----------------------------|----------------------------|-------------------------------|---------------------------|-----------------------------|-----------------------------|------------------------------|------------------------------|----------------------------|------------------------------|--------------------------|-----------------------------|-----------------------------|--------------------------------|-----------------------|--|------------------------------|-----------------------------|------------------------------|--|
| 35 I.A.C. | Lower | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6.5 | 0 | 0 | 0 | 0 | 0 |
| 845.600 | Upper | 0.006 | 0.010 | 2.0 | 0.004 | 2 | 0.005 | | 200 | 0.1 | 0.006 | 4.0 | 0.0075 | 0.04 | 0.002 | 0.1 | 9.0 | 5 | 0.05 | 400 | 0.002 | 1200 |
| G308 | 04/21/2021 | <0.003 | <0.001 | 0.022 | <0.001 | 2.5 | <0.001 | 210 | 19 | <0.004 | <0.002 | 0.616 | <0.001 | <0.02 | <0.0002 | 0.0013 | 7.2 | 0.607 | <0.001 | 1100 | <0.001 | 2000 |
| G308 | 05/05/2021 | <0.003 | <0.001 | 0.023 | <0.001 | 2.8 | <0.001 | 220 | 19 | <0.004 | <0.002 | <2.5 | <0.001 | <0.02 | <0.0002 | 0.0015 | 7.2 | 0.00738 | 0.0011 | 1200 | <0.001 | 1800 |
| G308 | 05/17/2021 | <0.003 | <0.001 | 0.021 | <0.001 | 2.5 | <0.001 | 220 | 20 | <0.004 | <0.002 | 0.647 | <0.001 | <0.02 | <0.0002 | 0.0014 | 7.2 | 0 | <0.001 | 1200 | <0.001 | 1900 |
| G308 | 06/14/2021 | <0.003 | <0.001 | 0.022 | <0.001 | 2.4 | <0.001 | 230 | 18 | <0.004 | <0.002 | 0.48 | <0.001 | <0.02 | <0.0002 | 0.0014 | 7.2 | 0.369 | <0.001 | 1100 | <0.001 | 1900 |
| G308 | 06/28/2021 | <0.003 | <0.001 | 0.025 | <0.001 | 2.5 | <0.001 | 220 | 18 | <0.004 | <0.002 | 0.481 | <0.001 | <0.02 | <0.0002 | 0.0014 | 7.2 | 0.121 | <0.001 | 1100 | <0.001 | 1800 |
| G308 | 07/14/2021 | <0.003 | <0.001 | 0.021 | <0.001 | 2.6 | <0.001 | 210 | 17 | <0.004 | <0.002 | 0.689 | <0.001 | <0.02 | <0.0002 | 0.0014 | 7.3 | 0.0838 | <0.001 | 1100 | <0.001 | 1900 |
| G308 | 07/27/2021 | <0.003 | <0.001 | 0.022 | <0.001 | 2.7 | <0.001 | 190 | 17 | <0.004 | <0.002 | 0.71 | <0.001 | <0.02 | 0.00022 | <0.001 | 7.3 | | <0.001 | 1100 | <0.001 | 1900 |
| G309 | 03/29/2021 | <0.003 | 0.0019 | 0.036 | <0.001 | 1.8 | <0.001 | 180 | 17 | 0.0045 | <0.002 | 0.369 | 0.0012 | <0.02 | <0.0002 | 0.0021 | 7.2 | 0.0737 | <0.001 | 840 | <0.001 | 1300 |
| G309 | 04/21/2021 | <0.003 | <0.001 | 0.023 | <0.001 | 1.8 | <0.001 | 180 | 19 | <0.004 | <0.002 | 0.532 | <0.001 | <0.02 | <0.0002 | 0.002 | 7.2 | 0.0702 | <0.001 | 740 | <0.001 | 1400 |
| G309 | 05/05/2021 | <0.003 | 0.0012 | 0.023 | <0.001 | 1.9 | <0.001 | 180 | 19 | <0.004 | <0.002 | 0.408 | <0.001 | <0.02 | <0.0002 | 0.0019 | 7.2 | 0.222 | <0.001 | 770 | <0.001 | 1400 |
| G309 | 05/17/2021 | <0.003 | 0.0013 | 0.023 | <0.001 | 7.5 | <0.001 | 190 | 21 | <0.004 | <0.002 | 0.438 | <0.001 | <0.02 | <0.0002 | 0.0017 | 7.3 | 0.36 | <0.001 | 840 | <0.001 | 1300 |
| G309 | 06/14/2021 | <0.003 | 0.0011 | 0.021 | <0.001 | 1.9 | <0.001 | 190 | 19 | <0.004 | <0.002 | 0.468 | <0.001 | <0.02 | <0.0002 | 0.0015 | 7.2 | 0 | <0.001 | 790 | <0.001 | 1400 |
| G309 | 06/28/2021 | <0.003 | <0.001 | 0.022 | <0.001 | 1.9 | <0.001 | 190 | 19 | <0.004 | <0.002 | 0.387 | <0.001 | <0.02 | <0.0002 | 0.0014 | 7.3 | 1.2 | <0.001 | 780 | <0.001 | 1300 |
| G309 | 07/13/2021 | <0.003 | <0.001 | 0.023 | <0.001 | 2.5 | <0.001 | 180 | 19 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.4 | 0.62 | <0.001 | 800 | <0.001 | 1400 |
| G309 | 07/27/2021 | <0.003 | <0.001 | 0.022 | <0.001 | 2 | <0.001 | 170 | 18 | <0.004 | <0.002 | 0.484 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.3 | | <0.001 | 740 | <0.001 | 1400 |
| G310 | 03/29/2021 | <0.003 | <0.001 | 0.016 | <0.001 | 1.6 | <0.001 | 170 | 20 | <0.004 | <0.002 | 0.252 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.1 | 0.642 | <0.001 | 910 | <0.001 | 1400 |
| G310 | 04/22/2021 | <0.003 | <0.001 | 0.022 | <0.001 | 1.7 | <0.001 | 190 | 22 | <0.004 | <0.002 | 0.295 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.0 | 0 | <0.001 | 2300 | <0.001 | 1500 |
| G310 | 05/04/2021 | <0.003 | <0.001 | 0.019 | <0.001 | 1.8 | <0.001 | 190 | 20 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.2 | 0.0501 | <0.001 | 870 | <0.001 | 1600 |
| G310 | 05/19/2021 | <0.003 | <0.001 | 0.016 | <0.001 | 1.7 | <0.001 | 180 | 22 | <0.004 | <0.002 | 0.31 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.2 | 2.25 | <0.001 | 860 | <0.001 | 1500 |
| G310 | 06/15/2021 | <0.003 | <0.001 | 0.018 | <0.001 | 2 | <0.001 | 200 | 21 | <0.004 | <0.002 | 0.29 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.2 | 0 | <0.001 | 860 | <0.001 | 1500 |
| G310 | 06/28/2021 | <0.003 | <0.001 | 0.018 | <0.001 | 1.8 | <0.001 | 190 | 21 | <0.004 | <0.002 | 0.286 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.1 | 0.83 | <0.001 | 820 | <0.001 | 1500 |
| G310 | 07/13/2021 | <0.003 | <0.001 | 0.018 | <0.001 | 2 | <0.001 | 180 | 24 | <0.004 | <0.002 | 0.331 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.2 | 0.298 | <0.001 | 420 | <0.001 | 1600 |



| Location | Sample Date | Antimony, total (mg/L) | Arsenic, total (mg/L) | Barium, total (mg/L) | Beryllium, total (mg/L) | Boron, total (mg/L) | Cadmium, total (mg/L) | Calcium, total (mg/L) | Chloride, total (mg/L) | Chromium, total (mg/L) | Cobalt, total (mg/L) | Fluoride, total (mg/L) | Lead, total (mg/L) | Lithium, total (mg/L) | Mercury, total (mg/L) | Molybdenum, total (mg/L) | pH (field) (SU) | Radium 226 and 228 combined (pCi/L) | Selenium, total (mg/L) | Sulfate, total (mg/L) | Thallium, total (mg/L) | Total Dissolved Solids (mg/L) |
|-----------|----------------|------------------------------|-----------------------------|----------------------------|-------------------------------|---------------------------|-----------------------------|-----------------------------|------------------------------|------------------------------|----------------------------|------------------------------|--------------------------|-----------------------------|-----------------------------|--------------------------------|-----------------------|--|------------------------------|-----------------------------|------------------------------|--|
| 35 I.A.C. | Lower | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6.5 | 0 | 0 | 0 | 0 | 0 |
| 845.600 | Upper | 0.006 | 0.010 | 2.0 | 0.004 | 2 | 0.005 | | 200 | 0.1 | 0.006 | 4.0 | 0.0075 | 0.04 | 0.002 | 0.1 | 9.0 | 5 | 0.05 | 400 | 0.002 | 1200 |
| G310 | 07/28/2021 | <0.003 | <0.001 | 0.017 | <0.001 | 1.8 | <0.001 | 190 | 21 | <0.004 | <0.002 | 0.394 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.2 | | <0.001 | 880 | <0.001 | 1600 |
| G311 | 03/30/2021 | <0.003 | <0.001 | 0.038 | <0.001 | 2.3 | <0.001 | 210 | 22 | <0.004 | 0.0033 | 0.356 | 0.001 | <0.02 | <0.0002 | <0.001 | 6.7 | 0.0742 | <0.001 | 770 | <0.001 | 1500 |
| G311 | 04/22/2021 | <0.003 | <0.001 | 0.031 | <0.001 | 2.3 | <0.001 | 210 | 31 | <0.004 | 0.0029 | 0.345 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.8 | 0.245 | <0.001 | 820 | <0.001 | 1500 |
| G311 | 05/04/2021 | <0.003 | <0.001 | 0.029 | <0.001 | 2.3 | <0.001 | 200 | 22 | <0.004 | 0.0027 | <0.25 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.0 | 0.108 | <0.001 | 820 | <0.001 | 1600 |
| G311 | 05/19/2021 | <0.003 | <0.001 | 0.031 | <0.001 | 2.4 | <0.001 | 210 | 24 | <0.004 | 0.0032 | 0.282 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.9 | 0.147 | <0.001 | 840 | <0.001 | 1500 |
| G311 | 06/15/2021 | <0.003 | 0.0011 | 0.03 | <0.001 | 2.9 | <0.001 | 240 | 22 | <0.004 | 0.0031 | 0.36 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.9 | 0.727 | <0.001 | 820 | <0.001 | 1600 |
| G311 | 06/29/2021 | <0.003 | <0.001 | 0.027 | <0.001 | 2.5 | <0.001 | 220 | 25 | <0.004 | 0.003 | 0.371 | <0.001 | 0.02 | <0.0002 | <0.001 | 7.0 | 1.12 | <0.001 | 810 | <0.001 | 1500 |
| G311 | 07/14/2021 | <0.003 | <0.001 | 0.026 | <0.001 | 2.6 | <0.001 | 200 | 24 | <0.004 | 0.0026 | 0.436 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.9 | 0.179 | <0.001 | 860 | <0.001 | 1600 |
| G311 | 07/27/2021 | <0.003 | <0.001 | 0.029 | <0.001 | 2.5 | <0.001 | 210 | 23 | <0.004 | 0.0028 | 0.422 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.1 | | <0.001 | 750 | <0.001 | 1600 |
| G311D | 03/30/2021 | <0.003 | 0.0018 | 0.22 | <0.001 | 0.32 | <0.001 | 98 | 12 | <0.004 | 0.0022 | 0.537 | <0.001 | <0.02 | <0.0002 | 0.013 | 7.1 | 0.838 | 0.0012 | 140 | <0.001 | 490 |
| G311D | 04/22/2021 | <0.003 | 0.0023 | 0.23 | <0.001 | 0.28 | <0.001 | 110 | 8.7 | <0.004 | 0.002 | 0.518 | <0.001 | <0.02 | <0.0002 | 0.011 | 7.0 | 0.512 | <0.001 | 120 | <0.001 | 580 |
| G311D | 05/04/2021 | <0.003 | 0.0026 | 0.24 | <0.001 | 0.3 | <0.001 | 110 | 8.9 | <0.004 | 0.002 | 0.393 | <0.001 | <0.02 | <0.0002 | 0.011 | 7.2 | 0.149 | <0.001 | 120 | <0.001 | 580 |
| G311D | 05/19/2021 | <0.003 | 0.0035 | 0.22 | <0.001 | 0.29 | <0.001 | 110 | 15 | <0.004 | 0.0021 | 0.531 | <0.001 | <0.02 | <0.0002 | 0.01 | 7.2 | 0.433 | <0.001 | 120 | <0.001 | 550 |
| G311D | 06/15/2021 | | | | | | | | | | | | | | | | | 1.01 | | | | |
| G311D | 06/29/2021 | | | | | | | | | | | | | | | | | 2.24 | | | | |
| G311D | 07/28/2021 | <0.003 | 0.0054 | 0.25 | <0.001 | 0.26 | <0.001 | 110 | <1 | <0.004 | <0.002 | 0.701 | <0.001 | <0.02 | <0.0002 | 0.01 | 7.2 | | <0.001 | 77 | <0.001 | 590 |
| G312 | 03/30/2021 | <0.003 | <0.001 | 0.023 | <0.001 | 1.5 | <0.001 | 190 | 20 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.5 | 0.0336 | <0.001 | 600 | <0.001 | 1300 |
| G312 | 04/22/2021 | <0.003 | <0.001 | 0.025 | <0.001 | 1.6 | <0.001 | 200 | 20 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.4 | 0.0769 | <0.001 | 650 | <0.001 | 1400 |
| G312 | 05/04/2021 | <0.003 | 0.0012 | 0.03 | <0.001 | 1.7 | <0.001 | 210 | 25 | <0.004 | 0.0029 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.0013 | 6.5 | 0.435 | <0.001 | 920 | <0.001 | 1600 |
| G312 | 05/19/2021 | <0.003 | <0.001 | 0.025 | <0.001 | 1.4 | <0.001 | 190 | 26 | <0.004 | 0.0025 | <0.25 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.4 | 0.825 | <0.001 | 1000 | <0.001 | 1700 |
| G312 | 06/15/2021 | <0.003 | <0.001 | 0.026 | <0.001 | 1.6 | <0.001 | 220 | 26 | <0.004 | 0.003 | <0.25 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.5 | 0.937 | <0.001 | 920 | <0.001 | 1800 |
| G312 | 06/29/2021 | <0.003 | <0.001 | 0.029 | <0.001 | 1.8 | <0.001 | 210 | 27 | <0.004 | 0.0039 | <0.25 | <0.001 | 0.021 | <0.0002 | <0.001 | 6.5 | 0.498 | <0.001 | 890 | <0.001 | 1600 |



TABLE 4-1. GROUNDWATER ANALYTICAL RESULTS

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Location | Sample Date | Antimony, total (mg/L) | Arsenic, total (mg/L) | Barium, total (mg/L) | Beryllium, total (mg/L) | Boron, total (mg/L) | Cadmium, total (mg/L) | Calcium, total (mg/L) | Chloride, total (mg/L) | Chromium, total (mg/L) | Cobalt, total (mg/L) | Fluoride, total (mg/L) | Lead, total (mg/L) | Lithium, total (mg/L) | Mercury, total (mg/L) | Molybdenum, total (mg/L) | pH (field) (SU) | Radium 226 and 228 combined (pCi/L) | Selenium, total (mg/L) | Sulfate, total (mg/L) | Thallium, total (mg/L) | Total Dissolved Solids (mg/L) |
|-----------|----------------|------------------------------|-----------------------------|----------------------------|-------------------------------|---------------------------|-----------------------------|-----------------------------|------------------------------|------------------------------|----------------------------|------------------------------|--------------------------|-----------------------------|-----------------------------|--------------------------------|-----------------------|--|------------------------------|-----------------------------|------------------------------|--|
| 35 I.A.C. | Lower | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6.5 | 0 | 0 | 0 | 0 | 0 |
| 845.600 | Upper | 0.006 | 0.010 | 2.0 | 0.004 | 2 | 0.005 | - | 200 | 0.1 | 0.006 | 4.0 | 0.0075 | 0.04 | 0.002 | 0.1 | 9.0 | 5 | 0.05 | 400 | 0.002 | 1200 |
| G312 | 07/13/2021 | <0.003 | <0.001 | 0.028 | <0.001 | 2.2 | <0.001 | 200 | 26 | <0.004 | 0.0036 | <0.25 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.3 | 1.12 | <0.001 | 930 | <0.001 | 1900 |
| G312 | 07/27/2021 | <0.003 | <0.001 | 0.023 | <0.001 | 3.5 | <0.001 | 240 | 22 | <0.004 | 0.0032 | 0.253 | <0.001 | 0.021 | <0.0002 | <0.001 | 6.5 | | <0.001 | 800 | <0.001 | 1800 |
| G313 | 03/30/2021 | <0.003 | <0.001 | 0.025 | <0.001 | 3.3 | <0.001 | 200 | 23 | <0.004 | <0.002 | 0.276 | <0.001 | 0.02 | <0.0002 | 0.0014 | 6.9 | 0.685 | <0.001 | 970 | <0.001 | 1600 |
| G313 | 04/22/2021 | <0.003 | <0.001 | 0.021 | <0.001 | 3.4 | <0.001 | 210 | 25 | <0.004 | <0.002 | 0.272 | <0.001 | <0.02 | <0.0002 | 0.0013 | 6.8 | 0.623 | <0.001 | 750 | <0.001 | 1600 |
| G313 | 05/04/2021 | <0.003 | <0.001 | 0.023 | <0.001 | 3.5 | <0.001 | 200 | 26 | <0.004 | <0.002 | 0.267 | <0.001 | <0.02 | <0.0002 | 0.0012 | 7.0 | 0.188 | <0.001 | 790 | <0.001 | 1600 |
| G313 | 05/18/2021 | <0.003 | 0.0014 | 0.023 | <0.001 | 3.3 | <0.001 | 210 | 25 | <0.004 | 0.0024 | 0.332 | <0.001 | <0.02 | <0.0002 | 0.0011 | 7.0 | 0.666 | <0.001 | 780 | <0.001 | 1600 |
| G313 | 06/14/2021 | <0.003 | <0.001 | 0.022 | <0.001 | 3.3 | <0.001 | 220 | 26 | <0.004 | 0.0022 | 0.251 | <0.001 | 0.021 | <0.0002 | 0.0012 | 7.1 | 0.65 | <0.001 | 770 | <0.001 | 1700 |
| G313 | 06/28/2021 | < 0.003 | <0.001 | 0.02 | <0.001 | 3.5 | <0.001 | 200 | 24 | <0.004 | <0.002 | 0.276 | <0.001 | 0.037 | <0.0002 | 0.0012 | 7.0 | 0.828 | <0.001 | 750 | <0.001 | 1600 |
| G313 | 07/13/2021 | <0.003 | <0.001 | 0.02 | <0.001 | 3.4 | <0.001 | 200 | 24 | <0.004 | <0.002 | 0.336 | <0.001 | 0.033 | <0.0002 | 0.0012 | 6.9 | 0 | <0.001 | 690 | <0.001 | 1800 |
| G313 | 07/27/2021 | < 0.003 | <0.001 | 0.019 | <0.001 | 3.5 | <0.001 | 200 | <250 | <0.004 | <0.002 | 0.351 | <0.001 | 0.022 | <0.0002 | 0.0012 | 6.9 | | <0.001 | 710 | <0.001 | 1600 |
| G314 | 03/30/2021 | <0.003 | <0.001 | 0.035 | <0.001 | 0.24 | <0.001 | 570 | 36 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.016 | 6.8 | 1.36 | 0.0015 | 2000 | <0.001 | 3400 |
| G314 | 04/21/2021 | <0.003 | <0.001 | 0.026 | <0.001 | 0.16 | <0.001 | 640 | 35 | <0.004 | 0.0037 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.01 | 6.6 | 2.01 | <0.001 | 2100 | <0.001 | 3700 |
| G314 | 05/04/2021 | <0.003 | <0.001 | 0.026 | <0.001 | 0.22 | <0.001 | 660 | 34 | <0.004 | 0.0047 | <0.25 | 0.0025 | <0.02 | <0.0002 | 0.01 | 7.1 | 0.32 | <0.001 | 2100 | <0.001 | 3600 |
| G314 | 05/17/2021 | < 0.003 | <0.001 | 0.021 | <0.001 | 0.42 | <0.001 | 630 | 37 | <0.004 | 0.006 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.0089 | 6.6 | 0.976 | 0.0043 | 2200 | <0.001 | 3600 |
| G314 | 06/14/2021 | < 0.003 | 0.0011 | 0.021 | <0.001 | 0.15 | <0.001 | 660 | 100 | <0.004 | 0.0088 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.0081 | 6.6 | 0.482 | <0.001 | 830 | <0.001 | 1900 |
| G314 | 06/28/2021 | < 0.003 | <0.001 | 0.021 | <0.001 | 0.12 | <0.001 | 620 | 36 | 0.0096 | 0.0095 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.0058 | 6.6 | 1.8 | <0.001 | 2000 | <0.001 | 3700 |
| G314 | 07/13/2021 | < 0.003 | <0.001 | 0.022 | <0.001 | 0.14 | <0.001 | 620 | 30 | <0.004 | 0.011 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.0048 | 6.7 | 0.604 | <0.001 | 2000 | <0.001 | 4000 |
| G314 | 07/27/2021 | <0.003 | <0.001 | 0.02 | <0.001 | 0.23 | <0.001 | 630 | 33 | <0.004 | 0.01 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.0043 | 6.6 | | <0.001 | 2400 | <0.001 | 3800 |
| G314D | 03/30/2021 | <0.003 | 0.0014 | 0.049 | <0.001 | 0.18 | <0.001 | 110 | 170 | <0.004 | <0.002 | 1.06 | <0.001 | 0.025 | <0.0002 | 0.026 | 7.3 | 2.51 | <0.001 | 1100 | <0.001 | 2400 |
| G314D | 04/21/2021 | <0.003 | 0.001 | 0.048 | <0.001 | 0.17 | <0.001 | 130 | 180 | <0.004 | <0.002 | 0.996 | <0.001 | 0.022 | <0.004 | 0.02 | 7.2 | 1.4 | <0.001 | 1000 | <0.001 | 2400 |
| G314D | 05/04/2021 | <0.003 | <0.001 | 0.045 | <0.001 | 0.18 | <0.001 | 130 | | <0.004 | <0.002 | | <0.001 | 0.022 | <0.0002 | 0.02 | 7.2 | 2.82 | <0.001 | | <0.001 | |
| G314D | 05/19/2021 | <0.003 | <0.001 | 0.052 | <0.001 | 0.16 | <0.001 | 140 | 130 | <0.004 | <0.002 | 0.84 | 0.0014 | <0.02 | <0.0002 | 0.014 | 7.2 | 4.09 | <0.001 | 820 | <0.001 | 1800 |



TABLE 4-1. GROUNDWATER ANALYTICAL RESULTS

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Location | Sample Date | Antimony, total (mg/L) | Arsenic, total (mg/L) | Barium, total (mg/L) | Beryllium, total (mg/L) | Boron, total (mg/L) | Cadmium, total (mg/L) | Calcium, total (mg/L) | Chloride, total (mg/L) | Chromium, total (mg/L) | Cobalt, total (mg/L) | Fluoride, total (mg/L) | Lead, total (mg/L) | Lithium, total (mg/L) | Mercury, total (mg/L) | Molybdenum, total (mg/L) | pH (field) (SU) | Radium 226 and 228 combined (pCi/L) | Selenium, total (mg/L) | Sulfate, total (mg/L) | Thallium, total (mg/L) | Total Dissolved Solids (mg/L) |
|-----------|----------------|------------------------------|-----------------------------|----------------------------|-------------------------------|---------------------------|-----------------------------|-----------------------------|------------------------------|------------------------------|----------------------------|------------------------------|--------------------------|-----------------------------|-----------------------------|--------------------------------|-----------------------|--|------------------------------|-----------------------------|------------------------------|--|
| 35 I.A.C. | Lower | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6.5 | 0 | 0 | 0 | 0 | 0 |
| 845.600 | Upper | 0.006 | 0.010 | 2.0 | 0.004 | 2 | 0.005 | | 200 | 0.1 | 0.006 | 4.0 | 0.0075 | 0.04 | 0.002 | 0.1 | 9.0 | 5 | 0.05 | 400 | 0.002 | 1200 |
| G314D | 06/28/2021 | | | | | | | | | | | | | | | | | 2.56 | | | | |
| G314D | 07/28/2021 | <0.003 | <0.001 | 0.046 | <0.001 | 0.14 | <0.001 | 160 | 93 | <0.004 | <0.002 | 0.659 | <0.001 | <0.02 | <0.0002 | 0.0095 | 7.2 | | <0.001 | 670 | <0.001 | 1600 |
| G315 | 03/30/2021 | <0.003 | <0.001 | 0.028 | < 0.001 | 1.2 | <0.001 | 190 | 1.9 | <0.004 | <0.002 | 0.261 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.9 | 0.622 | <0.001 | 1100 | <0.001 | 1500 |
| G315 | 04/22/2021 | <0.003 | <0.001 | 0.026 | <0.001 | 1.2 | <0.001 | 200 | 64 | <0.004 | <0.002 | 0.344 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.8 | 0.0124 | <0.001 | 880 | <0.001 | 1600 |
| G315 | 05/05/2021 | <0.003 | <0.001 | 0.024 | <0.001 | 1.3 | <0.001 | 190 | 19 | <0.004 | <0.002 | 0.253 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.8 | 0.0233 | <0.001 | 900 | <0.001 | 1500 |
| G315 | 05/18/2021 | <0.003 | <0.001 | 0.024 | <0.001 | 1.2 | <0.001 | 190 | 20 | <0.004 | <0.002 | 0.25 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.9 | 0.45 | <0.001 | 880 | <0.001 | 1500 |
| G315 | 06/15/2021 | <0.003 | <0.001 | 0.025 | <0.001 | 1.3 | <0.001 | 210 | 19 | <0.004 | <0.002 | 0.307 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.9 | 1.27 | <0.001 | 870 | <0.001 | 1500 |
| G315 | 06/29/2021 | <0.003 | <0.001 | 0.023 | <0.001 | 1.3 | <0.001 | 190 | 19 | <0.004 | <0.002 | 0.395 | <0.001 | <0.02 | <0.0002 | <0.001 | 7.0 | 0.528 | <0.001 | 930 | <0.001 | 1400 |
| G315 | 07/14/2021 | <0.003 | <0.001 | 0.028 | <0.001 | 1.3 | <0.001 | 190 | 17 | <0.004 | <0.002 | 0.316 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.8 | 0.864 | <0.001 | 860 | <0.001 | 1700 |
| G315 | 07/28/2021 | <0.003 | <0.001 | 0.023 | <0.001 | 1.3 | <0.001 | 190 | 18 | <0.004 | <0.002 | 0.394 | <0.001 | <0.02 | <0.0002 | <0.001 | 6.7 | | <0.001 | 850 | <0.001 | 1600 |
| G316 | 03/30/2021 | <0.003 | 0.0073 | 0.063 | <0.001 | 0.35 | <0.001 | 200 | 25 | <0.004 | 0.0035 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.0036 | 7.0 | 0.479 | <0.001 | 840 | <0.001 | 1600 |
| G316 | 04/22/2021 | <0.003 | 0.0063 | 0.064 | <0.001 | 0.37 | <0.001 | 200 | 52 | <0.004 | 0.0034 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.0036 | 7.0 | 0.622 | <0.001 | 770 | <0.001 | 1100 |
| G316 | 05/05/2021 | <0.003 | 0.007 | 0.063 | <0.001 | 0.35 | <0.001 | 210 | 26 | <0.004 | 0.0034 | <0.25 | 0.014 | <0.02 | <0.0002 | 0.0037 | 6.9 | 0.884 | <0.001 | 740 | <0.001 | 1600 |
| G316 | 05/17/2021 | <0.003 | 0.0071 | 0.059 | <0.001 | 0.55 | <0.001 | 200 | 28 | <0.004 | 0.0035 | 0.28 | <0.001 | <0.02 | <0.0002 | 0.0037 | 7.1 | 17.5 | <0.001 | 760 | <0.001 | 1700 |
| G316 | 06/14/2021 | <0.003 | 0.0073 | 0.062 | <0.001 | 0.42 | <0.001 | 210 | 23 | <0.004 | 0.003 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.004 | 7.1 | 0.75 | <0.001 | 750 | <0.001 | 1700 |
| G316 | 06/28/2021 | <0.003 | 0.0077 | 0.065 | <0.001 | 0.46 | <0.001 | 190 | 22 | <0.004 | 0.003 | 0.273 | <0.001 | <0.02 | <0.0002 | 0.0041 | 7.1 | 0.196 | <0.001 | 330 | <0.001 | 1600 |
| G316 | 07/13/2021 | <0.003 | 0.0085 | 0.069 | <0.001 | 0.49 | <0.001 | 190 | 25 | <0.004 | 0.0032 | 0.305 | <0.001 | <0.02 | <0.0002 | 0.0043 | 7.0 | 0.705 | <0.001 | 680 | <0.001 | 1600 |
| G316 | 07/27/2021 | <0.003 | 0.0077 | 0.062 | <0.001 | 0.52 | <0.001 | 190 | 30 | <0.004 | 0.0029 | 0.296 | <0.001 | <0.02 | <0.0002 | 0.0042 | 7.0 | | <0.001 | 660 | <0.001 | 1600 |
| G317 | 03/30/2021 | <0.003 | 0.001 | 0.049 | <0.001 | 0.034 | <0.001 | 210 | 16 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.0049 | 6.5 | 3.01 | 0.0011 | 780 | <0.001 | 1500 |
| G317 | 04/22/2021 | <0.003 | <0.001 | 0.058 | <0.001 | 0.021 | <0.001 | 230 | 18 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.004 | 6.5 | 1.26 | <0.001 | 910 | <0.001 | 1600 |
| G317 | 05/05/2021 | <0.003 | 0.0011 | 0.04 | <0.001 | 0.019 | <0.001 | 280 | 14 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.0034 | 6.6 | 1.1 | <0.001 | 1000 | <0.001 | 1800 |
| G317 | 05/18/2021 | <0.003 | <0.001 | 0.038 | <0.001 | 0.034 | <0.001 | 260 | 15 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.0028 | 6.6 | 1.08 | <0.001 | 980 | <0.001 | 1800 |



TABLE 4-1. GROUNDWATER ANALYTICAL RESULTS

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Location | Sample Date | Antimony, total (mg/L) | Arsenic, total (mg/L) | Barium, total (mg/L) | Beryllium, total (mg/L) | Boron, total (mg/L) | Cadmium, total (mg/L) | Calcium, total (mg/L) | Chloride, total (mg/L) | Chromium, total (mg/L) | Cobalt, total (mg/L) | Fluoride, total (mg/L) | Lead, total (mg/L) | Lithium, total (mg/L) | Mercury, total (mg/L) | Molybdenum, total (mg/L) | pH (field) (SU) | Radium 226 and 228 combined (pCi/L) | Selenium, total (mg/L) | Sulfate, total (mg/L) | Thallium, total (mg/L) | Total Dissolved Solids (mg/L) |
|-----------|----------------|------------------------------|-----------------------------|----------------------------|-------------------------------|---------------------------|-----------------------------|-----------------------------|------------------------------|------------------------------|----------------------------|------------------------------|--------------------------|-----------------------------|-----------------------------|--------------------------------|-----------------------|--|------------------------------|-----------------------------|------------------------------|--|
| 35 I.A.C. | Lower | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6.5 | 0 | 0 | 0 | 0 | 0 |
| 845.600 | Upper | 0.006 | 0.010 | 2.0 | 0.004 | 2 | 0.005 | | 200 | 0.1 | 0.006 | 4.0 | 0.0075 | 0.04 | 0.002 | 0.1 | 9.0 | 5 | 0.05 | 400 | 0.002 | 1200 |
| G317 | 06/15/2021 | <0.003 | 0.0013 | 0.039 | <0.001 | 0.034 | < 0.001 | 260 | 14 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.0025 | 6.6 | 1.05 | <0.001 | 900 | <0.001 | 1600 |
| G317 | 06/28/2021 | <0.003 | <0.001 | 0.034 | <0.001 | 0.024 | <0.001 | 230 | 12 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.0026 | 6.7 | 0.863 | <0.001 | 950 | <0.001 | 1900 |
| G317 | 07/13/2021 | <0.003 | 0.0014 | 0.021 | <0.001 | 0.019 | <0.001 | 310 | 14 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.0027 | 6.6 | 1.33 | <0.001 | 1100 | <0.001 | 2000 |
| G317 | 07/28/2021 | <0.003 | <0.001 | 0.023 | <0.001 | 0.045 | <0.001 | 290 | 2.8 | <0.004 | <0.002 | <0.25 | <0.001 | <0.02 | <0.0002 | 0.0023 | 6.5 | | <0.001 | 1000 | <0.001 | 1800 |

Notes:

Detected at concentration greater than the GWPS

-- = data not available

GWPS = Groundwater protection standard

mg/L = milligrams per liter

pCi/L = picocuries per liter

SU = standard units

< = concentration is less than the concentration shown, which corresponds to the reporting limit for the method. Estimated concentrations below the reporting limit and associated qualifiers are not provided since they are not utilized in statistics to determine exceedances above Part 845 standards.</p>

35 I.A.C. 845.600 = Residuals in Surface Impoundments: Title 35 of the Illinois Administrative Code § 845



COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Sample Location | Sample Date | Dissolved Oxygen (mg/L) | Oxidation Reduction Potential (mV) | pH (field) (SU) | Specific Conductance (micromhos/cm) | Temperature (deg. C) | Turbidity (NTU) |
|--------------------|----------------|----------------------------|---------------------------------------|--------------------|-------------------------------------|-------------------------|--------------------|
| G281 | 11/20/2015 | 0 | -18 | 7.0 | 1310 | 16.8 | 375 |
| G281 | 02/11/2016 | 2.40 | 171 | 7.1 | 1330 | 8.0 | 12 |
| G281 | 05/10/2016 | 0 | 40 | 7.0 | 1350 | 15.5 | |
| G281 | 08/01/2016 | 0 | 56 | 7.0 | 1405 | 16.7 | 19.4 |
| G281 | 11/16/2016 | 0 | 58 | 6.9 | 1305 | 13.6 | 16 |
| G281 | 02/10/2017 | 0 | 65 | 6.7 | 1200 | 14.5 | 23.5 |
| G281 | 05/16/2017 | 0 | 63 | 6.9 | 1230 | 15.4 | 19.8 |
| G281 | 07/12/2017 | 0 | 62 | 7.0 | 1295 | 16.5 | 11.3 |
| G281 | 10/25/2017 | 0 | 75 | 7.0 | 877 | 13.0 | 26.4 |
| G281 | 05/11/2018 | 0 | 45 | 7.1 | 1430 | 14.3 | 11.4 |
| G281 | 08/03/2018 | 0 | 62 | 7.0 | 1182 | 16.1 | 20.4 |
| G281 | 01/23/2019 | 0 | 65 | 7.0 | 1190 | 11.9 | 20 |
| G281 | 08/13/2019 | 0 | 65 | 6.9 | 1090 | 17.4 | 12 |
| G281 | 01/24/2020 | 6.60 | 151 | 7.3 | 739.1 | 9.7 | 7.83 |
| G281 | 08/12/2020 | 0.66 | 129 | 6.9 | 1322 | 21.5 | 1.8 |
| G281 | 01/29/2021 | 2.20 | 110 | 7.1 | 1121 | 9.4 | 29.4 |
| G281 | 03/31/2021 | 1.40 | 257 | 7.0 | 1356 | 11.1 | 14.1 |
| G281 | 04/21/2021 | 2.20 | 41.7 | 6.9 | 1311 | 12.0 | 2.14 |
| G281 | 05/05/2021 | 1.50 | 189 | 7.1 | 1340 | 14.0 | 14.9 |
| G281 | 05/17/2021 | 0.14 | 181 | 7.1 | 1359 | 15.0 | 2.06 |
| G281 | 06/14/2021 | 1.10 | 54.1 | 7.1 | 1357 | 20.8 | 66.5 |
| G281 | 06/28/2021 | 1.80 | 26.1 | 7.2 | 1311 | 20.7 | 11.4 |
| G281 | 07/12/2021 | 1.60 | 210 | 7.2 | 1096 | 19.9 | 13.3 |
| G281 | 07/27/2021 | 0.85 | 72.7 | 7.1 | 1319 | 20.4 | 18.9 |
| G301 | 11/20/2015 | 0 | -37 | 6.9 | 1630 | 16.5 | 270 |
| G301 | 02/23/2016 | 0 | 127 | 6.6 | 1640 | 11.3 | 26 |
| G301 | 05/20/2016 | 0 | 136 | 6.4 | 1660 | 15.7 | 74 |
| G301 | 08/15/2016 | 0 | 125 | 6.8 | 1720 | 18.3 | 32 |
| G301 | 11/17/2016 | 0 | 109 | 6.9 | 1560 | 14.4 | 40.8 |
| G301 | 02/16/2017 | 0 | 122 | 7.0 | 1500 | 15.8 | 63 |
| G301 | 05/17/2017 | 0 | 103 | 7.1 | 1590 | 15.4 | 67.9 |
| G301 | 07/12/2017 | 0 | 121 | 6.8 | 1490 | 17.2 | 27.4 |
| G301 | 10/26/2017 | 0 | 96 | 6.8 | 1500 | 13.0 | 34.1 |
| G301 | 05/11/2018 | 0 | 98 | 6.9 | 1680 | 13.7 | 50.5 |
| G301 | 08/03/2018 | 0 | 109 | 6.9 | 1615 | 15.6 | 41.8 |
| G301 | 01/23/2019 | 0 | 112 | 7.0 | 1590 | 12.0 | 41 |
| G301 | 08/19/2019 | 0 | 101 | 6.9 | 1520 | 17.4 | 39.8 |
| G301 | 01/23/2020 | 1.40 | 147 | 6.7 | 1661 | 8.6 | 104 |
| G301 | 08/11/2020 | 0.30 | -102 | 6.6 | 1682 | 21.1 | 0.45 |
| G301 | 01/27/2021 | 0.76 | 50.6 | 6.6 | 1710 | 9.1 | 6.08 |
| G302 | 11/20/2015 | 0 | -120 | 6.9 | 1850 | 16.4 | 145 |
| G302 | 02/23/2016 | 0 | 27 | 6.8 | 1730 | 11.6 | |
| G302 | 05/20/2016 | 0 | -118 | 6.8 | 1930 | 15.9 | 34 |
| G302 | 08/15/2016 | 1.13 | 95 | 7.0 | 1490 | 17.7 | 56 |
| G302 | 11/17/2016 | 1.08 | 71 | 7.1 | 1280 | 15.1 | 60.8 |
| G302 | 02/16/2017 | 0 | 71 | 7.1 | 1262 | 15.3 | 78.1 |



COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Sample Location | Sample Date | Dissolved Oxygen (mg/L) | Oxidation Reduction Potential (mV) | pH (field) (SU) | Specific Conductance (micromhos/cm) | Temperature (deg. C) | Turbidity (NTU) |
|--------------------|----------------|----------------------------|---------------------------------------|--------------------|-------------------------------------|-------------------------|--------------------|
| G302 | 05/17/2017 | 0 | 70 | 7.0 | 1160 | 15.5 | 80.7 |
| G302 | 07/12/2017 | 0 | 112 | 7.0 | 1260 | 17.1 | 46.6 |
| G302 | 10/26/2017 | 0 | 78 | 7.1 | 1420 | 13.3 | 54.2 |
| G302 | 05/11/2018 | 0 | 87 | 7.1 | 1470 | 15.0 | 46.2 |
| G302 | 08/03/2018 | 0 | 93 | 7.0 | 1465 | 15.2 | 50.4 |
| G302 | 01/23/2019 | 0 | 94 | 7.0 | 1407 | 12.2 | 53 |
| G302 | 08/19/2019 | 0 | 87 | 7.0 | 1505 | 17.0 | 60.1 |
| G302 | 01/23/2020 | 4.10 | 44.7 | 7.1 | 1462 | 9.2 | 258 |
| G302 | 08/11/2020 | 2.30 | 5.6 | 6.9 | 1339 | 20.1 | 11.1 |
| G302 | 01/27/2021 | 2.40 | 63 | 6.6 | 1525 | 9.8 | 5.05 |
| G303 | 11/20/2015 | 0 | -29 | 6.9 | 2260 | 16.4 | 348 |
| G303 | 02/23/2016 | 0.81 | 121 | 7.0 | 2110 | 11.0 | |
| G303 | 05/20/2016 | 0.61 | -77 | 6.9 | 2270 | 20.2 | 7.6 |
| G303 | 08/15/2016 | 0.07 | -2 | 6.9 | 2480 | 17.9 | 7.8 |
| G303 | 11/17/2016 | 0.20 | -2 | 6.9 | 2260 | 15.0 | 9.8 |
| G303 | 02/19/2017 | 0 | -31 | 6.9 | 2009 | 16.0 | 12.9 |
| G303 | 05/17/2017 | 0 | -26 | 7.1 | 1850 | 15.7 | 13.8 |
| G303 | 07/13/2017 | 0 | 59 | 7.0 | 1870 | 17.4 | 15.7 |
| G303 | 10/26/2017 | 0 | -3 | 7.0 | 2230 | 13.3 | 26.1 |
| G303 | 05/14/2018 | 0 | -1 | 7.0 | 2200 | 13.4 | 7.5 |
| G303 | 08/03/2018 | 0 | -60 | 7.0 | 1877 | 15.3 | 44.1 |
| G303 | 01/23/2019 | 0 | -69 | 7.0 | 1869 | 11.5 | 30.1 |
| G303 | 08/19/2019 | 0 | -59 | 7.0 | 1903 | 17.3 | 39.7 |
| G303 | 01/23/2020 | 2.30 | 33.8 | 7.0 | 2102 | 9.4 | 3.71 |
| G303 | 08/11/2020 | 1.50 | -69.9 | 6.9 | 2254 | 19.9 | 95.6 |
| G303 | 01/26/2021 | 0.48 | 55.5 | 6.8 | 2205 | 8.9 | 1.2 |
| G304 | 11/20/2015 | 0 | 19 | 7.1 | 1970 | 16.8 | 209 |
| G304 | 02/23/2016 | 0 | 132 | 7.1 | 1960 | 12.1 | 14 |
| G304 | 05/20/2016 | 0 | 15 | 7.1 | 1990 | 18.6 | 50 |
| G305 | 05/19/2016 | 0 | -29 | 7.1 | 1990 | 18.1 | 832 |
| G305 | 07/01/2016 | 0 | 108 | 7.2 | 1960 | 24.4 | 0 |
| G305 | 08/16/2016 | 0 | 161 | 7.3 | 2060 | 19.6 | 2.3 |
| G305 | 09/29/2016 | 0 | 27 | 6.9 | 2000 | 18.5 | 0 |
| G305 | 11/17/2016 | 0 | 169 | 7.1 | 1830 | 14.4 | 3.8 |
| G306 | 05/19/2016 | 0 | -21 | 6.7 | 1250 | 16.6 | 1000 |
| G306 | 07/01/2016 | 0 | 139 | 6.5 | 1230 | 20.8 | |
| G306 | 08/16/2016 | 0 | 225 | 6.9 | 1250 | 17.6 | 4 |
| G306 | 09/29/2016 | 0 | 178 | 6.6 | 1230 | 18.1 | |
| G306 | 11/16/2016 | 0 | 205 | 7.0 | 1144 | 13.7 | 1.3 |
| G306 | 02/19/2017 | 0 | 122 | 7.0 | 1290 | 14.8 | 74 |
| G306 | 05/17/2017 | 0 | 109 | 7.1 | 1190 | 15.8 | 66.9 |
| G306 | 07/13/2017 | 0 | 122 | 7.0 | 1017 | 17.3 | 12.2 |
| G306 | 10/27/2017 | 0 | 210 | 6.9 | 1210 | 13.9 | 4.2 |
| G306 | 05/14/2018 | 0 | 200 | 6.9 | 1140 | 15.6 | 0.3 |
| G306 | 08/03/2018 | 0 | 92 | 7.0 | 1205 | 15.1 | 27.4 |
| G306 | 01/23/2019 | 0 | 95 | 7.0 | 1032 | 11.2 | 33 |



ASH POND NO. 1 COFFEEN, ILLINOIS

| Sample Location | Sample Date | Dissolved Oxygen (mg/L) | Oxidation Reduction Potential (mV) | pH (field) (SU) | Specific Conductance (micromhos/cm) | Temperature (deg. C) | Turbidity (NTU) |
|--------------------|----------------|----------------------------|---------------------------------------|--------------------|-------------------------------------|-------------------------|--------------------|
| G306 | 08/19/2019 | 0 | 99 | 7.0 | 1178 | 16.8 | 33.1 |
| G306 | 01/21/2020 | 5.50 | 212 | 7.0 | 1079 | 9.9 | 835 |
| G306 | 08/11/2020 | 0.90 | 132 | 6.9 | 1173 | 18.7 | 1.3 |
| G306 | 01/26/2021 | 2.80 | 115 | 6.8 | 1012 | 10.4 | 0 |
| G306 | 03/29/2021 | 4.70 | 227 | 6.7 | 1097 | 14.5 | 59.3 |
| G306 | 04/21/2021 | 3.00 | 102 | 6.8 | 1053 | 12.5 | 8.96 |
| G306 | 05/05/2021 | 2.00 | 132 | 6.8 | 1053 | 14.7 | 25.6 |
| G306 | 05/18/2021 | 1.40 | 149 | 6.9 | 1102 | 14.0 | 21.6 |
| G306 | 06/15/2021 | 1.10 | 156 | 6.8 | 1087 | 17.0 | 29.3 |
| G306 | 06/28/2021 | 1.90 | 149 | 7.0 | 1148 | 23.4 | 9.97 |
| G306 | 07/14/2021 | 1.20 | 134 | 6.8 | 1065 | 18.6 | 17.5 |
| G306 | 07/27/2021 | 1.00 | 114 | 6.8 | 1002 | 19.6 | 2.78 |
| G307 | 08/16/2016 | 0 | 167 | 7.0 | 2010 | 19.0 | |
| G307 | 09/29/2016 | 0 | -7 | 6.9 | 1950 | 18.8 | |
| G307 | 11/16/2016 | 0 | 174 | 6.9 | 2130 | 15.8 | |
| G307 | 02/19/2017 | 0 | 162 | 7.0 | 2305 | 16.5 | 7.9 |
| G307 | 05/17/2017 | 0 | 140 | 7.2 | 2540 | 15.7 | 6.6 |
| G307 | 07/13/2017 | 0 | 170 | 7.0 | 1940 | 17.9 | 9.2 |
| G307 | 10/27/2017 | 0 | 175 | 7.0 | 2050 | 13.4 | 0 |
| G307 | 05/14/2018 | 0 | 105 | 7.0 | 1850 | 16.0 | 9.4 |
| G307 | 08/03/2018 | 0 | 161 | 7.0 | 1460 | 16.1 | 92.6 |
| G307 | 08/19/2019 | 0 | 155 | 7.0 | 1495 | 17.1 | 1000 |
| G307 | 02/26/2020 | 0.50 | 128 | 7.0 | 1885 | 10.4 | 45.2 |
| G307 | 05/06/2020 | 1.00 | 87.6 | 7.3 | 1914 | 14.4 | 18 |
| G307 | 08/11/2020 | 0.70 | 50.1 | 7.3 | 1828 | 19.0 | 0.41 |
| G307 | 01/27/2021 | 0.83 | 65.7 | 7.4 | 1711 | 5.7 | 0.59 |
| G307D | 03/29/2021 | 1.20 | 186 | 7.3 | 1958 | 14.4 | 16.4 |
| G307D | 04/21/2021 | 1.20 | -15.1 | 7.2 | 1856 | 14.0 | 16.7 |
| G307D | 05/04/2021 | 2.70 | -2.9 | 7.3 | 1739 | 14.0 | 19.7 |
| G307D | 05/18/2021 | 0.17 | -50.3 | 7.3 | 1840 | 15.3 | 10.2 |
| G307D | 07/27/2021 | 2.20 | -62.4 | 7.2 | 1554 | 24.1 | 2.37 |
| G308 | 03/29/2021 | 0.63 | 213 | 7.3 | 2389 | 13.5 | 15.5 |
| G308 | 04/21/2021 | 0.87 | 32.1 | 7.2 | 2221 | 11.6 | 0.99 |
| G308 | 05/05/2021 | 0.51 | 103 | 7.2 | 2131 | 13.6 | 0 |
| G308 | 05/17/2021 | 0.47 | 42.7 | 7.2 | 2258 | 13.9 | 0 |
| G308 | 06/14/2021 | 0.25 | -8.3 | 7.2 | 2207 | 19.0 | 0.72 |
| G308 | 06/28/2021 | 0.36 | 26.1 | 7.2 | 9092 | 20.3 | 0.8 |
| G308 | 07/14/2021 | 0.40 | 118 | 7.3 | 2092 | 17.3 | 0.06 |
| G308 | 07/27/2021 | 0.30 | 37.2 | 7.3 | 1141 | 22.6 | 1.14 |
| G309 | 03/29/2021 | 0.71 | 206 | 7.2 | 1709 | 14.8 | 84.3 |
| G309 | 04/21/2021 | 1.10 | 61.7 | 7.2 | 1582 | 13.8 | 10.9 |
| G309 | 05/05/2021 | 1.00 | 93.6 | 7.2 | 1770 | 14.7 | 19.4 |
| G309 | 05/17/2021 | 0.36 | 26.6 | 7.3 | 1664 | 16.0 | 28.8 |
| G309 | 06/14/2021 | 0.51 | -28.6 | 7.2 | 1371 | 21.2 | 2.4 |
| G309 | 06/28/2021 | 0.49 | -48.6 | 7.3 | 1491 | 21.4 | 1.11 |
| G309 | 07/13/2021 | 0.80 | -35.9 | 7.4 | 1565 | 16.5 | 21.7 |



ASH POND NO. 1 COFFEEN, ILLINOIS

| Sample Location | Sample Date | Dissolved Oxygen (mg/L) | Oxidation Reduction Potential (mV) | pH (field) (SU) | Specific Conductance (micromhos/cm) | Temperature (deg. C) | Turbidity (NTU) |
|--------------------|----------------|----------------------------|---------------------------------------|--------------------|-------------------------------------|-------------------------|--------------------|
| G309 | 07/27/2021 | 0.44 | -55.2 | 7.3 | 1729 | 20.0 | 2.22 |
| G310 | 03/29/2021 | 0.84 | 214 | 7.1 | 1800 | 14.0 | 4.55 |
| G310 | 04/22/2021 | 0.40 | 102 | 7.0 | 1889 | 13.2 | 1.22 |
| G310 | 05/04/2021 | 0.79 | 153 | 7.2 | 1952 | 12.9 | 0.47 |
| G310 | 05/19/2021 | 0.29 | 100 | 7.2 | 1934 | 14.9 | 1.22 |
| G310 | 06/15/2021 | 0.25 | 181 | 7.2 | 1930 | 15.8 | 2.67 |
| G310 | 06/28/2021 | 0.37 | 44.5 | 7.1 | 1853 | 17.3 | 0.61 |
| G310 | 07/13/2021 | 0.36 | 65.5 | 7.2 | 1929 | 18.8 | 0.74 |
| G310 | 07/28/2021 | 0.35 | 51.3 | 7.2 | 1970 | 18.9 | 0.13 |
| G311 | 03/30/2021 | 1.30 | 330 | 6.7 | 1854 | 13.3 | 54.4 |
| G311 | 04/22/2021 | 0.78 | 208 | 6.8 | 1986 | 13.1 | 21.1 |
| G311 | 05/04/2021 | 0.60 | 165 | 7.0 | 2052 | 13.2 | 54.9 |
| G311 | 05/19/2021 | 0.31 | 101 | 6.9 | 2039 | 15.7 | 47.2 |
| G311 | 06/15/2021 | 0.24 | 91.6 | 6.9 | 2040 | 17.8 | 42.8 |
| G311 | 06/29/2021 | 1.00 | 91.5 | 7.0 | 1558 | 21.4 | 34.3 |
| G311 | 07/14/2021 | 0.60 | 204 | 6.9 | 2037 | 15.8 | 4.13 |
| G311 | 07/27/2021 | 2.80 | 33 | 7.1 | 2117 | 19.9 | 41.5 |
| G311D | 03/30/2021 | 3.40 | 65.8 | 7.1 | 883 | 17.8 | 56.9 |
| G311D | 04/22/2021 | 3.40 | 106 | 7.0 | 897.6 | 15.0 | 3.2 |
| G311D | 05/04/2021 | 2.30 | 101 | 7.2 | 953.1 | 14.8 | 8.15 |
| G311D | 05/19/2021 | 2.70 | -52.9 | 7.2 | 979 | 17.0 | 0.93 |
| G311D | 07/28/2021 | 1.60 | -170 | 7.2 | 1080 | 19.6 | 1.28 |
| G312 | 03/30/2021 | 2.40 | 421 | 6.5 | 1471 | 12.4 | 0.12 |
| G312 | 04/22/2021 | 0.78 | 114 | 6.4 | 1645 | 13.0 | 3.42 |
| G312 | 05/04/2021 | 1.00 | 136 | 6.5 | 1788 | 13.0 | 6.97 |
| G312 | 05/19/2021 | 0.31 | 142 | 6.4 | 1725 | 15.8 | 1.15 |
| G312 | 06/15/2021 | 0.29 | 130 | 6.5 | 1761 | 17.2 | 3.63 |
| G312 | 06/29/2021 | 1.60 | 138 | 6.5 | 1954 | 21.2 | 3.39 |
| G312 | 07/13/2021 | 0.61 | 112 | 6.3 | 1460 | 19.5 | 3.39 |
| G312 | 07/27/2021 | 0.42 | 85.5 | 6.5 | 1846 | 18.2 | 0 |
| G313 | 03/30/2021 | 0.64 | 243 | 6.9 | 2611 | 12.8 | 58 |
| G313 | 04/22/2021 | 0.74 | 97.7 | 6.8 | 1558 | 12.1 | 14.3 |
| G313 | 05/04/2021 | 0.16 | 81.4 | 7.0 | 2115 | 13.3 | 48.9 |
| G313 | 05/18/2021 | 0.29 | 38.5 | 7.0 | 2132 | 15.2 | 28.1 |
| G313 | 06/14/2021 | 0.22 | 17.7 | 7.1 | 2132 | 20.7 | 27 |
| G313 | 06/28/2021 | 1.10 | 46.3 | 7.0 | 2104 | 23.9 | 6.74 |
| G313 | 07/13/2021 | 0.40 | 17.8 | 6.9 | 2099 | 21.7 | 5.27 |
| G313 | 07/27/2021 | 0.30 | 13.8 | 6.9 | 1605 | 22.4 | 1.16 |
| G314 | 03/30/2021 | 3.40 | 177 | 6.8 | 3921 | 14.0 | 19.4 |
| G314 | 04/21/2021 | 0.95 | 96.8 | 6.6 | 3977 | 11.7 | 1.58 |
| G314 | 05/04/2021 | 4.70 | 82.1 | 7.1 | 3303 | 14.9 | 21.1 |
| G314 | 05/17/2021 | 0.32 | 64.9 | 6.6 | 3877 | 14.7 | 0.75 |
| G314 | 06/14/2021 | 0.46 | 41.1 | 6.6 | 3551 | 17.6 | 6.91 |
| G314 | 06/28/2021 | 0.90 | -14 | 6.6 | 3553 | 20.1 | 42.1 |
| G314 | 07/13/2021 | 1.70 | -17.9 | 6.7 | 4012 | 16.9 | 1.36 |
| G314 | 07/27/2021 | 0.34 | -39.1 | 6.6 | 4091 | 20.0 | 0.36 |



TABLE 4-2. GROUNDWATER FIELD PARAMETERS

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Sample Location | Sample Date | Dissolved Oxygen (mg/L) | Oxidation Reduction Potential (mV) | pH (field) (SU) | Specific Conductance (micromhos/cm) | Temperature (deg. C) | Turbidity (NTU) |
|--------------------|----------------|----------------------------|---------------------------------------|--------------------|--|-------------------------|--------------------|
| G314D | 03/30/2021 | 0.60 | -21.8 | 7.3 | 3751 | 15.9 | 15.9 |
| G314D | 04/21/2021 | 0.76 | 62.7 | 7.2 | 3428 | 13.0 | 12.1 |
| G314D | 05/04/2021 | 0.89 | 77.7 | 7.2 | 3110 | 14.4 | 1.52 |
| G314D | 05/19/2021 | 0.90 | 130 | 7.2 | 2761 | 15.4 | 42.4 |
| G314D | 07/28/2021 | 5.40 | 94.8 | 7.2 | 2522 | 20.8 | 1.74 |
| G315 | 03/30/2021 | 0.92 | 192 | 6.9 | 2014 | 13.9 | 6.47 |
| G315 | 04/22/2021 | 1.40 | 108 | 6.8 | 1682 | 12.7 | 2.66 |
| G315 | 05/05/2021 | 0.59 | 157 | 6.8 | 1940 | 14.7 | 0.03 |
| G315 | 05/18/2021 | 0.36 | 156 | 6.9 | 1936 | 14.1 | 1.56 |
| G315 | 06/15/2021 | 0.20 | 135 | 6.9 | 1926 | 17.6 | 3.33 |
| G315 | 06/29/2021 | 2.60 | 162 | 7.0 | 1933 | 19.8 | 5.01 |
| G315 | 07/14/2021 | 0.35 | 18.8 | 6.8 | 1898 | 17.6 | 20.5 |
| G315 | 07/28/2021 | 0.25 | 45.1 | 6.7 | 1881 | 17.8 | 0.24 |
| G316 | 03/30/2021 | 0.36 | -81.7 | 7.0 | 2351 | 11.5 | 28.9 |
| G316 | 04/22/2021 | 0.63 | -80.3 | 7.0 | 1626 | 10.6 | 11.8 |
| G316 | 05/05/2021 | 0.37 | -71.1 | 6.9 | 2170 | 12.5 | 2.01 |
| G316 | 05/17/2021 | 0.26 | -99.4 | 7.1 | 2202 | 14.4 | 2 |
| G316 | 06/14/2021 | 0.21 | -107 | 7.1 | 2171 | 17.7 | 8.05 |
| G316 | 06/28/2021 | 0.80 | -112 | 7.1 | 1790 | 18.0 | 27.7 |
| G316 | 07/13/2021 | 0.56 | -108 | 7.0 | 2208 | 19.6 | 4.92 |
| G316 | 07/27/2021 | 0.27 | -114 | 7.0 | 1987 | 18.6 | 1.11 |
| G317 | 03/30/2021 | 4.70 | 94.2 | 6.5 | 1981 | 14.4 | 1.09 |
| G317 | 04/22/2021 | 3.60 | 114 | 6.5 | 2011 | 13.3 | 0.26 |
| G317 | 05/05/2021 | 3.50 | 104 | 6.5 | 2280 | 21.0 | 0.16 |
| G317 | 05/18/2021 | 2.80 | 89.7 | 6.6 | 2209 | 15.1 | 1.83 |
| G317 | 06/15/2021 | 4.70 | 103 | 6.6 | 2069 | 17.0 | 6.82 |
| G317 | 06/28/2021 | 5.30 | 180 | 6.7 | 2127 | 17.2 | 10.2 |
| G317 | 07/13/2021 | 5.60 | 116 | 6.6 | 2031 | 17.9 | 134 |
| G317 | 07/28/2021 | 6.70 | 150 | 6.5 | 1616 | 16.4 | 9.41 |

Notes:

Field readings are reported with as many significant figures as provided by analytical laboratory. -- = data not available

cm = centimeter

deg. C = degrees Celsius mg/L = milligrams per liter mV = millivolts

NTU = nephelometric turbidity units

SU = standard units

generated 10/22/2021, 11:51:40 AM CDT



5 of 5

FIGURES

PART 845 REGULATED UNIT (SUBJECT UNIT)
PROPERTY BOUNDARY
COFFEEN LAKE STATE FISH AND WILDLIFE AREA

SITE LOCATION MAP

FIGURE 1-1





■ COAL MINE SHAFT

PART 845 REGULATED UNIT (SUBJECT UNIT)

SITE FEATURE

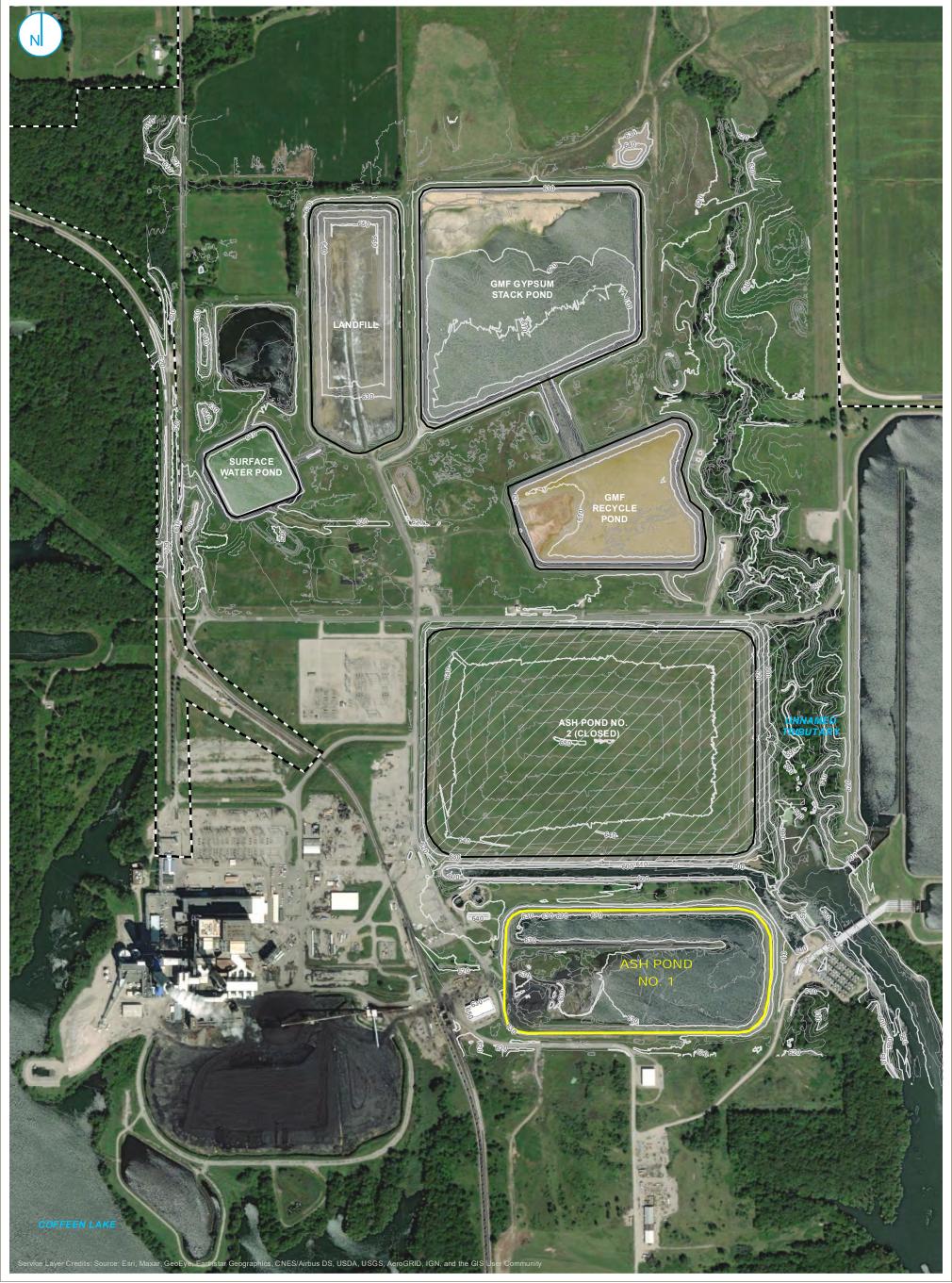
LIMITS OF FINAL COVER

PROPERTY BOUNDARY

SITE MAP

FIGURE 1-2





10-FT ELEVATION CONTOUR 2-FT ELEVATION CONTOUR

PART 845 REGULATED UNIT (SUBJECT UNIT)

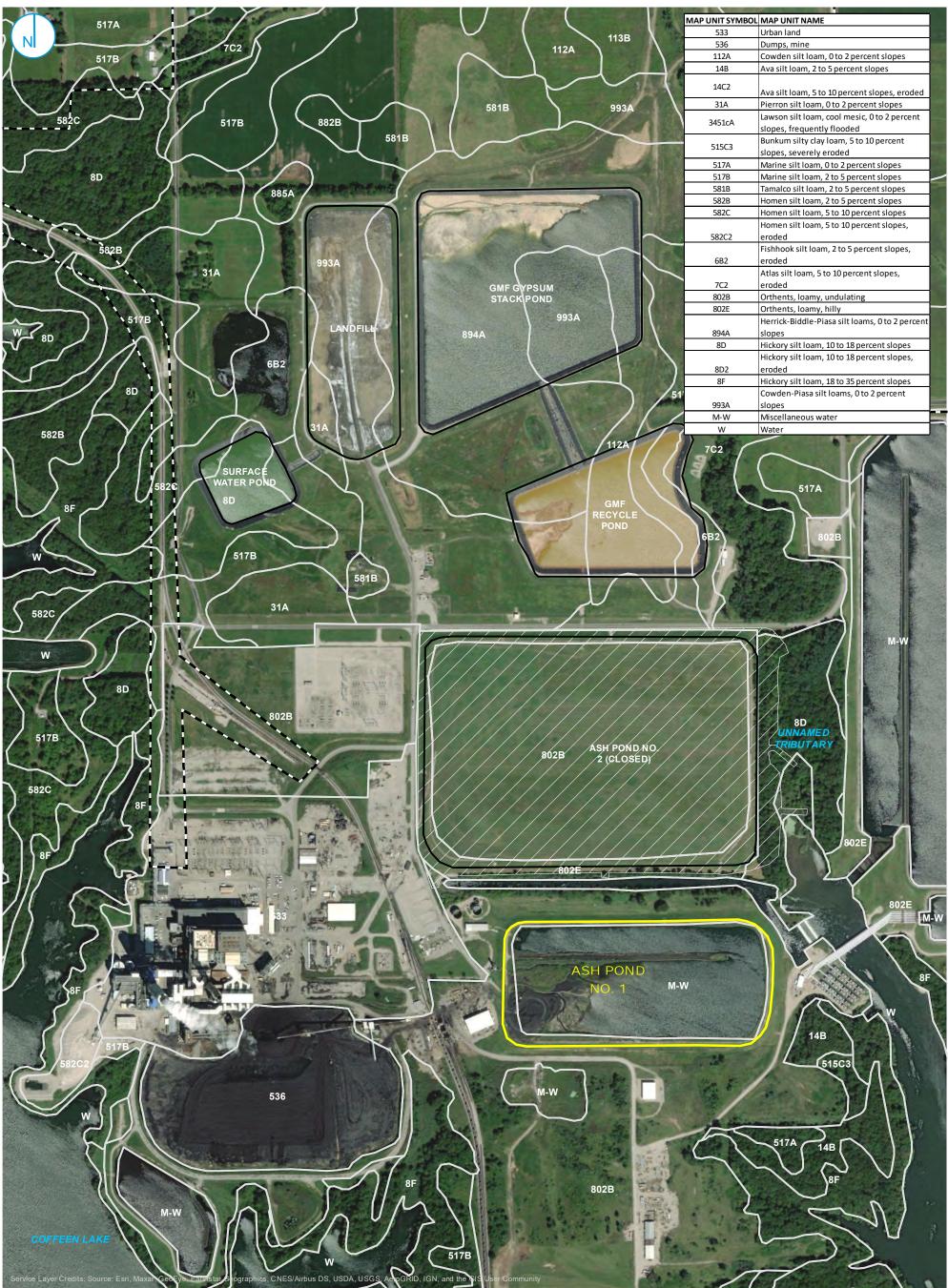
SITE FEATURE
LIMITS OF FINAL COVER
PROPERTY BOUNDARY

NOTE
ELEVATION CONTOURS SHOWN IN FEET, NORTH
AMERICAN VERTICAL DATUM OF 1988

SITE TOPOGRAPHIC MAP

FIGURE 2-1





PART 845 REGULATED UNIT (SUBJECT UNIT)

SITE FEATURE
LIMITS OF FINAL COVER

PROPERTY BOUNDARY

NRCS SOIL SURVEY MAP UNIT BOUNDARY

SOIL SURVEY MAP

FIGURE 2-2



PART 845 REGULATED UNIT (SUBJECT UNIT)

SITE FEATURE

LIMITS OF FINAL COVER

PROPERTY BOUNDARY

CAHOKIA ALLUVIUM (INCLUDES ALLUVIAL FAN FACIES)

HAGARSTOWN MEMBER

VANDALIA TILL MEMBER

WATER

750

1,500

___ Feet

Service Layer Credits: Source: Esri, Maxar, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USSS, AeroGRID, IGN, and the GIS U

ILLINOIS STATE GEOLOGICAL SURVEY (ISGS)

SURFICIAL GEOLOGIC DEPOSITS

RAMBOLL AMERICAS ENGINEERING SOLUTIONS, INC.

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT

ASH POND NO. 1

COFFEEN POWER PLANT
COFFEEN, ILLINOIS

FIGURE 2-3

GENERALIZED STRATIGRAPHIC COLUMN

FIGURE 2-4



GEOLOGICAL SURVEY, BULLETIN 100, CHAMPAIGN, ILLINOIS."

PROJECT: 169000XXXX | DATED: 10/12/2021 | DESIGNER: HOTCALD

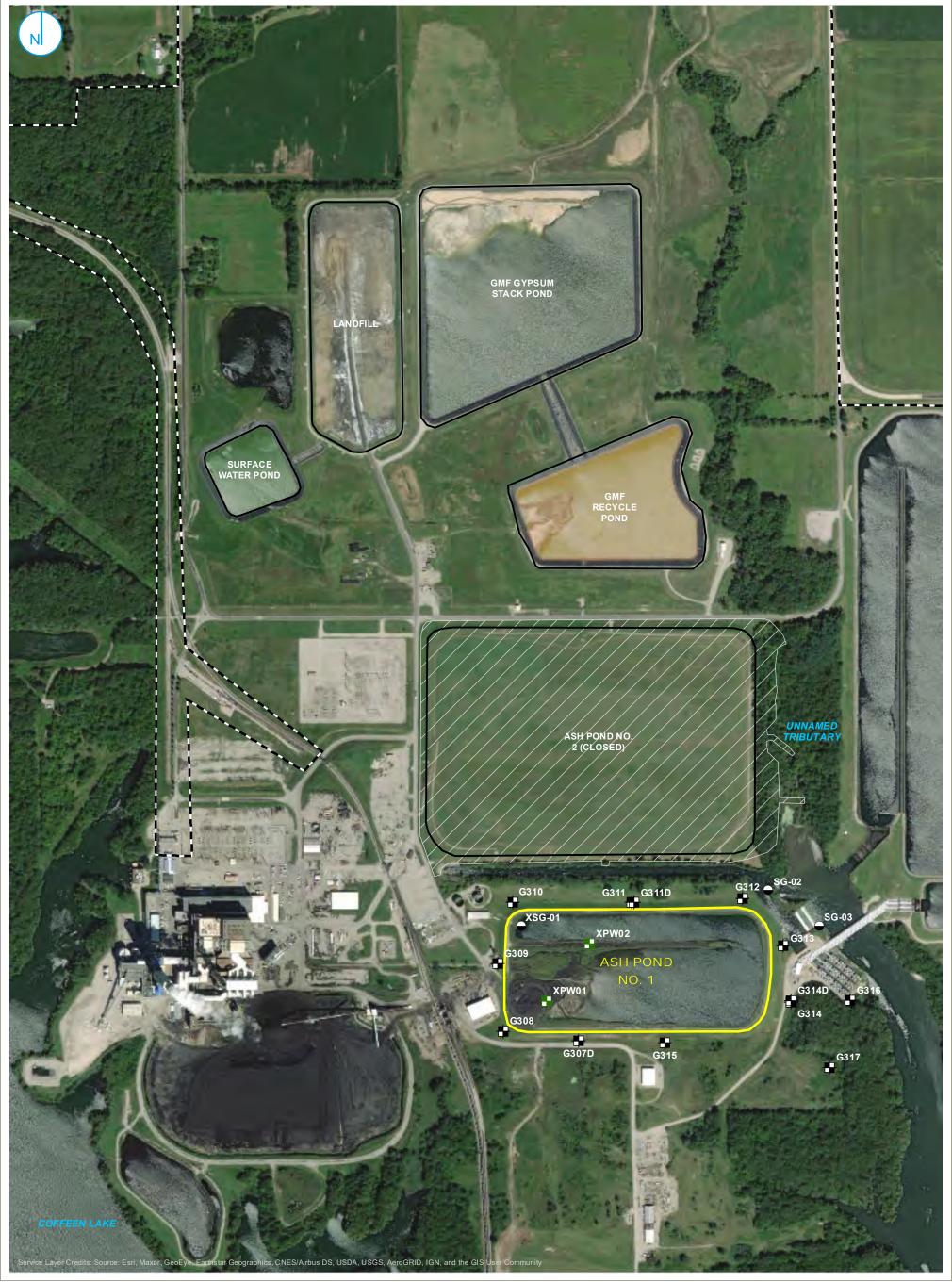
Y:\Mapping\Projects\22\2285\MXD\845_Operating_Permit\Coffeen\AP1\Figure 2-5_Major Structural Features of Illinois AP1.mxd

MAJOR STRUCTURAL FEATURES OF ILLINOIS

FIGURE 2-5

RAMBOLL AMERICAS ENGINEERING SOLUTIONS, INC.

RAMBOLL



MONITORING WELL

SOURCE SAMPLE LOCATION

STAFF GAGE

PART 845 REGULATED UNIT (SUBJECT UNIT)

SITE FEATURE

LIMITS OF FINAL COVER

PROPERTY BOUNDARY

275

550

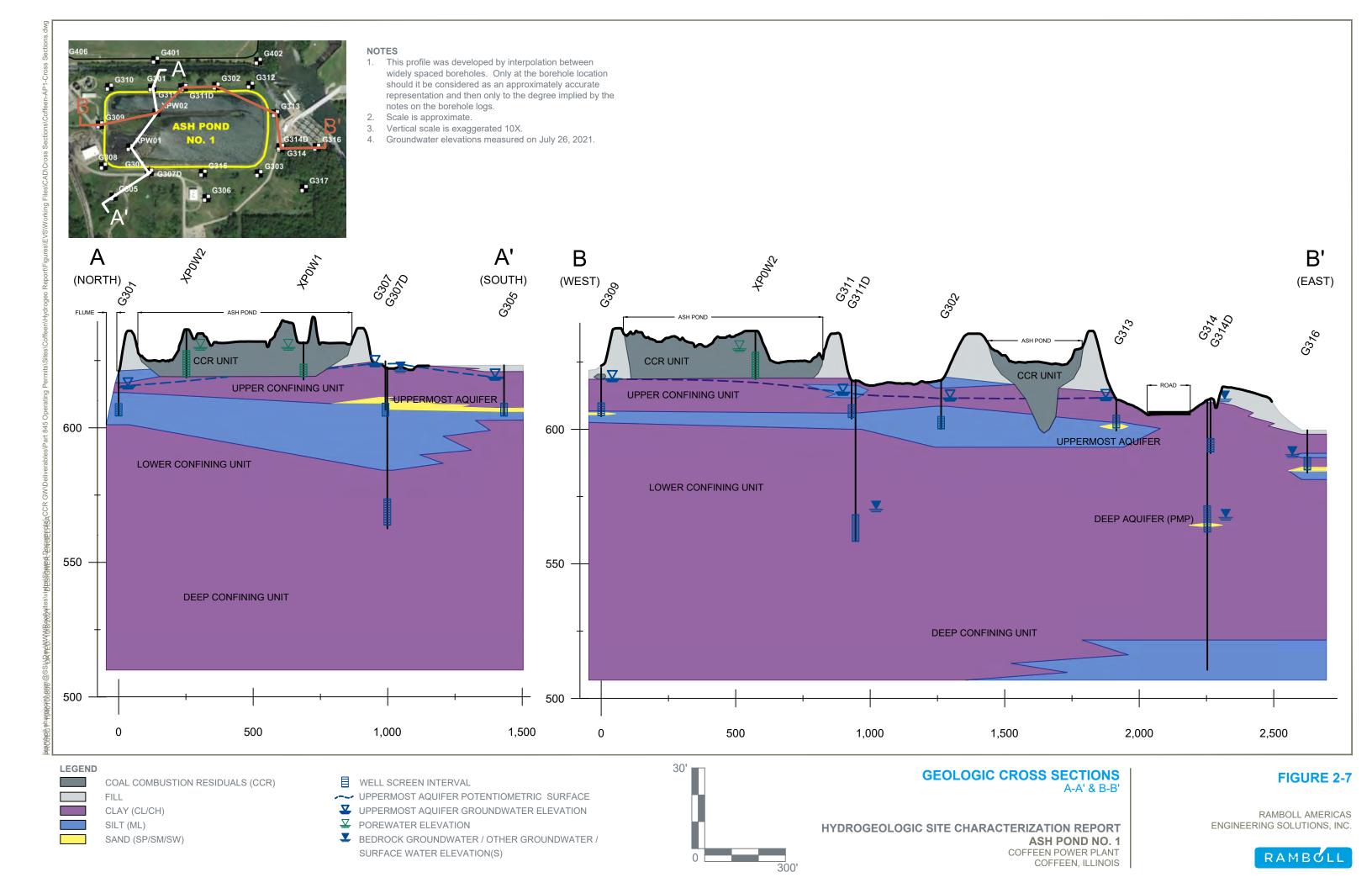
___ Feet

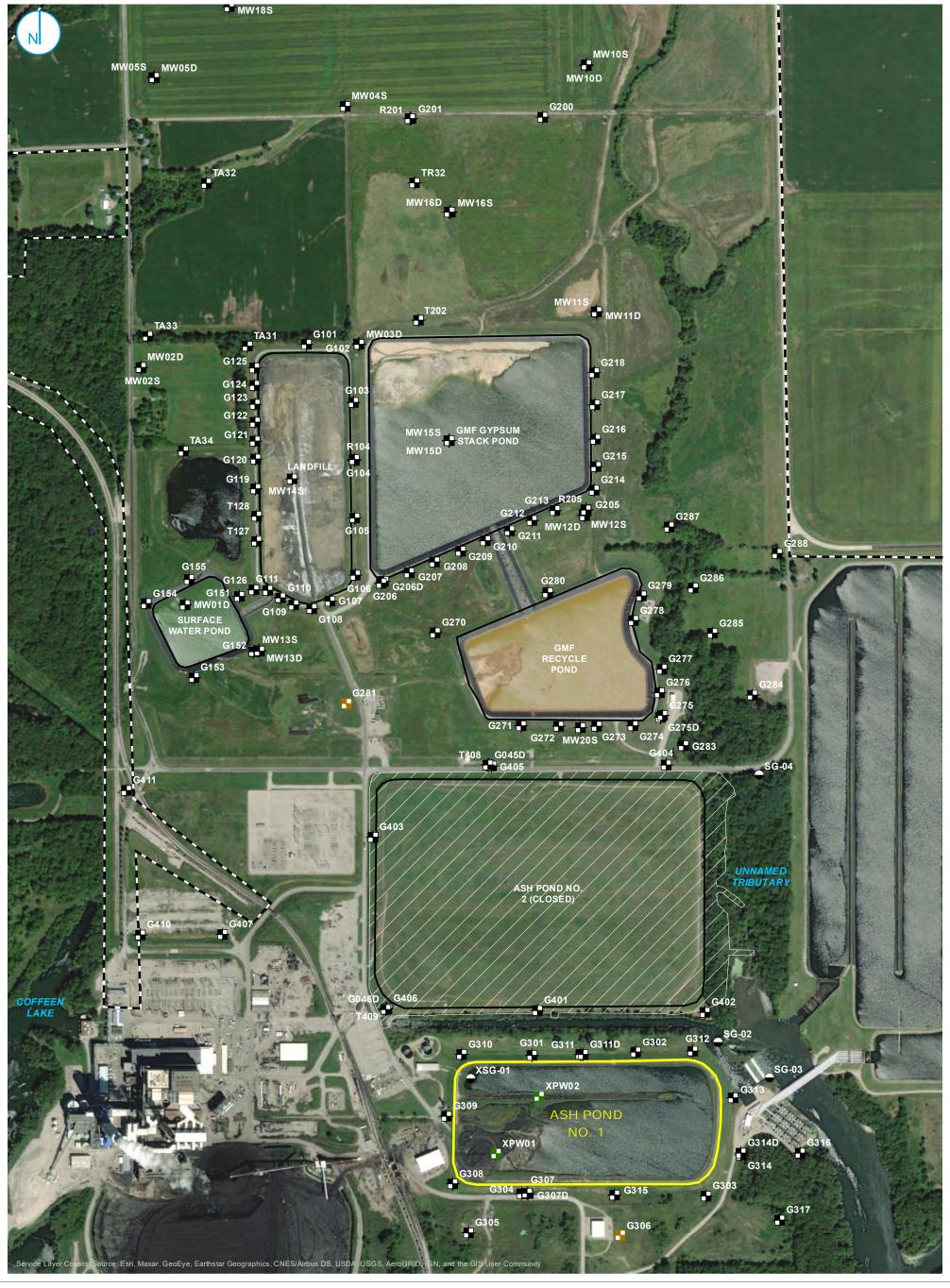
FIELD INVESTIGATION LOCATION MAP

RAMBOLL AMERICAS ENGINEERING SOLUTIONS, INC.

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT ASH POND NO. 1 COFFEEN POWER PLANT COFFEEN, ILLINOIS

FIGURE 2-6





BACKGROUND WELL

MONITORING WELL

SOURCE SAMPLE LOCATION

STAFF GAGE

PART 845 REGULATED UNIT (SUBJECT UNIT)

SITE FEATURE LIMITS OF FINAL COVER

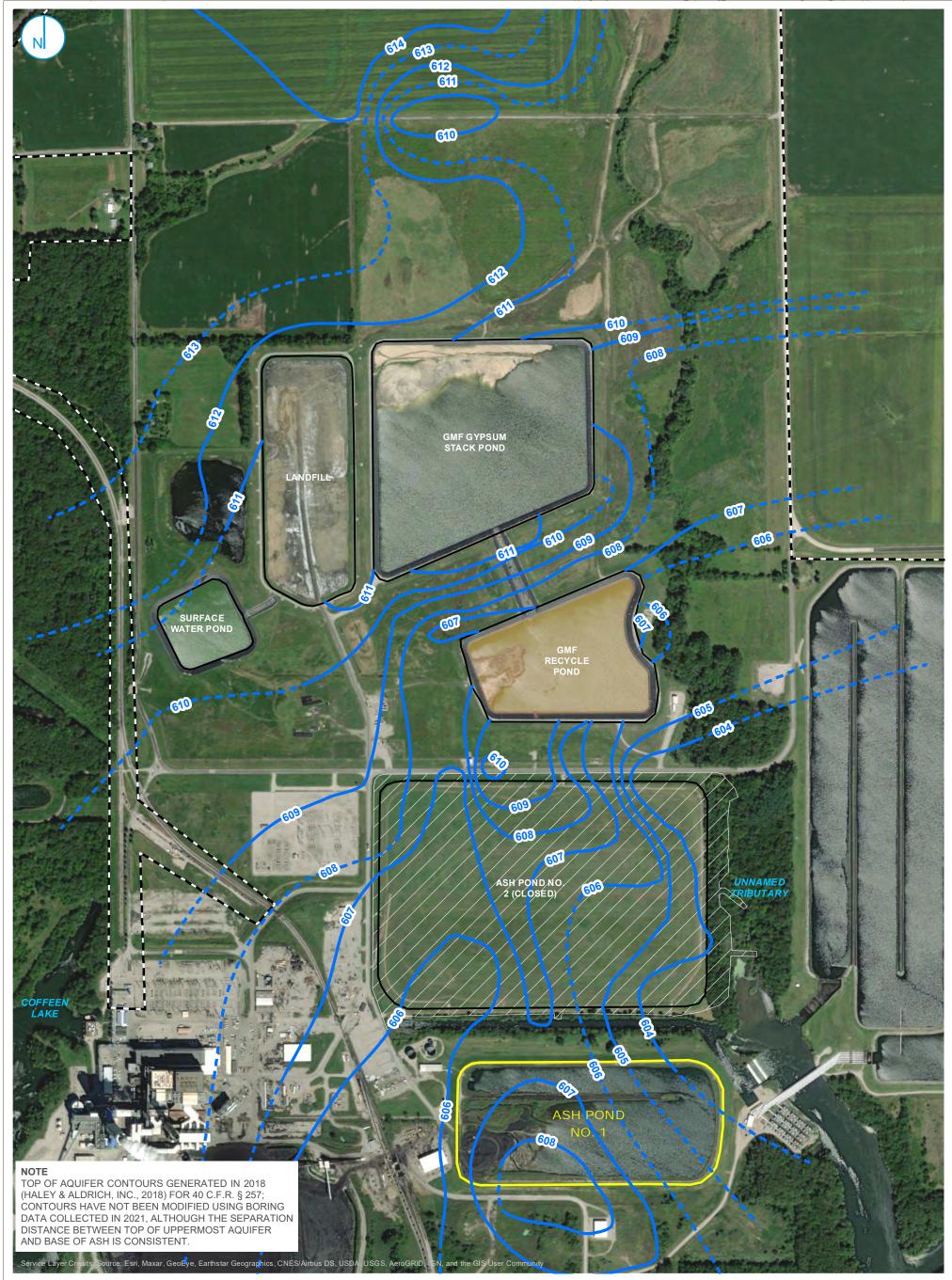
PROPERTY BOUNDARY 550

MONITORING WELL LOCATION MAP

RAMBOLL AMERICAS ENGINEERING SOLUTIONS, INC.

RAMBOLL

FIGURE 3-1



■ HAGARSTOWN MEMBER ELEVATION CONTOUR (1-FT INTERVAL, NAVD88)

■ ■ INFERRED HAGARSTOWN MEMBER ELEVATION CONTOUR

PART 845 REGULATED UNIT (SUBJECT UNIT)

SITE FEATURE

275

LIMITS OF FINAL COVER

550

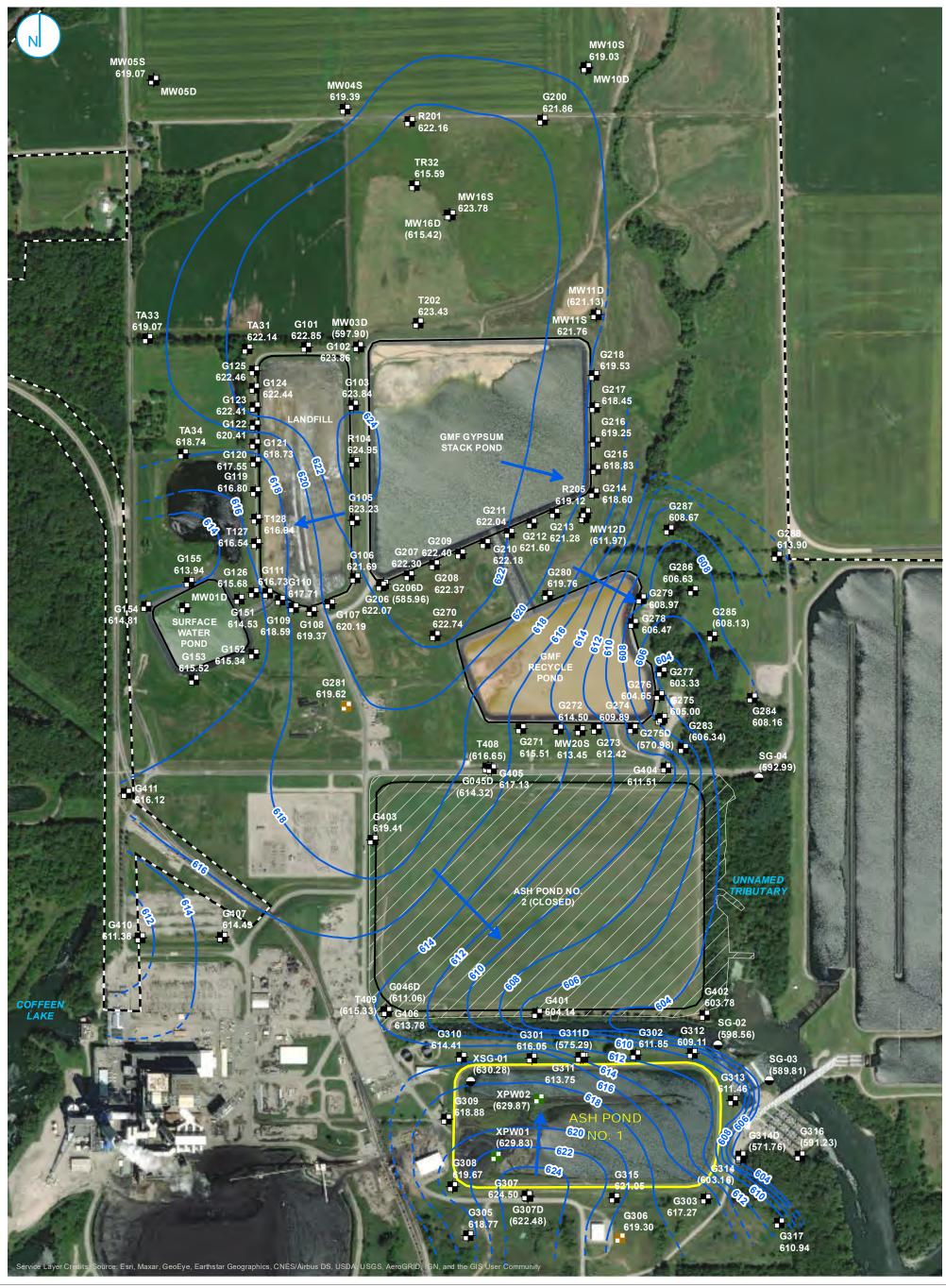
☐ Feet

PROPERTY BOUNDARY

TOP OF UPPERMOST AQUIFER

FIGURE 3-2





BACKGROUND WELL

MONITORING WELL

SOURCE SAMPLE LOCATION

→ STAFF GAGE

GROUNDWATER ELEVATION CONTOUR (2-FT CONTOUR INTERVAL, NAVD88)

INFERRED GROUNDWATER ELEVATION CONTOUR

GROUNDWATER FLOW DIRECTION
0 275 550

PART 845 REGULATED UNIT (SUBJECT UNIT)

SITE FEATURE
LIMITS OF FINAL COVER
PROPERTY BOUNDARY

ELEVATIONS IN PARENTHESES WERE NOT USED

FOR CONTOURING.

UPPERMOST AQUIFER GROUNDWATER ELEVATION CONTOURS APRIL 20, 2021

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT ASH POND NO. 1

ASH POND NO. 1
COFFEEN POWER PLANT
COFFEEN, ILLINOIS

FIGURE 3-3





MONITORING WELL

SOURCE SAMPLE LOCATION

STAFF GAGE

GROUNDWATER ELEVATION CONTOUR (2-FT CONTOUR INTERVAL, NAVD88)

INFERRED GROUNDWATER ELEVATION CONTOUR

GROUNDWATER FLOW DIRECTION 275 550

PART 845 REGULATED UNIT (SUBJECT UNIT)

Esri, Maxar, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AeroGl

FOR CONTOURING.

SITE FEATURE LIMITS OF FINAL COVER PROPERTY BOUNDARY

ELEVATIONS IN PARENTHESES WERE NOT USED

UPPERMOST AQUIFER GROUNDWATER ELEVATION CONTOURS JULY 26, 2021

(622.26)

618.18

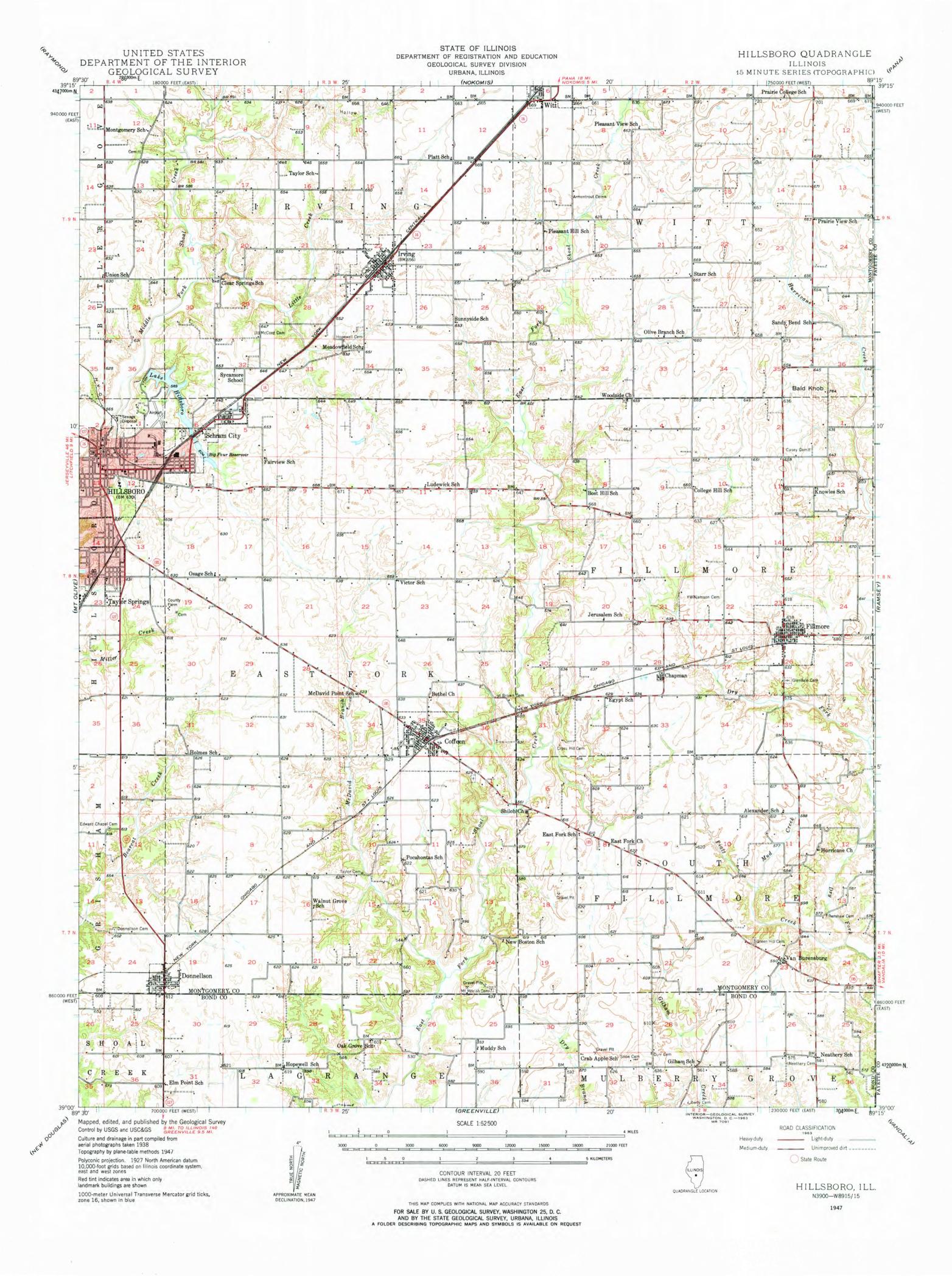
HYDROGEOLOGIC SITE CHARACTERIZATION REPORT ASH POND NO. 1

COFFEEN POWER PLANT COFFEEN, ILLINOIS FIGURE 3-4

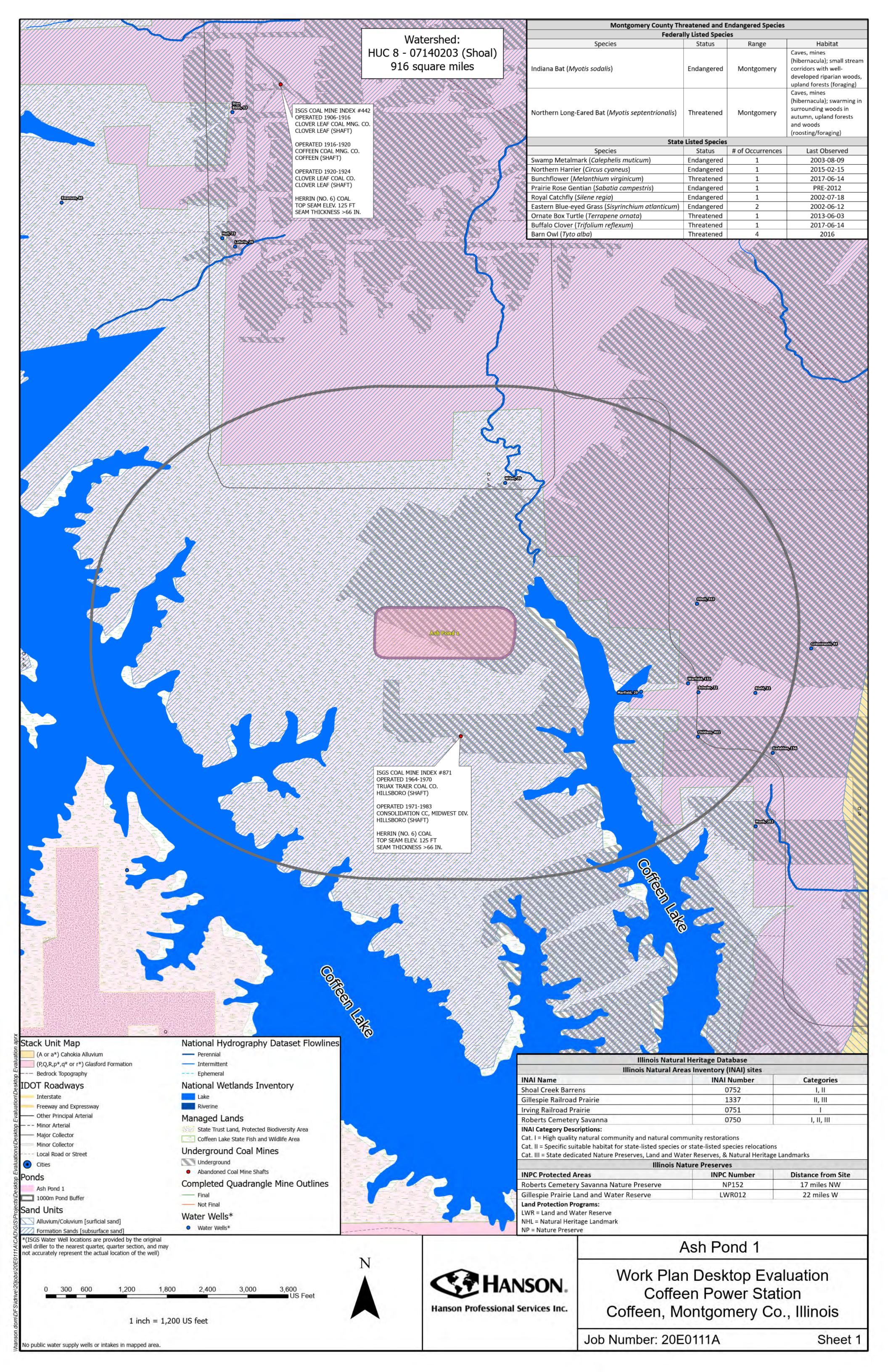


APPENDICES

APPENDIX A HISTORIC TOPOGRAPHIC MAPS



APPENDIX B INFORMATION PERTINENT TO 35 I.A.C. § 845.220(a)(3)





| Private Water Well | Тор | Bottom |
|--|-----|--------|
| clay | 0 | 29 |
| Total Depth | | 29 |
| Casing: 36" CONCRETE from 1' to 29' | | |
| Water from clay at 0' to 0'. | | |
| Ch Javia II | | |
| Owner Address: East St Louis, IL Location source: Location from permit | | |
| nocation source. nocation from permit | | |
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Permit Date: Permit #:

COMPANY Bekemeyer, Gust **FARM** Marfield, Mac

DATE DRILLED September 15, 1970 NO.

ELEVATION 0 COUNTY NO. 01717

LOCATION NE NW NE

LATITUDE 39.055977 **LONGITUDE** -89.386252

COUNTY Montgomery API 121350171700 14 - 7N - 3W

 $_{\mathtt{Page}-1}$ ILLINOIS STATE GEOLOGICAL SURVEY

| Private Water Well | Тор | Bottom |
|--|-----|--------|
| clay | 0 | 25 |
| sand | 25 | 32 |
| Total Depth Casing: 36" CONCRETE from 1' to 32' Size hole below casing: 36" Water from sand at 0' to 0'. | | 32 |
| Driller's Log filed Owner Address: Granite City, IL Location source: Location from permit | | |
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Permit Date: Permit #:

COMPANY Bekemeyer, Gust
FARM Schuler, Paul

DATE DRILLED February 4, 1971 NO.

ELEVATION 0 COUNTY NO. 01726

LOCATION NW NE NE

LATITUDE 39.055952 **LONGITUDE** -89.383929

COUNTY Montgomery API 121350172600 14 - 7N - 3W

 $_{\mathtt{Page}-1}$ ILLINOIS STATE GEOLOGICAL SURVEY

| Private Water Well | Top | Bottom |
|---------------------------------------|-----|--------|
| clay | 0 | 32 |
| Total Depth | | 32 |
| Casing: 30" CONCRETE from 0' to 33' | | |
| Water from clay at 0' to 0'. | | |
| | | |
| Owner Address: Coffeen, IL | | |
| Location source: Location from permit | | |
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Permit Date:

Permit #: 28886

NO.

COMPANY Bekemeyer, Gust
FARM Hueitt, Bill

DATE DRILLED May 5, 1974

ELEVATION 0 COUNTY NO. 21824

LOCATION NE NE NE

LATITUDE 39.055928 **LONGITUDE** -89.381606

COUNTY Montgomery API 121352182400 14 - 7N - 3W

| Private Water Well | Тор | Bottom |
|---------------------------------------|-----|--------|
| clay | 0 | 32 |
| Total Depth | | 32 |
| Casing: 30" CONCRETE from 0' to 33' | | |
| Water from clay at 0' to 0'. | | |
| Owner Address: Coffeen, IL | | |
| Location source: Location from permit | | |
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Permit Date: Permit #: 28887

COMPANY Bekemeyer, Gust
FARM Stahl, Louis

DATE DRILLED May 5, 1974

ELEVATION 0 COUNTY NO. 21825

LOCATION NE NE NE

LATITUDE 39.055928 **LONGITUDE** -89.381606

COUNTY Montgomery API 121352182500 14 - 7N - 3W

NO.

| Private Water Well | Тор | Bottom |
|--|-----|--------|
| tan clay | 0 | 37 |
| gray clay | 37 | 106 |
| limestone | 106 | 110 |
| gray shale | 110 | 136 |
| sandstone | 136 | 151 |
| Total Depth Casing: 5" VALLEY STEEL from -1' to 112' Size hole below casing: 4.75" | | 151 |
| Water from sandstone at 136' to 151'. Static level 47' below casing top which is 1' above GL Pumping level 92' when pumping at 5 gpm for 2 hours | | |
| Driller's Log filed | | |
| Owner Address: R.R. #1 Coffeen, IL | | |
| Location source: Location from permit | | |
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Permit Date: April 28, 1977 **Permit #:** 59626

COMPANY Courson, Richard C.
FARM Warfield, William

DATE DRILLED May 10, 1977 NO. 1

ELEVATION 630GL COUNTY NO. 22214

LOCATION 200'N line, 1100'E line of NE

LATITUDE 39.056309 **LONGITUDE** -89.384343

COUNTY Montgomery API 121352221400 14 - 7N - 3W

| Private Water Well | Top | Bottom |
|--|-----|--------|
| brown top soil | 0 | 1 |
| yellow clay | 1 | 8 |
| yellow clay & sand | 8 | 18 |
| yellow gravel & sand | 18 | 30 |
| yellow sand & gravel | 30 | 39 |
| Total Depth Casing: 36" CONCRETE from -1' to 39' " from 0' to 0' | | 39 |
| Grout: CONCRETE from 0 to 10. Grout: GRAVEL from 10 to 39. | | |
| Size hole below casing: 0" | | |
| Water from at 22' to 39'. Permanent pump installed at 38' on December 1, 1981, with a capacity of 10 gpm | | |
| Owner Address: 109 Laredo Ave. St. Louis, MO Location source: Location from permit | | |
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COMPANY Kohnen, Clarence **FARM** Wibel, William

DATE DRILLED November 30, 1981 NO.

ELEVATION 0 COUNTY NO. 22832

LOCATION 115'S line, 102'W line of SE SE NW **LATITUDE** 39.064493 **LONGITUDE** -89.391801

COUNTY Montgomery API 121352283200 11 - 7N - 3W

 $_{\mathtt{Page}-1}$ ILLINOIS STATE GEOLOGICAL SURVEY

| Private Water Well | Тор | Bottom |
|--|-----|--------|
| brown sandy clay | 0 | 7 |
| orangish brown clay sandy & pebble hard | 7 | 9 |
| brown clay very sandy & pebble hard | 9 | 40 |
| gray clay very sandy & pebble hard | 40 | 43 |
| greenish gray clay tacky | 43 | 50 |
| brn sandy clay pebble hard & cobblestone | 50 | 72 |
| gray clay sandy pebble hard | 72 | 85 |
| brown clay tacky stiff | 85 | 101 |
| grn-gry shale w/f strk dk red/brn rock | 101 | 107 |
| gray shale sandy (H) | 107 | 115 |
| gray sandstone clean tight | 115 | 117 |
| gray shale very sandy | 117 | 135 |
| gray sandstone clean cemented (H) | 135 | 157 |
| gray shale sticky | 157 | 177 |
| gray shale very soft (cavey) | 177 | 180 |
| gray shale sticky little sandy | 180 | 187 |
| lime gray & dull gray (H-M) | 187 | 196 |
| gray & black shale sandy firm | 196 | 201 |
| gray shale sandy & sticky | 201 | 263 |
| gray & dk gry shale w/f pieces brn lime | 263 | 274 |
| gray & lt gray shale & sticky | 274 | 288 |
| gray sandstone loose (dirty) | 288 | 290 |
| gray sandstone w/streak of gry sandstone | 290 | 297 |
| gray sandstone clean loose semi loose | 297 | 301 |

COMPANY Kohnen, Clarence

FARM O'Dell, Kenneth & Chong

DATE DRILLED August 6, 1996 NO.

ELEVATION 0 COUNTY NO. 23802

LOCATION NW SE SE

LATITUDE 39.05958 **LONGITUDE** -89.383966

COUNTY Montgomery API 121352380200 11 - 7N - 3W

ILLINOIS STATE GEOLOGICAL SURVEY Page 2

| ray shale very sandy | 301 | 307 |
|--|-----|-----|
| ray sandstone clean loose fine cuttings | 307 | 315 |
| ray sandstone w/streak of gray shale | 315 | 317 |
| ray sandstone clean semi loose | 317 | 325 |
| ray sandstone clean loose water bearing | 325 | 363 |
| Cotal Depth Casing: 6" PVC SDR 21 from 0' to 116' 4.5" PVC SDR 17 from 102' to 362' 4.5" SLOTTED @ 321'-322'& from 342' to 362' Grout: BENTONITE SLRY from 0 to 116. | | 363 |
| Vater from light gray sandstone at 322' to 362'. Static level 300' below casing top which is 1' above GI Cumping level 362' when pumping at 15 gpm for 0 hours | | |
| Remarks: TDS 800, shale trap @ 116'-302'-322'-330' Owner Address: 169 O'Dell Lane Coffeen, IL Accation source: Location from permit | | |

Kohnen, Clarence

O'Dell, Kenneth & Chor

COUNTY Montgomery API 121352380200 11 - 7N - 3W

 $_{\mathtt{Page}-1}$ ILLINOIS STATE GEOLOGICAL SURVEY

| Private Water Well | Top | Bottom |
|---|-----|--------|
| brown clay firm sticky | 0 | 15 |
| brown clay sandy & pebble firm | 15 | 27 |
| brn gvl coarse clean loose water bearing | 27 | 29 |
| gray clay hard sandy & pebble | 29 | 65 |
| greenish brown clay sandy firm | 65 | 82 |
| brown shale very sandy S-M | 82 | 84 |
| gray-brown sandstone clean-dirty | 84 | 93 |
| brown shale soft & sandy | 93 | 99 |
| gray & brown shale in layers soft | 99 | 123 |
| gry brn sandstone loose clean wtr bearin | 123 | 153 |
| gray shale sandy | 153 | 178 |
| dark gray shale | 178 | 197 |
| gray & dull gray & dark gray lime | 197 | 204 |
| dark gray & black shale | 204 | 208 |
| gray shale | 208 | 218 |
| coal | 218 | 219 |
| <pre>lt gray shale w/pieces brown lime & coal</pre> | 219 | 240 |
| shale & gray sandstone in fine sheets | 240 | 250 |
| gray shale sandy & sticky | 250 | 257 |
| gry sandy & sticky shale w/strk brn lime | 257 | 262 |
| dark gray & black shale sticky | 262 | 267 |
| gry-lt gry shale sticky w/fine strk lime | 267 | 281 |
| gray sandstone clean semi loose | 281 | 300 |
| gray shale sticky (M) chips | 300 | 302 |
| | | |

Permit Date: May 15, 1996 Permit #:

COMPANY Kohnen, Clarence **FARM** Childers, Joe

DATE DRILLED August 5, 1996 NO.

ELEVATION 0 COUNTY NO. 23803

LOCATION SW NE NE

LATITUDE 39.054141 **LONGITUDE** -89.383921

COUNTY Montgomery API 121352380300 14 - 7N - 3W

ILLINOIS STATE GEOLOGICAL SURVEY Page 2

| rage 2 | | |
|---|-----|-----|
| | | |
| gray sandstone loose clean | 302 | 306 |
| gray sandy shale chips & sticky chips | 306 | 324 |
| gray sandstone loose clean w/pieces lime | 324 | 398 |
| off white lime H & tan soft | 398 | 399 |
| dark gray shale sticky chips | 399 | 401 |
| Total Depth Casing: 6" PVC SDR 21 from -1' to 86' 4.5" PV SDR 17 from 41' to 401' 4.5" SLOTTED from 361' to 401' | | 401 |
| Grout: BENTONITE SLRY from 0 to 86. | | |
| Water from gry-lt gry sandstone at 341' to 398'. Static level 295' below casing top which is 0' above G Pumping level 401' when pumping at 10 gpm for 0 hours | L | |
| Remarks: TDS 550, shale trap @ 86' & 341' & 339' | | |
| Owner Address: 261 Lvndale Northlake, IL Add'l loc. info: Subdivision: Holtz Claw | | |
| Location source: Location from permit | | |
| | | |
| | | |
| | | |
| | | |
| | | |
| | | |
| | | |

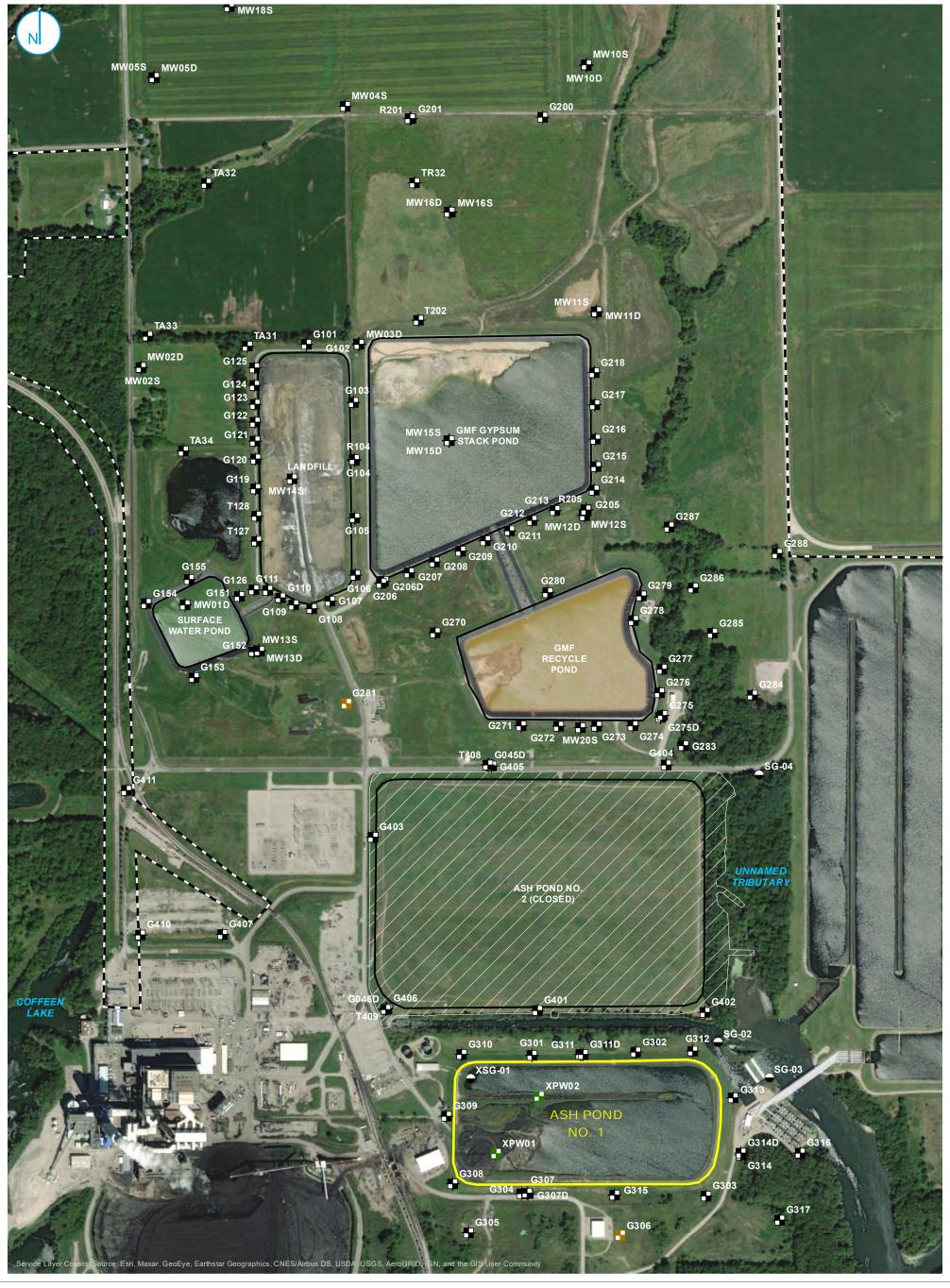
Kohnen, Clarence

Childers, Jo

COUNTY Montgomery API 121352380300 14 - 7N - 3W

APPENDIX C BORING AND WELL CONSTRUCTION LOGS

BORING AND WELL LOCATIONS MAP



BACKGROUND WELL

MONITORING WELL

SOURCE SAMPLE LOCATION

STAFF GAGE

PART 845 REGULATED UNIT (SUBJECT UNIT)

SITE FEATURE

LIMITS OF FINAL COVER

PROPERTY BOUNDARY 550

MONITORING WELL LOCATION MAP

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT

RAMBOLL AMERICAS ENGINEERING SOLUTIONS, INC.

ASH POND NO. 1 COFFEEN POWER PLANT COFFEEN, ILLINOIS



FIGURE C1

BORING LOGS

CLIENT: Natural Resources Technology, Inc. Site: Coffeen Power Station - Ash Pond 2 Location: 134 CIPS Lane, Coffeen, IL 62017

Project: 16E0080

DATES: Start: 8/16/2016 Finish: 8/17/2016

WEATHER: Cloudy, rain, (hi-70s)

CONTRACTOR: Bulldog Drilling, Inc. Rig mfg/model: CME-750 ATV Drill Drilling Method: 4 1/4" Hollow Stem Auger

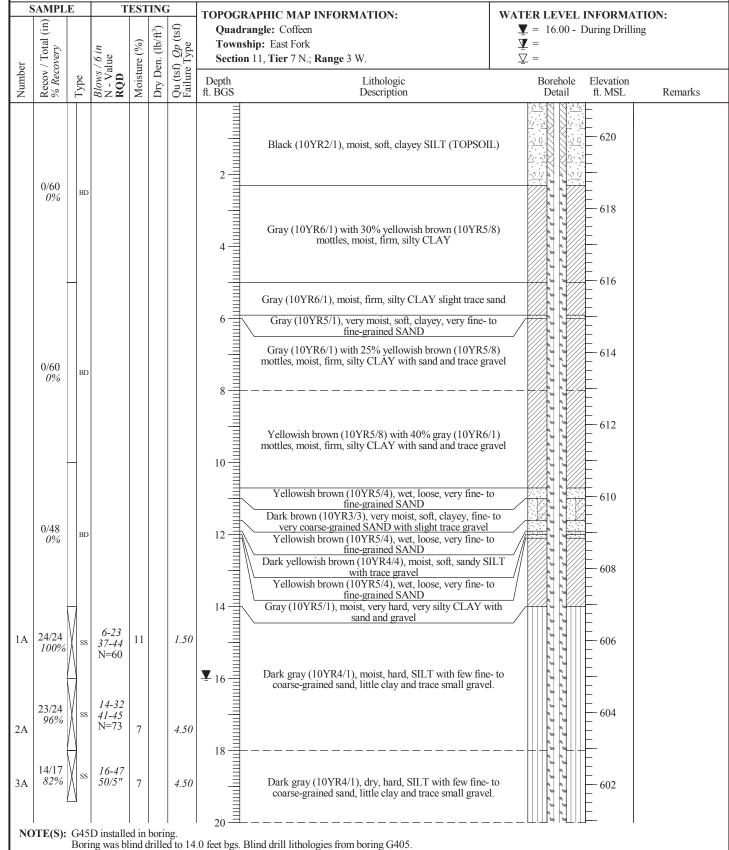
FIELD STAFF: Driller: J. Dittmaier Helper: M. Hill

Eng/Geo: K. Theesfeld



BOREHOLE ID: G405D Well ID: G45D

> Surface Elev: 620.94 ft. MSL Completion: 42.00 ft. BGS **Station:** 873,998.03N 2,515,322.23E



CLIENT: Natural Resources Technology, Inc.
Site: Coffeen Power Station - Ash Pond 2
Location: 134 CIPS Lane, Coffeen, IL 62017

Project: 16E0080

DATES: Start: 8/16/2016 **Finish:** 8/17/2016

WEATHER: Cloudy, rain, (hi-70s)

CONTRACTOR: Bulldog Drilling, Inc.
Rig mfg/model: CME-750 ATV Drill
Drilling Method: 4 1/4" Hollow Stem Auger

FIELD STAFF: Driller: J. Dittmaier Helper: M. Hill

Helper: M. Hill Eng/Geo: K. Theesfeld **HANSON**

BOREHOLE ID: G405D **Well ID:** G45D

 Surface Elev:
 620.94 ft. MSL

 Completion:
 42.00 ft. BGS

 Station:
 873,998.03N

 2,515,322.23E

| | E | | | ING | | TOPOGRAPHIC M | AP INFORMATION: | WATER LEVEL INFORMATION: | |
|--|------|----------------------------------|---------------|-------------------|-------------------------------------|---|--|--|------|
| Recov / Total (in) | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Qp (tsf) Failure Type | Quadrangle: Cof Township: East F Section 11, Tier 7 | ork | $\underline{\Psi}$ = 16.00 - During Drilling $\underline{\Psi}$ = $\underline{\nabla}$ = | |
| Recov / % Recor | Type | Blows N - V. RQD | Moist | Dry D | Qu (ts Failur | Depth ft. BGS | Lithologic Description | Borehole Elevation Detail ft. MSL Rema | arks |
| 19/24 79% | ss | 15-36 32-36 N=68 | 8 | | 4.50 | coars | ray (10YR4/1), dry, hard, SILT with few fine- e-grained sand, little clay and little small grave by (10YR4/1), moist, dense, fine- to coarse-gra SAND. | el. / [Side] | |
| A 19/24 79% | ss | 10-18 30-33 N=48 | 8 | | 4.50 | Dark g | ray (10YR4/1), dry, hard, SILT with few fine- e-grained sand, little clay and little small grave | | |
| A 11/24 46% | ss | 22-42 34-36 N=76 | 8 | | 4.50 | 26 | | 596 | |
| 7A 11/24 46% | SS | 28-26 23-26 N=49 | 11 | | 4.50 | -∃ (10Y | gray (10YR4/1) with 5% light brownish gray (6/2) mottles, dry, hard, SILT with few fine- tegrained sand, little clay and little small grave | to 594 | |
| 3A 23/24 96% | ss | 7-11 16-25 N=27 | 10 | | 4.50 | Darl (10YR6, hard, SII | gray (10YR4/1) with 5% light brownish gray (2) and dark greenish gray (10YR4/2) mottles, T with few fine- to coarse-grained sand, little and little small gravel. | s, dry, e clay 592 | |
| OA 17/24 | ss | 7-14 12-12 N=26 | 16 14 9 | | | Coars Dark gra | ray (10YR4/1), dry, hard, SILT with few fine- e-grained sand, little clay and little small grave by (10YR4/1), dry, very stiff, SILT with some fine-grained SAND. ark gray (10YR3/1), moist, very stiff, CLAY we few silt and little medium-grained sand. | el. • very 590 | |
| 24/24 100% | SS | 2-5 8-13 N=13 | 15 | | 3.25 | | ark gray (10YR3/1), moist, very stiff, CLAY w | with 588 | |
| 1-1 1-2 22/24 92% 1-3 1-4 | SH | | 15 | | | 34 Very da | little silt and little medium-grained sand. | 586 | |
| 24/24 100% | SS | 2-5 8-10 N=13 | 16 | | 2.00 | Very da little silt, | ark gray (10YR3/1), moist, very stiff, CLAY was little medium-grained sand, and trace small gr | with ravel. | |
| 3A 22/24 92% | ss | 2-5 7-8 N=12 | 16 | | 2.00 | mott | dark gray (10YR3/1) with 5% black (10YR2/les, moist, very stiff, CLAY with little silt, little edium-grained sand, and trace small gravel. | | |

CLIENT: Natural Resources Technology, Inc. Site: Coffeen Power Station - Ash Pond 2 Location: 134 CIPS Lane, Coffeen, IL 62017

Project: 16E0080

DATES: Start: 8/16/2016 Finish: 8/17/2016

WEATHER: Cloudy, rain, (hi-70s)

CONTRACTOR: Bulldog Drilling, Inc. Rig mfg/model: CME-750 ATV Drill **Drilling Method:** 4 1/4" Hollow Stem Auger

FIELD STAFF: Driller: J. Dittmaier Helper: M. Hill

Eng/Geo: K. Theesfeld

HANSON

BOREHOLE ID: G405D Well ID: G45D

> Surface Elev: 620.94 ft. MSL **Completion:** 42.00 ft. BGS **Station:** 873,998.03N 2,515,322.23E

| | S | AMPL | E | Т | EST | INC | j | TOPOGRA | PHIC MAP INFORMATION: | WATER LEVEL | INFORMAT | TION: |
|---|--------|------------------|------|------------------------|----------|-----------|---------------------|------------------|--|---|-------------------|---------|
| ١ | | 1 (in) | | | | /ft³) | (tsf) | Quadran | gle: Coffeen | T = 16.00 - 1 | During Drillin | |
| | er | / Total overy | | /6 in ılue | ture (%) | Den. (lb) | $O_{\rm Type}$ | | p: East Fork 1, Tier 7 N.; Range 3 W. | $\overline{\Lambda} = \overline{\Lambda}$ | | |
| | Number | Recov % Rec | Type | Blows N - Va RQD | Moist | Dry Do | Qu (tsf) Failure | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks |
| | 14A | 23/24 96% | SS | 1-3 7-7 N=10 | 16 | | 3.50 | 42 | Very dark gray (10YR3/1) with 5% black (10YR2/1 mottles, moist, very stiff, CLAY with little silt, little medium-grained sand, and trace small gravel. [Continued from previous page] | | 580 | |
| П | | | | | | | | 72 | End of Boring = 42.0 ft. BGS | | | |

CLIENT: Natural Resources Technology, Inc.

Site: Coffeen Energy Center Location: Coffeen, Illinois

Project: 15E0030 **DATES: Start:** 5/1/2007

Finish: 5/1/2007 **WEATHER:** Partly sunny, warm

CONTRACTOR: Reynolds Drilling Corp. **Rig mfg/model:** CME-550 ATV Drill

Drilling Method: 41/4" Hollow stem auger with split spoon

sampler

FIELD STAFF: Driller: A. Rachford Helper: M. Brown

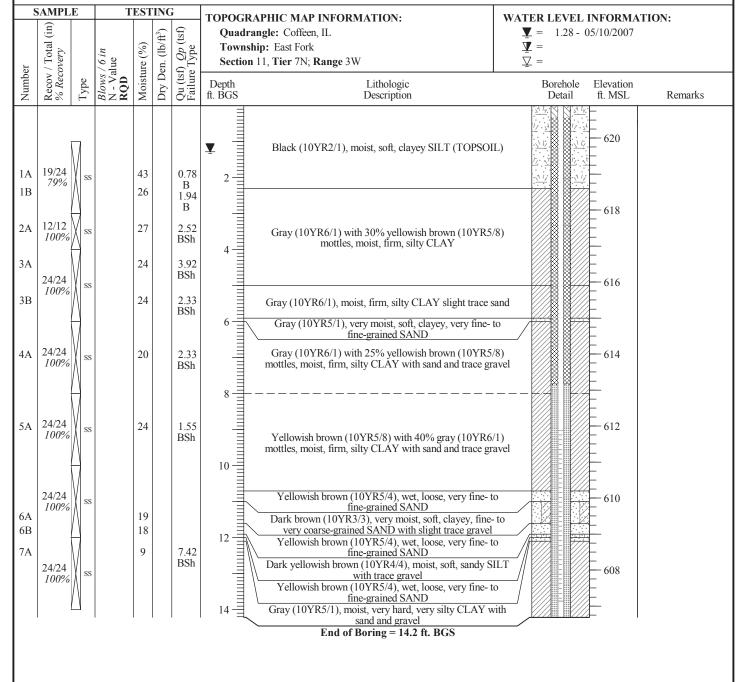
Eng/Geo: R. Hasenyager



BOREHOLE ID: SB21 Formerly MW21S

Well ID: G405

Surface Elev: 620.90 ft. MSL Completion: 14.21 ft. BGS Station: 873,996.79N 2,515,335.70E



CLIENT: Natural Resources Technology, Inc.
Site: Coffeen Power Station - Ash Pond 2
Location: 134 CIPS Lane, Coffeen, IL 62017

Project: 16E0080

DATES: Start: 8/19/2016

Finish: 8/19/2016 WEATHER: Sunny, (mid-70s)

CONTRACTOR: Bulldog Drilling, Inc.
Rig mfg/model: CME-750 ATV Drill
Drilling Method: 4 1/4" Hollow Stem Auger

FIELD STAFF: Driller: J. Dittmaier Helper: M. Hill

Eng/Geo: K. Theesfeld



BOREHOLE ID: G406D **Well ID:** G46D

 Surface Elev:
 621.91 ft. MSL

 Completion:
 52.00 ft. BGS

 Station:
 872,519.70N

 2,514,697.78E

| - 1 | AMPLI | Ľ | T | EST | ING | | TOPOGRAPHIC MAP INFORMATION: | WATER LEVEL INFORMATION: | | | |
|--------|-------------------------------|------|----------------------------------|--------------|-------------------|-------------------------------------|---|---|-------------------|---------|--|
| | Recov / Total (in) % Recovery | | / 6 in Iue | re (%) | Dry Den. (lb/ft³) | Qu (tsf) Qp (tsf) Failure Type | Quadrangle: Coffeen Township: East Fork Section 11, Tier 7 N.; Range 3 W. | | Ouring Drilling | | |
| | Recov % Recc | Type | Blows / 6 in N - Value RQD | Moisture (%) | Dry De | Qu (tsf Failure | Depth Lithologic ft. BGS Description | Borehole Detail | Elevation ft. MSL | Remarks | |
| 1 | | | | 11 | | 1.50 | Dark brown (10YR3/3), moist, stiff, SILT with few clay and trace organics. | y | | | |
| В | 18/24 75% | ss | 4-3 4-6 N=7 | 15 | | 3.00 | = | | 620 | | |
| A | 12/24 50% | SS | 4-6 3-3 N=9 | 12 | | 2.50 | mottles, SILT with some clay and trace small gravel. | ,,,,, | | | |
| B A | 3/24 13% | ss | 3-3 4-7 N=7 | 18 24 | | 2.00 | Brown (10YR5/3) with 10% dark brown (10YR3/3) mottles, SILT with some clay. Grayish brown (10YR5/2) with 5% dark yellowish brow (10YR4/6) mottles, moist, stiff, CLAY with few silt and little fine-grained sand. Very pale brown (10YR7/4) with 25% yellowish brown (10YR5/6) mottles, moist, medium, CLAY with trace sil | i / | 618 | | |
| A | 20/24 83% | SS | 2-3 4-5 N=7 | 21 | | 1.25 | Brown (10YR5/3) with 10% dark brown (10YR3/3) mottles, SILT with some clay and trace small gravel. Brown (10YR5/3) with 10% dark brown (10YR3/3) mottles, SILT with some clay. Grayish brown (10YR5/2) with 5% dark yellowish brown (10YR4/6) mottles, moist, stiff, CLAY with few silt and little fine-grained sand. Very pale brown (10YR7/4) with 25% yellowish brown (10YR5/6) mottles, moist, medium, CLAY with trace sill clay with little silt and trace fine- to medium-grained sand. Gray (10YR5/1) with 10% yellowish brown (10YR5/6) and 5% very dark gray (10YR3/1) mottles, moist, stiff, CLAY with little silt, little fine- to medium-grained sand sand trace small gravel. Gray (10YR5/1) with 10% yellowish brown (10YR5/6) and 5% very dark gray (10YR3/1) mottles, moist, stiff, CLAY with few fine- to medium-grained sand, little silt and trace small gravel. Gray (10YR6/1) with 25% brownish yellow (10YR6/8) and 5% strong brown (7.5YR4/6) mottles, moist, stiff, CLAY with few fine- to medium-grained sand, little silt and trace small gravel. | | 616 | | |
| A | 19/24 79% | ss | 1-3 4-6 N=7 | 18 | | 1.75 | Gray (10YR5/1) with 10% yellowish brown (10YR5/6 and 5% very dark gray (10YR3/1) mottles, moist, stiff, CLAY with little silt, little fine- to medium-grained sand and trace small gravel. | | 612 | | |
| δA | 23/24 96% | ss | 2-2 4-5 N=6 | 18 | | 2.50 | Gray (10YR5/1) with 10% yellowish brown (10YR5/6 and 5% very dark gray (10YR3/1) mottles, moist, stiff, CLAY with few fine- to medium-grained sand, little silt and trace small gravel. | , | | | |
| 'A | 21/24 88% | ss | 1-3 4-5 N=7 | 16 | | 1.00 | \exists | | 610 | | |
| A | 23/24 96% | ss | 1-2 2-2 N=4 | 18 | | 0.75 | Gray (10YR6/1) with 10% brownish yellow (10YR6/8 and 5% strong brown (7.5YR4/6) mottles, moist, stiff, CLAY with some fine- to medium-grained sand, little sil and trace small gravel. Gray (10YR6/1) with 5% brownish yellow (10YR6/6) mottles, wet, loose, fine-grained SAND with some clay. | | 608 | | |
| В | | 1 | | 17 | | 0.75 | Gray (10YR6/1) with 5% brownish yellow (10YR6/6) mottles, wet, loose, fine-grained SAND with some clay. | | 606 | | |
| A | 22/24 92% | ss | 4-13 27-23 N=40 | 8 | | | Gray (10YR6/1) with 5% brownish yellow (10YR6/6) mottles, moist, loose, fine-grained SAND with some clay | | | | |
| В | | 1 | | 8 | | | 18 | | 604 | | |
|)A | 17/24 71% | ss | 13-31 33-42 N=64 | 7 | | 4.50 | Gray (10YR6/1) with 5% brownish yellow (10YR6/6) mottles, moist, loose, fine-grained SAND with some clay Gray (10YR5/1), dry, hard, SILT with few clay, few fine to coarse-grained sand and trace small gravel. | ÷ | 602 | | |

CLIENT: Natural Resources Technology, Inc. Site: Coffeen Power Station - Ash Pond 2 Location: 134 CIPS Lane, Coffeen, IL 62017

Project: 16E0080

DATES: Start: 8/19/2016 **Finish:** 8/19/2016

WEATHER: Sunny, (mid-70s)

CONTRACTOR: Bulldog Drilling, Inc.
Rig mfg/model: CME-750 ATV Drill
Drilling Method: 4 1/4" Hollow Stem Auger

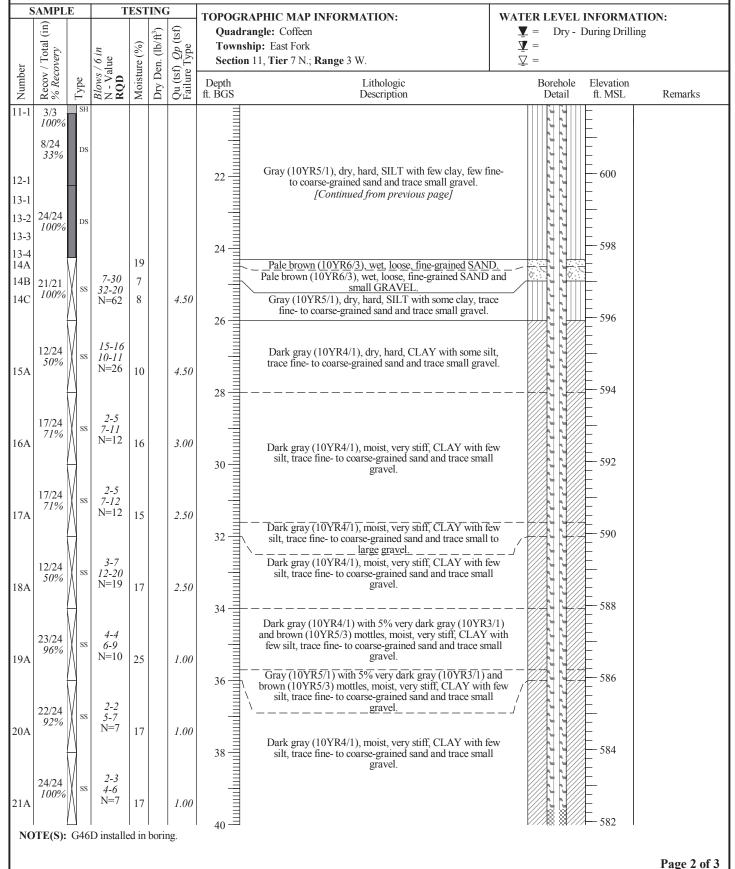
FIELD STAFF: Driller: J. Dittmaier Helper: M. Hill

Eng/Geo: K. Theesfeld



BOREHOLE ID: G406D **Well ID:** G46D

Surface Elev: 621.91 ft. MSL Completion: 52.00 ft. BGS Station: 872,519.70N 2,514.697.78E



CLIENT: Natural Resources Technology, Inc. Site: Coffeen Power Station - Ash Pond 2 Location: 134 CIPS Lane, Coffeen, IL 62017

Project: 16E0080

DATES: Start: 8/19/2016 **Finish:** 8/19/2016

WEATHER: Sunny, (mid-70s)

CONTRACTOR: Bulldog Drilling, Inc.
Rig mfg/model: CME-750 ATV Drill
Drilling Method: 4 1/4" Hollow Stem Auger

FIELD STAFF: Driller: J. Dittmaier Helper: M. Hill

Eng/Geo: K. Theesfeld

HANSON

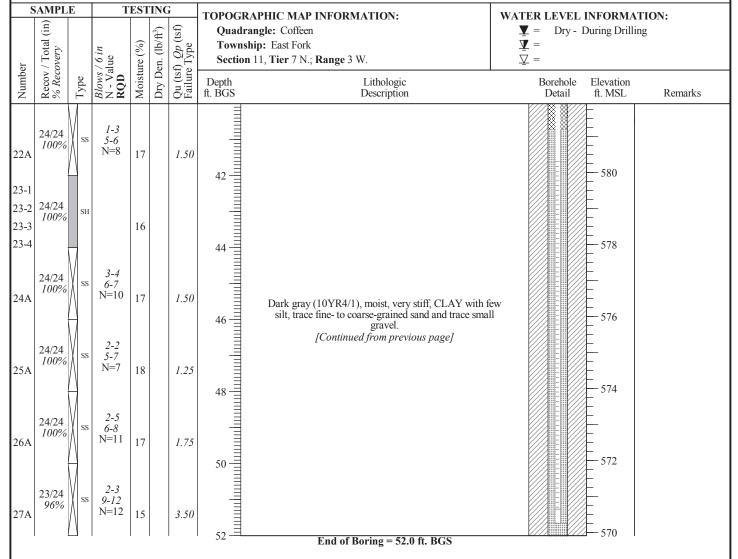
BOREHOLE ID: G406D **Well ID:** G46D

 Surface Elev:
 621.91 ft. MSL

 Completion:
 52.00 ft. BGS

 Station:
 872,519.70N

 2,514,697.78E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A **DATES: Start:** 2/2/2010

Finish: 2/2/2010

WEATHER: Overcast, cold (lo-30's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill **Drilling Method:** 41/4" HSA w/SS samplers

FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby Eng/Geo: S. Suzanna Simpson

HANSON

BOREHOLE ID: G101 Well ID: G101

Surface Elev: 625.27 ft. MSL Completion: 21.92 ft. BGS **Station:** 876,551.76N 2,514,214.31E

| | MPLI | C | T | EST | INC | | TOPOGRAPHIC MAP INFORMATION: | WATER LEVEL INFORMATION: | | | |
|----------------|-------------------------------|------|----------------------------------|--------------|-------------------|--|---|---|--|--|--|
| | Recov / Total (1n) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) <i>Qp</i> (tsf) Failure Type | Quadrangle: Coffeen, IL Township: East Fork Section 10, Tier 7N; Range 3W | $\underline{\Psi}$ = 15.50 - While drilling $\underline{\Psi}$ = 12.38 - Upon Completion $\underline{\nabla}$ = 7.31 - 3/1/2010 | | | |
| indilinci G | Recov % Re | Type | Blows N - V RQD | Moist | Dry D | Qu (ts Failur | Depth Lithologic ft. BGS Description | Borehole Elevation Detail ft. MSL Remarks | | | |
| A 1 | 18/24 75% | ss | 1-1 2-3 N=3 | 24 | | | TOPSOIL - Brown (10YR5/3), moist, soft, silty CI with slight trace sand and gravel, roots. Dark grayish brown (10YR4/2), moist, soft, silty CI with slight trace sand, trace roots. | | | | |
| | 18/24 75% | SS | 1-3 3-5 N=6 | 30 | | | Dark grayish brown (10YR4/2) with 15% yellowish (10YR5/4) mottles, moist, medium, silty CLAY, sl trace roots. Grayish brown (10YR5/2) with 15% yellowish brown (10YR5/4) mottles, moist, medium, silty CLAY, sl trace roots. | ight | | | |
| A 1 | 19/24 79% | SS | 2-3 4-4 N=7 | 26 | | | Gray (10YR5/1) with 25% yellowish brown (10YR mottles, moist, medium, silty CLAY, slight trace ro | (5/6) oots. — 620 | | | |
| | 19/24 79% | SS | 1-3 4-3 N=7 | 21 | | | Gray (10YR5/1) with 10% yellowish brown (10YR mottles, moist, medium, silty CLAY with slight trace | 25/6) sand. | | | |
| | 22/24 92% | SS | 1-3 3-4 N=6 | 23 | | | Gray (10YR5/1) with 10% yellowish brown (10YR mottles, moist, medium, silty CLAY with trace sand slight trace gravel. | 5/6) and -616 | | | |
| | 20/24 83% | SS | 1-2 2-3 N=4 | 24 | | | Gray (10YR6/1) with 35% yellowish brown (10YR mottles, moist, soft, silty CLAY with trace sand and trace gravel. | 15/6) slight | | | |
| | 22/24 92% | SS | 1-2 3-2 N=5 | 17 | | | Gray (10YR5/1) with 25% yellowish brown (10YR mottles, very moist, medium, silty, sandy CLAY with | 15/6) 1 trace | | | |
| BA BB 1 | 14/24 58% | SS | 1-2 5-8 N=7 | 15 13 | | | Brown (10YR5/3), very moist, medium, silty, clayey fine- to coarse-grained SAND with slight trace gra Brown (10YR5/3), very moist, loose, silty, very fin coarse-grained SAND with slight trace gravel. | vel | | | |
| 9A 1 | 6/24 67% | SS | 2-5 15-25 N=20 | 16 | | | Brown (10YR5/3), very moist, medium dense, silty, | very 608 | | | |
| | 7/24 71% | SS | 19-20 22-18 N=42 | 14 | | | Brown (10YR5/3), very moist, dense, silty, very fin coarse-grained SAND with slight trace gravel. | e- to | | | |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 2/2/2010 **Finish:** 2/2/2010

WEATHER: Overcast, cold (lo-30's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby **Eng/Geo:** S. Suzanna Simpson

HANSON

BOREHOLE ID: G101 **Well ID:** G101

 Surface Elev:
 625.27 ft. MSL

 Completion:
 21.92 ft. BGS

 Station:
 876,551.76N

 2,514,214.31E

| | | | | | | | | | | | · · · · · |
|-------------|----------------|------|--------------------------|----------|----------|---------------------|------------------|---|---|-------------------|-----------|
| | SAMPL | E | Т | EST | INC | j | TOPOGRA | PHIC MAP INFORMATION: | WATER LEVEL | INFORMAT | ION: |
| | Total (in) | | u | (%) | (lb/ft³) | Qp (tsf) ype | Quadrar | ngle: Coffeen, IL p: East Fork | $\underline{\underline{Y}} = 15.50 - \underline{\underline{Y}} = 12.38 - \underline{\underline{Y}}$ | While drilling | |
| l i | / To | | / 6 i. Jue | | Den. (| | Section 1 | 0, Tier 7N; Range 3W | $\underline{\nabla} = 7.31 - 1$ | 3/1/2010 | |
| Number | Recov % Rec | Type | Blows N - Va RQD | Moisture | Dry De | Qu (tsf) Failure | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks |
| 11 <i>A</i> | 16/23 70% | SS | 2-16 42-60/5' N=58 | 8 | | | | Brown (10YR5/3), slightly moist, hard, clayey SILT v slight trace sand and gravel. Dark gray (10YR4/1), slightly moist, hard, clayey SII with slight trace sand and slight trace gravel. | <i>j</i> ′ | 604 | |
| 1 | ' | _ | | | | • | | End of Boring = 21.9 ft. BGS | | | |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A **DATES: Start:** 4/28/2006

Finish: 4/28/2006 WEATHER: Partly cloudy, mild (mid-60's) CONTRACTOR: Testing Service Corp. Rig mfg/model: CME-650 Track Drill Drilling Method: 4½" HSA (blind drill)

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

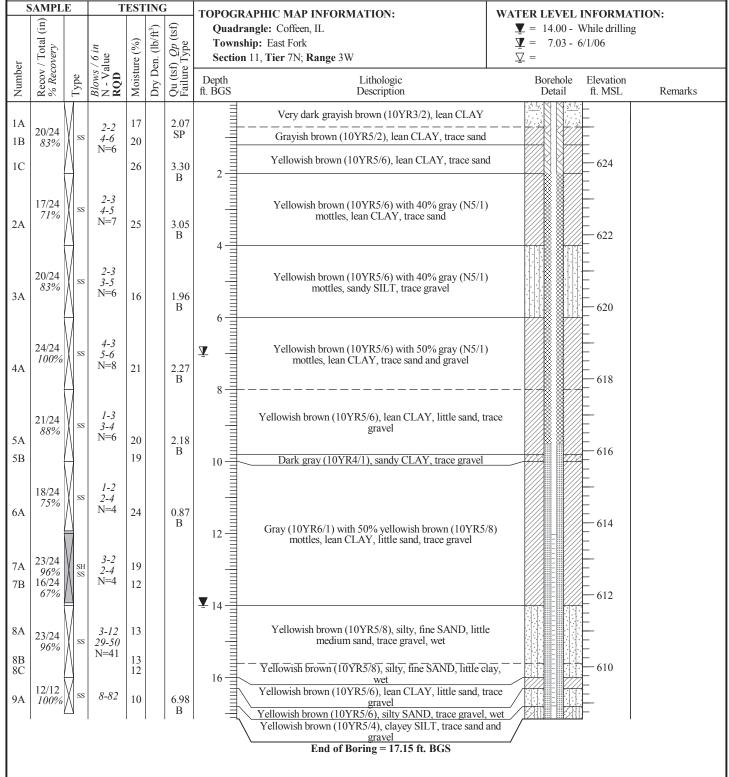
Eng/Geo: R. Hasenyager



BOREHOLE ID: SB-03a

Well ID: G102 (MW3S)
Surface Elev: 625.70 ft. MSL
Completion: 17.15 ft. BGS
Station: 876.554.77N

2,514,531.48E



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A DATES: Start: 4/27/2006

Finish: 4/27/2006 **WEATHER:** Sunny, mild (high-50's)

CONTRACTOR: Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS sampler & 41/4" HSA overdrill

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

BOREHOLE ID: SB-03

Station:

Well ID: MW3D

Surface Elev: 626 ft. MSL **Completion:** 58 ft. BGS

HANSON

876,554.5N 2,514,535.3E

Page 1 of 3

| | | | ınny, mil | , | | | | Eng/Geo: R. Hasenyager | Т | | 2,514,535.3E |
|----------|------------------------------|-------|----------------------------------|--------------|-------------------|-----------------------|---|--|---|---------------------------|--|
| | Recov / Total (in) | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quad Town | RAPHIC MAP INFORMATION: rangle: Coffeen, IL ship: East Fork n 11, Tier 7N; Range 3W | WATER LEVEL I Y = 14.00 - V Y = 7.03 - N Y = 55.40 - N | Vhile drillir IW03S on | ng 6/1/06 |
| Number | Recov % Rec | Type | Blows N - V | Moist | Dry D | Qu (ts Failur | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks |
| 1A | | | | 17 | | 2.07 | = | Very dark grayish brown (10YR3/2), lean CLA | \mathbf{Y} | _ | |
| 1B | 20/24 83% | ss | 2-2 4-6 | 20 | | SP SP | | Grayish brown (10YR5/2), lean CLAY, trace sar | nd and | - | |
| 1C | | ^\ | N=6 | 26 | | 3.30 | | Yellowish brown (10YR5/6), lean CLAY, trace sa | and | _ 624 | |
| 2A | 17/24 71% | ss | 2-3 4-5 N=7 | 25 | | 3.05 B | 2 = = = = = = = = = = = = = = = = = = = | Yellowish brown (10YR5/6) with 40% gray (N5/mottles, lean CLAY, trace sand | (1) | | |
| 3A | 20/24 83% | ss | 2-3 3-5 N=6 | 16 | | 1.96 B | 6- | Yellowish brown (10YR5/6) with 40% gray (N5/mottles, sandy SILT, trace gravel | (1) | | |
| 4A | 24/24 100% | ss | 4-3 5-6 N=8 | 21 | | 2.27 B | 8 - | Yellowish brown (10YR5/6) with 50% gray (N5/mottles, lean CLAY, trace sand and gravel | (1) | | |
| 5A 5B | 21/24 88% | ss | 1-3 3-4 N=6 | 20 19 | | 2.18 B | 10 | Yellowish brown (10YR5/6), lean CLAY, little sand gravel Dark gray (10YR4/1), sandy CLAY, trace grave | | | |
| 6A | 18/24 75% | ss | 1-2 2-4 N=4 | 24 | | 0.87 B | 12 — | Gray (10YR6/1) with 50% yellowish brown (10YR mottles, lean CLAY, little sand, trace gravel | 2.5/8) | | Shelby tube taken |
| 7A 7B | 23/24 96% 16/24 67% | SH | 3-2 2-4 N=4 | 19 12 | | | ¥ 14 | | | | from shallow well borehole at indicated depth. |
| 8A | 23/24 | SS | 3-12 29-50 | 13 | | | | Yellowish brown (10YR5/8), silty, fine SAND, li medium sand, trace gravel, wet | ttle | <u> </u> | |
| 8B 8C | 96% | | N=41 | 13 12 | | | 16- | Yellowish brown (10YR5/8), silty, fine SAND, little | clay, | - - - - 610 | |
| 9A | 14/24 58% | ss | 8-82 85-72 | 10 | | 6.98 B | | Yellowish brown (10YR5/6), lean CLAY, little sand gravel Yellowish brown (10YR5/6), silty SAND, trace gravel | / BBBU NBB | - - - | |
| 9B | 3070 | ^\ | N=167 | 13 | | 6.18 <i>BSh</i> | 18 — | Yellowish brown (10YR5/4), clayey SILT, trace san gravel | / Milli Naii | 608 | |
| 10A | 18/24 75% | ss | 6-21 32-49 N=53 | 8 | 11-11 | 11.95 Sh | 20 | Gray (10YR5/1), sandy SILT, trace gravel | 7,7,7,7 | | |
| | NOTE(| s): N | 1W03D i | nsta | iled i | ın SB-(| J3. | | | | Dage 1 of 2 |

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A

DATES: Start: 4/27/2006

Finish: 4/27/2006

Finish: 4/27/2006 **WEATHER:** Sunny, mild (high-50's)

TESTING

SAMPLE

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS sampler & 41/4" HSA overdrill

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

2,514,535.3E

WATER LEVEL INFORMATION:

BOREHOLE ID: SB-03

Surface Elev:

Completion:

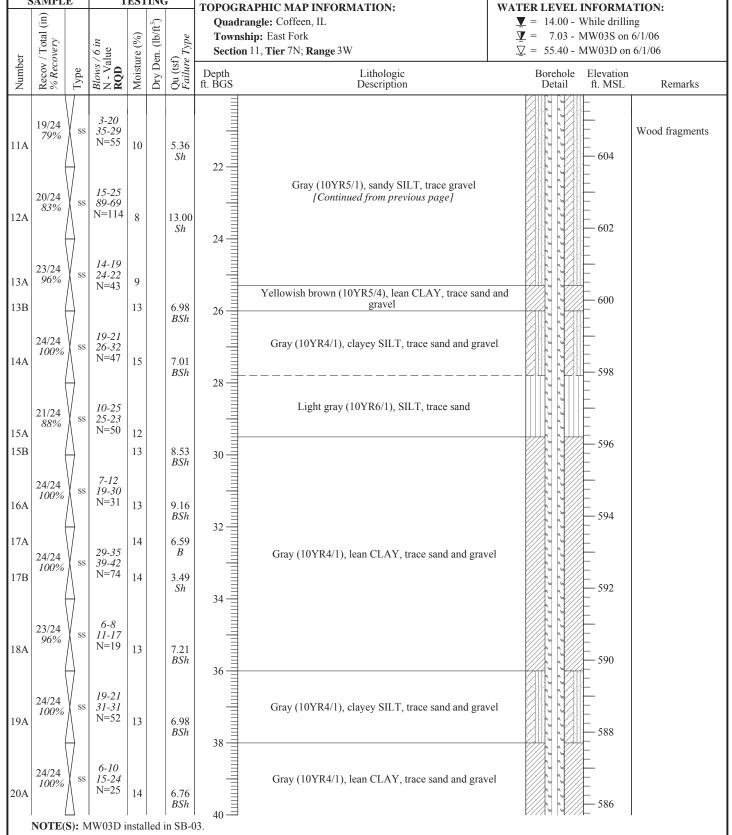
Station:

Well ID: MW3D

626 ft. MSL

58 ft. BGS

876,554.5N



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A

DATES: Start: 4/27/2006

Finish: 4/27/2006

Finish: 4/27/2006 WEATHER: Sunny, mild (high-50's) **CONTRACTOR:** Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS sampler & 41/4" HSA overdrill

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

HANSON

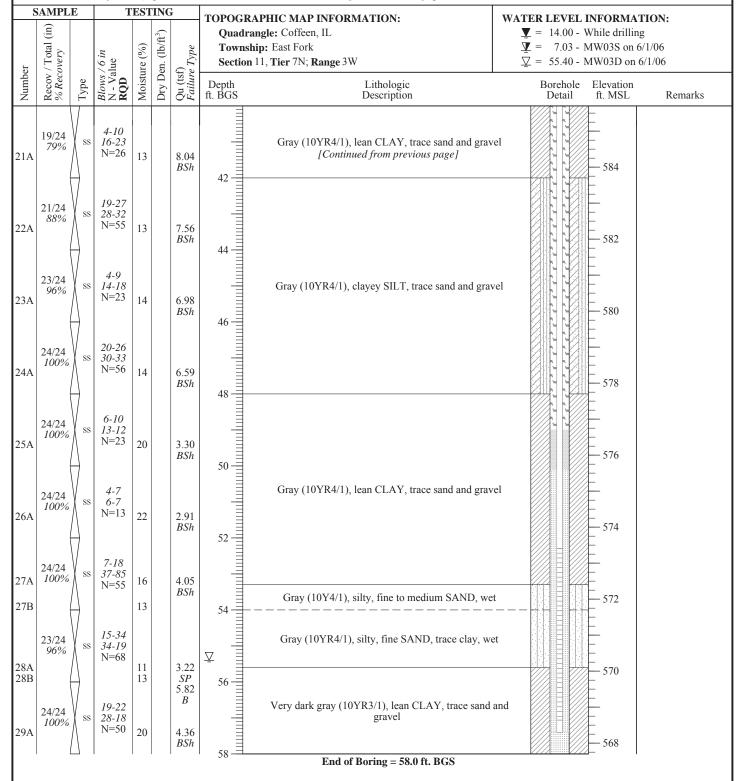
BOREHOLE ID: SB-03 **Well ID:** MW3D

 Surface Elev:
 626 ft. MSL

 Completion:
 58 ft. BGS

 Station:
 876,554.5N

 2,514,535.3E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois

Project:

DATES: Start: 2/15/2010

Finish: 2/15/2010

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill **Drilling Method:** 41/4" HSA w/SS samplers

FIELD STAFF: Driller: T. List

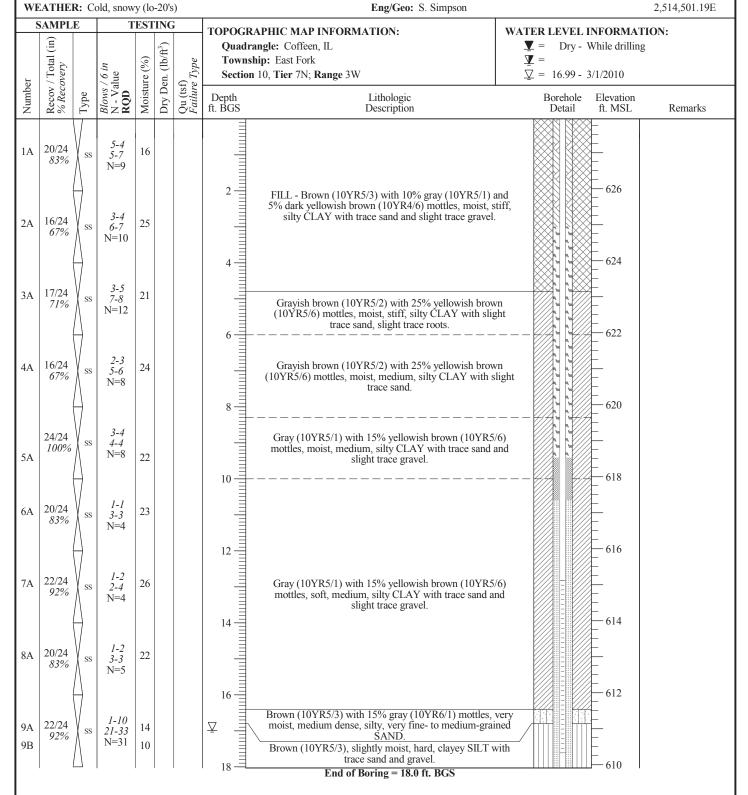
Helper: M. Herbst/S. Hamby

BOREHOLE ID: G103

Well ID: G103

Surface Elev: 627.94 ft. MSL Completion: 18.03 ft. BGS **Station:** 876,199.48N

HANSON



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A **DATES:** Start: 2/15/2010

Finish: 2/15/2010
WEATHER: Overcast, cold, windy (lo-20's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby **Eng/Geo:** S. Suzanna Simpson

HANSON

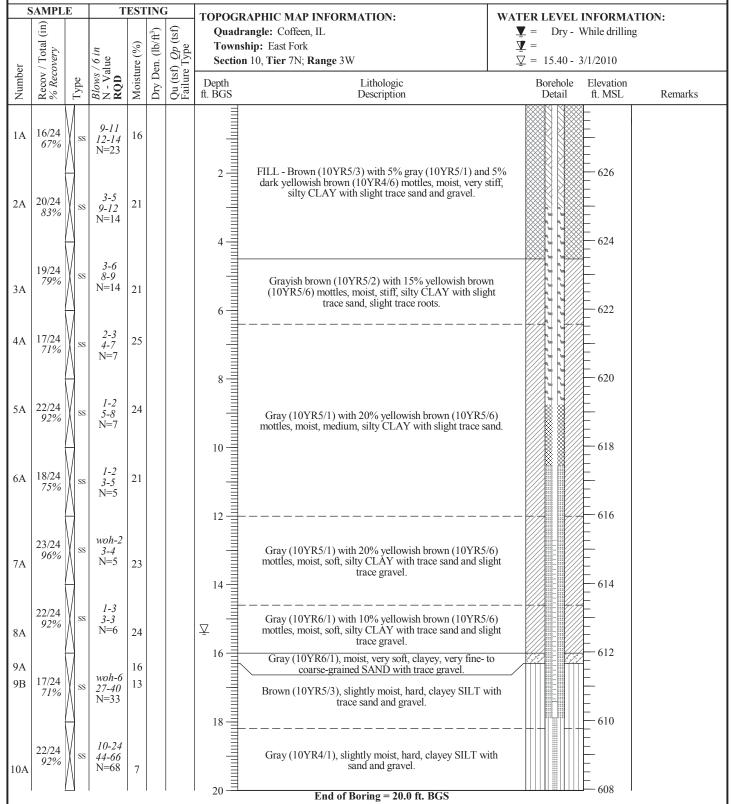
BOREHOLE ID: G104 **Well ID:** G104

 Surface Elev:
 627.96 ft. MSL

 Completion:
 20.00 ft. BGS

 Station:
 875,849.26N

 2.514,504.98E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois

Project:

DATES: Start: 2/16/2010

Finish: 2/16/2010

WEATHER: Sunny, cold, windy (mid-20's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby

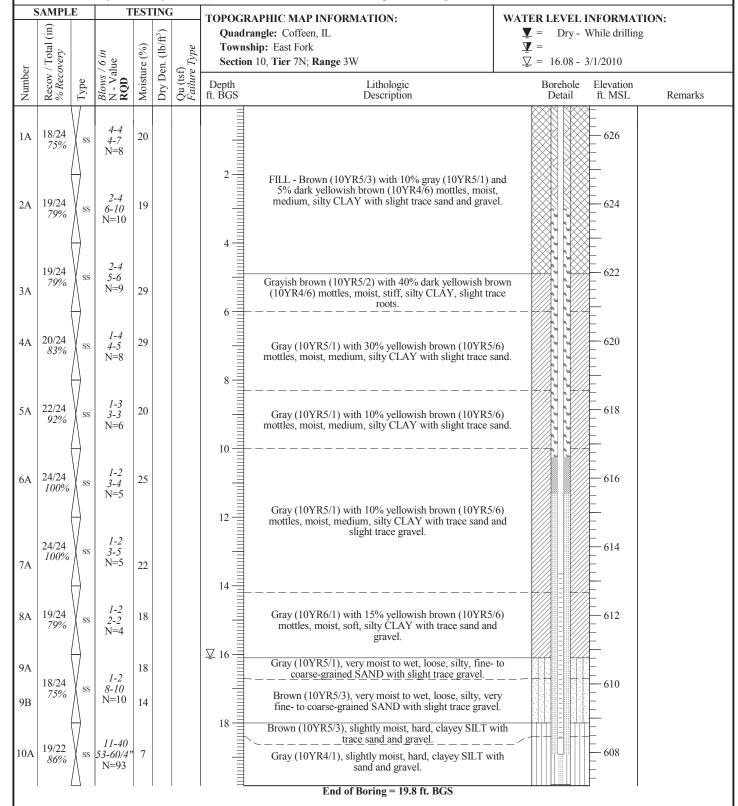
Eng/Geo: S. Simpson

HANSON

BOREHOLE ID: G105 Well ID: G105

Surface Elev: 626.86 ft. MSL Completion: 19.83 ft. BGS

Station: 875,499.70N 2,514,509.15E



NOTE(S): Well completed prior to construction of berm road. Boring surface elevation is as of the well install date and not the final constructed elevation.

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A **DATES: Start:** 2/16/2010

Finish: 2/16/2010

WEATHER: Overcast, cold, windy (mid-20's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 4½" HSA w/SS samplers

FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby **Eng/Geo:** S. Suzanna Simpson

HANSON

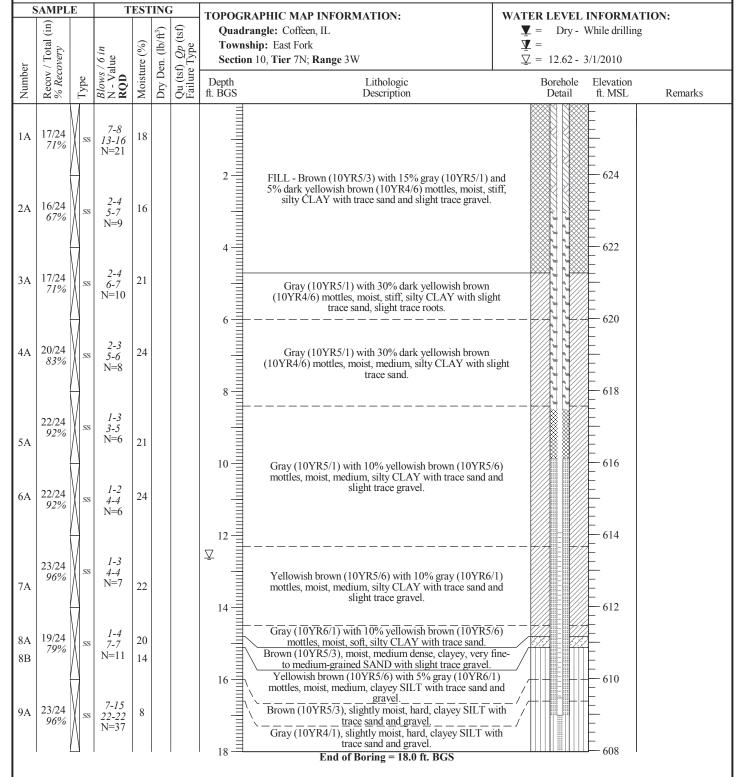
BOREHOLE ID: G106 Well ID: G106

 Surface Elev:
 625.96 ft. MSL

 Completion:
 18.00 ft. BGS

 Station:
 875,149.76N

 2.514.512.79E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois

Project:

DATES: Start: 2/17/2010

Finish: 2/17/2010

WEATHER: Overcast, cold, windy (mid-20's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby

Eng/Geo: S. Simpson

HANSON

BOREHOLE ID: G107 Well ID: G107

Surface Elev: 627.11 ft. MSL **Completion:** 20.00 ft. BGS **Station:** 874,994.33N 2,514,358.25E

SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: Ξ Quadrangle: Coffeen, IL $\mathbf{Y} = 16.80$ - While drilling Dry Den. (lb/ft3 Recov / Total (% Recovery Township: East Fork Moisture (%) TypeBlows / 6 in N - Value RQD Section 10, Tier 7N; Range 3W ∇ = 10.40 - 3/1/2010 Qu (tsf) Failure 1 Number Lithologic Borehole Elevation Description Detail ft. MSL Remarks 0/18BD 0% **GRAVEL FILL** 626 5/6 SS 1A 12 83% 3 FILL - Brown (10YR5/3) with 10% gray (10YR5/1) and 14/24 2A 17 6-8 5% dark yellowish brown (10YR4/6) mottles, moist, stiff, 624 58% N=9silty CLAY with trace sand and slight and gravel. 3-5 5-7 16/24 20 3A 622 67% N=10 Grayish brown (10YR5/2) with 30% yellowish brown (10YR5/6) mottles, moist, stiff, silty CLAY with slight trace sand and gravel. 18/24 4A 27 6-7 75% 620 N=9 2-3 4-5 22/24 5A 18 92% 618 ∇ Gray (10YR5/1) with 10% yellowish brown (10YR5/6) 1-3 22/24 mottles, moist, medium, silty CLAY with trace sand and 3-4 616 92% N=6 slight trace gravel. 23 **V** 1-2 24/24 27 7A 3-4 100% 614 Gray (10YR6/1) with 35% yellowish brown (10YR5/6) mottles, moist, medium, silty CLAY with trace sand and 1-3 slight trace gravel. 2/24 23 8A 2-3 612 8% N=5Brown (10YR5/3), very moist to wet, very loose, clayey, very fine- to coarse-grained SAND. 9A 22 woh-3 20/24 8-12 Brown (10YR5/3), slightly moist, stiff, clayey SILT with 83% 610 9B N = 11trace sand and gravel. 10 Brown (10YR5/3), slightly moist, hard, clayey SILT with trace sand and gravel. 8-25 20/24 11 26-58 608 83% Gray (10YR4/1), slightly moist, hard, clayey SILT with N=51trace sand and gravel. End of Boring = 20.0 ft. BGS

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois

Project:

DATES: Start: 2/12/2010

WEATHER: Overcast, cold ~25F

Finish: 2/12/2010

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill **Drilling Method:** 41/4" HSA w/SS samplers

FIELD STAFF: Driller: T. List Helper: M. Herbst/S. Hamby

Eng/Geo: D. Lamb

BOREHOLE ID: G108 Well ID: G108

Surface Elev: 625.58 ft. MSL **Completion:** 20.00 ft. BGS **Station:** 874,948.81N

2,514,248.25E

HANSON

| SAMPL | E | T | EST | ING | r | TODOCDA | DUIC MAD INFORMATION. | WATER LEVEL INFORMATION | | | |
|--|-------------|----------------------------------|--------------|-------------------|--------------------------|--|---|---|--|--|--|
| Number Recov / Total (in) % Recovery | | | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadrar Townshi | PHIC MAP INFORMATION: ngle: Coffeen, IL p: East Fork 10, Tier 7N; Range 3W | WATER LEVEL INFORMATION: $\underline{\Psi}$ = 14.50 - While drilling $\underline{\Psi}$ = 19.00 - Upon completion $\underline{\nabla}$ = 8.93 - 3/1/2010 | | | |
| Number Recov // % Recov | Type | Blows / 6 in N - Value RQD | Moistu | Dry Do | Qu (ts1 Failur | Depth ft. BGS | Lithologic Description | Borehole Elevation Detail ft. MSL Remarks | | | |
| A 23/24 96% | SS | 24-25 13-13 N=38 | 16 | | | 2 | FILL - Grayish brown (10YR5/2) with 10% yellowish brown (10YR5/6) mottles, moist, hard, silty CLAY wis slight trace gravel. | | | | |
| A 13/24 54% | SS | 4-5 8-11 N=13 | 26 | | | 4- | FILL - Grayish brown (10YR5/2) with 10% yellowish brown (10YR5/6) mottles, moist, stiff, silty CLAY with trace sand and slight trace gravel. | | | | |
| A 20/24 83% | SS | 2-2 5-7 N=7 | 28 | | | 6 | Grayish brown (10YR5/2) with 25% yellowish brown (10YR5/8) and 5% very dark brown (10YR2/2) mottle moist, medium, clayey SILT with trace sand and sligh trace gravel. | s, $ $ | | | |
| 24/24 100% | SS | 2-3 5-6 N=8 | 18 | | | = | | 618 | | | |
| 5A 23/24 96% | SS | 1-2 3-4 N=5 | 20 | | | 8 - 10 - 10 - 10 - 10 - 10 - 10 - 10 - 1 | Gray (10YR5/1) with 10% brownish yellow (10YR6/8 mottles, moist, medium, silty CLAY with trace sand at slight trace gravel. | B) - 616 | | | |
| 5A 24/24 100% | SS | 1-3 3-5 N=6 | 19 | | | 12 — | Grayish brown (10YR5/2) with brownish yellow (10YR6/8) mottles, moist, soft, sandy CLAY with trace | 614 | | | |
| 7A 19/24 79% | SS | 1-1 1-2 N=2 | 19 | | | | gravel. Brownish yellow (10YR6/8), very moist, soft, sandy CLAY with trace gravel. | 612 | | | |
| AA 23/24 96% | SS | 2-4 7-10 N=11 | 19 13 | | | 14 | Brownish yellow (10YR6/8), very moist, soft, sandy SI with trace gravel. Brownish yellow (10YR6/6), wet, medium, SILT. | | | | |
| A 22/24 92% | SS | 10-24 25-10 | 11 | | | 16 — | Light yellowish brown (10YR6/4) with 10% yellowish brown (10YR5/6) mottles, moist, stiff, clayey SILT witrace sand and gravel. | h th | | | |
| 9В | \bigwedge | N=49 | 8 | | | 18 | Gray (10YR5/1), slightly moist, hard, SILT with grave | 608 | | | |
| 0A 24/24 | \bigvee | 10-25 | 10 | | | <u></u> - | Gray (10YR5/1), wet, hard, SILT with grave | - - - - - - - - - | | | |
| 0A 24/24 100% | SS | 40-40 N=65 | 10 | | | <u> </u> | Gray (10YR5/1), very moist, hard, SILT with gravel. | | | | |

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois

Project:

DATES: Start: 2/11/2010

Finish: 2/11/2010
WEATHER: Sunny, cold ~32F

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 4¼" HSA w/SS samplers

FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby

Eng/Geo: D. Lamb

HANSON

BOREHOLE ID: G109 **Well ID:** G109

 Surface Elev:
 624.79 ft. MSL

 Completion:
 18.00 ft. BGS

 Station:
 874,970.10N

 2,514,137.84E

SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: Ξ Quadrangle: Coffeen, IL Ψ = 14.20 - While drilling Dry Den. (lb/ft3 Recov / Total (% Recovery Township: East Fork Moisture (%) Blows / 6 in N - Value RQD Section 10, Tier 7N; Range 3W ∇ = 8.85 - 3/1/2010 Qu (tsf) Failure 1 Number Lithologic Borehole Elevation Description Detail ft. MSL Remarks 624 24/24 7-8 SS 100% N = 141A 22 FILL - Grayish brown (10YR5/2) with 40% yellowish brown (10YR5/6) mottles, moist, stiff, silty CLAY with slight trace gravel. 3-5 622 19/24 5-6 N=102A 27 Light yellowish brown (10YR6/4) with 50% brownish yellow (10YR6/8) mottles, moist, medium, silty CLAY, slight trace roots. 620 20/24 6-8 83% N=113A 24 Light brownish gray (10YR6/2) with 10% brownish yellow 618 24/24 5-6 (10YR6/6) mottles, moist, medium, silty CLAY with slight 100% N=9trace sand and gravel. 19 $\bar{\Delta}$ 22/24 4-5 92% 20 5A Light brownish gray (10YR6/2) with 10% brownish yellow (10YR6/6) and 2% very dark gray (10YR3/1) mottles, 10 moist, medium, silty CLAY with slight trace sand and gravel. 1-3 24/24 614 3-4 100% N=6Ā 19 6A 12 Light brownish gray (10YR6/2) with 30% brownish yellow (10YR6/8) mottles, moist, medium, sandy CLAY with 612 23/24 slight trace gravel. 96% 19 7A **▼** 14 8-15 610 22/24 Brownish yellow (10YR6/6), wet, dense, silty SAND with 15-21 92% trace gravel. N = 308A 14 Brownish yellow (10YR6/8), wet, dense, SAND with trace 12-29 gravel. 608 24/24 SS 44-45 100% N = 739A Grayish brown (10YR5/2), slightly moist, hard, gravelly SILT with sand. End of Boring = 18.0 ft. BGS

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 2/11/2010

Finish: 2/11/2010 WEATHER: Sunny, cold 10-20F CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 4½" HSA w/SS samplers

FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby

Eng/Geo: .

BOREHOLE ID: G110

Well ID: G110

Surface Elev: 624.81 ft. MSL Completion: 18.00 ft. BGS Station: 875,015.42N 2,514,057.73E

SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: (iii Qu (tsf) *Qp* (tsf) Failure Type $\mathbf{V} = 15.00$ - While drilling Dry Den. (lb/ft³) Quadrangle: Coffeen, IL Recov / Total (% Recovery Township: East Fork Moisture (%) Blows / 6 in N - Value RQD Section 10, Tier 7N; Range 3W ∇ = 9.50 - 3/1/2010 Number Lithologic Borehole Elevation ft. BGS Description ft. MSL Remarks 8-6 24/24 624 6-8 100% N = 121 A 17 FILL - Yellowish brown (10YR5/6) with 20% light 2-4 5-7 brownish gray (10YR6/2) mottles, moist, stiff, silty CLAY 14/24 622 25 2A with slight trace sand. 58% N=9620 22/24 5-9 92% 22 3A Grayish brown (10YR5/2) with 20% yellowish brown 3-6 (10YR5/6) and 5% very dark brown (10YR2/2) mottles, 24/24 618 8-9 moist, medium, silty CLAY. 100% N=1418 24/24 616 4-6 Grayish brown (10YR5/2) with 20% yellowish brown 100% ∇ 21 (10YR5/6) and 5% very dark brown (10YR2/2) mottles, 5A moist, medium, silty CLAY with slight trace sand and 10 24/24 4-6 100% N=821 6A Light brownish gray (10YR6/2) with 30% brownish yellow (10YR6/8) mottles, moist, medium, clayey SILT with trace sand and gravel. 24/24 Light brownish gray (10YR6/2) with 30% brownish yellow (10YR6/8) mottles, very moist, medium, sandy CLAY with 3-3 100% 7A 22 trace gravel. Light brownish gray (10YR6/2) with 30% brownish yellow (10YR6/8) mottles, moist, soft, clayey SILT with trace sand and slight trace gravel. 610 19/24 \blacksquare 8A 24 2-1 79% N=4Gray (10YR6/1) with 30% brownish yellow (10YR6/8) mottles, wet, soft, sandy CLAY. 7-26 608 24/24 SS 49-60 Grayish brown (10YR5/2), slightly moist, hard, clayey 100% N=75 9A 6 SILT with trace sand and gravel. End of Boring = 18.0 ft. BGS

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois

Project:

DATES: Start: 2/10/2010

WEATHER: Sunny, breezy ~25F

Finish: 2/11/2010

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: T. List

Eng/Geo: D. Lamb

Helper: M. Herbst/S. Hamby

WATER LEVEL INFORMATION:

BOREHOLE ID: G111

Well ID: G111

Surface Elev: 625.28 ft. MSL

Completion: 18.00 ft. BGS

Station: 875,058.70N

2,513,981.72E

SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: Œ, Quadrangle: Coffeen, IL $\mathbf{Y} = 14.50$ - While drilling Dry Den. (lb/ft3 Recov / Total (% Recovery Township: East Fork **T** = Moisture (%) Blows / 6 in N - Value RQD Section 10, Tier 7N; Range 3W ∇ = 10.50 - 3/1/2010 Qu (tsf) Failure 1 Number Lithologic Borehole Elevation Description ft. MSL Remarks 20/24 6-9 SS 83% 624 N = 131 A 18 FILL - Grayish brown (10YR5/2) with 10% yellowish 13/24 2A 20 brown (10YR5/6) mottles, moist, stiff, silty CLAY with 7-8 54% slight trace sand and gravel. 622 N=1218/24 6-8 75% N=10 620 20 3A Grayish brown (10YR5/2) with 20% yellowish brown (10YR5/6) and 5% dark brown (10YR3/3) mottles, moist, medium, clayey SILT with slight trace sand, slight trace 4-12 16/24 20-17 67% roots. 618 N=3218 Grayish brown (10YR5/2) with 5% yellowish brown (10YR5/6) mottles, moist, medium, clayey SILT with trace 22/24 21 4-5 sand 92% 616 $\bar{\Delta}$ 2-3 24/24 23 6A 6-6 100% 614 N=9Grayish brown (10YR5/2) with 5% yellowish brown (10YR5/6) mottles, moist, stiff, silty CLAY with slight trace sand. 24/24 20 5-6 N=9 100% 612 Gravish brown (10YR5/2) with 30% yellowish brown (10YR5/8) mottles, moist, stiff, clayey SILT with trace 14 sand and gravel. 24/24 17 8A 2-2 100% Yellowish brown (10YR5/8), wet, soft, clayey SAND with N=4 610 trace gravel. 12-50 18/18 Grayish brown (10YR5/2) with 20% brownish yellow 66 9A 100% (10YR6/6) mottles, slightly moist, hard, clayey SILT with N=116608 gravel. 0/6 0% End of Boring = 18.0 ft. BGS

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois

Project:

DATES: Start: 2/9/2010

Finish: 2/9/2010

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby

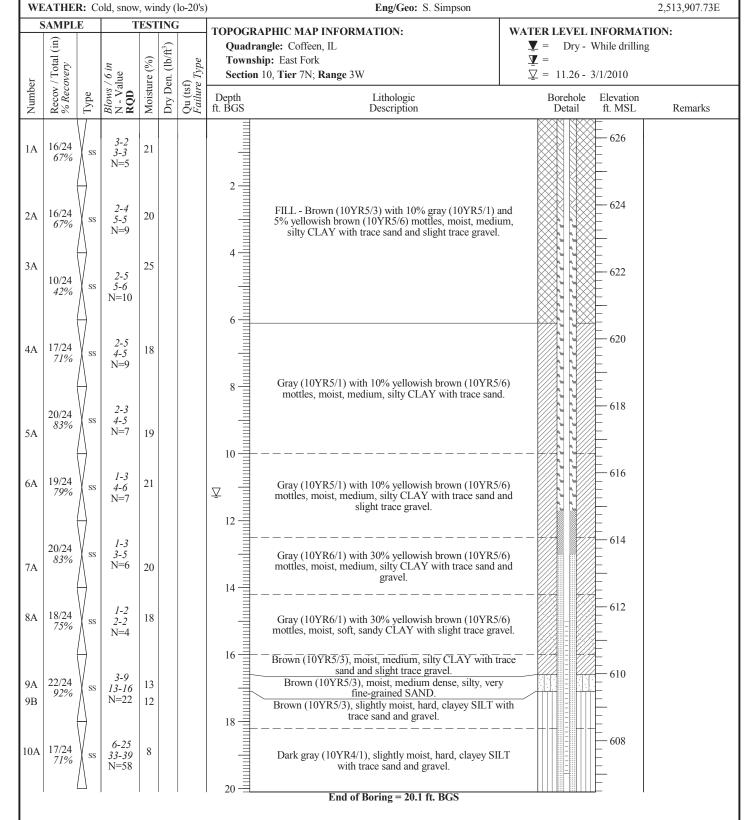
Eng/Geo: S. Simpson

HANSON

BOREHOLE ID: G119 Well ID: G119

> Surface Elev: 626.57 ft. MSL **Completion:** 20.10 ft. BGS **Station:** 875,675.04N

> > 2,513,907.73E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A **DATES: Start: 2/8/2010**

Finish: 2/8/2010

WEATHER: Cold, snow, windy (mid-20's)

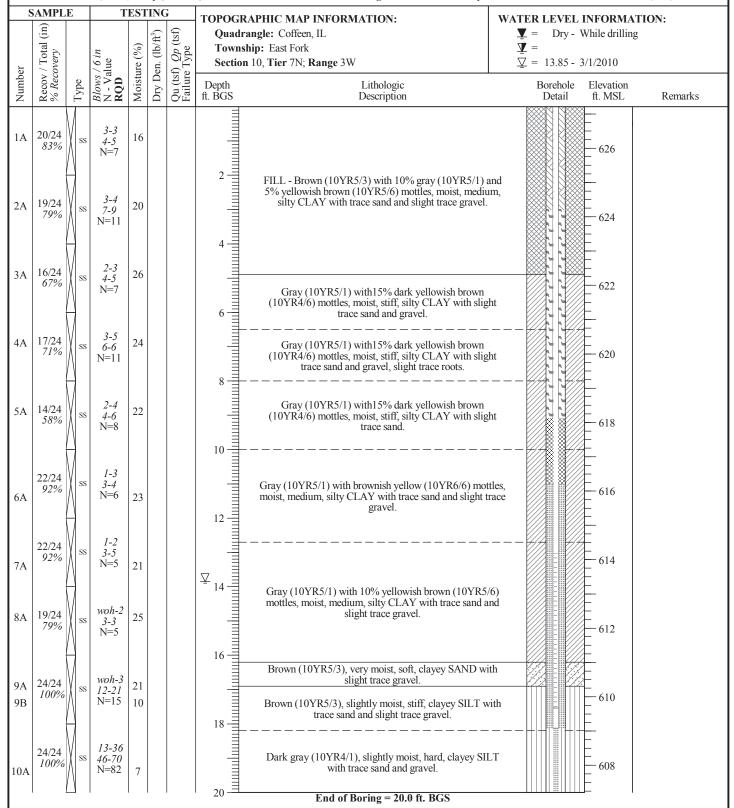
CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill **Drilling Method:** 41/4" HSA w/SS samplers

FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby Eng/Geo: S. Suzanna Simpson

BOREHOLE ID: G120 Well ID: G120

> Surface Elev: 627.21 ft. MSL Completion: 20.00 ft. BGS **Station:** 875,854.43N 2,513,905.84E



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois

Project:

DATES: Start: 2/4/2010

Finish: 2/4/2010 WEATHER: Overcast, cold (lo-30's) CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 4'4" HSA w/SS samplers

FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby

Eng/Geo: S. Simpson

HANSON

BOREHOLE ID: G121 **Well ID:** G121

 Surface Elev:
 627.94 ft. MSL

 Completion:
 22.00 ft. BGS

 Station:
 875,964.59N

2,513,904.35E

| 5 | SAMPL | E | T | EST | ING | ř | TOPOGRA | PHIC MAP INFORMATION: | WATER LEVEL I | NEORMATION: | | | |
|--------|----------------------------------|----------------------------------|----------------------------------|--------------|-------------------|---------------------|--|--|--|--|--|--|--|
| ber | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | tst) tre Type | Quadrar Townshi Section 1 | ngle: Coffeen, IL p: East Fork 0, Tier 7N; Range 3W | $\underline{\underline{V}}$ = Dry - \underline{V} $\underline{\underline{V}}$ = $\underline{\underline{V}}$ = 14.44 - 3 | $\underline{\underline{Y}} = \underline{\underline{Y}} = 14.44 - 3/1/2010$ | | | |
| Number | Reco % Re | Type | Blow N - V RQD | Mois | Dry I | Qu (tsf) Failure | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL Remarks | | | |
| 1A | 22/24 92% | SS | 4-4 7-8 N=11 | 15 | | | 2 | | | | | | |
| 2A | 20/24 83% | SS | 3-5 8-12 N=13 | 16 | | | | FILL - Brown (10YR4/3) with 10% gray (10YR5/1) a 5% dark yellowish brown (10YR4/6) mottles, moist, s silty CLAY with slight trace sand and gravel. | nd iff, | | | | |
| 3A | 18/24 75% | SS | 1-4 5-6 N=9 | 27 | | | | | | - - - - - - | | | |
| | 18/24 | SS | 2-3 5-6 | | | | 6- | Dark yellowish brown (10YR4/4), moist, medium, si CLAY with slight trace sand. | ty | — 622 — | | | |
| 4A | 75% | $\stackrel{\wedge}{\rightarrow}$ | N=8 | 25 | | | 8 | Gray (10YR5/1) with 25% dark yellowish brown (10YR4/6) mottles, moist, medium, clayey SILT with t sand. | race | 620 | | | |
| 5A | 18/24 75% | SS | 2-2 3-4 N=5 | 24 | | | 8 | Gray (10YR6/1) with 10% yellowish brown (10YR5/ | 6) | | | | |
| 6A | 13/24 54% | SS | 2-2 4-4 N=6 | 23 | | | 10 = | mottles, moist, medium, silty CLAY with slight trace s | and. | | | | |
| 7A | 19/24 79% | SS | woh-2 3-4 N=5 | 23 | | | 12 = - | | | — 616 — — | | | |
| 8A | 18/24 75% | SS | 1-2 2-2 N=4 | 23 | | | 14 — □ □ □ □ □ □ □ □ □ □ □ □ □ □ □ □ □ □ | Gray (10YR6/1) with 10% yellowish brown (10YR5/mottles, moist, medium, silty CLAY with trace sand a slight trace gravel. | | 614 | | | |
| | 23/24 | SS | woh-wol | i | | | 16 | Brown, (10YR5/3), very moist, very soft, clayey SAN | ID. | 612 | | | |
| 9A | 96% | | - - | 21 | | | 18 | with slight trace gravel. | | 610 | | | |
| 10A | 22/24 92% | SS | 4-12 26-30 N=38 | 8 | | | 20 | Brown (10YR5/3), slightly moist, hard, very silty CLA with trace sand and gravel. | ΛY | | | | |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois

Project:

DATES: Start: 2/4/2010

WEATHER: Overcast, cold (lo-30's)

Finish: 2/4/2010

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill **Drilling Method:** 4¹/₄" HSA w/SS samplers

FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby

Eng/Geo: S. Simpson

HANSON

BOREHOLE ID: G121 Well ID: G121

> Surface Elev: 627.94 ft. MSL **Completion:** 22.00 ft. BGS **Station:** 875,964.59N

> > 2,513,904.35E

| | SAMPL | E | Т | EST | ING | r | TOPOGRA | PHIC MAP INFORMATION: | WATER LEVEL INFORMATION: | | | |
|--------|----------------|------|------------------------|----------|---------------|---------------------|--------------------|---|--|--|--|--|
| er | / Total (in) | | / 6 in Ilue | ıre (%) | Den. (lb/ft³) | f) e Type | Quadran Townshi | gle: Coffeen, IL p: East Fork 0, Tier 7N; Range 3W | $\underline{\Psi}$ = Dry - While drilling $\underline{\Psi}$ = $\underline{\nabla}$ = 14.44 - 3/1/2010 | | | |
| Number | Recov % Rec | Type | Blows N - Vz RQD | Moisture | Dry D | Qu (tsf) Failure | Depth ft. BGS | Lithologic Description | Borehole Elevation Detail ft. MSL Remarks | | | |
| 11A | 24/24 100% | SS | 13-23 31-48 N=54 | 7 | | | 22 | Dark gray (10YR4/1), slightly moist, hard, clayey SII with sand and gravel. End of Boring = 22.0 ft, BGS | LT 606 | | | |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois

Project:

DATES: Start: 2/4/2010

Finish: 2/4/2010

WEATHER: Overcast, cold (lo-30's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby

Eng/Geo: D. Lamb

BOREHOLE ID: G122 Well ID: G122

> Surface Elev: 628.05 ft. MSL **Completion:** 20.00 ft. BGS **Station:** 876,080.14N 2,513,902.82E

SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: Ξ Quadrangle: Coffeen, IL $\mathbf{Y} = 17.00$ - While drilling Dry Den. (lb/ft3 Recov / Total (% Recovery Township: East Fork **T** = Moisture (%) Blows / 6 in N - Value RQD Section 10, Tier 7N; Range 3W ∇ = 12.84 - 3/1/2010 Qu (tsf) Failure 1 Number Lithologic Borehole Description Remarks 23/24 6-11 96% N=111A 16 FILL - Grayish brown (10YR5/2) with 15% gray 626 (10YR5/1) and 5% yellowish brown (10YR5/6) mottles, moist, stiff, silty CLAY with trace sand and slight trace 20/24 gravel. 5-5 83% 22 2A 624 20/24 5-6 83% 25 3A Dark yellowish brown (10YR4/4), moist, medium, silty 622 19/24 29 4A 5-6 79% N=10620 Gray (10YR5/1) with 20% dark yellowish brown (10YR4/6) mottles, moist, medium, silty CLAY. 20/24 5A 21 3-3 83% N=6618 Grayish brown (10YR5/2), moist, medium, clayey SILT 19/24 22 6A 3-3 79% Yellowish brown (10YR5/6) mottles, moist, medium, silty 616 CLAY with trace gravel. 1-2 ∇ 16/24 7A 21 Gray (10YR5/1), moist, medium, clayey SILT with fine 3-4 67% Brown (10YR4/3), moist, medium, silty CLAY with trace 614 gravel. 19/24 2-2 Grayish brown (10YR5/2), moist, soft, sandy SILT. 79% N=38A 21 Yellowish brown (10YR5/4) with 40% dark yellowish 612 brown (10YR4/6) mottles, moist, medium, silty CLAY with slight trace sand. 20/24 4-16 83% N=59A 14 Dark yellowish brown (10YR4/6), wet, medium dense, 18 silty SAND. 610 10-38 24/24 6 51-58 Brownish yellow (10YR6/6), slightly moist, hard, clayey 100% N=89 SILT with trace sand and gravel. Gray (10YR5/1), slightly moist, hard, clayey SILT with gravel End of Boring = 20.0 ft. BGS

NOTE(S): Well completed prior to construction of berm road. Boring surface elevation is as of the well install date and not the final constructed elevation.

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois

Project:

DATES: Start: 2/3/2010

Finish: 2/4/2010

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill **Drilling Method:** 41/4" HSA w/SS samplers

FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby

Eng/Geo: D. Lamb

HANSON

BOREHOLE ID: G123 Well ID: G123

Surface Elev: 628.12 ft. MSL **Completion:** 24.00 ft. BGS **Station:** 876,189.60N

2.513.901.46E

WEATHER: Overcast, cold (lo-30's) **SAMPLE** TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: Ξ Quadrangle: Coffeen, IL $\mathbf{Y} = 16.50$ - While drilling Dry Den. (lb/ft3 Recov / Total (% Recovery Township: East Fork **T** = Moisture (%) Blows / 6 in N - Value RQD Section 10, Tier 7N; Range 3W ∇ = 15.98 - 3/1/2010 Qu (tsf) Failure 1 Number Elevation Lithologic Borehole ft. BGS Description ft. MSL Remarks 628 6-8 22/24 9-11 SS 92% N = 171 A 16 FILL - Grayish brown (10YR5/2) with 10% gray 626 (10YR5/1) and 5% yellowish brown (10YR5/6) mottles, moist, stiff, silty CLAY with trace sand and slight trace 19/24 2A 18 6-7 gravel. N=11624 17/24 3A 24 5-6 71% N=8Dark grayish brown (10YR4/2) with 20% yellowish brown (10YR5/6) mottles, moist, medium, silty CLAY with slight trace sand, slight trace roots. 622 18/24 24 5-8 Gray (10YR5/1) with 30% yellowish brown (10YR5/6) 75% mottles, moist, medium, silty CLAY with slight trace sand. N=8620 20/24 4-5 83% 18 5A Gray (10YR5/1) with 10% yellowish brown (10YR5/6) mottles, moist, medium, silty CLAY with trace sand and 618 slight trace gravel. 19/24 3-5 21 6A 79% Gray (10YR5/1) with 10% yellowish brown (10YR5/6) mottles, moist, medium, silty CLAY with sand and slight 23/24 trace gravel. 96% 19 7A Dark yellowish brown (10YR3/6) with dark yellowish 614 brown (10YR4/6) mottles, moist, medium, silty CLAY with trace gravel. 1-2 22/24 3-3 92% N=58A 17 Gray (10YR6/1) with 30% yellowish brown (10YR5/6) ⊻ 16 mottles, moist, medium, sandy SILT. 612 ▼ 22/24 Dark yellowish brown (10YR4/6), wet, soft, clayey SAND. 9A 19 610 3-3 10A 12/2416 Yellowish brown (10YR5/6), wet, medium, sandy SILT 3-4 SS 50% with trace gravel. N=620 NOTE(S): Well completed prior to construction of berm road. Boring surface elevation is as of the well install date and not the final constructed elevation.

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois

Project:

DATES: Start: 2/3/2010

Finish: 2/4/2010

WEATHER: Overcast, cold (lo-30's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby

Eng/Geo: D. Lamb



BOREHOLE ID: G123 Well ID: G123

Surface Elev: 628.12 ft. MSL **Completion:** 24.00 ft. BGS **Station:** 876,189.60N

2,513,901.46E

| | SAMPL | E | TESTING | | | | TOPOGRAPHIC MAP INFORMATION: | | WATER LEVEL INFORMATION: | |
|--------|----------------------------|------|------------------------|----------|---------------|---------------------|---|--|--|------------------------------|
| l l | / Total (in) | | alue | ıre (%) | Den. (lb/ft³) | f) e Type | Quadrangle: Coffeen, IL Township: East Fork Section 10, Tier 7N; Range 3W | | $ \mathbf{V} = 16.50 $ - While drilling $ \mathbf{V} = \mathbf{V} = 15.98 - 3/1/2010 $ | |
| Number | Recov / Tota % Recovery | Type | Blows N - Va RQD | Moisture | Dry D | Qu (tsf) Failure | Depth ft. BGS | Lithologic Description | | Elevation ft. MSL Remarks |
| 11A | 20/24 83% | SS | 6-12 12-12 N=24 | 11 | | | 22 | Yellowish brown (10YR5/6), wet, medium, sandy SII with trace gravel. [Continued from previous page] Gray (10YR5/1), moist, very stiff, clayey SILT with tragravel. | | -608 |
| 12A | 19/24 79% | SS | 3-8 13-9 N=21 | 9 | | | 24 | Dark gray (10YR4/1), moist, very stiff, sandy SILT w trace clay and gravel. End of Boring = 24.0 ft. BGS | | |

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois

Project:

DATES: Start: 2/3/2010

Finish: 2/3/2010 WEATHER: Sunny, cold (mid-30's) CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 4'/" HSA w/SS samplers

Drilling Method: 4¹/₄" HSA w/SS sar

FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby

Eng/Geo: S. Simpson

HANSON

BOREHOLE ID: G124 **Well ID:** G124

 Surface Elev:
 628.70 ft. MSL

 Completion:
 20.00 ft. BGS

 Station:
 876,304.85N

 2,513,900.34E

SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: Ξ Quadrangle: Coffeen, IL ▼ = Dry - While drilling Dry Den. (lb/ft3 Recov / Total (% Recovery Township: East Fork **T** = Moisture (%) Blows / 6 in N - Value RQD Section 10, Tier 7N; Range 3W ∇ = 10.99 - 3/1/2010 Qu (tsf) Failure 1 Number Lithologic Borehole Description ft. MSL Remarks 628 24/24 5-6 100% N=917 1A FILL - Brown (10YR5/3) with 10% gray (10YR5/1) and 5% yellowish brown (10YR5/6) mottles, moist, stiff, silty 626 22/24 2A 21 CLAY with slight trace sand and gravel. 7-8 92% N=12 2-4 6-7 624 19/24 79% N=1025 3A Dark grayish brown (10YR4/2) with 5% yellowish brown (10YR5/6) mottles, moist, stiff, silty CLAY. 4A 28 3-3 Dark grayish brown (10YR4/2) with 5% yellowish brown 622 13/24 6-6 (10YR5/6) mottles, moist, stiff, silty CLAY, slight trace 54% N=9 Gray (10YR5/1) with 15% yellowish brown (10YR5/6) 620 20/24 5-6 mottles, moist, medium, silty CLAY with slight trace sand 83% N=821 and gravel. 5A 10 618 17/24 22 $\overline{\Delta}$ 6A 3-4 71% N=6 Gray (10YR5/1) with 15% yellowish brown (10YR5/6) mottles, moist, medium, silty CLAY with trace sand and 1-3 616 18/24 slight trace gravel. 7A 23 3-4 75% N=6woh-woi 614 20/24 28 8A 2-3 83% Gray (10YR5/1) with 30% yellowish brown (10YR5/6) mottles, moist, very soft, silty CLAY with trace sand and 8B22 slight trace gravel. Gray (10YR6/1) with 5% yellowish brown (10YR5/6) 612 mottles, moist, medium, sandy CLAY with slight trace 19/24 9A 22 3-3 79% gravel 9B N=5Gray (10YR6/1) with 20% yellowish brown (10YR5/6) 17 mottles, moist, medium, sandy CLAY with slight trace 18 gravel Yellowish brown (10YR5/4), moist, medium, clayey SILT with trace sand and slight trace gravel. 4-10 610 20/24 17-23 Yellowish brown (10YR5/4), slightly moist, stiff, clayey 83% N=2710A 12 SILT with trace sand and slight trace gravel. Gray (10YR5/1), slightly moist, stiff, clayey SILT with trace sand and slight trace grave End of Boring = 20.0 ft. BGS

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 2/2/2010 **Finish:** 2/3/2010

WEATHER: Sunny, cold (mid-30's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 41/4" HSA w/SS samplers

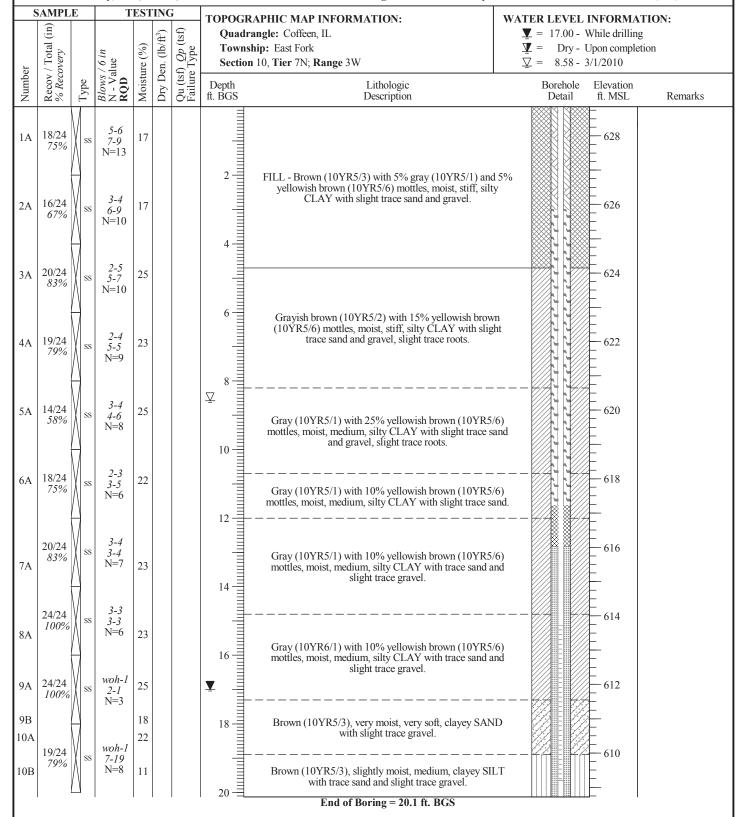
FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby **Eng/Geo:** S. Suzanna Simpson

HANSON

BOREHOLE ID: G125 Well ID: G125

> Surface Elev: 628.85 ft. MSL Completion: 20.13 ft. BGS Station: 876,409.47N 2,513,899.12E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois

Project:

DATES: Start: 2/10/2010

Finish: 2/10/2010

WEATHER: Partly cloudy, wind 10 mph, ~25F

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: T. List

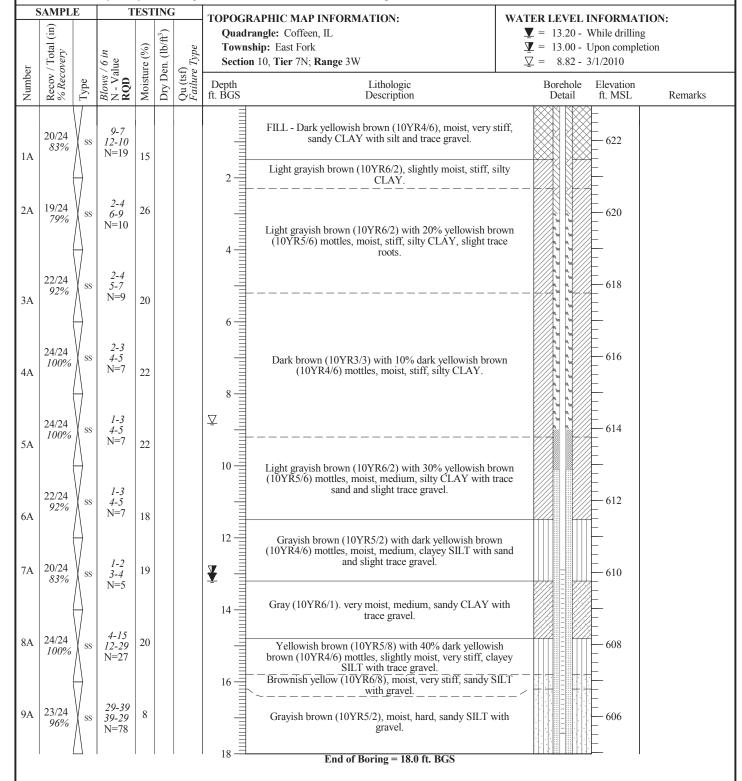
Helper: M. Herbst/S. Hamby

Eng/Geo: D. Lamb

BOREHOLE ID: G126 Well ID: G126

> Surface Elev: 622.96 ft. MSL Completion: 18.00 ft. BGS **Station:** 875,062.44N

> > 2,513,895.37E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 12/19/2011 **Finish:** 12/19/2011

WEATHER: Cloudy, rain (mid-60's)

CONTRACTOR: Testing Service Corp.
Rig mfg/model: CME-550 ATV Drill
Drilling Method: 4½" HSA w/SS samplers

FIELD STAFF: Driller: B. Williamson Helper: R. McCuan

Eng/Geo: R. Fiorito



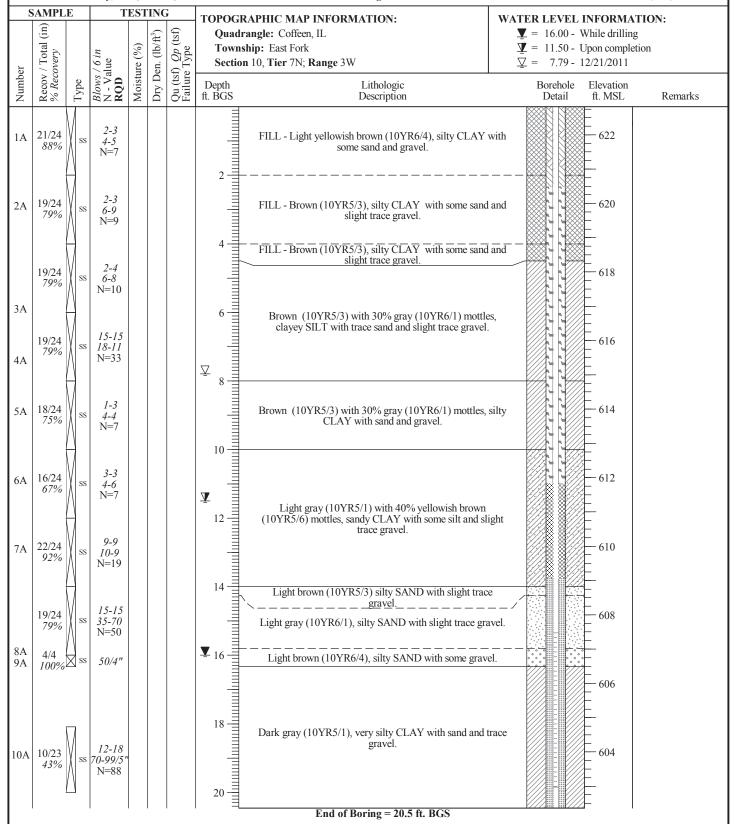
BOREHOLE ID: G151 **Well ID:** G151

 Surface Elev:
 622.82 ft. MSL

 Completion:
 20.46 ft. BGS

 Station:
 875,023.67N

 2,513,805.93E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 12/20/2011 **Finish:** 12/20/2011

WEATHER: Cloudy, (mid-40's), rainy later.

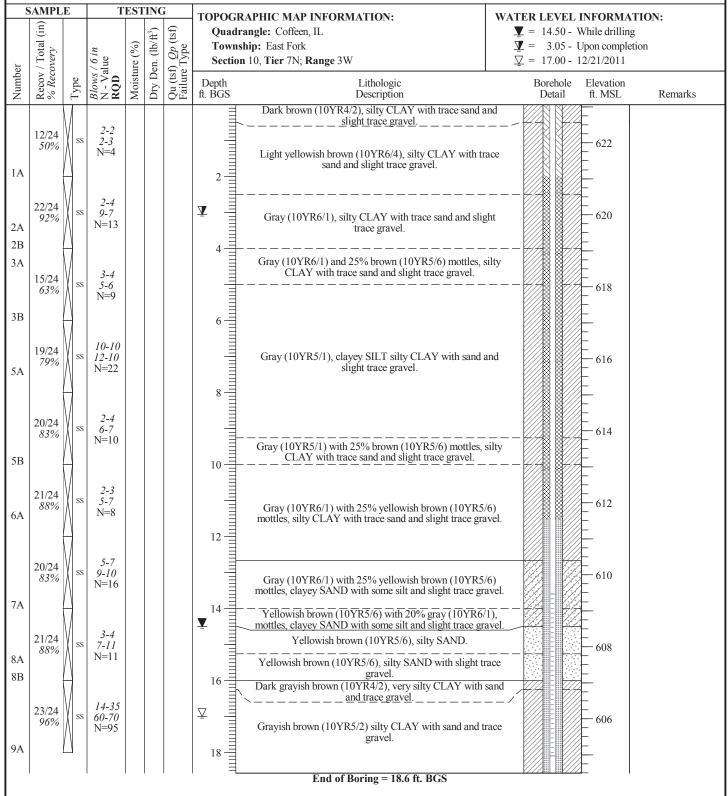
CONTRACTOR: Testing Service Corp.
Rig mfg/model: CME-550 ATV Drill
Drilling Method: 4½" HSA w/SS samplers

FIELD STAFF: Driller: B. Williamson Helper: R. McCuan

Eng/Geo: R. Fiorito

BOREHOLE ID: G152 **Well ID:** G152

Surface Elev: 623.06 ft. MSL Completion: 18.57 ft. BGS Station: 874,687.53N 2,513,894.46E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

SAMPLE

DATES: Start: 12/15/2011 Finish: 12/15/2011

WEATHER: Cloudy, windy, (mid-high 30's)

TESTING

CONTRACTOR: Testing Service Corp. Rig mfg/model: CME-550 ATV Drill **Drilling Method:** 41/4" HSA w/SS samplers

FIELD STAFF: Driller: B. Williamson Helper: R. McCuan

TOPOGRAPHIC MAP INFORMATION:

Eng/Geo: R. Fiorito

2,513,532.68E WATER LEVEL INFORMATION:

> $\mathbf{V} = 16.00$ - While drilling $\mathbf{V} = 15.70$ - Upon completion

BOREHOLE ID: G153

Well ID: G153

Surface Elev: 623.30 ft. MSL

Completion: 20.76 ft. BGS

Station: 874,532.71N

Œ) Qu (tsf) *Qp* (tsf) Failure Type Dry Den. (lb/ft³) Quadrangle: Coffeen, IL Recov / Total (% Recovery Moisture (%) Township: East Fork Blows / 6 in N - Value RQD Section 10, Tier 7N; Range 3W ∇ = 17.55 - 12/21/2011 Number Lithologic Borehole Elevation ft. BGS Description Detail ft. MSL Remarks FILL - Light yellowish brown (10YR6/4), silty CLAY with sand and slight trace gravel. 16/24 1A SS 67% 622 1B FILL - Gray (10YR6/1), silty CLAY with sand and slight trace gravel. woh-3 17/24 4-6 71% N=7620 2A Gray (10YR6/1) with 50% brownish yellow (10YR6/8) mottles, silty CLAY with trace sand. 18/24 3A 5-5 75% 618 4-5 21/24 4A 6-8 Gray (10YR5/1), silty CLAY with trace sand. 88% N=11616 20/24 4-5 83% N=85A Gray (10YR6/1), silty CLAY with sand and slight trace gravel. Gray (10YR6/1), silty CLAY with sand and slight trace gravel. 1-4 20/24 4-6 83% Gray (10YR6/1) with 50% brownish yellow (10YR6/8) N=8612 mottles, silty CLAY with sand and slight trace gravel. 6A 23/24 Gray (10YR6/1) with 25% brownish yellow (10YR6/8) 6-15 96% mottles, clayey SAND with trace silt. N=12610 7A 15-23 19/24 84 37-50 79% 608 N = 60Yellowish brown (10YR5/8), silty SAND with slight trace 9/12 9A 50-99 606 ∇ Brownish yellow (10YR6/8), silty CLAY with sand and trace gravel. 18 23-50 20/24 58-109 83% Dark gray (10YR4/1), silty CLAY with sand and trace N=108604 gravel. 20 11A End of Boring = 20.8 ft. BGS

NOTE(S): G153 installed in borehole.

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 12/16/2011

Finish: 12/16/2011 **WEATHER:** Ptly. cloudy (mid-30's)

CONTRACTOR: Testing Service Corp.

Rig mfg/model: CME-550 ATV Drill

Drilling Method: 4½" HSA w/SS samplers

FIELD STAFF: Driller: B. Williamson Helper: R. McCuan

Eng/Geo: R. Fiorito

HANSON

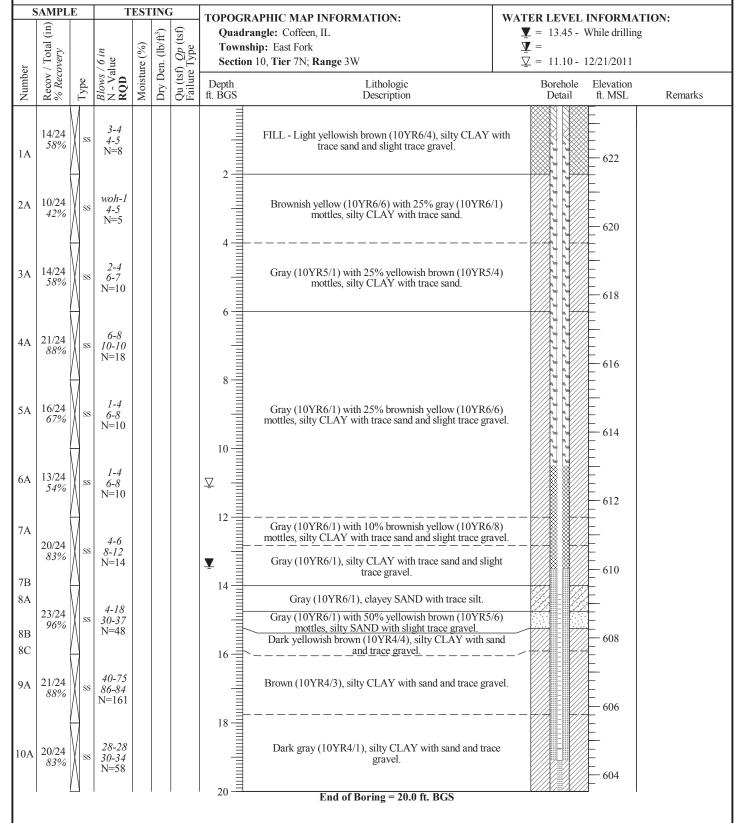
BOREHOLE ID: G154 **Well ID:** G154

 Surface Elev:
 623.52 ft. MSL

 Completion:
 20.00 ft. BGS

 Station:
 874,978.38N

 2.513.243.10E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

SAMPLE

(iii

DATES: Start: 12/19/2011 Finish: 12/19/2011

WEATHER: Cloudy, rainy, (mid-40's)

TESTING

CONTRACTOR: Testing Service Corp. Rig mfg/model: CME-550 ATV Drill **Drilling Method:** 41/4" HSA w/SS samplers

FIELD STAFF: Driller: B. Williamson Helper: R. McCuan

Eng/Geo: R. Fiorito

2,513,501.75E

BOREHOLE ID: G155

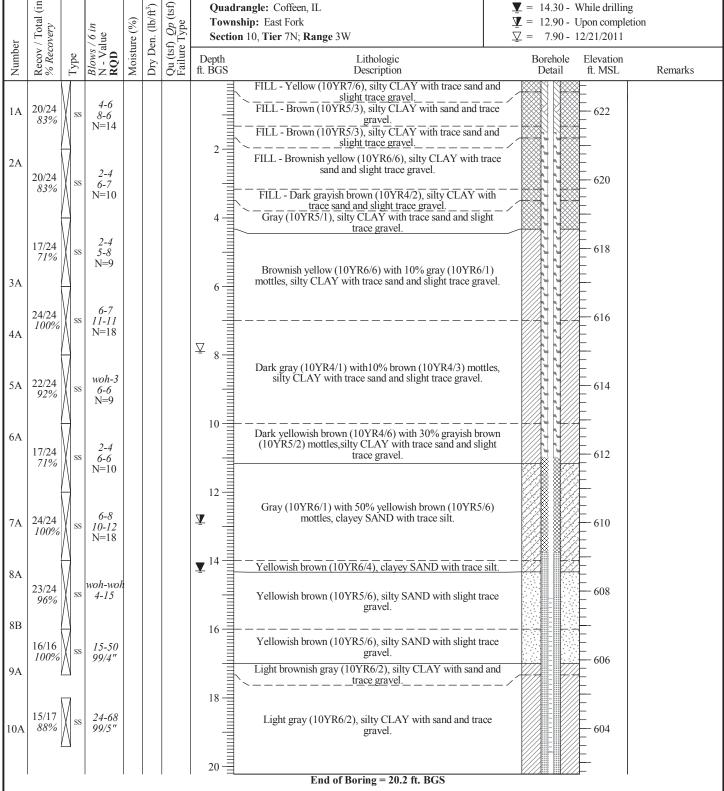
Well ID: G155

Surface Elev: 622.89 ft. MSL

Completion: 20.23 ft. BGS

Station: 875,127.65N

TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: Quadrangle: Coffeen, IL $\mathbf{V} = 14.30$ - While drilling Township: East Fork $\mathbf{V} = 12.90$ - Upon completion Section 10, Tier 7N; Range 3W ∇ = 7.90 - 12/21/2011



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 2/25/2008 **Finish:** 2/25/2008

WEATHER: Overcast, cold

CONTRACTOR: Testing Service Corp. **Rig mfg/model:** CME-650 Track Drill

Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

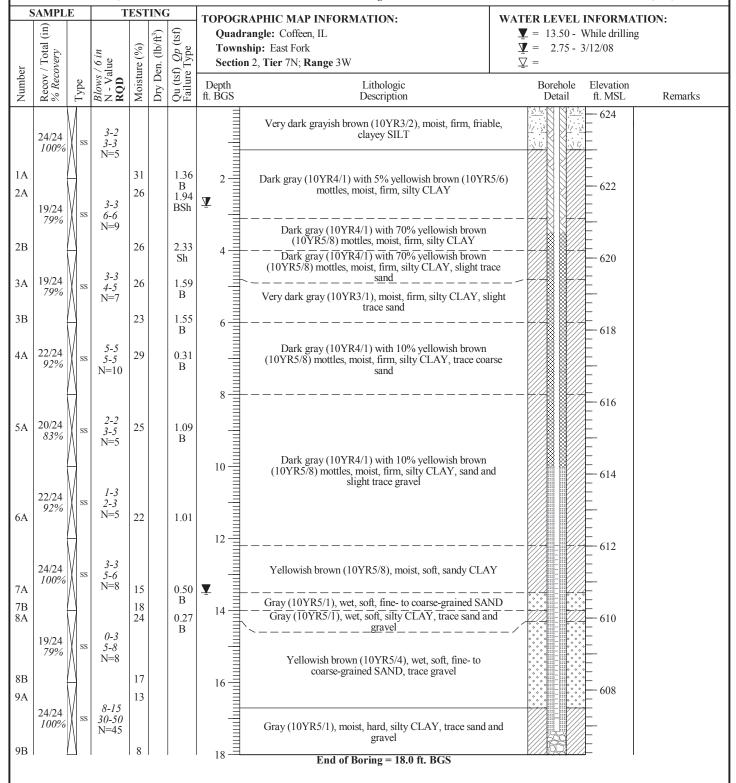
Eng/Geo: .

HANSO

BOREHOLE ID: G200 **Well ID:** G200

Surface Elev: 624.20 ft. MSL Completion: 18.00 ft. BGS Station: 877.930.59N

2,515,649.96E



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A DATES: Start: 2/25/2008

Finish: 2/25/2008
WEATHER: Overcast, cold

CONTRACTOR: Testing Service Corp. **Rig mfg/model:** CME-650 Track Drill

Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: .



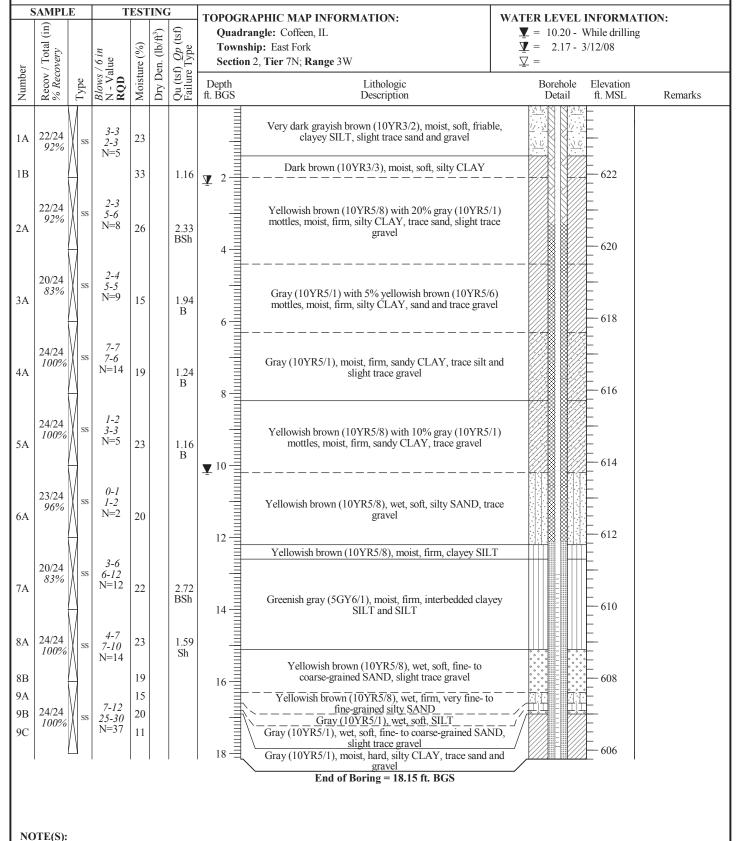
BOREHOLE ID: G201 **Well ID:** G201

 Surface Elev:
 623.90 ft. MSL

 Completion:
 18.15 ft. BGS

 Station:
 877,924.94N

 2.514,849.47E



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 2/21/2008 **Finish:** 2/21/2008

WEATHER: Overcast, cold

CONTRACTOR: Testing Service Corp.
Rig mfg/model: CME-650 Track Drill

Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: .

BOREHOLE ID: G205

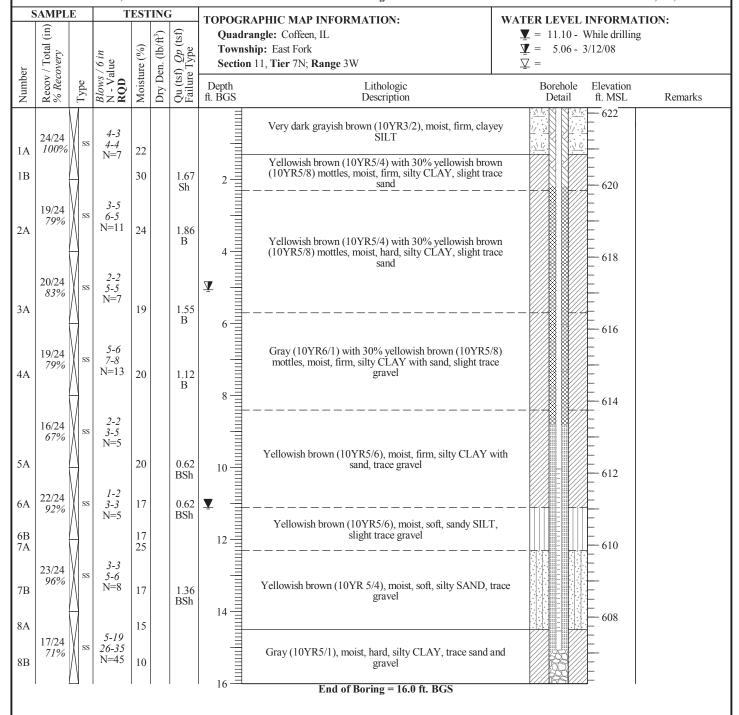
Well ID: G205

 Surface Elev:
 622.15 ft. MSL

 Completion:
 16.00 ft. BGS

 Station:
 875,550.19N

 2,515,914.87E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/14/2010

Finish: 10/14/2010

WEATHER: Sunny, warm, breezy (lo-70's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .

HANSON PARENCE ID. COOK

BOREHOLE ID: G206 **Well ID:** G206

Surface Elev: 630.54 ft. MSL Completion: 24.00 ft. BGS Station: 875,103.91N 2,514,669.16E

| | MPLI | | Т | EST | ING | | TOPOGRAPHIC MAP INFORMATION: | WATER LEVEL INFORMATION: | | | |
|-------------------|-------------|------|----------------------------------|--------------|-------------------|--|---|---|--|--|--|
| v / Total (in) | % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) <i>Qp</i> (tsf) Failure Type | Quadrangle: Coffeen, IL Township: East Fork Section 11, Tier 7N; Range 3W | $\underline{\underline{\mathbf{Y}}}$ = 22.00 - While drilling $\underline{\underline{\mathbf{Y}}}$ = 21.54 - Upon completion $\underline{\underline{\nabla}}$ = | | | |
| Number Recov / | % Re | Type | Blow. N - V RQD | Mois | Dry I | Qu (t Failu | Depth Lithologic ft. BGS Description | Borehole Elevation Detail ft. MSL Remark | | | |
| 1A 12 5 | 2/24 | ss | 2-2 3-2 N=5 | 18 | | | FILL - Grayish brown (10YR5/2), moist, firm, silty of with trace sand and gravel. FILL - Dark gray (10YR4/1) with 30% dark yellow brown (10YR4/6) mottles, moist, firm, silty CLAY trace sand and gravel. Very dark gray (10YR3/1) with 20% dark yellowish (10YR4/6) mottles, moist, firm, silty CLAY with trace sand, trace roots. Dark grayish brown (10YR4/2) with 35% dark yellow brown (10YR4/6) mottles, moist, firm, silty CLAY trace sand. Gray (10YR5/1) with 20% dark yellowish brown (10YR4/6) mottles, moist, firm, clayey SILT with the sand and gravel. Gray (10YR5/1) with 15% dark yellowish brown (10YR4/6) mottles, moist, firm, silty CLAY with trace sand. | CLAY = 630 | | | |
| 2A 20 8 | 0/24 | ss | 2-2 3-5 N=5 | 16 | | | 4 | 628 | | | |
| 3A 20 8 | 0/24 | SS | 4-9 6-8 N=15 | 19 | | | FILL - Dark gray (10YR4/1) with 30% dark yellov brown (10YR4/6) mottles, moist, firm, silty CLAY trace sand and gravel. | | | | |
| 4A 19 | 9/24 | ss | 2-4 5-6 N=9 | 20 | | | | 624 | | | |
| 5A 17 | 7/24 71% | ss | 2-3 4-5 N=7 | 30 | | | Very dark gray (10YR3/1) with 20% dark yellowish (10YR4/6) mottles, moist, firm, silty CLAY with the sand, trace roots. Dark grayish brown (10YR4/2) with 35% dark yellow brown (10YR4/6) mottles, moist, firm, silty CLAY trace sand. | race 622 | | | |
| | 2/24 | ss | 2-3 4-6 N=7 | 19 | | | Gray (10YR5/1) with 20% dark yellowish brow (10YR4/6) mottles, moist, firm, clayey SILT with t sand and gravel. | | | | |
| 7A 23 9 | 3/24 96% | ss | 1-2 3-4 N=5 | 23 | | | Gray (10YR5/1) with 15% dark yellowish brow (10YR4/6) mottles, moist, firm, silty CLAY with trac and gravel. | | | | |
| | 2/24 | ss | 1-1 3-3 N=4 | 22 | | | Gray (10YR5/1) with 15% dark yellowish brow (10YR4/6) mottles, moist, soft, silty CLAY with trac and gravel. | e sand | | | |
| | 4/24 00% | ss | 1-1 2-2 N=3 | 21 | | | Dark yellowish brown (10YR4/6) with 30% gravel. Gray (10YR5/1) with 15% dark yellowish brown (10YR4/6) mottles, moist, soft, silty CLAY with trace and gravel. Gray (10YR5/1) with 15% dark yellowish brown (10YR4/6) mottles, moist, soft, silty CLAY with trace and gravel. Gray (10YR5/1) with 15% dark yellowish brown (10YR4/6) mottles, moist, very soft, silty CLAY with sand and gravel. Gray (10YR5/1) with 15% dark yellowish brown (10YR4/6) mottles, moist, very soft, silty CLAY with sand and gravel. | e sand 614 n e sand | | | |
| 10A 24 | 4/24 00% | ss | woh-wol 1-5 | 25 | | | Gray (10YR5/1) with 15% dark yellowish brow (10YR4/6) mottles, moist, very soft, silty CLAY with sand and gravel. Gray (10YR5/1), moist, very soft, very fine- to fine-g sandy CLAY with trace gravel. | n trace 612 | | | |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

SAMPLE

DATES: Start: 10/14/2010

Finish: 10/14/2010

WEATHER: Sunny, warm, breezy (lo-70's)

TESTING

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill **Drilling Method:** 41/4" HSA w/SS samplers

FIELD STAFF: Driller: D. Mahurin

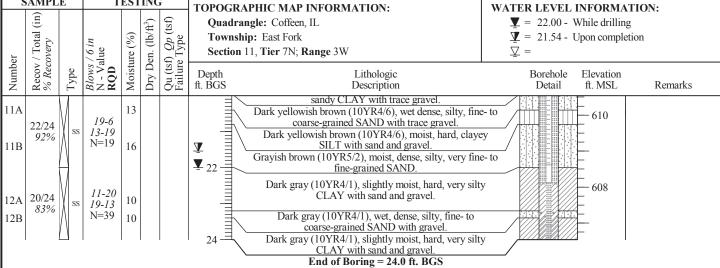
Helper: J. Litsch/D. Smail Eng/Geo: .

HANSON

BOREHOLE ID: G206 Well ID: G206

> Surface Elev: 630.54 ft. MSL Completion: 24.00 ft. BGS **Station:** 875,103.91N 2,514,669.16E

WATER LEVEL INFORMATION:



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

DATES: Start: 10/8/2010

Finish: 10/8/2010 WEATHER: Sunny, mild

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill **Drilling Method:** 41/4" HSA w/SS samplers

FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: G207 Well ID: G207

> Surface Elev: 630.61 ft. MSL **Completion:** 24.00 ft. BGS **Station:** 875,166.36N 2,514,837.94E

| SAMPI | Æ | T | EST | INC | | TOPOGR | APHIC MAP INFORMATION: | WATER | LEVEL | INFORMAT | ION: |
|--|------|----------------------------------|--------------|-------------------|--|--|---|--|--|-----------------------------------|---------|
| Recov / Total (in) % Recovery | | / 6 in lue | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) <i>Qp</i> (tsf) Failure Type | Quadra Townsl | angle: Coffeen, IL hip: East Fork 11, Tier 7N; Range 3W | $\bar{\Lambda} = \bar{\Lambda} = $ | Dry - ' | While drilling Upon completion | |
| Number Recov / / / / / / / / / / / / / / / / / / / | Type | Blows / 6 in N - Value RQD | Moistu | Dry De | Qu (tsf Failure | Depth ft. BGS | Lithologic Description | I | Borehole Detail | Elevation ft. MSL | Remarks |
| 23/24 96% | ss | 6-5 5-8 N=10 | 15 | | | 2 | FILL - Yellowish brown (10YR5/6) with 10% gray (10YR6/1) and 5% black (10YR2/1) mottles, slightl moist, hard, silty CLAY with trace sand and slight tra gravel. | у 🛞 | | 630 | |
| 24/24 100% | ss | 4-4 7-8 N=11 | 15 | | | | FILL - Gray (10YR5/1) with 20% yellowish brown (10YR5/8) mottles, moist, hard, silty CLAY with sand trace gravel | and | | 628 | |
| 23/24 96% | ss | 3-6 7-9 N=13 | 17 | | | 4 | FILL - Yellowish brown (10YR5/8) with 20% gray (10YR6/1) mottles, moist, hard, silty CLAY with sand trace gravel. | and | | 626 | |
| 4A 24/24 100% | ss | 3-4 6-7 N=10 | 16 | | | | FILL - Dark yellowish brown (10YR4/4), moist, hard, CLAY with slight trace sand and gravel. FILL - Gray (10YR5/1) with 20% yellowish brown (10YR5/8) mottles, moist, hard, silty CLAY with slig trace sand and gravel. | | 7, | 624 | |
| 5A 24/24 100% | ss | 2-2 3-4 N=5 | 22 | | | | Yellowish brown (10YR5/6) with 25% gray (10YR5/mottles, moist, firm, silty CLAY with slight trace sand gravel. Gray (10YR5/1) with 15% yellowish brown (10YR5/1) | and (8) $-$ | | 622 | |
| 5B 22/24 92% | ss | 2-2 2-5 N=4 | 27 | | | 8 10 10 11 11 11 11 11 11 11 11 11 11 11 | mottles, moist, firm, silty CLAY with slight trace sand gravel. Gray (10YR5/1) with 40% yellowish brown (10YR5, mottles, very moist, firm, silty CLAY with slight trace sand gravel. | (8) | (7,7,7,7,7,7,7,7,7,7,7,7,7,7,7,7,7,7,7, | 620 | |
| 7A 24/24 100% | ss | 2-2 2-3 N=4 | 27 | | | 12 | Yellowish brown (10YR5/8) with 30% gray (10YR6/mottles, very moist, soft, silty CLAY with trace sand a gravel. | (1) nd | 7,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1 | 618 | |
| 3A 24/24 100% | ss | woh-1 2-3 N=3 | 25 | | | | Gray (10YR6/1) with 30% yellowish brown (10YR5/mottles, very moist, soft, silty CLAY with sand and sli | (8) | | 616 | |
| 9A 23/24 96% | ss | woh-2 2-3 N=4 | 22 | | | 16 = | Yellowish brown (10YR5/6) with 25% gray (10YR6/mottles, very moist, very soft, sandy, silty CLAY with t gravel. | (1) race | | 614 | |
| 0A 24/24 100% | ss | woh-woh 2-3 | 19 | | | 20 | Yellowish brown (10YR5/6) with 30% gray (10YR6/mottles, very moist, very soft, sandy CLAY with silt a trace gravel. | (1) nd | | 612 | |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/8/2010 **Finish:** 10/8/2010

WEATHER: Sunny, mild

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 41/4" HSA w/SS samplers

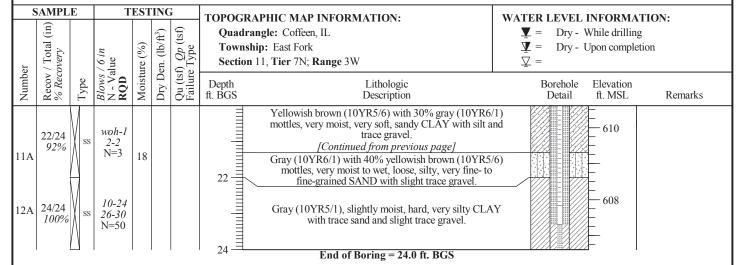
FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: G207 **Well ID:** G207

> Surface Elev: 630.61 ft. MSL Completion: 24.00 ft. BGS Station: 875,166.36N 2.514.837.94E



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/7/2010 **Finish:** 10/7/2010

WEATHER: Sunny, warm (lo-70's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .



BOREHOLE ID: G208 **Well ID:** G208

 Surface Elev:
 630.57 ft. MSL

 Completion:
 24.00 ft. BGS

 Station:
 875,231.46N

 2,514,993.57E

| | SAMPL | Ξ | T | EST | ING | | TOPOGRAPHIC MAP INFORMATION: | WATER LEVEL INFORMATION: |
|-----------|----------------------------------|------|----------------------------------|--------------|-------------------|-------------------------------------|---|--|
| 151 | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Qp (tsf) Failure Type | Quadrangle: Coffeen, IL Township: East Fork Section 11, Tier 7N; Range 3W | $ \mathbf{\underline{\Psi}} = \text{Dry - While drilling} $ $ \mathbf{\underline{\Psi}} = 23.92 - \text{Upon completion} $ $ \mathbf{\underline{\nabla}} = $ |
| IMITITION | Recov % Re | Type | Blows N - V RQD | Moist | Dry L | Qu (ts Failur | Depth Lithologic ft. BGS Description | Borehole Elevation Detail ft. MSL Remarks |
| A | 19/24 79% | ss | 4-3 3-5 N=6 | 23 | | | FILL - Brown (10YR4/3) with 5% dark gray (10Y and 5% dark yellowish brown (10YR4/6) mottles, firm, silty CLAY with trace sand and gravel. | moist, |
| A | 24/24 100% | ss | 2-3 4-6 N=7 | 14 | | | FILL - Brown (10YR4/3) with 15% dark gray (10' and 5% dark yellowish brown (10YR4/6) mottles, firm, silty CLAY with trace sand and gravel. Very dark gray (10YR3/1), moist, firm, silty CLAY trace sand and gravel, trace roots. Dark gray (10YR4/1) with 10% dark yellowish b (10YR4/6) mottles, moist, firm, silty CLAY with sand, trace roots. Dark gray (10YR4/1) with 15% dark yellowish b (10YR4/6) mottles, moist, firm, silty CLAY with sand, trace roots. | 628 |
| A | 24/24 100% | ss | 2-4 4-7 N=8 | 21 | | | FILL - Brown (10YR4/3) with 15% dark gray (10' and 5% dark yellowish brown (10YR4/6) mottles, firm, silty CLAY with trace sand and gravel. | moist, |
| A | 24/24 100% | ss | 2-4 6-8 N=10 | 17 | | | 8 = 8 | 624 |
| A | 20/24 83% | ss | 2-2 4-5 N=6 | 24 | | | Very dark gray (10YR3/1), moist, firm, silty CLA' trace sand and gravel, trace roots. Dark gray (10YR4/1) with 10% dark yellowish b (10YR4/6) mottles, moist, firm, silty CLAY with sand, trace roots. | rown |
| A | 23/24 96% | ss | 1-2 4-4 N=6 | 26 | | | Dark gray (10YR4/1) with 15% dark yellowish b (10YR4/6) mottles, moist, firm, silty CLAY with sand, trace roots. | rown trace 620 |
| A | 19/24 79% | ss | 1-2 2-3 N=4 | 23 | | | Dark gray (10YR4/1) with 15% dark yellowish b (10YR4/6) mottles, moist, soft, silty CLAY with tra | rown ce sand. |
| A | 22/24 92% | ss | 1-1 2-3 N=3 | 24 | | | trace roots. | |
| Α | 24/24 100% | SS | 1-1 2-3 N=3 | 24 | | | Dark gray (10YR4/1) with 15% dark yellowish be (10YR4/6) mottles, moist, soft, silty CLAY with training and gravel, trace roots. Gray (10YR5/1) with 20% dark yellowish brown (10YR4/6) mottles, very moist, soft, silty, very find fine-grained sandy CLAY with trace gravel. | |
| В | | | woh-wol | 20 | | | Gray (10YR5/1) with 20% dark yellowish bro (10YR4/6) mottles, very moist, soft, silty, very fir fine-grained sandy CLAY with trace gravel. | ne- to |
| 0A 0B | 22/24 92% | SS | 1-2 | 20 17 | | | Dark yellowish brown (10YR4/6) with 15% gr (10YR5/1) mottles, very moist to wet, soft, clayey fine- to medium-grained SAND with trace grav | , very |

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/7/2010 **Finish:** 10/7/2010

WEATHER: Sunny, warm (lo-70's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .

HANSON
BOREHOLE ID: G208

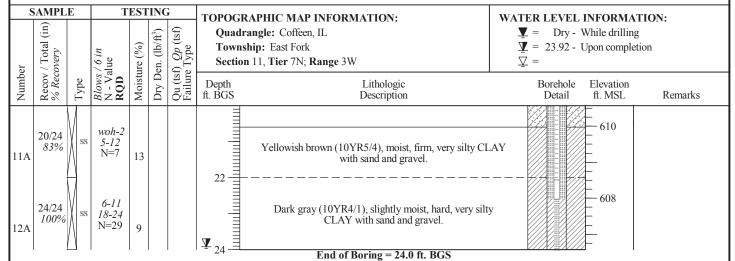
Well ID: G208

 Surface Elev:
 630.57 ft. MSL

 Completion:
 24.00 ft. BGS

 Station:
 875,231.46N

 2,514,993.57E



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/7/2010 **Finish:** 10/7/2010

WEATHER: Sunny, cool (lo-50's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 4½" HSA w/SS samplers

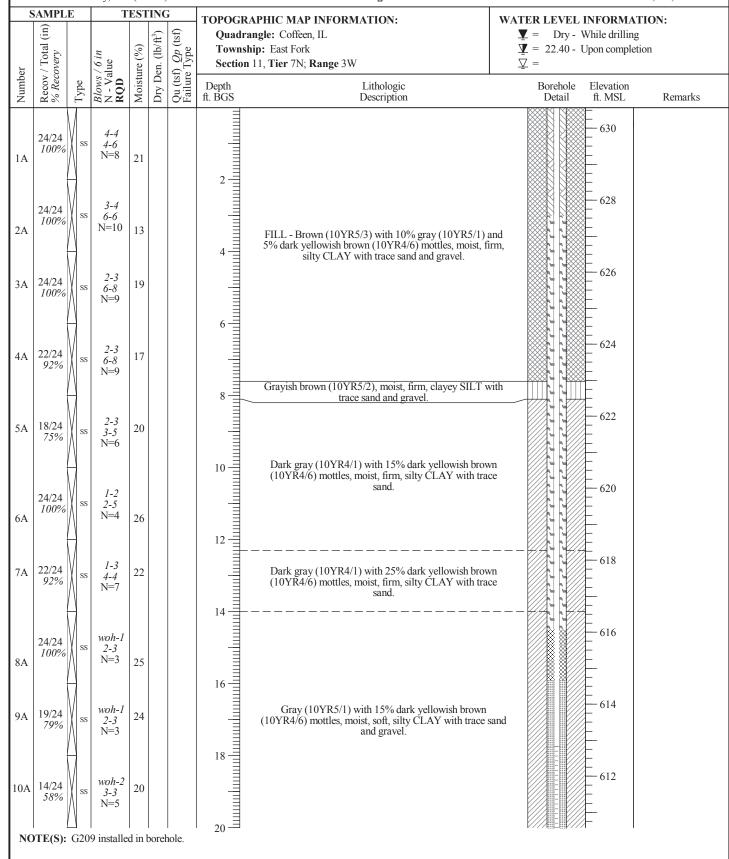
FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .



BOREHOLE ID: G209 **Well ID:** G209

Surface Elev: 630.57 ft. MSL Completion: 24.00 ft. BGS Station: 875,298.23N 2,515,149.56E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/7/2010

Finish: 10/7/2010 **WEATHER:** Sunny, cool (lo-50's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 4½" HSA w/SS samplers

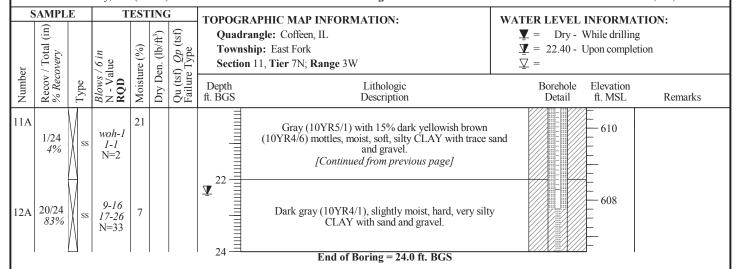
FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .

HANSON

BOREHOLE ID: G209 **Well ID:** G209

Surface Elev: 630.57 ft. MSL Completion: 24.00 ft. BGS Station: 875,298.23N 2,515,149.56E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/6/2010 **Finish:** 10/6/2010

WEATHER: Sunny, warm (mid-70's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .



BOREHOLE ID: G210 **Well ID:** G210

 Surface Elev:
 630.48 ft. MSL

 Completion:
 25.00 ft. BGS

 Station:
 875,359.71N

 2,515,298.97E

| S | AMPL | E | Т | EST | ING | | TOPOGRA | APHIC MAP INFORMATION: | WATER LEVEL INFORMATION: |
|--------|----------------------------------|------|----------------------------------|--------------|-------------------|--|--|---|---|
| oer | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) <i>Qp</i> (tsf) Failure Type | Townsh | ngle: Coffeen, IL ip: East Fork 11, Tier 7N; Range 3W | $\underline{\underline{\mathbf{Y}}}$ = 20.00 - While drilling $\underline{\underline{\mathbf{Y}}}$ = 19.90 - Upon completion $\underline{\underline{\mathbf{Y}}}$ = |
| Number | Recov % Re | Type | Blows N - V RQD | Moist | Dry I | Qu (ts Failu | Depth ft. BGS | Lithologic Description | Borehole Elevation Detail ft. MSL Remarks |
| A | 20/24 83% | ss | 4-3 5-6 N=8 | 16 | | | 2 10 10 10 10 10 10 10 1 | | 630 |
| A | 24/24 100% | ss | 3-4 7-7 N=11 | 15 | | | 4- | FILL - Brown (10YR4/3) with 20% dark gray (N5/1 mottles, moist, firm, silty CLAY with trace sand and gra |) - 628 |
| A | 24/24 100% | SS | 3-5 10-9 N=15 | 19 | | | 6- | | 626 |
| A | 24/24 100% | ss | 3-6 9-11 N=15 | 17 | | | | FILL - Dark grayish brown (10YR4/2), slightly moist, f clayey SILT with trace sand and gravel. | |
| | 1 | | | | | | 8 | Gray (10YR5/1) with 10% dark grayish brown (10YR- mottles, moist, firm, silty CLAY with trace sand. | 4/2) |
| iΑ | 24/24 100% | ss | 3-4 5-7 N=9 | 15 | | | | Dark gray (10YR4/1), moist, firm, silty CLAY with trasand, trace roots. Gray (10YR5/1) with 15% yellowish brown (10YR5/mottles, moist, firm, silty CLAY with trace sand. | |
| 5A | 22/24 92% | SS | 2-2 4-6 N=6 | 26 | | | 10 = - | Gray (10YR5/1) with 15% yellowish brown (10YR5/mottles, moist, firm, silty CLAY with trace sand and gra | ivel. |
| 7A | 19/24 79% | ss | 1-3 3-5 N=6 | 23 | | | 14 | Gray (10YR5/1) with 5% dark yellowish brown (10YR mottles, moist to very moist, firm, silty CLAY with sar | 4/6) ad. |
| 3A | 24/24 100% | ss | 2-2 2-4 N=4 | 26 | | | 16 | Gray (10YR5/1) with 5% dark yellowish brown (10YR mottles, moist, soft, silty CLAY with sand and trace gra | |
| ЭА | 24/24 100% | ss | 1-1 2-3 N=3 | 24 | | | 16 | Gray (10YR5/1) with 15% dark yellowish brown (10YR4/6) mottles, moist, soft, silty CLAY with sand a trace gravel. | and |
| 0A | 20/24 83% | SS | 1-1 2-2 N=3 | 24 | | | ¥ 20 | Gray (N6/1), very moist, very soft, silty, very fine-to fine-grained sandy CLAY with trace gravel. | 612 |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

DATES: Start: 10/6/2010

Finish: 10/6/2010

SAMPLE

WEATHER: Sunny, warm (mid-70's)

TESTING

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill **Drilling Method:** 41/4" HSA w/SS samplers

FIELD STAFF: Driller: D. Mahurin

Helper: J. Litsch/D. Smail Eng/Geo: .

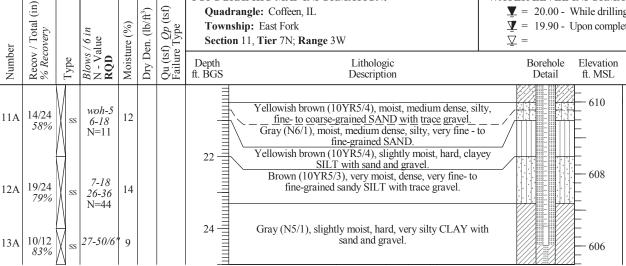


BOREHOLE ID: G210 Well ID: G210

Surface Elev: 630.48 ft. MSL Completion: 25.00 ft. BGS **Station:** 875,359.71N 2,515,298.97E

Remarks





Quadrangle: Coffeen, IL

Township: East Fork

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/11/2010

Finish: 10/11/2010 **WEATHER:** Sunny, warm (lo-70's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .



BOREHOLE ID: G211 **Well ID:** G211

 Surface Elev:
 630.31 ft. MSL

 Completion:
 24.00 ft. BGS

 Station:
 875,424.49N

 2,515,449.06E

| - 2 | SAMPL | Ľ | Т | EST | INC | j | TOPOGR | APHIC MAP INFORMATION: | WATER LEVEL INFORMATION: |
|--------|----------------------------------|------|----------------------------------|--------------|-------------------|--|---|---|---|
| er | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) <i>Qp</i> (tsf) Failure Type | Towns | angle: Coffeen, IL hip: East Fork 11, Tier 7N; Range 3W | $\underline{\underline{\mathbf{Y}}}$ = 20.00 - While drilling $\underline{\underline{\mathbf{Y}}}$ = 20.60 - Upon completion $\underline{\underline{\mathbf{Y}}}$ = |
| Number | Recov % Rec | Type | Blows N - V RQD | Moist | Dry D | Qu (ts Failur | Depth ft. BGS | Lithologic Description | Borehole Elevation Detail ft. MSL Remarks |
| lΑ | 20/24 83% | ss | 5-3 4-5 N=7 | 23 | | | 2- | FILL - Brown (10YR4/3) with 20% dark gray (10YR4 mottles, moist, firm, silty CLAY with trace sand and gray | avel. |
| 2A | 20/24 83% | ss | 3-5 5-8 N=10 | 17 | | | | | 628 |
| 3A | 24/24 100% | ss | 2-3 5-7 N=8 | 24 | | | 6 | FILL - Dark gray (10YR4/1) with 20% brown (10YR4 and 5% dark yellowish brown (10YR4/6) mottles, mo firm, silty CLAY with trace sand and gravel. | ist, |
| 4A | 24/24 100% | ss | 3-5 7-9 N=12 | 29 | | | | | 624 |
| 5A | 24/24 100% | ss | 2-2 3-5 N=5 | 31 | | | 8 = = = = = = = = = = = = = = = = = = = | Dark gray (10YR4/1) with 20% dark yellowish brow (10YR4/6) mottles, moist, firm, silty CLAY, slight traroots. | n 622 |
| 6A | 17/24 71% | ss | 1-2 4-4 N=6 | 19 | | | 10 = 12 = 12 | Dark gray (10YR4/1) with 20% dark yellowish brow (10YR4/6) mottles, moist, firm, silty CLAY with trac sand. | 620 m |
| 7A | 24/24 100% | ss | 1-2 2-4 N=4 | 22 | | | | Dark gray (10YR4/1) with 20% dark yellowish brow | n 618 |
| 8A | 24/24 100% | ss | 1-1 3-2 N=4 | 28 | | | 14 = 16 = 16 = 16 | (10YR4/6) mottles, moist, soft, silty CLAY with trace s and gravel. | and 616 |
| 9A | 22/24 92% | ss | 1-1 1-2 N=2 | 19 | | | 18 | Dark yellowish brown (10YR4/6) with 30% gray (10YR5/1) mottles, very moist, soft, very fine-to fine-grained sandy CLAY with trace gravel. | 614 |
| 0A | 19/24 79% | ss | 1-4 5-11 N=9 | 13 | | | 18 ———————————————————————————————————— | Dark yellowish brown (10YR4/4) with 15% grayish brown (10YR5/2) mottles, moist, firm, clayey SILT with sand gravel. | own and 612 |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

DATES: Start: 10/11/2010

Finish: 10/11/2010

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill **Drilling Method:** 41/4" HSA w/SS samplers

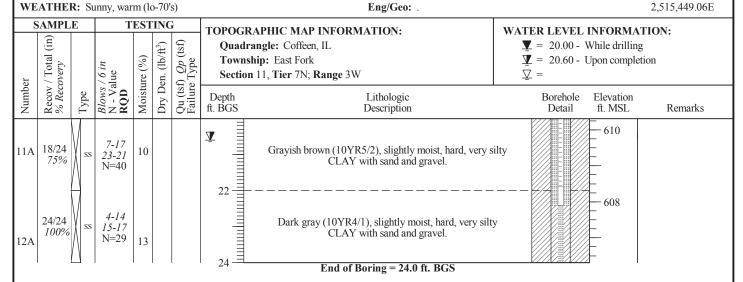
FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .



BOREHOLE ID: G211 Well ID: G211

> Surface Elev: 630.31 ft. MSL **Completion:** 24.00 ft. BGS **Station:** 875,424.49N 2,515,449.06E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/11/2010

Finish: 10/11/2010 WEATHER: Sunny, warm (lo-80's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .



BOREHOLE ID: G212 **Well ID:** G212

 Surface Elev:
 630.59 ft. MSL

 Completion:
 24.00 ft. BGS

 Station:
 875,486.50N

 2,515,583.03E

| SAMPL | Ł | 1 | ESI | INC | | TOPOGR | APHIC MAP INFORMATION: | WATER LEVEL INFORMATION: | | | | |
|--------------------|------|----------------------------------|--------------|-------------------|--|-------------------|--|--------------------------|-------------------|---------|--|--|
| Recov / Total (in) | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) <i>Qp</i> (tsf) Failure Type | Quadra Townsl | angle: Coffeen, IL nip: East Fork 11, Tier 7N; Range 3W | | _ | on | | |
| Recov / % Recov | Type | Blows N - V RQD | Moist | Dry D | Qu (ts Failur | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks | | |
| A 24/24 100% | SS | 4-3 3-6 N=6 | 17 | | | | FILL - Brown (10YR4/3), slightly moist, firm, silty CL with trace sand and gravel. | AY | 630 | | | |
| A 24/24 100% | SS | 2-3 4-5 N=7 | 21 | | | 2 = | FILL - Dark gray (10YR4/1) with 20% brown (10YR4 and 10% dark yellowish brown (10YR4/6) mottles, mother firm, silty CLAY with trace sand. | 1/3) ist, | 628 | | | |
| 24/24 100% | ss | 2-5 6-7 N=11 | 13 | | | 4 | FILL - Brown (10YR4/3) with 15% dark gray (10YR4/3) | 1/1) | 626 | | | |
| A 24/24 100% | ss | 2-5 7-10 N=12 | 15 | | | 6 | and 10% dark yellowish brown (10YR4/6) mottles, mot firm, silty CLAY with trace sand and gravel. | 11St, | 624 | | | |
| 5A 24/24 100% | SS | 2-2 4-7 N=6 | 29 | | | | Dark gray (10YR4/1) with 10% dark yellowish brow (10YR4/6) mottles, moist, firm, silty CLAY, slight tra | m ce | 622 | | | |
| 5A 18/24 75% | ss | 2-3 4-6 N=7 | 23 | | | 10 = | Dark gray (10YR4/1) with 10% dark yellowish brow (10YR4/6) mottles, moist, firm, silty CLAY with trac sand. | m se | 620 | | | |
| 7A 17/24 71% | SS | 1-2 2-2 N=4 | 25 | | | 12 = | | | 618 | | | |
| 3A 24/24 100% | ss | woh-1 2-3 N=3 | 27 | | | 16 | Dark gray (10YR4/1) with 15% dark yellowish brow (10YR4/6) mottles, moist, soft, silty CLAY with trace s and gravel. | n and | 616 | | | |
| 9A 22/24 92% | ss | 1-1 2-2 N=3 | 25 | | | 16 = | | | 614 | | | |
| 0A 24/24 100% | SS | woh-woh 1-2 | 19 | | | 18 − − | Gray (10YR5/1) with 30% dark yellowish brown (10YR4/6) mottles, very moist, very soft, silty, very fine fine-grained sandy CLAY with trace gravel. Gray (10YR5/1), loose, wet, silty, very fine- to | e- to | 612 | | | |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

DATES: Start: 10/11/2010

Finish: 10/11/2010

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill **Drilling Method:** 41/4" HSA w/SS samplers

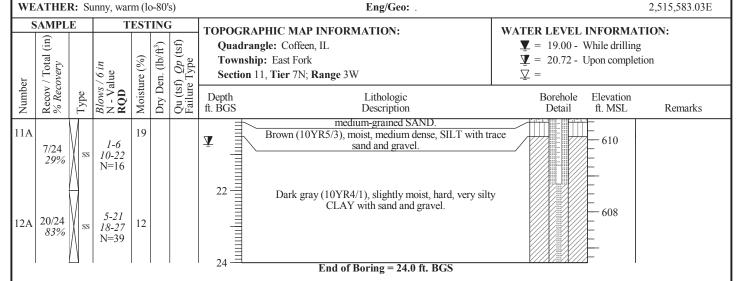
FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .



BOREHOLE ID: G212 Well ID: G212

> Surface Elev: 630.59 ft. MSL **Completion:** 24.00 ft. BGS **Station:** 875,486.50N 2,515,583.03E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/12/2010

Finish: 10/12/2010
WEATHER: Partly cloudy, mild (mid-50's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 4½" HSA w/SS samplers

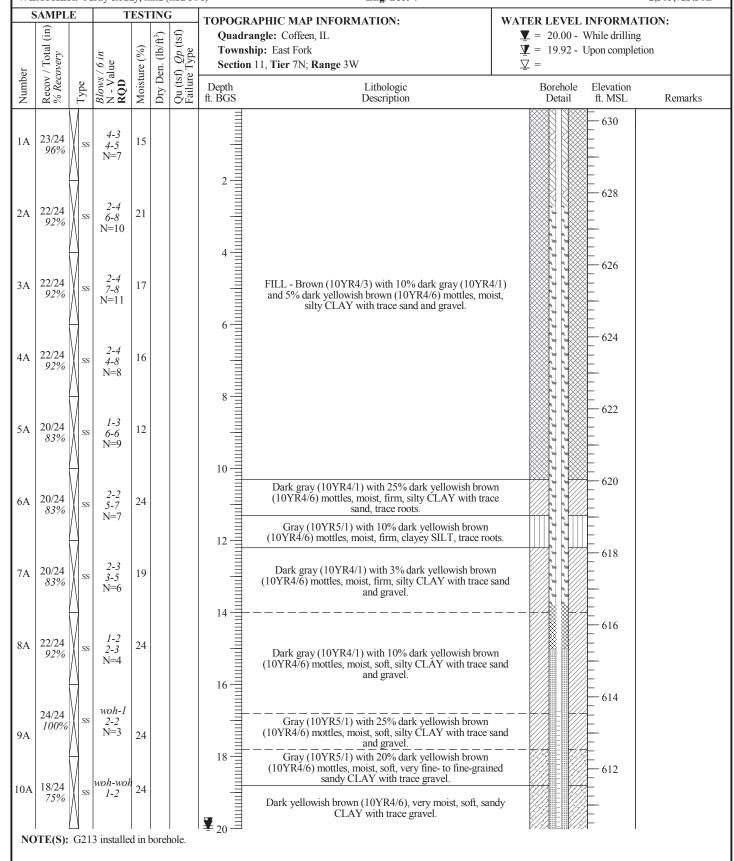
FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .



BOREHOLE ID: G213 Well ID: G213

> Surface Elev: 630.34 ft. MSL Completion: 24.00 ft. BGS Station: 875,544.37N 2,515,723.51E



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/12/2010

Finish: 10/12/2010 **WEATHER:** Partly cloudy, mild (mid-50's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 4½" HSA w/SS samplers

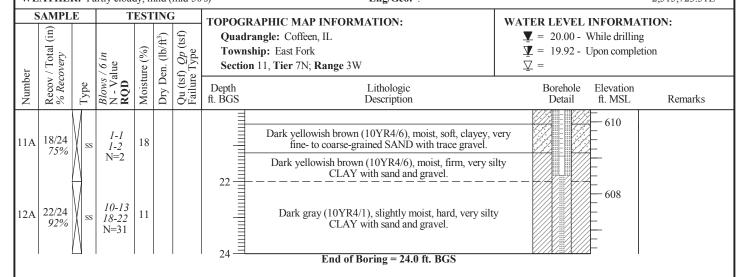
FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .

HANSON
BOREHOLE ID: G213

Well ID: G213

Surface Elev: 630.34 ft. MSL Completion: 24.00 ft. BGS Station: 875,544.37N 2,515,723.51E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/14/2010

Finish: 10/14/2010 WEATHER: Sunny, cool (lo-40's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .



BOREHOLE ID: G214 **Well ID:** G214

 Surface Elev:
 630.39 ft. MSL

 Completion:
 24.00 ft. BGS

 Station:
 875,668.02N

 2,515,960.84E

| 5 | SAMPLI | 7. | Т | EST | INC | 2 | Eng/Geo: . | 2,515,960.84 |
|----------|----------------------------|------|----------------------------------|--------------|-------------------|---------------------------------------|---|---|
| | l (in) | | | | | Qu (tsf) <i>Qp</i> (tsf) Failure Type | TOPOGRAPHIC MAP INFORMATION: Quadrangle: Coffeen, IL Township: East Fork Section 11, Tier 7N; Range 3W | WATER LEVEL INFORMATION: $\underline{\Psi} = \text{Dry - While drilling}$ $\underline{\Psi} = \text{Dry - Upon completion}$ $\underline{\nabla} =$ |
| Number | Recov / Tota % Recovery | Type | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure T | Depth Lithologic ft. BGS Description | Borehole Elevation Detail ft. MSL Remarks |
| 1A | 24/24 100% | ss | 6-7 7-9 N=14 | 15 | | | FILL - Brown (10YR4/3) with 10% dark gra and 10% dark yellowish brown (10YR4/6) n firm, silty CLAY with trace sand and gravel. | nottles, moist, gravel. |
| 2A | 24/24 100% | SS | 3-3 6-5 N=9 | 22 | | | FILL - Dark gray (10YR4/1) with 15% dar brown (10YR4/6) mottles, moist, firm, silty trace sand and gravel. | k yellowish CLAY with — |
| 3A | 24/24 100% | ss | 3-4 6-8 N=10 | 18 | | | | - 626 |
| 4A | 24/24 100% | ss | 3-4 7-10 N=11 | 17 | | | FILL - Brown (10YR4/3) with 10% dark yel (10YR4/6) and 5% dark gray (10YR4/1) m firm, silty CLAY with trace sand and g | ottles, moist, |
| 5A | 24/24 100% | ss | 3-2 4-5 N=6 | 19 | | | 6 FILL - Brown (10YR4/3) with 10% dark yel (10YR4/6) and 5% dark gray (10YR4/1) m firm, silty CLAY with trace sand and gray and 10% dark yellowish brown (10YR4/6) m firm, clayey SILT with trace sand and 10% dark yellowish brown (10YR4/6) mottle silty CLAY with trace sand and gray 12 | nottles, moist, |
| 6A | 24/24 100% | SS | 2-3 4-7 N=7 | 24 | | | Brown (10YR4/3) with 15% dark gray (10 10% dark yellowish brown (10YR4/6) mottle silty CLAY with trace sand and gra | es, moist, firm, |
| 7A 7B | 24/24 100% | ss | 2-3 4-6 N=7 | 22 16 | | | Gray (10YR6/1) with 30% dark yellowi (10YR4/6) mottles, moist, soft, silty C | |
| 8A | 24/24 100% | SS | woh-2 3-4 N=5 | 22 | | | Dark gray (10YR4/1) with 10% dark yello (10YR4/6) mottles, moist, firm, silty CLAY v and gravel. | wish brown with trace sand 616 |
| 9A | 22/24 92% | SS | 1-2 2-3 N=4 | 21 | | | Dark gray (10YR4/1) with 10% dark yello (10YR4/6) mottles, moist, soft, silty CLAY wand gravel. Gray (10YR5/1) with 30% dark yellowing (10YR4/6) mottles, moist, soft, silty CLAY wand gravel. | wish brown cith trace sand 614 sh brown |
| 10A | 22/24 92% | SS | woh-2 2-2 N=4 | 15 | | | and gravel. Gray (10YR5/1), wet, loose, silty, very medium-grained SAND with trace gravel and | 612 |
| 10B | 1 [| | | 21 | borel | | medium-grained SAND with trace gravel and | clayey seams. |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

DATES: Start: 10/14/2010

Finish: 10/14/2010

WEATHER: Sunny, cool (lo-40's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill **Drilling Method:** 41/4" HSA w/SS samplers

FIELD STAFF: Driller: D. Mahurin

Eng/Geo: .

Helper: J. Litsch/D. Smail



BOREHOLE ID: G214 Well ID: G214

> Surface Elev: 630.39 ft. MSL **Completion:** 24.00 ft. BGS **Station:** 875,668.02N 2,515,960.84E

| | SAMPL | E | T | EST | INC | j | TOPOGR | APHIC MAP INFORMATION: | WATER LEVEL INFORMATION: |
|------------|----------------------------|------|------------------------|----------|---------------|-------------------------|-----------------------------|---|---|
| er | / Total (in) | | / 6 in Ilue | ıre (%) | Den. (lb/ft³) | f) <i>Qp</i> (tsf) Type | Quadra Townsh Section | ngle: Coffeen, IL ip: East Fork 11, Tier 7N; Range 3W | $\underline{\Psi}$ = Dry - While drilling $\underline{\Psi}$ = Dry - Upon completion $\underline{\nabla}$ = |
| Number | Recov / Tota % Recovery | Type | Blows N - Vz RQD | Moisture | Dry D | Qu (tsf) Failure | Depth ft. BGS | Lithologic Description | Borehole Elevation Detail ft. MSL Remarks |
| 11A 11B | 83% | SS | woh-woh 3-12 | 24 14 | | | 22 | Gray (10YR5/1), wet, loose, silty, very fine- to medium-grained SAND with trace gravel and clayey sea [Continued from previous page] Dark yellowish brown (10YR4/6), moist, firm, very si CLAY with trace sand and gravel. | |
| 12A | 24/24 100% | SS | 12-28 32-28 N=60 | 7 | | | | Dark gray (10YR4/1), slightly moist, hard, very silty CLAY with trace sand and gravel. | y 608 |
| 1 | | | | | | | 24 === | End of Boring = 24.0 ft. BGS | , |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/13/2010 **Finish:** 10/13/2010

WEATHER: Sunny, warm, windy (hi-60's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .



BOREHOLE ID: G215 **Well ID:** G215

 Surface Elev:
 630.48 ft. MSL

 Completion:
 24.31 ft. BGS

 Station:
 875,810.19N

 2,515,971.55E

| S | AMPL | E | Т | EST | INC | | TOPOGR | APHIC MAP INFORMATION: | WATER LEVEL INFORMATION: | |
|--------|----------------------------------|------|----------------------------------|--------------|-------------------|--|---|---|--|-------|
| ber | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) <i>Qp</i> (tsf) Failure Type | Quadra Townsh Section | angle: Coffeen, IL nip: East Fork 11, Tier 7N; Range 3W | $ \mathbf{Y} = \text{Dry - While drilling} $ $ \mathbf{Y} = \text{Dry - Upon completion} $ $ \mathbf{Y} = 22.52 - 10/14/10 $ | |
| Number | Reco' | Type | Blow, N - V RQD | Mois | Dry I | Qu (t Failu | Depth ft. BGS | Lithologic Description | Borehole Elevation Detail ft. MSL Rea | marks |
| 1A | 23/24 96% | ss | 5-3 3-5 N=6 | 18 | | | | | 630 | |
| 2A | 19/24 79% | ss | 3-3 5-6 N=8 | 17 | | | 4- | FILL - Brown (10YR4/3) with 30% dark gray (10YR4 and 10% dark yellowish brown (10YR4/6) mottles, motifirm, silty CLAY with trace sand and gravel. | 4/1) bist, ———————————————————————————————————— | |
| 3A | 20/24 83% | ss | 2-3 7-7 N=10 | 13 | | | | | 626 | |
| 4A | 23/24 96% | ss | 3-6 6-7 N=12 | 16 | | | 6 - | FILL - Dark grayish brown (10YR4/2), moist, firm, si CLAY with trace sand and gravel. | | |
| 4B | | | | 27 | | | 8 | FILL - Gray (10YR5/1) with 15% dark yellowish brov (10YR4/6) mottles, moist, firm, silty CLAY with traces and. | wn ce | |
| 5A | 20/24 83% | SS | 3-3 3-5 N=6 | 20 | | | | Very dark gray (10YR3/1), moist, firm, silty CLAY w trace sand, trace roots. | vith 622 | |
| 6A | 13/24 54% | ss | 2-2 3-5 N=5 | 24 | | | 8 10 11 12 12 12 12 12 12 12 12 12 12 12 12 | Dark gray (10YR4/1) with 30% dark yellowish brow (10YR4/6) moist, firm, silty CLAY with trace sand. | | |
| 7A | 19/24 79% | SS | 2-3 4-6 N=7 | 17 | | | | Gray (10YR5/1) with 30% dark yellowish brown (10YR4/6) mottles, moist, firm, clayey SILT with transand. | ce | |
| 8A | 20/24 83% | ss | 2-3 4-5 N=7 | 19 | | | 14 - | Dark gray (10YR4/1), moist, firm, clayey SILT with tr sand. | race616 | |
| 9A | 22/24 92% | ss | 1-3 3-4 N=6 | 19 | | | 18 | Dark gray (10YR4/1) with 30% Dark yellowish brow (10YR4/6) mottles, moist, firm, silty CLAY with trace s and gravel. | wn sand 614 | |
| 10A | 24/24 100% | ss | woh-1 2-2 N=3 | 17 | | | | Dark gray (10YR4/1) with 30% Dark yellowish brow (10YR4/6) mottles, moist, soft, sandy CLAY with tragravel. | vn | |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

DATES: Start: 10/13/2010 Finish: 10/13/2010

WEATHER: Sunny, warm, windy (hi-60's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill **Drilling Method:** 41/4" HSA w/SS samplers

FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .

HANSON

BOREHOLE ID: G215 Well ID: G215

> Surface Elev: 630.48 ft. MSL Completion: 24.31 ft. BGS **Station:** 875,810.19N 2,515,971.55E

SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: Recov / Total (in) % Recovery Qu (tsf) *Qp* (tsf) Failure Type Dry Den. (lb/ft³) Quadrangle: Coffeen, IL ▼ = Dry - While drilling Moisture (%) **Township:** East Fork $\underline{\Psi}$ = Dry - Upon completion Blows / 6 in N - Value RQD Section 11, Tier 7N; Range 3W ∇ = 22.52 - 10/14/10 Depth Lithologic Borehole Elevation ft. BGS Detail Remarks

Number Description ft. MSL Dark yellowish brown (10YR4/6), moist, medium dense, 610 clayey SILT with sand and trace gravel. 2-4 20/24 17 11A 4-4 Yellowish brown (10YR5/6), moist, medium dense, silty, 83% very fine- to fine-grained SAND.

Dark yellowish brown (10YR4/6) with 30% dark gray (10YR4/1) mottles, moist, firm, sandy CLAY with trace N=822 gravel. ∇ 608 Gravish brown (10YR5/2), slightly moist, very firm, very 7-11 17-19 24/24 silty CLAY with sand and gravel. 12A 11 SS 100% N = 28Dark gray (10YR4/1), slightly moist, hard, very silty 12B 9 0/4 CLAY with sand and gravel. BD 0%

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/13/2010 **Finish:** 10/13/2010

WEATHER: Partly cloudy, mild, windy (lo-60's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .



BOREHOLE ID: G216 Well ID: G216

 Surface Elev:
 630.28 ft. MSL

 Completion:
 26.00 ft. BGS

 Station:
 875,976.05N

 2,515,968.53E

| SAMPL | E | Т | EST | INC | | TOPOGRA | APHIC MAP INFORMATION: | WATER LEVEL | INFORMAT | ION: |
|--------------------|------|----------------------------------|--------------|-------------------|--|---|---|--------------------|-----------------------------------|---------|
| Recov / Total (in) | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) <i>Qp</i> (tsf) Failure Type | Townsh | ngle: Coffeen, IL nip: East Fork 11, Tier 7N; Range 3W | | While drilling Upon completion | on |
| Recov / % Recov | Type | Blows N - V RQD | Moist | Dry D | Qu (ts Failur | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks |
| 24/24 100% | SS | 3-2 2-4 N=4 | 22 | | | 2 — | | | 630 | |
| A 19/24 79% | ss | 2-2 5-4 N=7 | 28 | | | 2 = 4 = = = = = = = = = = = = = = = = = | FILL - Brown (10YR4/3) with 20% dark gray (10YR4 and 5% dark yellowish brown (10YR4/6) mottles, motifirm, silty CLAY with trace sand and gravel. | 1/6) ist, | 628 | |
| A 24/24 100% | ss | 2-2 4-5 N=6 | 19 | | | | FILL - Dark gray (10YR4/1) with 15% brown (10YR4 and 10% dark yellowish brown (10YR4/6) mottles, mother firm, clayey SILT with trace sand and gravel. | 1/3) iist, | 626 | |
| A 22/24 92% | ss | 3-4 6-6 N=10 | 19 | | | 8 = 10 = 10 | FILL - Dark grayish brown (10YR4/2) with 10% dar yellowish brown (10YR4/6) mottles, moist, firm, silt CLAY with trace sand and gravel. | k y | 624 | |
| A 20/24 83% | SS | 2-3 3-6 N=6 | 18 | | | 10 | Dark gray (10YR4/1) with 40% gray (10YR6/1) and 1 | 0% | 622 | |
| A 18/24 75% | SS | 2-3 3-4 N=6 | 17 | | | | dark yellowish brown (10YR4/6) mottles, moist, firn clayey SILT with trace sand. | 1, | 620 | |
| A 16/24 67% | SS | 1-2 3-4 N=5 | 20 | | | 12 | Gray (10YR5/1) with 20% dark yellowish brown (10YR4/6) mottles, moist, soft, silty CLAY with trace s and gravel. | and | 618 | |
| A 22/24 92% | ss | 2-2 5-5 N=7 | 20 | | | | Very dark gray (10YR3/1), moist, firm, silty CLAY w trace sand. | ith | 616 | |
| A 23/24 96% | ss | woh-2 3-3 N=5 | 18 | | | 16 | Gray (10YR5/1) with 10% dark yellowish brown (10YR4/6) mottles, moist, firm, silty CLAY with trace s and gravel. | sand | 614 | |
| OA 24/24 100% | ss | woh-woh 1-2 | 17 | | | 18 = - | Gray (10YR5/1) with 10% dark yellowish brown (10YR4/6) mottles, moist, firm, sandy CLAY with tra | ce | 612 | |

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/13/2010 **Finish:** 10/13/2010

WEATHER: Partly cloudy, mild, windy (lo-60's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 41/4" HSA w/SS samplers

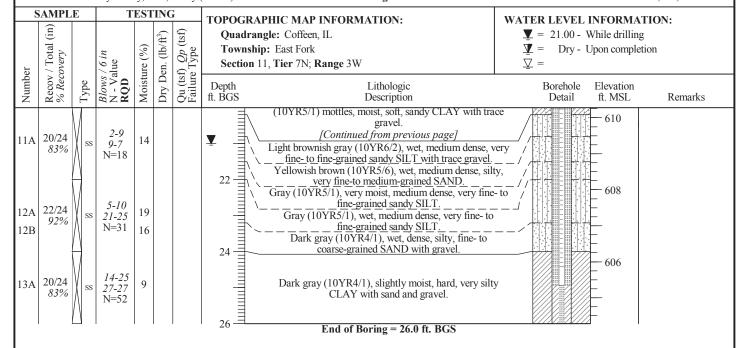
FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .



BOREHOLE ID: G216 **Well ID:** G216

Surface Elev: 630.28 ft. MSL Completion: 26.00 ft. BGS Station: 875,976.05N 2,515,968.53E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/12/2010

Finish: 10/12/2010 WEATHER: Sunny, warm (lo-80's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .



BOREHOLE ID: G217 **Well ID:** G217

 Surface Elev:
 630.67 ft. MSL

 Completion:
 26.00 ft. BGS

 Station:
 876,185.57N

 2,515,963.02E

| SAMPL | E | Т | EST | INC | | TOPOGRAPHIC MAP INFORMATION: | | WATER LEVEL INFORMATION: | | | | |
|-------------------------------|------|----------------------------------|--------------|-------------------|--|------------------------------|---|---|-------------------|---------|--|--|
| Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) <i>Qp</i> (tsf) Failure Type | Townsh | ingle: Coffeen, IL nip: East Fork 11, Tier 7N; Range 3W | $ \mathbf{Y} = 23.00 - 10 $ $ \mathbf{Y} = 24.82 - 10 $ $ \mathbf{Y} = 23.98 - 10 $ | Upon completi | on | | |
| Recov / '% Recov | Type | Blows N - V RQD | Moist | Dry I | Qu (t Failu | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks | | |
| A 20/24 83% | SS | 5-2 3-4 N=5 | 21 | | | | FILL - Brown (10YR4/3) with 10% dark gray (10YR4 | //) | 630 | | | |
| A 19/24 79% | SS | 2-3 5-6 N=8 | 28 | | | 2 = 4 = 4 | and 5% dark yellowish brown (10YR4/6) mottles, moi firm, silty CLAY with trace sand and gravel. | | 628 | | | |
| 3A 19/24 79% | SS | 2-3 6-7 N=9 | 14 | | | | FILL - Dark gray (10YR4/1) with 25% dark yellowis brown (10YR4/6) mottles, moist, firm, silty CLAY witrace sand and gravel. | sh th | - 626 | | | |
| 23/24 96% | SS | 5-6 7-8 N=13 | 15 | | | 8 = | FILL - Brown (10YR4/3) with 10% dark gray (10YR4 and 10% dark yellowish brown (10YR4/6) mottles, mother, silty CLAY with trace sand and gravel. | //1) ist, | | | | |
| 5A 20/24 83% | SS | 3-5 7-6 N=12 | 13 | | | | FILL - Dark grayish brown (10YR4/2) with 5% dark yellowish brown (10YR4/6) slightly moist, firm, clayer SILT with trace sand and gravel. | ey | 622 | | | |
| 5A 19/24 79% | SS | 3-3 4-5 N=7 | 27 | | | 10 | FILL - Very dark gray (10YR3/1), moist, firm, silty CL with trace sand and gravel. Dark gray (10YR4/1), moist, firm, silty CLAY with trace sand and gravel. Gray (10YR5/1) with 15% dark yellowish brown (10YR4/6) mottles, moist, firm, silty CLAY with trace sand, trace roots. | ace | 620 | | | |
| 7A 18/24 75% | SS | 3-4 6-8 N=10 | 28 | | | 12 == | Dark grayish brown (10YR4/2) with 10% dark yellow brown (10YR4/6) mottles, moist, firm, silty CLAY trasand, trace roots. | ish ce | 618 | | | |
| 3A 20/24 83% | SS | 2-4 6-8 N=10 | 16 | | | 14 = | Dark gray (10YR4/1), moist, firm, silty CLAY with transand and gravel. | ace | 616 | | | |
| 9A 19/24 79% | SS | 2-3 4-5 N=7 | 26 | | | 16 = | Dark gray (10YR4/1) with 10% yellowish brown (10YR5/6) mottles, moist, firm, silty CLAY with trace s and gravel. | sand | 614 | | | |
| 0A 19/24 79% | SS | 1-2 2-3 N=4 | 18 | | | 18 | Gray (10YR5/1) with 5% dark yellowish brown (10YR mottles, moist, soft, silty CLAY with sand and trace gra | | 612 | | | |

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/12/2010

Finish: 10/12/2010 **WEATHER:** Sunny, warm (lo-80's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 4½" HSA w/SS samplers

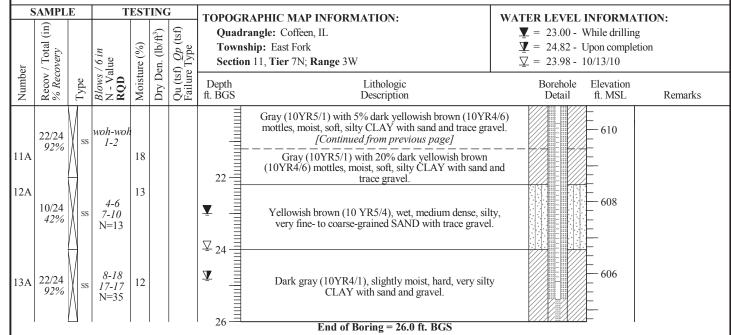
FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .



BOREHOLE ID: G217 **Well ID:** G217

Surface Elev: 630.67 ft. MSL Completion: 26.00 ft. BGS Station: 876,185.57N 2,515,963.02E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/12/2010

Finish: 10/12/2010 **WEATHER:** Partly cloudy, warm (lo-70's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 4¼" HSA w/SS samplers

FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: .



BOREHOLE ID: G218 **Well ID:** G218

 Surface Elev:
 630.64 ft. MSL

 Completion:
 26.00 ft. BGS

 Station:
 876,380.92N

 2,515,962.16E

| 4-1 2-1 N=3 2-2 3-5 N=5 | (%) Woisture (%) 20 | Dry Den. ($1b/1T$) Qu ($1sf$) Qp ($1sf$) Failure Type | | APHIC MAP INFORMATION: Ingle: Coffeen, IL Ingl: East Fork 11, Tier 7N; Range 3W Lithologic Description FILL - Brown (10YR4/3) with 15% dark gray (10YR4, and 5% dark yellowish brown (10YR4/6) mottles, mois soft, silty CLAY with trace sand and gravel. | ist, |
|--|---|--|---|---|--|
| 4-1 2-1 N=3 2-2 3-5 N=5 | 20 | Dry D Qu (ts Failur | | Description FILL - Brown (10YR4/3) with 15% dark gray (10YR4 and 5% dark yellowish brown (10YR4/6) mottles, mot | Detail ft. MSL Remarks |
| 2-1 N=3 2-2 3-5 N=5 | | | 2-11 | and 5% dark yellowish brown (10YR4/6) mottles, mois | -/1) st, |
| 3-5 N=5 | 20 | | | | |
| 4-8 | | | 4- | FILL - Dark gray (10YR4/1) with 30% brown (10YR4 | 628 |
| | 17 | | | and 10% dark yellowish brown (10YR4/6) mottles, mofirm, silty CLAY with trace sand and gravel. | ist, = 626 |
| 2-5 6-8 N=11 | 14 | | 8- | FILL - Brown (10YR5/3) with 10% dark gray (10YR4 mottles, slightly moist, firm, clayey SILT with trace sai and gravel. | 624 |
| 3-4 8-7 N=12 | 17 | | | Dark grayish brown (10YR4/2) with 5% dark yellowis | 622 |
| 2-2 3-5 | 19 25 | | 10 | brown (10YR4/6) mottles, moist, firm, clayey SILT wi trace sand. Gray (10YR5/1) with 30% dark yellowish brown | ith620 |
| 2-3 5-7 N=8 | 22 | | | sand, slight trace roots. | 618 |
| 2-3 4-5 N=7 | 19 | | 14 - | Dark gray (10YR4/1) with 15% dark yellowish brown (10YR4/6) mottles, moist, firm, clayey SILT with trac sand. | m — 616 |
| 2-2 2-4 N=4 | 19 | | 16 — | Gray (10YR5/1) with 10% dark yellowish brown (10YR4/6) mottles, moist, soft, silty CLAY with trace so and gravel. | and |
| 1-2 2-3 | 18 | | | | 612 |
| 1 | 2-3 5-7 N=8 2-3 4-5 N=7 2-2 2-4 N=4 | 2-3 5-7 N=8 22 N=7 19 N=7 19 1-2 2-3 N=4 18 | 2-3 5-7 N=8 2-3 4-5 N=7 19 N=4 19 | 2-3 4-5 N=7 14 = 14 14 = 14 16 = 16 16 = 18 18 = 18 | Dark gray (10YR4/1) with 15% dark yellowish brow (10YR4/6) mottles, moist, firm, clayey SILT with trace sand. 19 Gray (10YR5/1) with 10% dark yellowish brown (10YR4/6) mottles, moist, soft, silty CLAY with trace sand gravel. |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

DATES: Start: 10/12/2010

Finish: 10/12/2010

WEATHER: Partly cloudy, warm (lo-70's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill **Drilling Method:** 41/4" HSA w/SS samplers

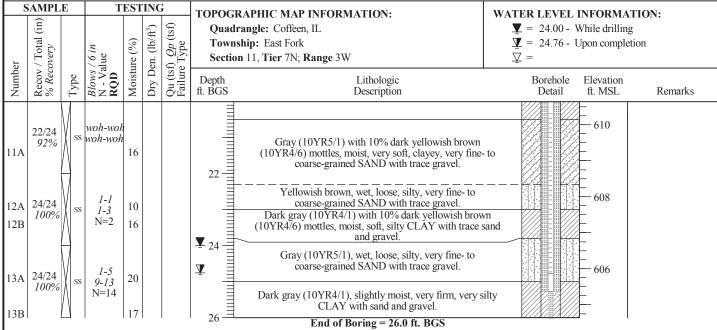
FIELD STAFF: Driller: D. Mahurin

Helper: J. Litsch/D. Smail Eng/Geo: .



BOREHOLE ID: G218 Well ID: G218

Surface Elev: 630.64 ft. MSL Completion: 26.00 ft. BGS **Station:** 876,380.92N 2,515,962.16E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 2/26/2008 **Finish:** 2/26/2008

WEATHER: Overcast, cold

NOTE(S):

CONTRACTOR: Testing Service Corp. **Rig mfg/model:** CME-650 Track Drill

Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: .

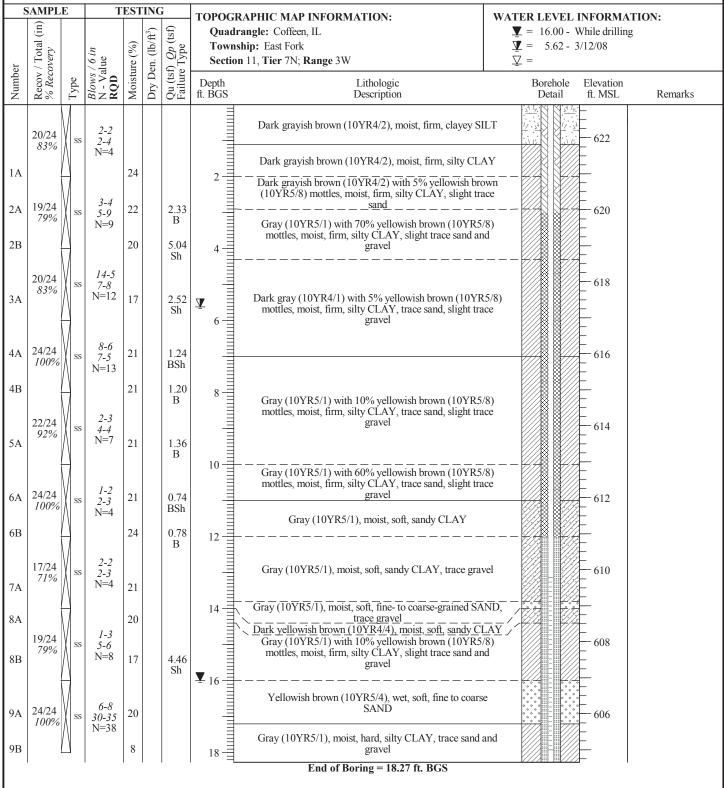
HANSO

BOREHOLE ID: G270 **Well ID:** G270

Surface Elev: 622.92 ft. MSL Completion: 18.27 ft. BGS Station: 874.801.92N

2,514,996.84E

Page 1 of 1



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 9/9/2009 Finish: 9/10/2009

WEATHER: Sunny, warm (70's)

CONTRACTOR: Layne-Western Co **Rig mfg/model:** CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: G. Mills Helper: J. Twellman

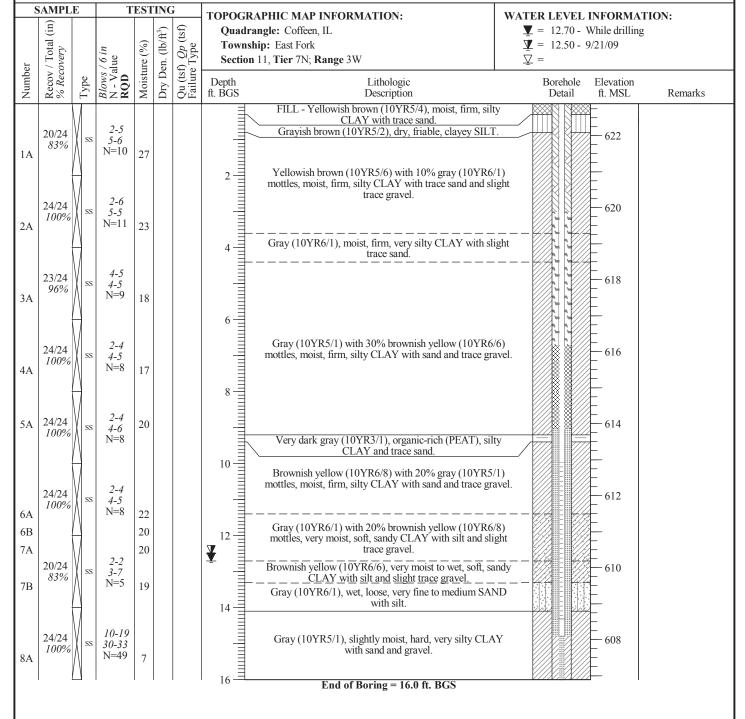
Eng/Geo: R. Hasenyager

BOREHOLE ID: G271

Well ID: G271

Surface Elev: 622.89 ft. MSL Completion: 16.00 ft. BGS Station: 874,239.38N

2,515,517.12E



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 9/10/2009 **Finish:** 9/10/2009

WEATHER: Sunny, warm (70's)

CONTRACTOR: Layne-Western Co **Rig mfg/model:** CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: G. Mills Helper: J. Twellman

Eng/Geo: R. Hasenyager

BOREHOLE ID: G272

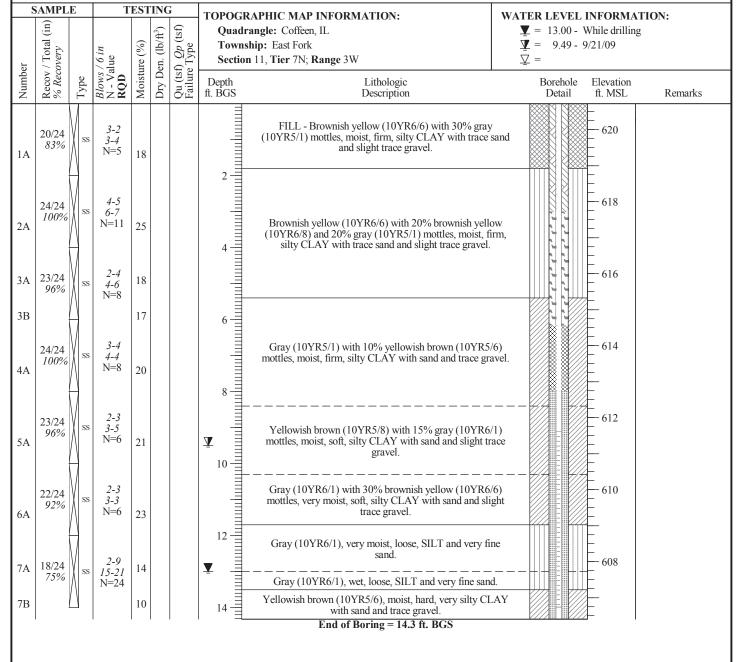
Well ID: G272

 Surface Elev:
 620.72 ft. MSL

 Completion:
 14.32 ft. BGS

 Station:
 874,234.83N

 2.515,744.99E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

DATES: Start: 9/10/2009 Finish: 9/10/2009 CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS & CME samplers

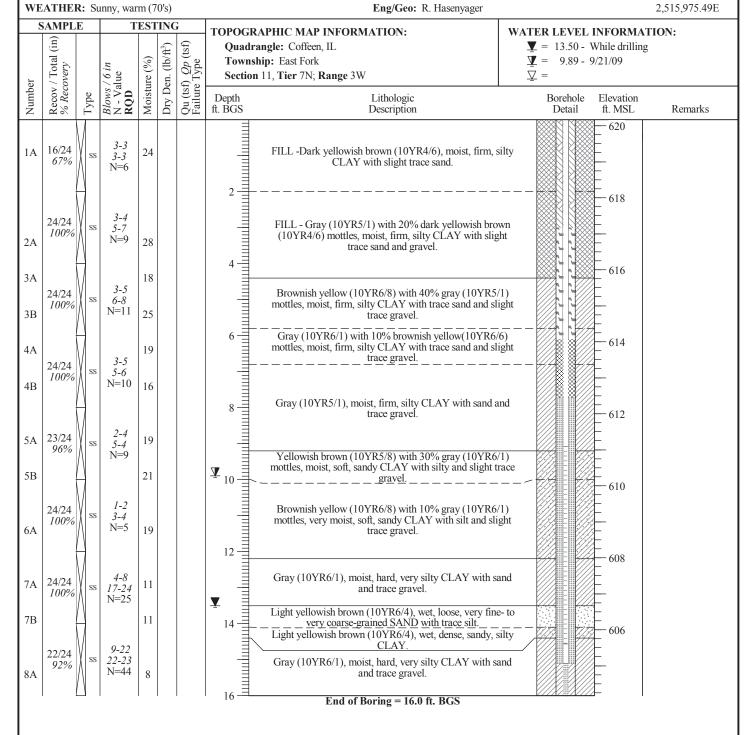
FIELD STAFF: Driller: G. Mills Helper: J. Twellman

Eng/Geo: R. Hasenyager



BOREHOLE ID: G273 Well ID: G273

> Surface Elev: 620.17 ft. MSL **Completion:** 16.00 ft. BGS **Station:** 874,235.24N 2,515,975.49E



NOTE(S):

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 9/16/2009 **Finish:** 9/16/2009

WEATHER: Sunny, warm (80's)

NOTE(S):

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: G. Mills Helper: J. Twellman

Eng/Geo: R. Hasenyager

BOREHOLE ID: G274 Well ID: G274

Surface Elev: 621.67 ft. MSL Completion: 18.06 ft. BGS Station: 874,239.25N 2,516,195.60E

Page 1 of 1

SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: Qu (tsf) *Qp* (tsf) Failure Type Quadrangle: Coffeen, IL $\mathbf{V} = 16.00$ - While drilling Dry Den. (lb/ft³) Recov / Total (% Recovery Moisture (%) Township: East Fork $\Psi = 13.12 - 9/21/09$ Blows / 6 in N - Value RQD Section 11, Tier 7N; Range 3W Number Borehole Lithologic Elevation ft. BGS Description ft. MSL Remarks 2-3 20/24 3-4 83% N=61 A 17 620 $FILL\ -\ Gray\ (10YR5/1)\ with\ 30\%\ yellowish\ brown\ (10YR5/6)\ mottles,\ moist,\ firm,\ silty\ CLAY\ with\ trace\ sand$ 4-6 24/24 7-9 and slight trace gravel. 100% N = 1325 2A 618 24/24 26 3A 6-9 100% N=103B 21 3-6 Gray (10YR5/1) with 20% yellowish brown (10YR5/6) 16/24 6-8 mottles, moist, firm, silty CLAY with slight trace sand and 67% N=12gravel. 24 4A 614 24/24 4-6 Dark gray (10YR4/1) with 15% yellowish brown (10YR5/8) mottles, moist, soft, silty CLAY with trace sand 100% N=8 20 5A and slight trace gravel. 1-3 22/24 4-6 92% 19 6A 610 Gray (10YR5/1) with 30% yellowish brown (10YR5/8) 23/24 <u>1</u> 4-4 mottles, moist, soft, silty CLAY with sand and trace gravel. 96% N=6 7A 21 608 1-3 22/24 3-6 92% N=68A 17 Yellowish brown (10YR5/8), very moist, soft, silty CLAY 606 **▼**16 with sand and trace gravel Brownish yellow (10YR6/6), wet, loose, very fine- to very coarse-grained SAND. wor-4 14/24 9A 13 SS 9-11 58% Brownish yellow (10YR6/6), moist, firm, very silty CLAY N=13with sand and gravel. Gray (10YR6/1), moist, hard, very silty CLAY with sand 9В and gravel. End of Boring = 18.1 ft. BGS

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 9/16/2009 **Finish:** 9/16/2009

WEATHER: Sunny, warm (80's)

CONTRACTOR: Layne-Western Co **Rig mfg/model:** CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS & CME samplers

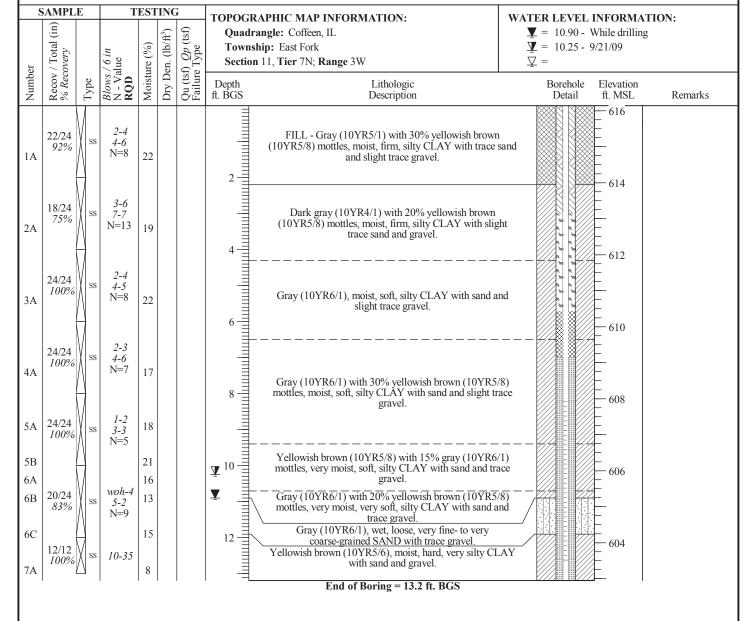
FIELD STAFF: Driller: G. Mills Helper: J. Twellman

Eng/Geo: R. Hasenyager

BOREHOLE ID: G275

Well ID: G275

Surface Elev: 616.14 ft. MSL Completion: 13.19 ft. BGS Station: 874,298.94N 2,516,375.86E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 9/16/2009

Finish: 9/16/2009
WEATHER: Sunny, mild (70'S)

CONTRACTOR: Layne-Western Co **Rig mfg/model:** CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: G. Mills Helper: J. Twellman

Eng/Geo: R. Hasenyager



BOREHOLE ID: G276 **Well ID:** G276

 Surface Elev:
 629.14 ft. MSL

 Completion:
 28.00 ft. BGS

 Station:
 874,438.60N

 2,516,358.83E

Page 1 of 2

| | WEATHER: Sunny, mild (70'S) SAMPLE TESTING | | | | | | | Eng/Geo: R. Hasenyager 2,516, TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: | | | | | |
|---|---|------|----------------------------------|--------------|-------------------|---------------------------------------|--|---|--------------------|---|-----------------------------------|--|--|
| Number Recov / Total (in) % Recovery Type | | | | | Dry Den. (lb/ft³) | Qu (tsf) <i>Qp</i> (tsf) Failure Type | TOPOGR Quadr Towns Section | APHIC MAP INFORMATION: angle: Coffeen, IL hip: East Fork 11, Tier 7N; Range 3W | | While drillin | | | |
| Number | Recov % Reco | Type | Blows / 6 in N - Value RQD | Moisture (%) | Dry De | Qu (tsf Failure | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks | | |
| 1A | 17/24 71% | ss | 5-8 9-10 N=17 | 10 | | | 2 | | | 628 | | | |
| 2A | 19/24 79% | SS | 7-7 10-14 N=17 | 15 | | | | FILL - Yellowish brown (10YR5/4) with 20% gray (10YR5/1) mottles, moist, hard, silty CLAY with trace s and slight trace gravel. | and | 626 626 | | | |
| 3A | 11/24 46% | ss | 5-10 14-27 N=24 | 14 | | | 4-1 | | | | Rock fragment in split spoon shoe | | |
| 4A | 24/24 100% | ss | 5-9 10-14 | 8 | | | | FILL - Yellowish brown (10YR5/4) with 20% gray (10YR5/1) mottles, slightly moist, hard, silty CLAY with trace sand and slight trace gravel. | th | | | | |
| 4B | | | N=19 | 5 | | | 8 | FILL - Yellowish brown (10YR5/4) with 10% gray (10YR5/1) mottles, slightly moist, hard, friable, clayer SILT with sand and trace gravel. | y | | | | |
| 5A | 17/24 71% | ss | 4-4 8-19 N=12 | 22 | | | 10- | | | | | | |
| 6A | 17/24 71% | ss | 4-5 8-14 N=13 | 14 | | | 10 12 12 13 13 14 15 15 15 15 15 15 15 | FILL - Yellowish brown (10YR5/4) with 25% gray (10YR5/1) mottles, slightly moist, firm, silty CLAY wis slight trace sand and gravel. | th | - - - - - - - - - - - - - - - - - - - | | | |
| 7A | 16/24 67% | SS | 6-7 2-4 N=9 | 20 | | | | | | 616 | | | |
| 8A | 20/24 83% | SS | 2-4 6-6 N=10 | 21 | | | 14 | Gray (10YR6/1) with 10% yellowish brown (10YR5/8 mottles, moist, firm, silty CLAY with slight trace sand a gravel. | 3) nd | 614 | | | |
| 9A | 22/24 | | 1-4 | 17 | | | 16- | | | | | | |
| 9B | 92% | SS | 5-7 N=9 | 13 | | | 18 | Gray (10YR6/1) with 20% yellowish brown (10YR5/t mottles, moist, soft, sandy CLAY with silt and slight tragravel. | 6) ce | 612 | | | |
| 10A | 23/24 96% | ss | 2-3 8-12 N=11 | 20 | | | 20 | Gray (10YR6/1) with 30% yellowish brown (10YR5/8 mottles, moist, firm, silty CLAY with sand and slight tragravel. | | 610 | | | |

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 9/16/2009

Finish: 9/16/2009 **WEATHER:** Sunny, mild (70'S)

CONTRACTOR: Layne-Western Co **Rig mfg/model:** CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: G. Mills

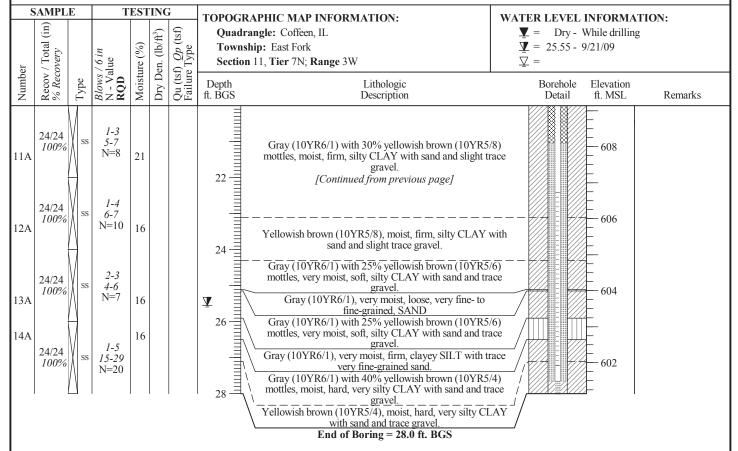
Helper: J. Twellman **Eng/Geo:** R. Hasenyager



BOREHOLE ID: G276 Well ID: G276

> Surface Elev: 629.14 ft. MSL Completion: 28.00 ft. BGS Station: 874,438.60N

> > 2,516,358.83E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 9/14/2009 **Finish:** 9/14/2009

WEATHER: Sunny, mild (70'S)

CONTRACTOR: Layne-Western Co **Rig mfg/model:** CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: G. Mills Helper: J. Twellman

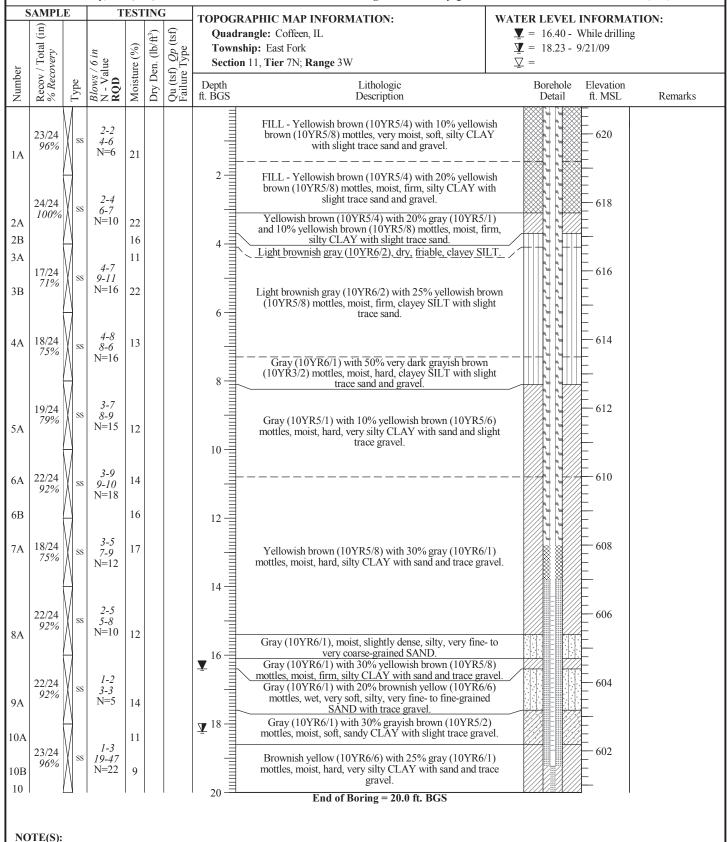
Eng/Geo: R. Hasenyager



BOREHOLE ID: G277 Well ID: G277

> Surface Elev: 620.79 ft. MSL Completion: 20.00 ft. BGS Station: 874,581.80N 2.516,370.51E

> > Page 1 of 1



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 9/11/2009

Finish: 9/11/2009 **WEATHER:** Sunny, warm (70's)

CONTRACTOR: Layne-Western Co **Rig mfg/model:** CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: G. Mills Helper: J. Twellman

 $\pmb{Eng/Geo\colon}\ R.\ Hasenyager$

BOREHOLE ID: G278 Well ID: G278

Surface Elev: 628.85 ft. MSL Completion: 24.06 ft. BGS

HANSON

Station: 874,875.37N 2,516,200.66E

| SAMPI | LE T | T | EST | INC | | TOPOGR | APHIC MAP INFORMATION: | WATER L | EVEL | INFORMA | TION: |
|---|------------------------|----------------------------------|--------------|-------------------|--|---|--|--|------------------|---|-----------------------------------|
| Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) <i>Qp</i> (tsf) Failure Type | Quadra Townsl Section | angle: Coffeen, IL nip: East Fork 11, Tier 7N; Range 3W | $ \underline{\underline{\mathbf{Y}}} = 2 $ $ \underline{\underline{\mathbf{Y}}} = 2 $ $ \underline{\underline{\mathbf{Y}}} = 2 $ | | While drillin 9/21/09 | g |
| Recov / / / / / / / / / / / / / / / / / / / | Туре | Blow N - V RQD | Moist | Dry I | Qu (t Failu | | Lithologic Description | | rehole Oetail | Elevation ft. MSL | Remarks |
| A 16/24 67% | ss | 3-4 6-7 N=10 | 19 | | | 2 | | | | | |
| A 24/24 | ss | 4-7 8-11 N=15 | 21 | | | 4- | | | | 626 | |
| A 22/24 92% | ss | 9-10 9-35 N=19 | 10 | | | 6 | | | | 624 | Rock fragment in split spoon shoe |
| A 4/24 17% | SS | 20-7 10-8 N=17 | | | | | FILL - Yellowish brown (10YR5/4) with 15% yellow brown(10YR5/8) mottles, moist, hard, silty CLAY w trace sand and slight trace gravel. | rish ith | | 622 | Rock fragment in split spoon shoe |
| A 14/24 58% | ss | 11-6 8-8 N=14 | 15 | | | 2 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | | | | - - - 620 - - - | Rock fragment in split spoon shoe |
| A 20/24 83% | ss | 6-4 8-9 N=12 | 26 | | | 12 — | | | | - - - - - - - - - - - | |
| 24/24 100% | SS | 2-4 8-11 N=12 | 18 | | | | Gray (10YR6/1) with 30% brownish yellow (10YR6 | /6) | | 616 | |
| A 20/24 83% | SS | 4-7 10-11 N=17 | 12 | | | 14 | mottles, moist, firm, clayey SILT with slight trace sar Very dark gray (10YR3/1), moist, firm, clayey SILT v slight trace sand and trace roots. | with | | 614 | |
| В | $\left(\cdot \right)$ | | 22 | | | 16 | Gray (10YR5/1) with 30% yellowish brown (10YR5 mottles, moist, firm, silty CLAY with sand and trace grant grant trace grant trace grant trace grant trace grant gr | /8) avel. | | | |
| A 22/24 92% | ss | 4-6 6-9 N=12 | 17 | | | 18 | Gray (10YR6/1) with 10% yellowish brown (10YR5 mottles, moist, firm, silty CLAY with sand and trace grays. | | | 612 | |
| 20/24 83% | ss | 2-4 5-8 N=9 | 21 | | | 20 | Yellowish brown (10YR5/8) with 20% gray (10YR5, mottles, moist, firm, silty CLAY with sand and trace grays. | | | 610 | |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

TESTING

Moisture (%)

19

16

10

▼ 24

Blows / 6 in N - Value RQD

N=11

1-5

10-18 N=15 SS

Dry Den. (lb/ft³)

Location: Coffeen, Illinois Project: 05S3004A

DATES: Start: 9/11/2009 Finish: 9/11/2009

WEATHER: Sunny, warm (70's)

SAMPLE

Recov / Total (in) % Recovery

18/24

20/24

83%

75%

Number

11A

11B

12A

12B

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: G. Mills Helper: J. Twellman

TOPOGRAPHIC MAP INFORMATION:

Quadrangle: Coffeen, IL

Township: East Fork

Eng/Geo: R. Hasenyager

2,516,200.66E WATER LEVEL INFORMATION:

BOREHOLE ID: G278

Well ID: G278

Surface Elev: 628.85 ft. MSL

Completion: 24.06 ft. BGS

Station: 874,875.37N

Remarks

▼ = Dry - While drilling $\mathbf{V} = 23.98 - 9/21/09$

 $\nabla =$

Qu (tsf) *Qp* (tsf) Failure Type Section 11, Tier 7N; Range 3W Depth Borehole Elevation Lithologic ft. BGS Description Detail ft. MSL Yellowish brown (10YR5/8) with 20% gray (10YR5/1) mottles, moist, firm, silty CLAY with sand and trace gravel. 608 [Continued from previous page] Yellowish brown (10YR5/6), very moist, soft, silty, very fine- to medium-grained SAND. 606 Yellowish brown (10YR5/4), moist, hard, very silty CLAY with sand and trace gravel.

End of Boring = 24.1 ft. BGS

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 9/10/2009

Finish: 9/10/2009 WEATHER: Sunny, warm (80's) **CONTRACTOR:** Layne-Western Co **Rig mfg/model:** CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: G. Mills Helper: J. Twellman

Eng/Geo: R. Hasenyager



BOREHOLE ID: G279 **Well ID:** G279

 Surface Elev:
 629.19 ft. MSL

 Completion:
 28.00 ft. BGS

 Station:
 875,028.06N

 2,516,245.60E

| SAMPLE TESTING | | | | | | TOPOGR | APHIC MAP INFORMATION: | WATER LEVEL INFORMATION: | | | |
|--------------------------------------|------|----------------------------------|--------------|-------------------|--|--|--|--|----------------------|---------|--|
| Number Recov / Total (in) % Recovery | (I) | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) <i>Qp</i> (tsf) Failure Type | Quadra Townsh Section | ingle: Coffeen, IL iip: East Fork 11, Tier 7N; Range 3W | $\underline{\underline{\mathbf{Y}}} = 23.60 - \underline{\underline{\mathbf{Y}}} = 24.68 - \underline{\underline{\mathbf{Y}}} = $ | 9/21/09 | | |
| Number Recov / '% Recov | Type | Blov N - N | Moi | Dry | Qu (Failt | | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks | |
| A 24/24 100% | SS | 3-3 5-6 N=8 | 18 | | | 2 | FILL - Brown (10YR4/3) with 30% yellowish brown (10YR5/6) mottles, moist, firm, silty CLAY with sand trace gravel. | n and | 628 | | |
| 24/24 100% | ss | 5-9 10-11 N=19 | 14 | | | 4- | | | - 626 | | |
| 3A 24/24 100% | ss | 5-9 9-10 N=18 | 17 | | | 6- | | 7,7,7,7,7,7 | 624 | | |
| 1A 24/24 100% | ss | 4-5 7-6 N=12 | 21 | | | 8- | FILL - dark gray (10YR4/1) with 10% brownish yellov (10YR6/6) mottles, moist, hard, silty CLAY with sand a trace gravel. | 7,7,7,7,7,7 | 622 | | |
| 5A 24/24 100% | SS | 3-3 5-7 N=8 | 19 | | | 4 ———————————————————————————————————— | | and | 620 | | |
| 5A 24/24 100% | ss | 3-4 6-9 N=10 | 17 | | | 12 — | | 1,2,2,2,2,2,2,2,2,2,2,2,2,2,2,2,2,2,2,2 | 618 | | |
| 7A 23/24 96% | ss | 2-5 5-6 N=10 | 23 | | | | | 7,7,7,7,7 | 616 | | |
| 24/24 100% | SS | 2-3 7-6 N=10 | 23 | | | 16.3 | Brownish yellow (10YR6/8) with 30% gray (10YR5/mottles, moist, firm, silty CLAY with slight trace sand gravel. | (1) and | 614 | | |
| 18/24 75% | SS | 4-7 8-9 N=15 | 25 | | | 16 | Yellowish brown (10YR5/8) with 20% gray (10YR6/mottles, moist, firm, silty CLAY with slight trace sand gravel. | and | 612 | | |
| 0A 24/24 100% | SS | 3-6 7-10 N=13 | 17 | | | 20 | Gray (10YR6/1) with 25% yellowish brown (10YR5/mottles, moist, firm, silty CLAY with sand and trace gra | (8) avel. | 610 | | |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 9/10/2009

Finish: 9/10/2009 WEATHER: Sunny, warm (80's) **CONTRACTOR:** Layne-Western Co **Rig mfg/model:** CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: G. Mills Helper: J. Twellman

Eng/Geo: R. Hasenyager

2,516,245.60E

BOREHOLE ID: G279

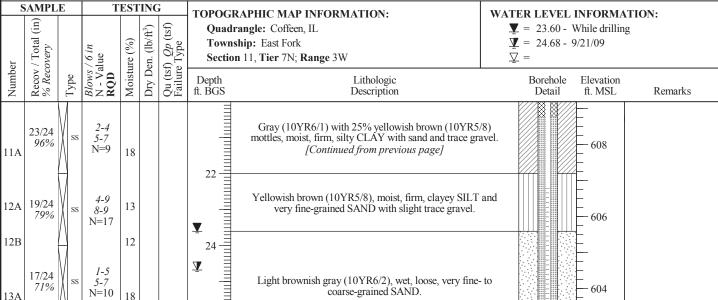
602

Well ID: G279

Surface Elev: 629.19 ft. MSL

Completion: 28.00 ft. BGS

Station: 875,028.06N



Brownish yellow (10YR6/6), moist, hard, very silty CLAY

with sand and trace gravel.

Gray (10YR6/1), moist, hard, very silty CLAY with sand and trace gravel.

End of Boring = 28.0 ft. BGS

26

16

14

10-10

N=28

ss | 18-18

14A

14B

24/24

100%

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

DATES: Start: 2/26/2008

NOTE(S):

Finish: 2/26/2008 WEATHER: Overcast, cold

CONTRACTOR: Testing Service Corp. Rig mfg/model: CME-650 Track Drill

Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo:

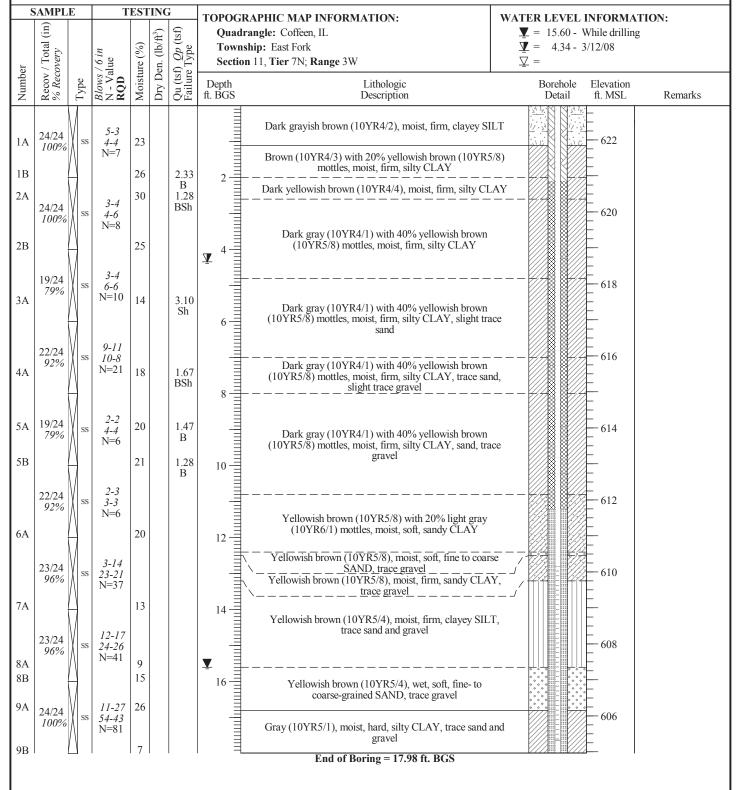
BOREHOLE ID: G280

Well ID: G280

Surface Elev: 622.95 ft. MSL Completion: 17.98 ft. BGS **Station:** 875,045.11N

2,515,679.48E

Page 1 of 1



CLIENT: Natural Resource Technology, Inc.

Site: Coffeen Energy Center Location: Coffeen, Illinois Project: 15E0030

DATES: Start: 9/8/2015

Finish: 9/8/2015 **WEATHER:** Sunny, hi 70's

CONTRACTOR: Ramsey Geotechnical Engineering, LLC

Rig mfg/model: D-50 Turbo Tracked MST 800ATV Drilling Method: Hollow Stem Auger (3¼"overdrill / 4¼")

FIELD STAFF: Driller: D. Crump Helper: D. Groves

Eng/Geo: K. Theesfeld



BOREHOLE ID: G281 **Well ID:** G281

Surface Elev: 623.82 ft. MSL Completion: 20.29 ft. BGS Station: 2,514,455.48N

874,375.37E

| | SAMPLE TESTING | | | | | | TOPOGR | APHIC MAP INFORMATION: | WATER LEVEL INFORMATION: | |
|--|-------------------|------|----------------------------------|--------------|-------------------|--|------------------|---|--|-----|
| Number Recov / Total (in) % Recovery | | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) <i>Qp</i> (tsf) Failure Type | Quadra Towns | angle: Coffeen, IL hip: East Fork 10, Tier 7N; Range 3W | $\underline{\underline{\mathbf{Y}}} = 14.00$ - During Drilling $\underline{\underline{\mathbf{Y}}} = \underline{\underline{\mathbf{Y}}} = \underline{\underline{\mathbf{Y}}} = \underline{\underline{\mathbf{Y}}}$ | |
| Number | Recov % Rec | Type | Blows N - Va RQD | Moist | Dry D | Qu (ts Failur | Depth ft. BGS | Lithologic Description | Borehole Elevation Detail ft. MSL Reman | rks |
| lA | 17/24 71% | SS | 15-10 7-6 N=17 | 14 | | | 2 | Light gray (10YR7/2), dry, very stiff, SILT with little cand trace gravel. Yellowish brown (10YR5/4) with 5% dark brown (10YR3/3) mottles, dry, very stiff, SILT with few clay trace gravel. | | |
| 2A | 19/24 79% | SS | 2-4 5-5 N=9 | 25 | | 1.50 | 4- | Yellowish brown (10YR5/4) with 15% dark yellowish brown (10YR4/6) and 5% dark brown (10YR3/3) mott moist, stiff, SILT with few clay. | sh ttles, | |
| βA | 22/24 92% | SS | 2-2 3-4 N=5 | 23 | | 0.40 | | Yellowish brown (10YR5/4) with 15% dark yellowish brown (10YR4/6) mottles, moist, medium, CLAY with some silt and trace fine-grained sand and small grave | ith /// | |
| ŀA | 24/24 100% | ss | 5-5 6-6 N=11 | 19 | | 1.20 | 8 10 10 | Yellowish brown (10YR5/4) with 15% dark yellowis brown (10YR4/6) and 5% dark brown (10YR3/3) mott moist, stiff, CLAY with some silt and trace fine-graine sand and small gravel. | tles, | |
| 5A | 20/24 83% | ss | 2-2 3-4 N=5 | 21 | | 1.40 | 10 | Yellowish brown (10YR5/4) with 30% dark yellowish brown (10YR4/6) and 5% dark brown (10YR3/3) mott moist, stiff, SILT with some clay and trace very fine-fine-grained sand and small gravel. | sh tles, to 614 | |
| 6A | 22/24 92% | ss | 2-2 3-3 N=5 | 18 | | 0.50 | 12 | Dark yellowish brown (01YR4/6) with 30% yellowis brown (10YR5/4) mottles, moist, soft, SILT with few c and little fine- to coarse-grained sand and small gravel, t wood fragments. | clay 😹 😹 🗀 | |
| 7A | 17/24 71% | ss | 3-4 5-5 N=9 | 19 | | 0.30 | ¥ 14 | Dark yellowish brown (01YR4/6) with 15% yellowish brown (10YR5/4) mottles, moist, soft, SILT with few cand very fine- to fine-grained sand and trace small graves. | clay | |
| | 19/24 79% | SS | 3-11 21-28 N=32 | | | | 16 | Dark yellowish brown (10YR4/4), wet, dense, very fine fine-grained SAND with some silt, few clay and trace sr gravel. | | |
| | 24/24 100% | SS | 21-36 39-50 N=75 | | | | 10 = | Dark yellowish brown (10YR4/4), wet, dense, very fine fine-grained SAND with few silt, little clay and trace sn gravel. Yellowish brown (10YR5/6) with 5% strong brown | mall | |
| 8A | 11/24 46% | ss | 16-9 30-50 N=39 | 7 | | 4.50 | 18 - 20 - 3 | (7.5YR5/6) mottles, moist, hard, SILT with few clay a little fine-grained sand and small gravel. Dark grayish brown (10YR4/2) with 5% strong brow (7.5YR5/6) mottles, moist, hard, SILT with few clay a little fine-grained sand and small gravel. | and | |
| | $\frac{0/3}{0\%}$ | BD | | | | | 20 = | End of boring = 20.29 feet | | |

CLIENT: Natural Resource Technology, Inc.

Site: Coffeen Energy Center Location: Coffeen, Illinois

DATES: Start: 9/4/2015 Finish: 9/4/2015

WEATHER: Sunny, hi 70's

Drilling Method: Hollow Stem Auger (31/4"overdrill / 41/4") Project: 15E0030

FIELD STAFF: Driller: D. Crump Helper: D. Groves

Eng/Geo: K. Theesfeld

CONTRACTOR: Ramsey Geotechnical Engineering, LLC

Rig mfg/model: D-50 Turbo Tracked MST 800ATV

HANSON

BOREHOLE ID: G301 Well ID: G301

> Surface Elev: 620.27 ft. MSL **Completion:** 16.21 ft. BGS **Station:** 2,515,582.97N 872,234.82E

| | SAMPLE TESTING | | | TOPOGRA | APHIC MAP INFORMATION: | WATER LEVEL INFORMATION: | | | | | |
|--------|----------------------------------|------|--|--------------|------------------------|--------------------------|--|--|---|---|---|
| er | Recov / Total (in) % Recovery | | / 6 in Ilue | Moisture (%) | Dry Den. (lb/ft³) | en. (lb/ft³) | en. (lb/ft³) | Qu (tsf) <i>Qp</i> (tsf) Failure Type | Quadra Townsh | ngle: Coffeen, IL ip: East Fork 11, Tier 7N; Range 3W | $\underline{\underline{V}} = 12.00 - \text{During Drilling}$ $\underline{\underline{V}} = \underline{\underline{\nabla}} = \underline{\underline{\nabla}} = \underline{\underline{\nabla}}$ |
| Number | Recov % Rec | Type | lype Blows / 6 in N - Value RQD | | Dry D | Qu (ts Failur | Depth ft. BGS | Lithologic Description | Borehole Elevation Detail ft. MSL Remarks | | |
| 1A | 19/24 79% | ss | 4-4 3-5 N=7 | 18 | | 1.80 | | Brown (10YR4/3), moist, stiff, SILT with few clay, tronganics. | | | |
| 2A | 22/24 92% | SS | 2-4 4-6 N=8 | 26 | | 2.40 | 2 4 4 4 | Brown (10YR5/3) with 30% yellowish brown (10YR5/2) mottles, moist, stiff, SILT with few clay, trace organic Brown (10YR5/3) with 30% yellowish brown (10YR5/2) mottles, moist, stiff, SILT with few clay, trace very fine medium-grained sand. | cs 618 5/6) e- to | | |
| 3A | 21/24 88% | SS | 2-2 3-4 N=5 | 22 | | 1.30 | | Brown (10YR5/3) with 15% yellowish brown (10YR5 mottles, moist, stiff, CLAY with some silt and trace verifine- to medium-grained sand. | 5/6) ery | | |
| 4A | 24/24 100% | SS | 6-4 6-6 N=10 | 19 | | 1.10 | 6 | Brown (10YR5/3) with 10% yellowish brown (10YR5 mottles, moist, medium to stiff, CLAY with some silt a little very fine- to coarse-grained sand and small grave | and ///🔉 🕅 /// 🗀 | | |
| 5A | 21/24 88% | SS | 1-2 3-4 N=5 | 21 | | | | Brown (10YR5/3) with 5% yellowish brown (10YR5 mottles, moist, stiff, SILT with some clay and little ve fine- to coarse-grained sand and small gravel. | 6/6) | | |
| 6A | 24/24 100% | SS | 3-2 3-3 N=5 | 19 | | 0.80 | 10 - 12 - 12 - 12 - 12 - 12 - 12 - 12 - 12 - 12 - 12 | Brown (10YR5/3) with 20% yellowish brown (10YR5 mottles, moist, stiff, SILT with some clay and little ve fine- to coarse-grained sand and small gravel. | 5/6) | | |
| 7A | 24/24 100% | SS | 2-4 6-21 N=10 | 13 | | 1.60 | | Yellowish brown (10YR5/6) with 10% grayish brow (10YR5/2) and 5% yellowish brown (10YR5/4) mottl wet, stiff, SILT with few clay and little fine- to coarse-grained sand and small gravel. | vn les, | | |
| 8A | 21/24 88% | SS | 20-27 50 N=77 | 7 | | 4.50 | 14 - | Grayish brown (10YR5/2) with 5% brown (10YR5/2) mottles, dry, hard, SILT with few clay, very fine-to coarse-grained sand and small gravel. | 3) | | |
| | 0% | | | | | ' | . — | End of boring = 16.21 feet | | | |

CLIENT: Natural Resource Technology, Inc.

Site: Coffeen Energy Center Location: Coffeen, Illinois Project: 15E0030

DATES: Start: 9/3/2015 **Finish:** 9/4/2015

WEATHER: Sunny, hi 70's

CONTRACTOR: Ramsey Geotechnical Engineering, LLC

Rig mfg/model: D-50 Turbo Tracked MST 800ATV **Drilling Method:** Hollow Stem Auger (3¹/₄"overdrill / 4¹/₄")

FIELD STAFF: Driller: D. Crump Helper: D. Groves

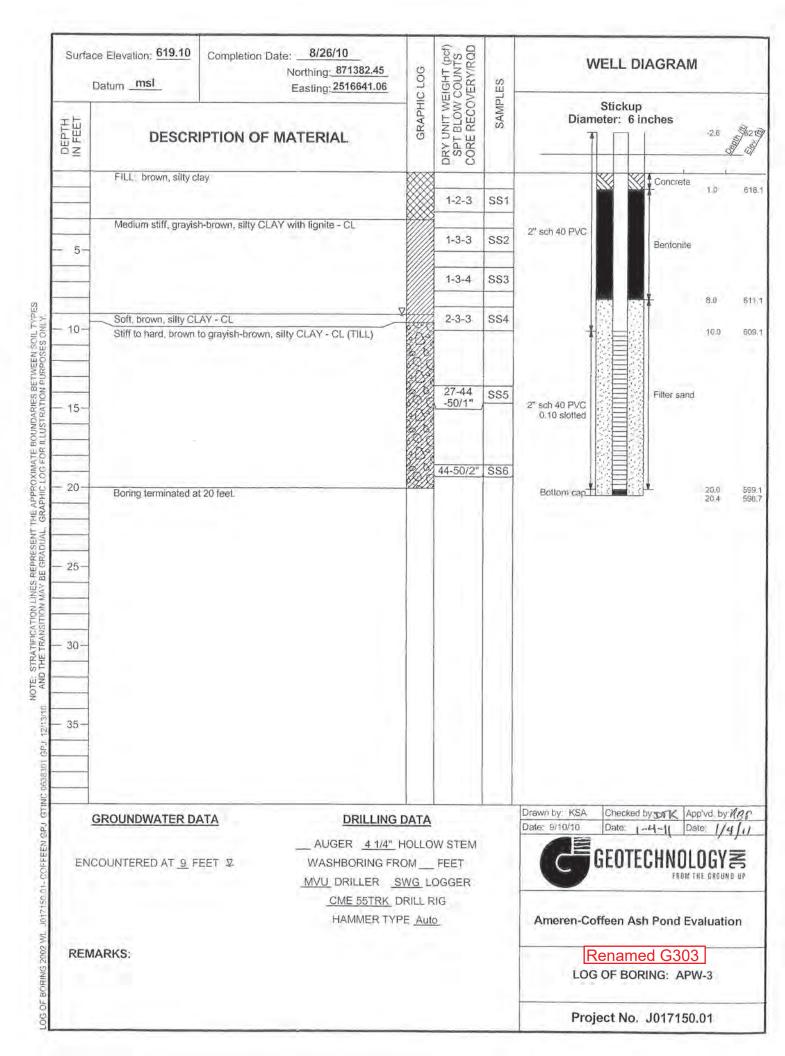
Eng/Geo: K. Theesfeld

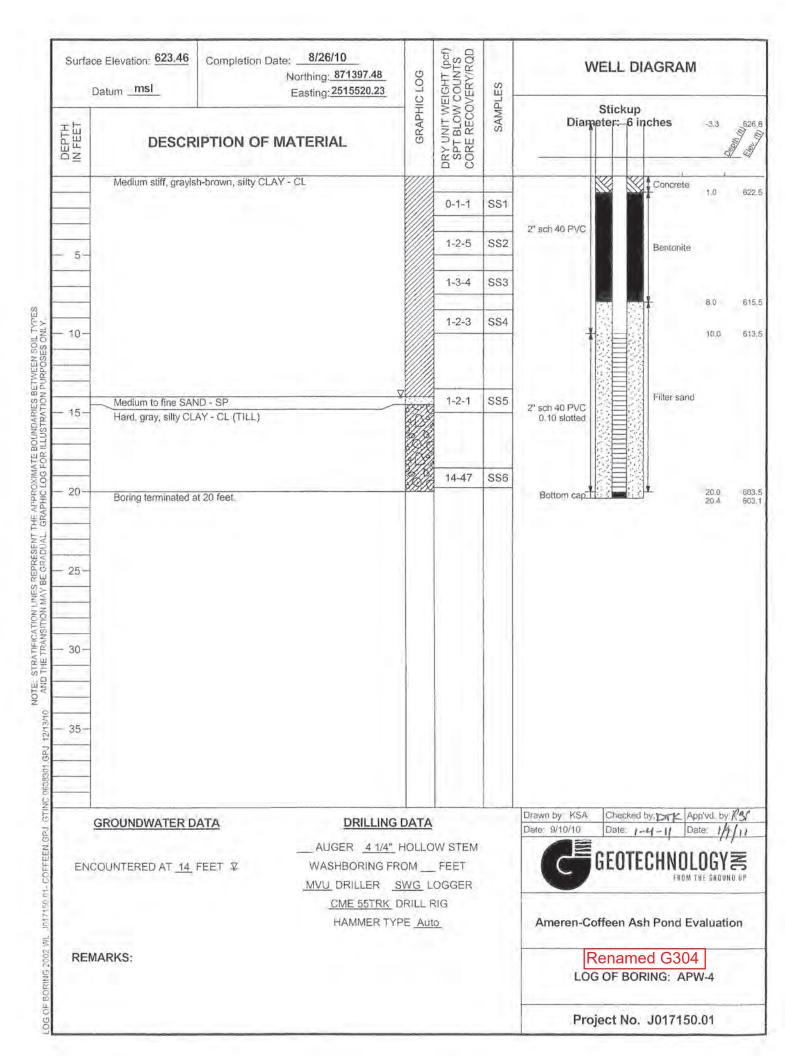
HANSON

BOREHOLE ID: G302 **Well ID:** G302

> Surface Elev: 617.95 ft. MSL Completion: 18.39 ft. BGS Station: 2,516,214.19N 872,252.95E

SAMPLE **TESTING** TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: (iii Qu (tsf) *Qp* (tsf) Failure Type $\mathbf{V} = 14.00$ - During Drilling Dry Den. (lb/ft³) Quadrangle: Coffeen, IL Recov / Total (% Recovery Moisture (%) Township: East Fork **T** = Blows / 6 in N - Value RQD $\nabla =$ Section 11, Tier 7N; Range 3W Number Lithologic Borehole Elevation ft. BGS Description ft. MSL Remarks Yellowish brown (10YR5/6) to dark yellowish brown 5-5 23/24 (10YR4/6), moist, hard, SILT with some clay and trace 5-6 96% fine-grained sand and small gravel. N=101 A 17 1.50 Very dark brown (10YR3/1), moist, hard, SILT with some clay and trace fine-grained sand and small gravel. 2-3 20/24 2A 27 2.60 4-4 83% N=7Dark grayish brown (10YR4/2) with very dark gray (10YR3/1) mottles, moist, stiff, CLAY with some silt and 614 trace sand. 21/24 3-4 Brown (10YR5/3) with dark yellowish brown (10YR4/6) 88% mottles, moist, stiff, CLAY with some silt and trace sand. 3A 26 1.80 24/24 18 1.60 8-8 100% N=15Brown (10YR5/3) with dark yellowish brown (10YR4/6) 610 mottles, moist, stiff, CLAY with some silt and few very fine- to fine-grained sand. 24/24 17 1.80 5-5 100% 608 Brown (10YR4/3) with dark yellowish brown (10YR4/6) 2-2 18/24 mottles, moist, stiff, SILT with some clay and few sand. 4-5 75% N=619 6A Dark gray (10YR4/1), moist, stiff, SILT with some clay 606 and few sand. Yellowish brown (10YR5/8) with reddish brown (5YR4/4) inclusions, moist, stiff, SILT with some clay and few sand. 24/24 8-8 100% N=157A 16 1.70 Dark gray (10YR4/1), moist, stiff, SILT with some clay, few sand and trace small gravel. **▼** 14 604 8A 18 0.80 8B 22/24 12 4.50 Grayish brown (10YR5/2), wet, hard, SILT with little clay 25-32 92% and very fine-grained sand and trace small gravel. N = 30602 Brown (10YR5/3), wet, hard, SILT with little clay and very fine-grained sand and trace small gravel. 7-24 24/24 48-38 100% N=72 4.50 9A 8 Brown (10YR5/3) grading to yellowish brown (10YR5/4), moist, hard, SILT with some clay, few small gravel. 0/50% End of boring = 18.39 feet





CLIENT: Natural Resource Technology, Inc.

Site: Coffeen Power Station

Location: Coffeen, Illinois

Project: 15E0030

DATES: Start: 5/3/2016 **Finish:** 5/3/2016

NOTE(S): G305 installed in borehole.

WEATHER: Cloudy, breezy, warm, lo 60s

CONTRACTOR: Ramsey Geotechnical Engineering LLC

Rig mfg/model: D-50 Turbo Tracked MST 800ATV **Drilling Method:** 4 1/4" HSA, split spoon sampler

FIELD STAFF: Driller: B. Williamson Helper: D. Crump

Eng/Geo: S. Keim

BOREHOLE ID: G305 Well ID: G305

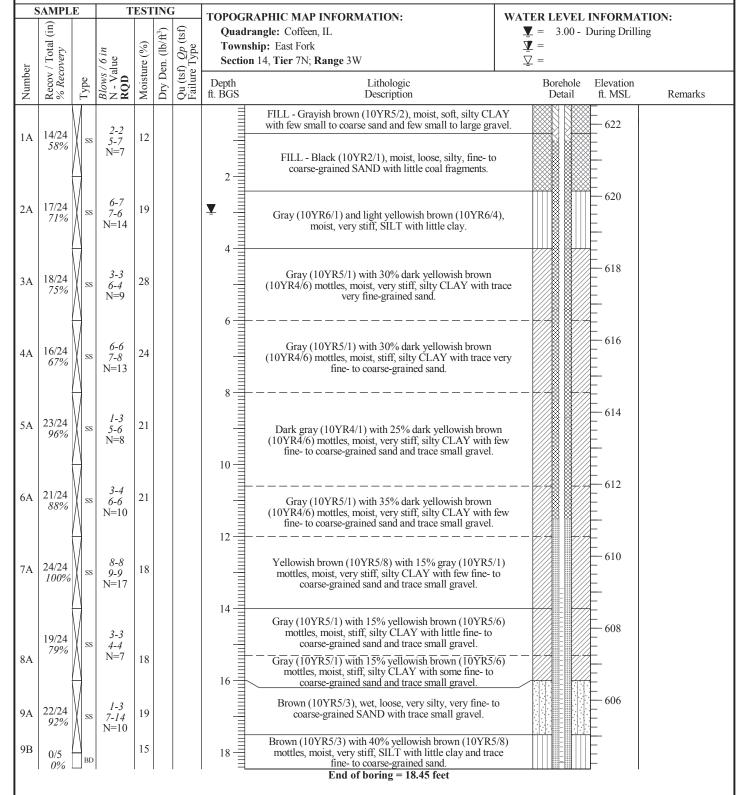
 Surface Elev:
 622.54 ft. MSL

 Completion:
 18.45 ft. BGS

 Station:
 2,515,199.36N

871,156.33E

Page 1 of 1



CLIENT: Natural Resource Technology, Inc.

Site: Coffeen Power Station
Location: Coffeen, Illinois
Project: 15E0030

DATES: Start: 5/3/2016 Finish: 5/3/2016 WEATHER: Sunny, calm, warm, lo 60s CONTRACTOR: Ramsey Geotechnical Engineering LLC

Rig mfg/model: D-50 Turbo Tracked MST 800ATV **Drilling Method:** 4 ½" HSA, split spoon sampler

FIELD STAFF: Driller: B. Williamson Helper: D. Crump

Eng/Geo: S. Keim

HANSON

BOREHOLE ID: G306 Well ID: G306

> Surface Elev: 622.84 ft. MSL Completion: 18.00 ft. BGS Station: 2,516,120.41N

871,140.98E

| SAMPLE TESTING TO | AND A SECOND ASSESSMENT OF A SECOND ASSESSMENT A SECOND ASSESSMENT | WATER LEVEL INCORMATION. | | | |
|--|--|--|--|--|--|
| (in) (in) (st) (st) | POGRAPHIC MAP INFORMATION: Quadrangle: Coffeen, IL | WATER LEVEL INFORMATION: ▼ = 5.50 - During Drilling | | | |
| Fotal (6 in ue (86)) O (10/4) O (10/4) Type (17/4) | Township: East Fork Section 14, Tier 7N; Range 3W | $\overline{\Lambda}$ = $\overline{\Lambda}$ = | | | |
| mber mber most / cov / cov / wws / w | epth Lithologic BGS Description | Borehole Elevation Detail ft. MSL Remarks | | | |
| 1A 12/24 SS 1-3 14 N=6 14 | Very dark brown (10YR2/2), moist, medium, SILT w little clay and few very fine- to medium-grained sand, ro trace coal fragments. | 1 | | | |
| 2A 24/24 21 21 | Dark gray (10YR4/1) with 5% dark yellowish brown (10YR3/6) mottles, moist, stiff, SILT with little clay a trace very fine- to medium-grained sand. | nnd | | | |
| 2B S S S S-4 N=9 19 | Gray (10YR6/1) with 10% yellowish brown (10YR5/mottles, moist, very stiff, SILT with little clay and travery fine-grained sand. | /6) ce | | | |
| $\begin{vmatrix} 3A & 22/24 \\ 92\% & ss & 2-2 \\ 8-2 & 3-3 \\ 8-5 & s \end{vmatrix} = 30$ | Gray (10YR6/1) with 20% yellowish brown (10YR5/mottles, moist, very stiff, SILT with some clay and travery fine-grained sand. | /6) ———————————————————————————————————— | | | |
| 4A 20/24 ss 3-4 6-6 N=10 26 | | 2005, | | | |
| 5A 24/24 ss 2-2 3-3 N=5 23 | Gray (10YR5/1) with 30% dark yellowish brown (10YR4/6) mottles, moist, very stiff, silty CLAY with the very fine- to coarse-grained sand. | 614 | | | |
| $ \begin{vmatrix} 6A & 22/24 \\ 92\% & ss & \begin{cases} 1-2 \\ 3-4 \\ N=5 \end{vmatrix} 20 $ | (10YR4/6) mottles, moist, very stiff, silty CLAY with the very fine- to coarse-grained sand. | -612 | | | |
| 7A $\begin{vmatrix} 20/24 \\ 83\% \end{vmatrix}$ ss $\begin{vmatrix} 5-6 \\ 6-6 \\ N=12 \end{vmatrix}$ 21 | Gray (10YR5/1) with 30% dark yellowish brown (10YR4/6) mottles, moist, stiff, silty CLAY with few v fine- to coarse-grained sand. | very - 610 | | | |
| 8A 20/24 ss 8-14 15 | Yellowish brown (10YR5/6), wet, soft, very fine-to- coarse-grained sandy CLAY with little silt. Yellowish brown (10YR5/6), wet, medium dense, silt | 608 | | | |
| 8B N=10 12 | very fine- to medium-grained SAND with trace coarse-grained sand. Yellowish brown (10YR5/6), moist, dense, fine- to | | | | |
| 9A 23/24 ss 28-50/5" 10 N=45 | coarse-grained SAND with little silt, little very fine-grains sand, and trace small gravel. Brown (10YR5/3) with 20% dark yellowish brown (10YR5/4) with 20% dark yellowish yel | 606 | | | |
| | Brown (10YR5/3) with 20% dark yellowish brown (10YR4/6) mottles, moist, hard, SILT with little clay, very fine- to coarse-grained sand, and trace small grave. End of boring = 18.0 feet | rel. | | | |

CLIENT: Illinois Power Generating Co.

Site: Coffeen Power Station Ash Pond 1

Location: Coffeen, Illinois **Project:** 16E0108

NOTE(S):

DATES: Start: 07/26/2016 **Finish:** 07/27/2016

WEATHER: Overcast, warm & humid (mid-80s)

CONTRACTOR: Bulldog Drilling, Inc.

Rig mfg/model: CME 55LC Track Drill **Drilling Method:** 41/4" Hollow Stem Auger w/Continuous Split

Spoon

FIELD STAFF: Driller: J. Gates

Helper: C. Clines

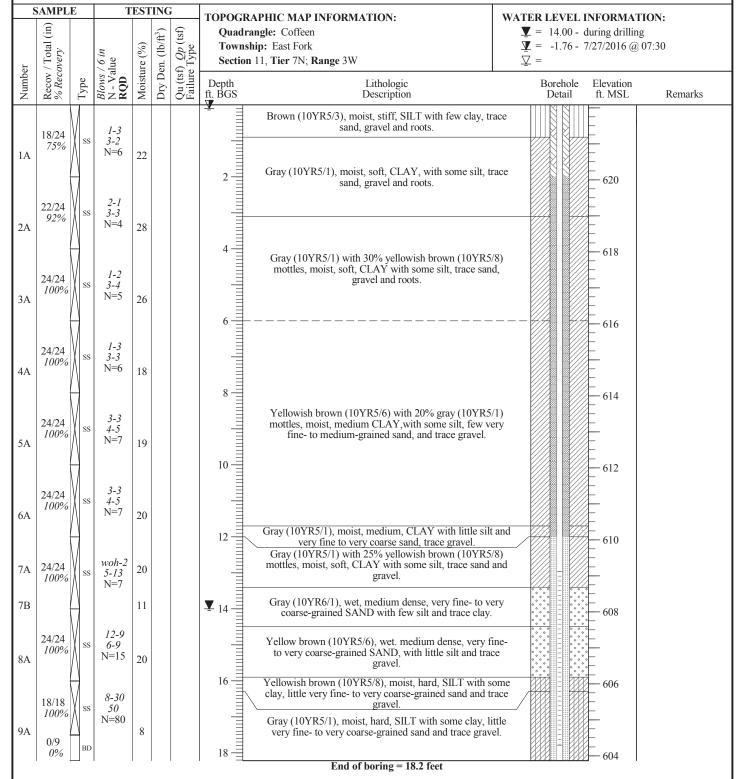
Eng/Geo: R. Hasenyager

BOREHOLE ID: G307

Well ID: G307 Surface Elev: 622.08 ft. MSL

Completion: 18.22 ft. BGS **Station:** 871,398.55N

2,515,553.26E



CLIENT: Natural Resource Technology, Inc.

Site: Coffeen Energy Center Location: Coffeen, Illinois Project: 15E0030

DATES: Start: 9/14/2015 **Finish:** 9/14/2015

NOTE(S): G401 installed in borehole.

WEATHER: Sunny, hi 60's

CONTRACTOR: Ramsey Geotechnical Engineering, LLC

Rig mfg/model: D-50 Turbo Tracked MST 800ATV Drilling Method: Hollow Stem Auger (3¼"overdrill / 4¼")

FIELD STAFF: Driller: D. Crump Helper: D. Groves

Eng/Geo: R. Hasenyager

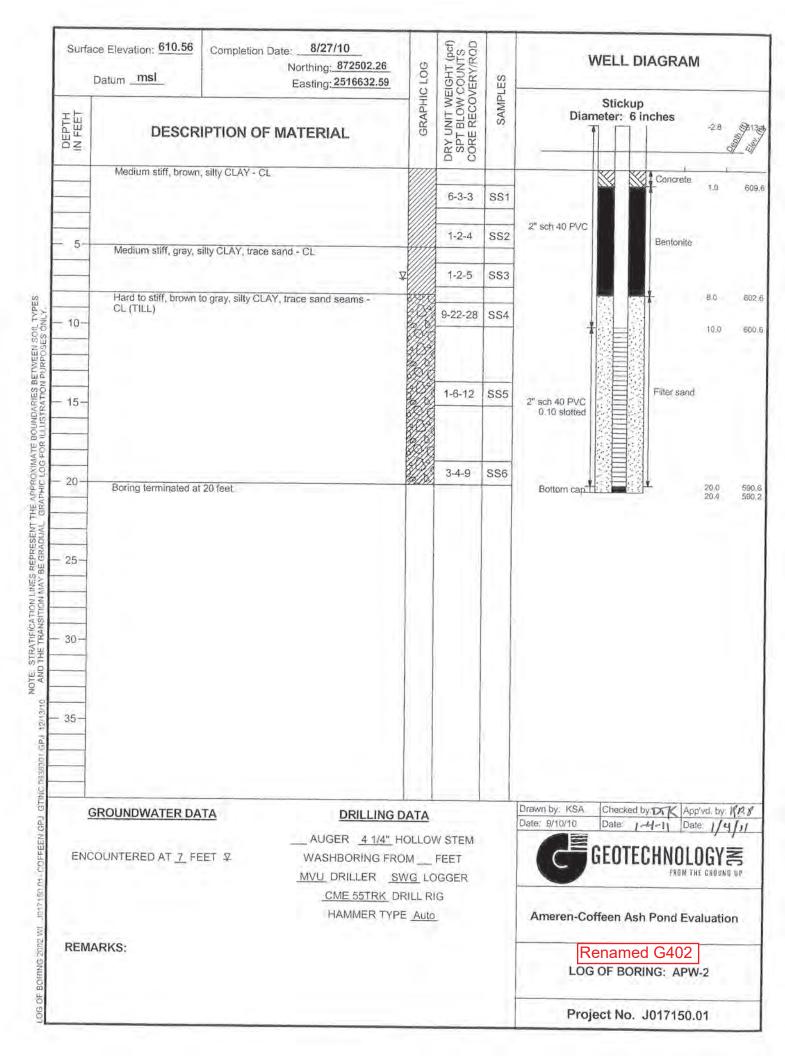
HANSON

BOREHOLE ID: G401 **Well ID:** G401

Surface Elev: 623.03 ft. MSL Completion: 19.30 ft. BGS Station: 2,515,614.84N

872,510.57E

| S | SAMPLE TESTING | | TOPOGR | APHIC MAP INFORMATION: | WATER LEVEL INFORMATION: | | | | |
|-----------|----------------------------------|------|----------------------------------|------------------------|--------------------------|--|---|--|--|
|)er | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) <i>Qp</i> (tsf) Failure Type | Quadra Towns | angle: Coffeen, IL hip: East Fork 11, Tier 7N; Range 3W | $ \mathbf{Y} = \text{Dry - During Drilling} $ $ \mathbf{Y} = \overline{\mathbf{Y}} = \overline{\mathbf{Y}} = \overline{\mathbf{Y}} = \overline{\mathbf{Y}} $ |
| Number | Recov % Rec | Type | Blows N - V: RQD | Moist | Dry D | Qu (ts Failur | Depth ft. BGS | Lithologic Description | Borehole Elevation Detail ft. MSL Remarks |
| 1A | 16/24 67% | ss | 2-2 3-7 N=5 | 17 | | | 2 = | Dark grayish brown (10YR4/2), moist, soft, CLAY w little silt and trace very fine- to fine-grained sand - FII Yellowish brown (10YR5/6) moist, medium, CLAY w some silt and trace very fine- to coarse-grained sand - F | LL622 |
| 2A 2B | 21/24 88% | SS | 8-11 8-9 N=19 | 17 | | 1.80 | 2-1 | Dark gray (10YR4/1), moist, stiff, SILT with little clay trace very fine-grained sand. Yellowish brown (10YR5/6), moist, stiff, CLAY with s silt and trace very fine- to fine-grained sand. | 620 |
| 3A | 23/24 96% | ss | 3-4 7-8 N=11 | 23 | | 2.50 | 10 12 11 11 11 11 11 11 11 11 11 11 11 11 | Gray (10YR5/1) with 20% yellowish brown (10YR5, mottles, moist, medium, CLAY with some silt and travery fine- to fine-grained sand. | /6) loe |
| 4A | 24/24 100% | SS | 8-9 12-14 N=21 | 21 | | 3.30 | | Gray (10YR5/1) with 30% yellowish brown (10YR5. | 616 |
| 4B | | | | 19 | | 2.80 | 8 | mottles, moist, stiff, SILT and very fine-grained SAND trace clay. | |
| 5A | 24/24 100% | ss | 2-3 4-5 N=7 | 21 | | 1.30 | 10 | | 614 |
| 6A | 24/24 100% | ss | 2-4 5-6 N=9 | 17 | | 2.50 | 12 | Gray (10YR5/1) with 30% yellowish brown (10YR5, mottles, moist, medium, CLAY with some silt and travery fine- to fine-grained sand. | /6) ace 612 |
| 7A | 24/24 100% | ss | 9-7 8-9 N=15 | 21 | | 1.40 | 14 — | | 610 |
| 8A 8B | 24/24 100% | ss | 2-3 2-4 N=5 | 17 19 | | 1.30 | 16 | Gray (10YR6/1), moist soft, CLAY with very fine-t fine-grained sand and little silt. | |
| 8В 9А | 20/24 83% | SS | 5-4 5-10 N=9 | 21 | | | | Yellowish brown (10YR5/6), wet, loose, very fine-t fine-grained SAND with trace silt. Yellowish brown (10YR5/6), wet medium, SILT with svery fine-grained sand and little clay. Yellowish brown (10YR5/6), wet, loose, very fine-t | some 606 |
| 9B 10A | 12/16 75% | ss | 23-41 50/4" | 16 6 | | 4.50 | 18 | medium-grained SAND with trace silt. Gray (10YR5/1), moist, very hard, SILT with few clay little very fine- to very coarse sand. End of boring = 19.3 feet | and |



CLIENT: Natural Resource Technology, Inc.

Site: Coffeen Energy Center Location: Coffeen, Illinois Project: 15E0030

DATES: Start: 9/11/2015

Finish: 9/11/2015 WEATHER: Raining, hi 60's

CONTRACTOR: Ramsey Geotechnical Engineering, LLC

Rig mfg/model: D-50 Turbo Tracked MST 800ATV **Drilling Method:** Hollow Stem Auger (31/4"overdrill / 41/4")

Eng/Geo: K. Theesfeld

FIELD STAFF: Driller: D. Crump

Helper: D. Groves

BOREHOLE ID: G403

Well ID: G403 Surface Elev: 623.81 ft. MSL

Completion: 18.15 ft. BGS **Station:** 2,514,616.63N 873,561.34E

HANSON

| SAMPL | E | T | EST | INC | j | TOPOC | RAPHIC MAP INFORMATION: | WATER LEVEL INFORMATION: |
|--|-----------|----------------------------------|--------------|-------------------|-----------------------|---|---|--|
| Number Recov / Total (in) % Recovery | | / 6 in Iue | Moisture (%) | Dry Den. (lb/ft³) | f) Qp (tsf) Type | Quad Town | rangle: Coffeen, IL ship: East Fork n 11, Tier 7N; Range 3W | Ψ = 15.00 - During Drilling Ψ = $\overline{\Psi}$ = $\overline{\Psi}$ = |
| Number Recov / % Recov | Type | Blows / 6 in N - Value RQD | Moist | Dry Do | Qu (tsf) Failure T | Depth ft. BGS | Lithologic Description | Borehole Elevation Detail ft. MSL Remarks |
| 19/24 79% | ss | 2-2 2-2 N=4 | 25 | | 0.80 | | Very dark brown (10YR2/2) grading to dark grayish br (10YR4/2), moist, medium, SILT with some clay, tra roots and grass. | own (4.3) (4 |
| 2A 22/24 | \bigvee | 2-2 | 29 | | | | Very dark brown (10YR2/2) grading to dark grayish br (10YR4/2), moist , stiff, SILT with some clay, trace we | own ood. |
| 2A 92% 2B | SS | 3-4 N=5 | 26 | | 1.50 | | Yellowish brown (10YR5/4) with 10% very dark brov (10YR2/2) mottles, moist, stiff, CLAY with little silt, to very fine-grained sand seams (<1/16" thick). | wn cace — 620 |
| 3A 8/24 33% | SS | 2-3 4-4 N=7 | 25 | | 1.50 | 4 = = = = = = = = = = = = = = = = = = = | Yellowish brown (10YR5/4), moist, stiff, CLAY with I silt and trace very fine-grained sand. | ittle |
| 21/24 88% | ss | 8-7 8-7 N=15 | 20 | | 1.30 | 6 = = = = = = = = = = = = = = = = = = = | Grayish brown (10YR5/2) with 15% yellowish brown (10YR5/6) and 5% very dark grayish brown (10YR3/mottles, moist, stiff, CLAY with little silt and trace ve fine-grained sand. | ['] (2) |
| 5A 20/24 83% | SS | 2-2 3-3 N=5 | 22 | | 0.70 | 10 | Grayish brown (10YR5/2) with 5% yellowish brown (10YR5/6) mottles, moist, medium, CLAY with little and trace very fine-grained sand. | n silt ———————————————————————————————————— |
| 6A 24/24 100% | ss | 2-2 3-4 N=5 | 23 | | 1.40 | | Grayish brown (10YR5/2) with 30% yellowish brow (10YR5/6) mottles, moist, very stiff, CLAY with little few very fine- to medium-grained sand, and trace grav | n silt, el. — 612 |
| 7A 21/24 88% | SS | 5-5 6-5 N=11 | 20 | | 0.90 | 12 ==================================== | Grayish brown (10YR5/3) with 45% yellowish brown (10YR5/6) and 5% dark brown (10YR3/3) mottles, mostiff, SILT with some clay, few very fine- to coarse-grain sand, and trace gravel. | n |
| 8A 24/24 100% | SS | 3-2 3-6 N=5 | 17 | | | 14 = 14 = 14 = 14 = 14 = 14 = 14 = 14 = | Grayish brown (10YR5/3) with 40% yellowish brow (10YR5/6) mottles, moist, medium, SILT with little clefew very fine- to coarse-grained sand, and trace grave Yellowish brown (10YR5/6) with 30% grayish brown (10YR5/2) mottles, moist, medium, SILT with little clefew very fine- to coarse-grained sand, and trace grave Yellowish brown (10YR5/6), wet, loose, SAND with so | n ay, |
| 9A 19/24 79% 0/2 0% | SS | 8-12 21-25 N=33 | 8 | | 4.50 | 16 | clay and few silt. Yellowish brown (10YR5/6) with 30% grayish brown (10YR5/2) mottles, moist, stiff, SILT with few clay, with 10 coarse-grained sand, and gravel. Yellowish brown (10YR5/6), moist, very stiff, SILT with some clay and few sand and gravel. Very dark grayish brown (10YR3/2), dry, hard, SILT with little clay and few very fine- to coarse-grained sand and grayel. | rith ———————————————————————————————————— |
| | | | | | | | gravel. End of boring = 18.15 feet | |
| | | | | | | | End of boring = 18.15 feet | |
| NOTE(S): | G40 | 3 installe | d in | boreł | nole. | | | |

CLIENT: Natural Resources Technology, Inc.

Site: Coffeen Energy Center

Location: Coffeen, Illinois **Project:** 15E0030

DATES: Start: 5/1/2007 **Finish:** 5/1/2007

WEATHER: Partly sunny, warm

CONTRACTOR: Reynolds Drilling Corp. **Rig mfg/model:** CME-550 ATV Drill

Drilling Method: 41/4" Hollow stem auger with split spoon

sampler

FIELD STAFF: Driller: A. Rachford

Helper: M. Brown Eng/Geo: R. Hasenyager

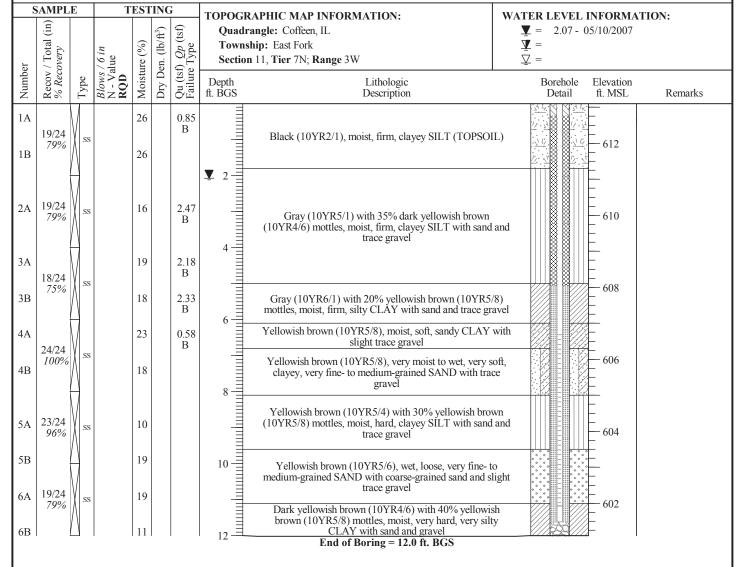
HANSON

BOREHOLE ID: SB22 Formerly MW22S

Well ID: G404

Surface Elev: 613.10 ft. MSL Completion: 12.00 ft. BGS Station: 873.999.77N

2,516,397.85E



CLIENT: Natural Resources Technology, Inc.

Site: Coffeen Energy Center Location: Coffeen, Illinois

Project: 15E0030 **DATES: Start:** 5/1/2007

Finish: 5/1/2007 WEATHER: Partly sunny, warm CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-550 ATV Drill

Drilling Method: 41/4" Hollow stem auger with split spoon

sampler

FIELD STAFF: Driller: A. Rachford Helper: M. Brown

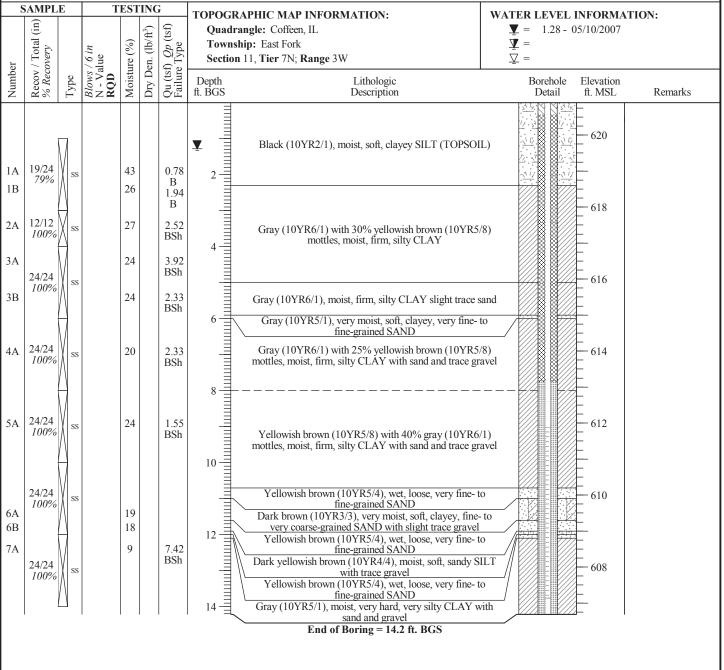
Eng/Geo: R. Hasenyager



BOREHOLE ID: SB21 Formerly MW21S

Well ID: G405

Surface Elev: 620.90 ft. MSL Completion: 14.21 ft. BGS **Station:** 873,996.79N 2,515,335.70E



CLIENT: Natural Resources Technology, Inc.
Site: Coffeen Power Station - Ash Pond 2
Location: 134 CIPS Lane, Coffeen, IL 62017

Project: 16E0080

DATES: Start: 8/19/2016 **Finish:** 8/19/2016

WEATHER: Sunny, (mid-70s)

CONTRACTOR: Bulldog Drilling, Inc.
Rig mfg/model: CME-750 ATV Drill
Drilling Method: 4 1/4" Hollow Stem Auger

FIELD STAFF: Driller: J. Dittmaier Helper: M. Hill

Eng/Geo: K. Theesfeld



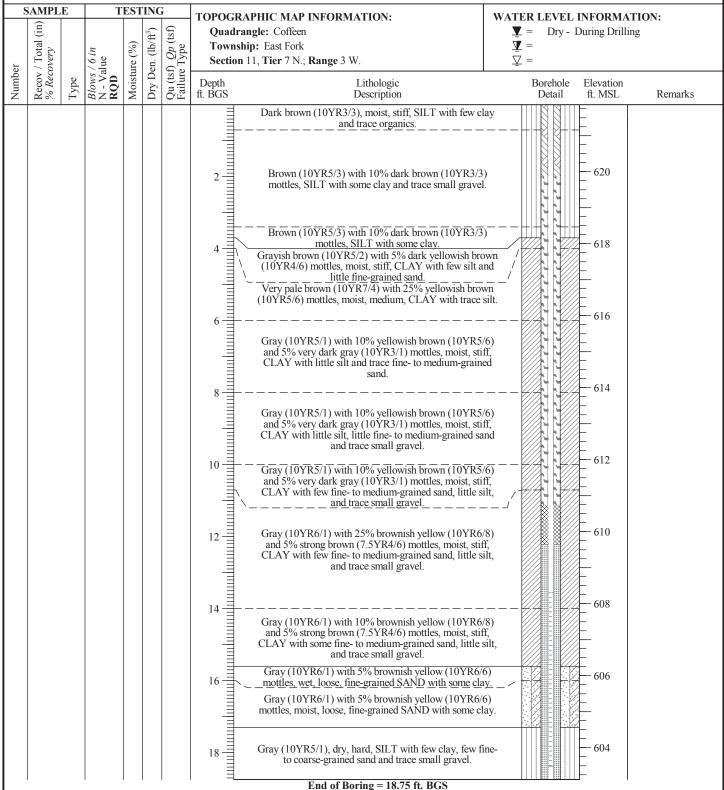
BOREHOLE ID: G406 **Well ID:** G406

 Surface Elev:
 621.86 ft. MSL

 Completion:
 18.75 ft. BGS

 Station:
 872,521.34N

 2.514,702.38E



NOTE(S): G406 installed in boring.

Boring was blind drilled adjacent to G406D.

CLIENT: Natural Resources Technology, Inc.
Site: Coffeen Power Station - Ash Pond 2
Location: 134 CIPS Lane, Coffeen, IL 62017

Project: 16E0080

DATES: Start: 8/19/2016

Finish: 8/19/2016 WEATHER: Sunny, (mid-70s)

CONTRACTOR: Bulldog Drilling, Inc.
Rig mfg/model: CME-750 ATV Drill
Drilling Method: 4 1/4" Hollow Stem Auger

FIELD STAFF: Driller: J. Dittmaier Helper: M. Hill

Eng/Geo: K. Theesfeld



BOREHOLE ID: G406D **Well ID:** G46D

 Surface Elev:
 621.91 ft. MSL

 Completion:
 52.00 ft. BGS

 Station:
 872,519.70N

 2,514,697.78E

| S | SAMPLE TESTING | | j | TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMAT | TION: | | | |
|----------|----------------------------------|------|---|---|--|--|--|---------|
| _ | Recov / Total (in) % Recovery | 6 in | .e (%) | Dry Den. (lb/ft³) | Qu (tsf) <i>Qp</i> (tsf) Failure Type | Quadrangle: Coffeen $\underline{\mathbf{Y}}$ = Dry - During DrillingTownship: East Fork $\underline{\underline{\mathbf{Y}}}$ = \underline | | |
| Number | Recov / % Reco | Type | Blows / 6 in N - Value RQD | Moisture (%) | Dry De | Qu (tsf) Failure | Depth Lithologic Borehole Elevation ft. BGS Description Detail ft. MSL | Remarks |
| 1A 1B | 18/24 75% | SS | 4-3 4-6 N=7 | 11 | | 1.50 3.00 | Dark brown (10YR3/3), moist, stiff, SILT with few clay and trace organics. Brown (10YR5/3) with 10% dark brown (10YR3/3) mottles, SILT with some clay and trace small gravel. | |
| 2A | 12/24 50% | ss | 4-6 3-3 N=9 | 12 | | 2.50 | 1 | |
| A A | 3/24 13% | ss | 3-3 4-7 N=7 | 18 24 | | 2.00 | Brown (10YRS/3) with 10% dark brown (10YR3/3) mottles, SILT with some clay. Grayish brown (10YR5/2) with 5% dark yellowish brown (10YR4/6) mottles, moist, stiff, CLAY with few silt and little fine-grained sand. Very pale brown (10YR7/4) with 25% yellowish brown (10YR5/6) mottles, moist, medium, CLAY with trace silt. 6 616 | |
| A | 20/24 83% | SS | 2-3 4-5 N=7 | 21 | | 1.25 | Gray (10YR5/1) with 10% yellowish brown (10YR5/6) and 5% very dark gray (10YR3/1) mottles, moist, stiff, CLAY with little silt and trace fine- to medium-grained sand. | |
| A | 19/24 79% | ss | 1-3 4-6 N=7 | 18 | | 1.75 | Gray (10YR5/1) with 10% yellowish brown (10YR5/6) and 5% very dark gray (10YR3/1) mottles, moist, stiff, CLAY with little silt, little fine- to medium-grained sand and trace small gravel. | |
| A | 23/24 96% | ss | 2-2 4-5 N=6 | 18 | | 2.50 | Gray (10YR5/1) with 10% yellowish brown (10YR5/6) and 5% very dark gray (10YR3/1) mottles, moist, stiff, CLAY with little silt, little fine- to medium-grained sand and trace small gravel. Gray (10YR5/1) with 10% yellowish brown (10YR5/6) and 5% very dark gray (10YR3/1) mottles, moist, stiff, CLAY with few fine- to medium-grained sand, little silt, and trace small gravel. Gray (10YR6/1) with 25% brownish yellow (10YR6/8) and 5% strong brown (7.5YR4/6) mottles, moist, stiff, CLAY with few fine- to medium-grained sand, little silt, and trace small gravel. | |
| A | 21/24 88% | SS | 1-3 4-5 N=7 | 16 | | 1.00 | ¬ V/// V/// - I | |
| Α | 23/24 96% | SS | 1-2 2-2 N=4 | 18 | | 0.75 | Gray (10YR6/1) with 10% brownish yellow (10YR6/8) and 5% strong brown (7.5YR4/6) mottles, moist, stiff, CLAY with some fine- to medium-grained sand, little silt, and trace small gravel. Gray (10YR6/1) with 5% brownish yellow (10YR6/6) mottles, wet, loose, fine-grained SAND with some clay. | |
| В | | | | 17 | | 0.75 | Gray (10YR6/1) with 5% brownish yellow (10YR6/6)mottles, wet, loose, fine-grained SAND with some clay606 | |
| A | 22/24 92% | ss | 4-13 27-23 N=40 | 8 | | | Gray (10YR6/1) with 5% brownish yellow (10YR6/6) mottles, moist, loose, fine-grained SAND with some clay. | |
| В | 17/24 71% | ss | 13-31 33-42 | 8 | | | Gray (10YR6/1) with 5% brownish yellow (10YR6/6) mottles, moist, loose, fine-grained SAND with some clay. Gray (10YR5/1), dry, hard, SILT with few clay, few fine-to coarse-grained sand and trace small gravel. | |
|)A NO | | G46 | N=64 D installe | 7 ed in | borii | 4.50 ng. | 20 | |

CLIENT: Natural Resources Technology, Inc. Site: Coffeen Power Station - Ash Pond 2 Location: 134 CIPS Lane, Coffeen, IL 62017

Project: 16E0080

DATES: Start: 8/19/2016 **Finish:** 8/19/2016

WEATHER: Sunny, (mid-70s)

CONTRACTOR: Bulldog Drilling, Inc.
Rig mfg/model: CME-750 ATV Drill
Drilling Method: 4 1/4" Hollow Stem Auger

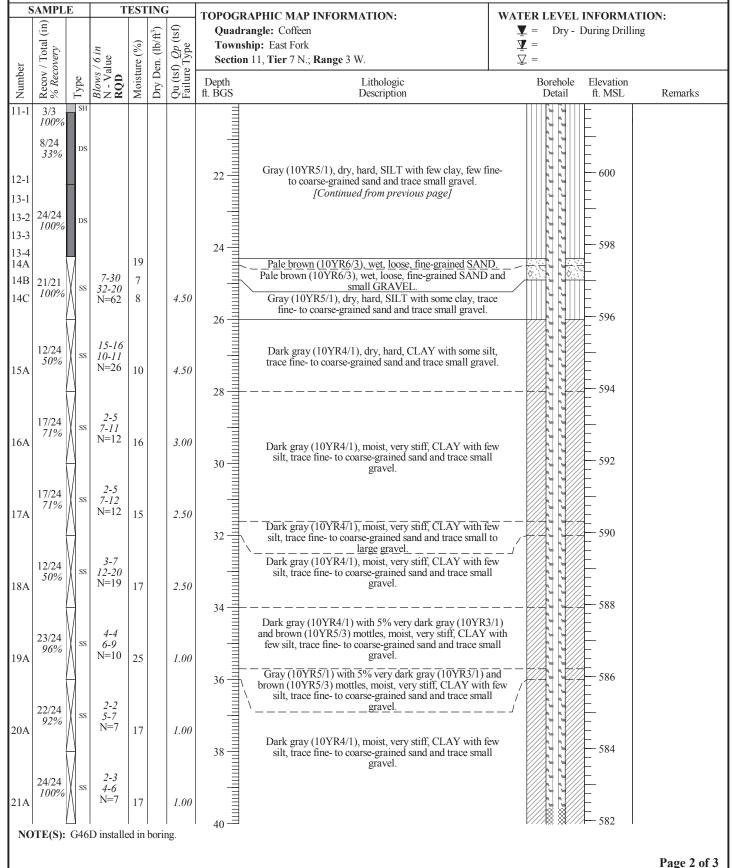
FIELD STAFF: Driller: J. Dittmaier Helper: M. Hill

Eng/Geo: K. Theesfeld



BOREHOLE ID: G406D **Well ID:** G46D

Surface Elev: 621.91 ft. MSL Completion: 52.00 ft. BGS Station: 872,519.70N 2,514.697.78E



CLIENT: Natural Resources Technology, Inc. Site: Coffeen Power Station - Ash Pond 2 Location: 134 CIPS Lane, Coffeen, IL 62017

Project: 16E0080

DATES: Start: 8/19/2016 Finish: 8/19/2016

WEATHER: Sunny, (mid-70s)

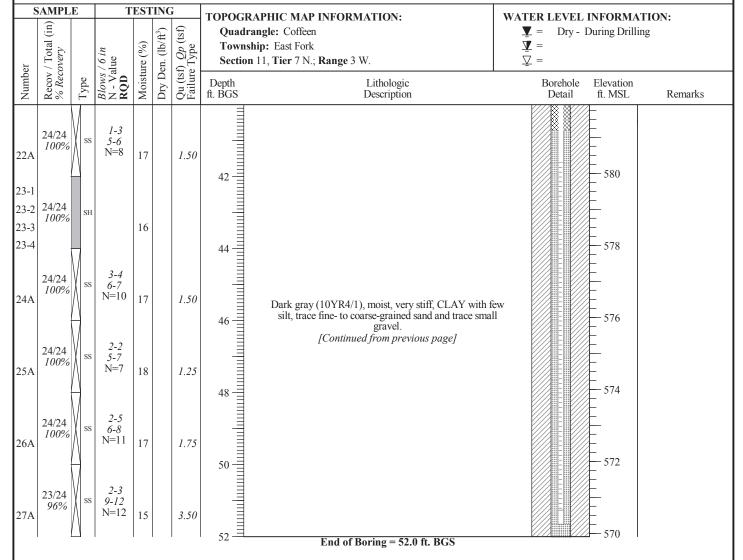
CONTRACTOR: Bulldog Drilling, Inc. Rig mfg/model: CME-750 ATV Drill

Drilling Method: 4 1/4" Hollow Stem Auger

FIELD STAFF: Driller: J. Dittmaier Helper: M. Hill Eng/Geo: K. Theesfeld

BOREHOLE ID: G406D Well ID: G46D

> Surface Elev: 621.91 ft. MSL Completion: 52.00 ft. BGS **Station:** 872,519.70N 2,514,697.78E



CLIENT: Natural Resources Technology, Inc.
Site: Coffeen Power Station - Ash Pond 2
Location: 134 CIPS Lane, Coffeen, IL 62017

Project: 16E0080

DATES: Start: 8/16/2016 **Finish:** 8/16/2016

WEATHER: Rain, (mid-70s)

CONTRACTOR: Bulldog Drilling, Inc.
Rig mfg/model: CME-750 ATV Drill
Drilling Method: 4 1/4" Hollow Stem Auger

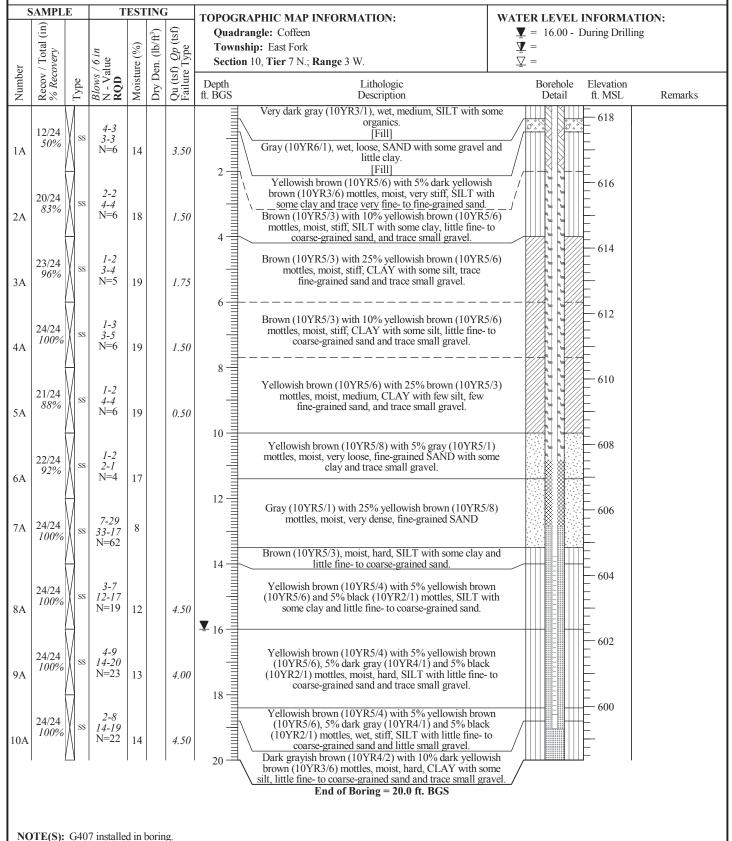
FIELD STAFF: Driller: J. Dittmaier Helper: M. Hill

Eng/Geo: K. Theesfeld



BOREHOLE ID: G407 **Well ID:** G407

> Surface Elev: 618.35 ft. MSL Completion: 20.00 ft. BGS Station: 2,513,705.87N 2,513,705.87E



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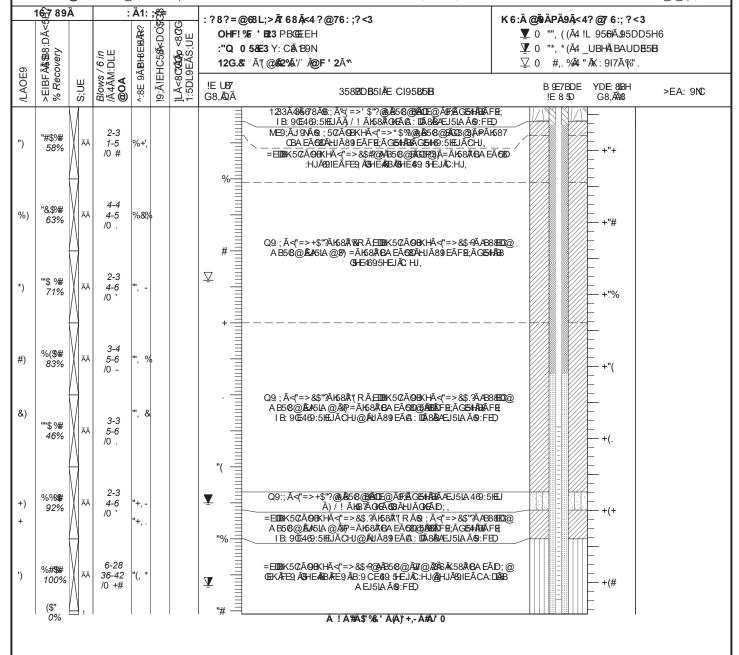


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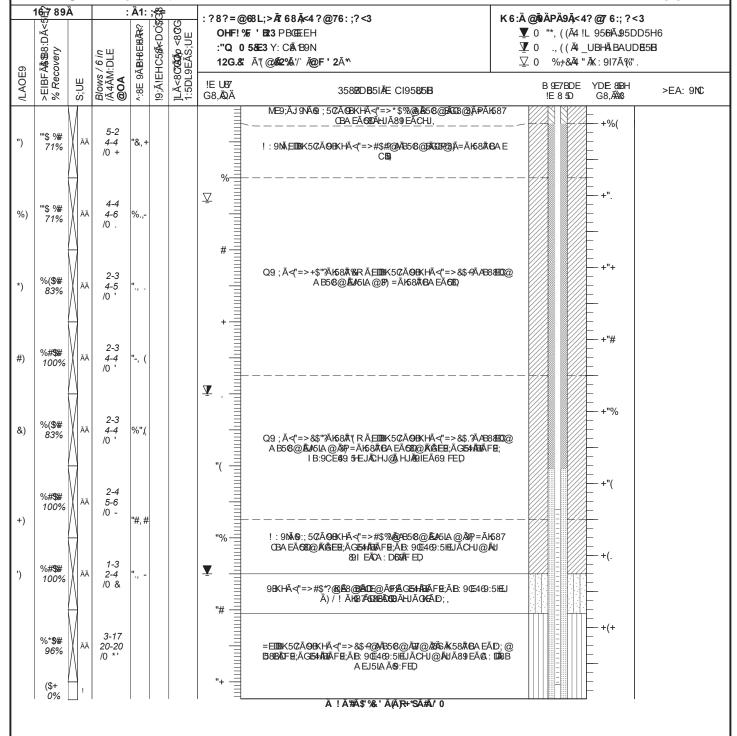


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CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A DATES: Start: 5/3/2006 Finish: 5/3/2006

Finish: 5/3/2006 **WEATHER:** Overcast, mild (mid-60's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 31/4" HSA w/SS sampler

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy Eng/Geo: R. Hasenyager **HANSON**

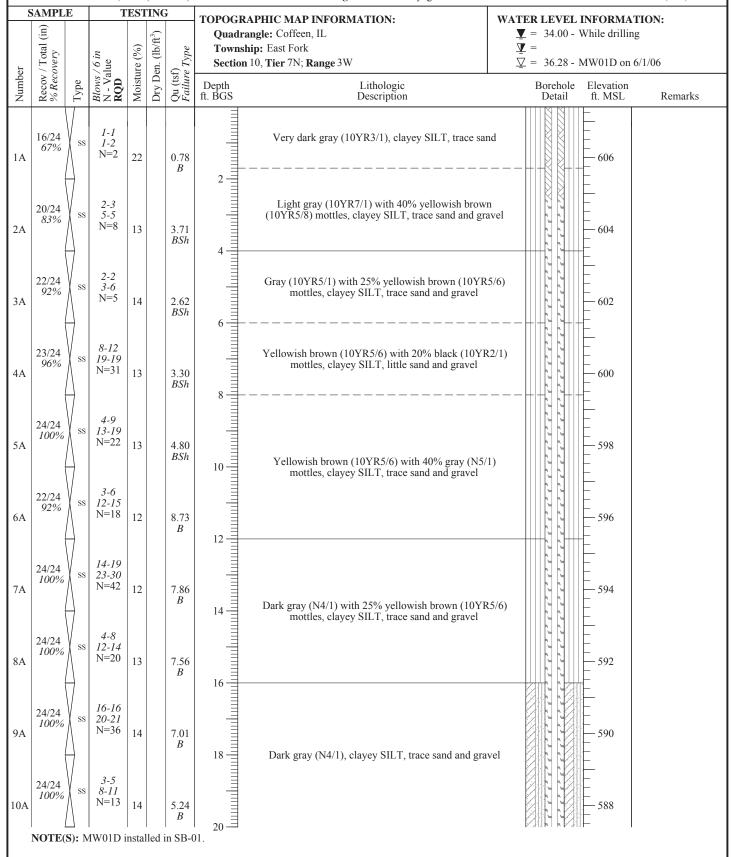
BOREHOLE ID: SB-01 **Well ID:** MW1D

 Surface Elev:
 607 ft. MSL

 Completion:
 40 ft. BGS

 Station:
 874,972.6N

 2,513,478.0E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A **DATES: Start:** 5/3/2006

Finish: 5/3/2006 **WEATHER:** Overcast, mild (mid-60's) **CONTRACTOR:** Testing Service Corporation Rig mfg/model: CME-650 Track Rig **Drilling Method:** 31/4" HSA w/SS sampler

Helper: R. Keedy

FIELD STAFF: Driller: B. Williamson

Eng/Geo: R. Hasenyager



BOREHOLE ID: SB-01 Well ID: MW1D

607 ft. MSL **Surface Elev: Completion:** 40 ft. BGS **Station:** 874,972.6N 2,513,478.0E

| S | SAMPL | E | Т | EST | INC | 3 | TOPOGRAPHIC MAP INFO | RMATION: | WATER LEVEL | INFORMA | TION: | | |
|--------|-------------------------------|-----------|----------------------------------|--------------|-------------------|--------------------------|--|---|--|----------------------|---|--|--|
| er | Recov / Total (in) % Recovery | | / 6 in ılue | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadrangle: Coffeen, IL Township: East Fork Section 10, Tier 7N; Range 3 | | $\underline{\Psi}$ = 34.00 - While drilling $\underline{\Psi}$ = $\underline{\nabla}$ = 36.28 - MW01D on 6/1/06 | | | | |
| Number | Recov % Rec | Type | Blows / 6 in N - Value RQD | Moist | Dry D | Qu (ts Failur | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks | | |
| 11A | 24/24 100% | SH | | 15 | | 3.69 B | 22 — 24 — 26 — 26 — 28 — 28 — 30 — 32 — 32 — 32 — 32 — 33 — 34 — 35 — 35 — 35 — 36 — 36 — 36 — 36 — 36 | | 222222 | | Shelby tube taken from shallow well borehole at indicated depth. | | |
| 12A | 24/24 100% | ss | 10-11 12-16 N=23 | 14 | | 5.24 B | 24 = | | | 584 | Shelby tube taken from shallow well | | |
| 13A | 6/24 25% | SH | | 14 | | 3.69 B | 26 | | | 582 | borehole at indicated depth. | | |
| 14A | 24/24 100% | ss | 10-12 18-18 N=30 | 15 | | 4.27 B | Dark gray (N4/1 [Conti |), clayey SILT, trace sand and grav nued from previous page] | rel | 580 | | | |
| 15A | 24/24 100% | ss | 5-9 11-16 N=20 | 14 | | 4.27 B | 30 - | | | 578 | | | |
| 16A | 24/24 100% | ss | 5-8 10-12 N=18 | 17 | | 2.72 BSh | 32 - | | | 576 | | | |
| 17A | 24/24 100% | ss | 8-14 14-16 N=28 | 14 | | 5.62 B | ¥ 34 = | | | 574 | | | |
| 18A | 23/24 96% | ss | 8-28 40-65 N=68 | 14 | | | | y, fine to medium SAND, little coaind, trace gravel, wet | rse | 572 | | | |
| 19A | 24/24 | \bigvee | 24-14 | 13 | | | ¥ | | | Ē | | | |
| 19B | 100% | ss | 17-16 N=31 | 19 | | 5.43 B | Very dark | gray (10YR3/1), silty CLAY | | 570 | | | |
| 20A | 24/24 100% | ss | 3-5 6-10 N=11 | 24 | | 3.50 BSh | Dark gray (N4/ | (1) with 30% dark yellowish brown (24/6) mottles, silty CLAY of Boring = 40.0 ft. BGS | | 568 | | | |
| | NOTE(| S): M | IW01D i | nstal | lled i | in SB-0 | | | | | Do an 2 of 2 | | |

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois
Project: 05S3004A

DATES: Start: 5/5/2006

Finish: 5/5/2006

CONTRACTOR: Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig **Drilling Method:** 41/4" HSA (blind drill)

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy **HANSON**

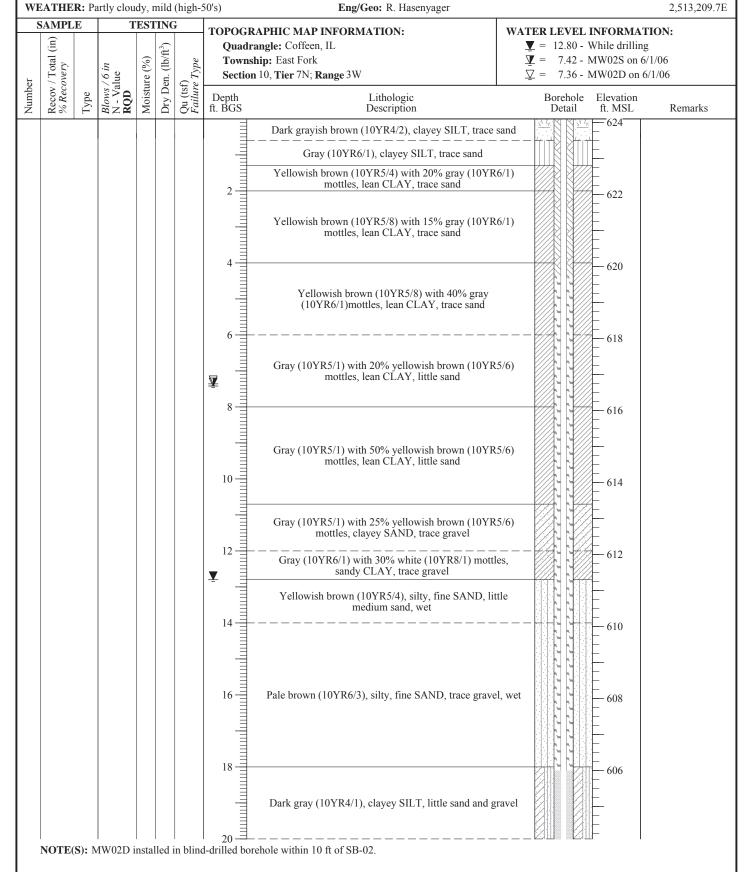
BOREHOLE ID: SB-02b **Well ID:** MW2D

 Surface Elev:
 624 ft. MSL

 Completion:
 27 ft. BGS

 Station:
 876,414.0N

 2,513,209.7E



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A

DATES: Start: 5/5/2006

Finish: 5/5/2006 **WEATHER:** Partly cloudy, mild (high-50's) CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 4¹/₄" HSA (blind drill)

FIELD STAFF: Driller: B. Williamson **Helper:** R. Keedy

Eng/Geo: R. Hasenyager

HANSON

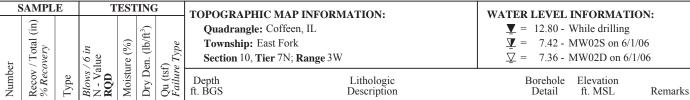
BOREHOLE ID: SB-02b **Well ID:** MW2D

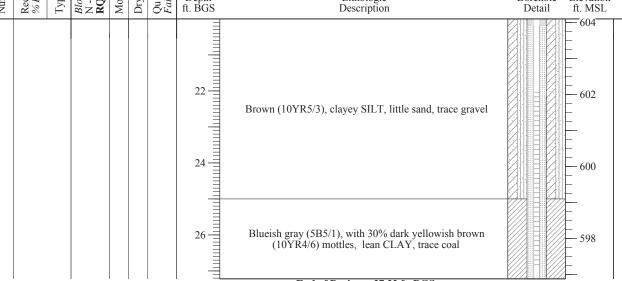
 Surface Elev:
 624 ft. MSL

 Completion:
 27 ft. BGS

 Station:
 876,414.0N

 2,513,209.7E





End of Boring = 27.22 ft. BGS See SB-02 for sample & testing details

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A **DATES: Start:** 5/5/2006

SAMPLE

Finish: 5/5/2006

WEATHER: Partly cloudy, mild (high-50's)

TESTING

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

TOPOGRAPHIC MAP INFORMATION:

Eng/Geo: R. Hasenyager

WATER LEVEL INFORMATION:

 $\mathbf{Y} = 12.80$ - While drilling $\nabla = 7.42 - MW02S \text{ on } 6/1/06$

BOREHOLE ID: SB-02

Surface Elev:

Completion:

Station:

Well ID: n/a

624 ft. MSL

50 ft. BGS

876,410.0N

2,513,210.0E

(E) Quadrangle: Coffeen, IL Dry Den. (lb/ft³) Recov / Total % Recovery Township: East Fork Qu (tsf) Failure Type Moisture (%) Blows / 6 in N - Value RQD Section 10, Tier 7N; Range 3W ∇ = 7.36 - MW02D on 6/1/06 Number Lithologic Borehole Elevation Description Detail ft. MSL Remarks -624 Dark grayish brown (10YR4/2), clayey SILT, trace sand 23 1A 3-3 24/24 4-5 Gray (10YR6/1), clayey SILT, trace sand SS 100% 1.96 1B 18 N=7Yellowish brown (10YR5/4) with 20% gray (10YR6/1) mottles, lean CLAY, trace sand B1C 29 1.94 622 3-4 24/24 Yellowish brown (10YR5/8) with 15% gray (10YR6/1) 4-6 100% mottles, lean CLAY, trace sand N=825 2A 2.89 620 3-5 24/24 Yellowish brown (10YR5/8) with 40% gray SS 5-7 100% (10YR6/1)mottles, lean CLAY, trace sand N=1020 3A 2.91 B618 10-8 24/24 Gray (10YR5/1) with 20% yellowish brown (10YR5/6) 8-10 100% mottles, lean CLAY, little sand N = 1617 2.91 B616 24/24 4-5 100% Gray (10YR5/1) with 50% yellowish brown (10YR5/6) 19 5A 1.94 mottles, lean CLAY, little sand В 614 18 6A 2.13 2-3 24/24 6-5 100% Gray (10YR5/1) with 25% yellowish brown (10YR5/6) N=9 6B 17 mottles, clayey SAND, trace gravel 612 Gray (10YR6/1) with 30% white (10YR8/1) mottles, sandy CLAY, trace gravel 7A 14 2.06 \blacksquare 24/24 7-10 100% Yellowish brown (10YR5/4), silty, fine SAND, little N=117В 17 medium sand, wet 610 15-23 24/24 33-68 100% N = 568A 10 Pale brown (10YR6/3), silty, fine SAND, trace gravel, wet 16 608 10/10 48-62/4 10 3.92 9A 100% 606 15-45 9 8.07 Dark gray (10YR4/1), clayey SILT, little sand and gravel BShNOTE(S): Borehole abandoned using bentonite grout pumped from bottom of borehole.

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A DATES: Start: 5/5/2006

DATES: Start: 5/5/2006 Finish: 5/5/2006 WEATHER: Partly cloudy, mild (high-50's) CONTRACTOR: Testing Service Corporation
Rig mfg/model: CME-650 Track Rig

Dillian Mathe 1, 21/11 USA m/SS & CME arms

Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

BOREHOLE ID: SB-02

 Well ID: n/a

 Surface Elev:
 624 ft. MSL

 Completion:
 50 ft. BGS

 Station:
 876,410.0N

 2,513,210.0E

SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: Œ, Quadrangle: Coffeen, IL $\mathbf{Y} = 12.80$ - While drilling Dry Den. (lb/ft³) Recov / Total (% Recovery Township: East Fork $\nabla = 7.42 - MW02S \text{ on } 6/1/06$ Moisture (%) Qu (tsf) Failure Type Section 10, Tier 7N; Range 3W ∇ = 7.36 - MW02D on 6/1/06 Number Lithologic Borehole Elevation Description Detail ft. MSL Remarks 9 11A 602 36/60 Brown (10YR5/3), clayey SILT, little sand, trace gravel CS 60% 600 11B 11 598 12A 21 Blueish gray (5B5/1), with 30% dark yellowish brown (10YR4/6) mottles, lean CLAY, trace coal 60/60 CS 100% - 596 12B 23 594 592 60/60 CS 100% 13A 14 Very dark gray (10Y3/1), lean CLAY, trace sand and gravel 588 60/60 CS 100% 586 14 14A NOTE(S): Borehole abandoned using bentonite grout pumped from bottom of borehole.

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A DATES: Start: 5/5/2006

SAMPLE

Finish: 5/5/2006 **WEATHER:** Partly cloudy, mild (high-50's)

TESTING

CONTRACTOR: Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

TOPOGRAPHIC MAP INFORMATION:

Eng/Geo: R. Hasenyager

WATER LEVEL INFORMATION:

HANSON

624 ft. MSL

50 ft. BGS

876,410.0N

2,513,210.0E

BOREHOLE ID: SB-02

Surface Elev:

Completion:

Station:

Well ID: n/a

Œ, Quadrangle: Coffeen, IL $\mathbf{Y} = 12.80$ - While drilling Dry Den. (lb/ft3) Recov / Total (% Recovery Qu (tsf) Failure Type Township: East Fork $\nabla = 7.42 - MW02S \text{ on } 6/1/06$ Moisture (%) ∇ = 7.36 - MW02D on 6/1/06 Section 10, Tier 7N; Range 3WNumber Lithologic Borehole Elevation Description Detail ft. MSL Remarks 582 60/60CS 100% 580 15A 14 Very dark gray (10Y3/1), lean CLAY, trace sand and gravel [Continued from previous page] 578 60/60 CS 100% - 576 13 16A End of Boring = 50.0 ft. BGS

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A DATES: Start: 5/5/2006

Finish: 5/5/2006 **WEATHER:** Partly cloudy, mild (high-50's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 31/4" HSA (blind drill)

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

HANSON

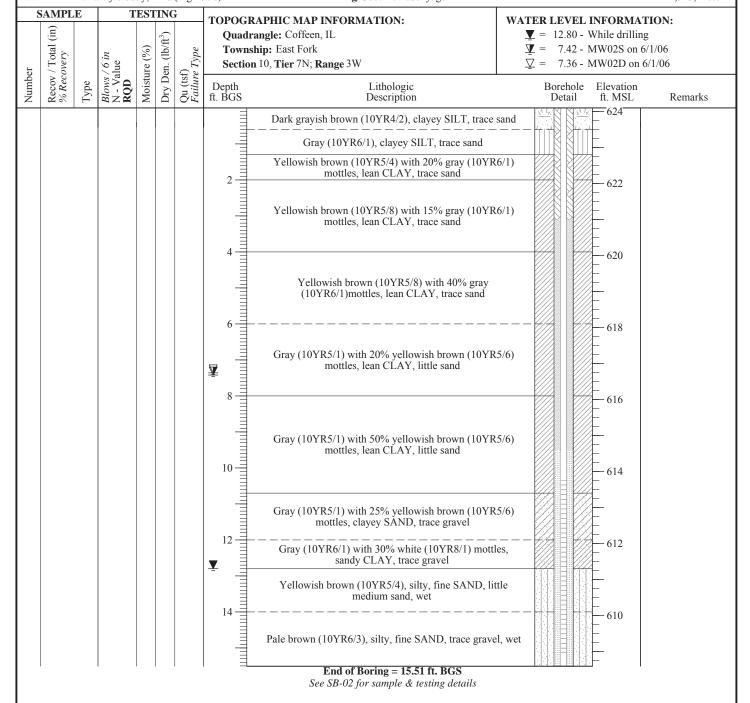
BOREHOLE ID: SB-02a **Well ID:** MW2S **Surface Elev:** 624 ft

 Surface Elev:
 624 ft. MSL

 Completion:
 16 ft. BGS

 Station:
 876,408.9N

 2,513,210.0E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A **DATES: Start:** 5/5/2006

SAMPLE

Finish: 5/5/2006

WEATHER: Partly cloudy, mild (high-50's)

TESTING

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

TOPOGRAPHIC MAP INFORMATION:

Eng/Geo: R. Hasenyager

WATER LEVEL INFORMATION:

 $\mathbf{Y} = 12.80$ - While drilling $\nabla = 7.42 - MW02S \text{ on } 6/1/06$

BOREHOLE ID: SB-02

Surface Elev:

Completion:

Station:

Well ID: n/a

624 ft. MSL

50 ft. BGS

876,410.0N

2,513,210.0E

(E) Quadrangle: Coffeen, IL Dry Den. (lb/ft³) Recov / Total % Recovery Township: East Fork Qu (tsf) Failure Type Moisture (%) Blows / 6 in N - Value RQD Section 10, Tier 7N; Range 3W ∇ = 7.36 - MW02D on 6/1/06 Number Lithologic Borehole Elevation Description Detail ft. MSL Remarks -624 Dark grayish brown (10YR4/2), clayey SILT, trace sand 23 1A 3-3 24/24 4-5 Gray (10YR6/1), clayey SILT, trace sand SS 100% 1.96 1B 18 N=7Yellowish brown (10YR5/4) with 20% gray (10YR6/1) mottles, lean CLAY, trace sand B1C 29 1.94 622 3-4 24/24 Yellowish brown (10YR5/8) with 15% gray (10YR6/1) 4-6 100% mottles, lean CLAY, trace sand N=825 2A 2.89 620 3-5 24/24 Yellowish brown (10YR5/8) with 40% gray SS 5-7 100% (10YR6/1)mottles, lean CLAY, trace sand N=1020 3A 2.91 B618 10-8 24/24 Gray (10YR5/1) with 20% yellowish brown (10YR5/6) 8-10 100% mottles, lean CLAY, little sand N = 1617 2.91 B616 24/24 4-5 100% Gray (10YR5/1) with 50% yellowish brown (10YR5/6) 19 5A 1.94 mottles, lean CLAY, little sand В 614 18 6A 2.13 2-3 24/24 6-5 100% Gray (10YR5/1) with 25% yellowish brown (10YR5/6) N=9 6B 17 mottles, clayey SAND, trace gravel 612 Gray (10YR6/1) with 30% white (10YR8/1) mottles, sandy CLAY, trace gravel 7A 14 2.06 \blacksquare 24/24 7-10 100% Yellowish brown (10YR5/4), silty, fine SAND, little N=117В 17 medium sand, wet 610 15-23 24/24 33-68 100% N = 568A 10 Pale brown (10YR6/3), silty, fine SAND, trace gravel, wet 16 608 10/10 48-62/4 10 3.92 9A 100% 606 15-45 9 8.07 Dark gray (10YR4/1), clayey SILT, little sand and gravel BShNOTE(S): Borehole abandoned using bentonite grout pumped from bottom of borehole.

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A DATES: Start: 5/5/2006

DATES: Start: 5/5/2006 Finish: 5/5/2006 WEATHER: Partly cloudy, mild (high-50's) CONTRACTOR: Testing Service Corporation
Rig mfg/model: CME-650 Track Rig

Dillian Mathe 1, 21/11 USA m/SS & CME arms

Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

BOREHOLE ID: SB-02

 Well ID: n/a

 Surface Elev:
 624 ft. MSL

 Completion:
 50 ft. BGS

 Station:
 876,410.0N

 2,513,210.0E

SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: Œ, Quadrangle: Coffeen, IL $\mathbf{Y} = 12.80$ - While drilling Dry Den. (lb/ft³) Recov / Total (% Recovery Township: East Fork $\nabla = 7.42 - MW02S \text{ on } 6/1/06$ Moisture (%) Qu (tsf) Failure Type Section 10, Tier 7N; Range 3W ∇ = 7.36 - MW02D on 6/1/06 Number Lithologic Borehole Elevation Description Detail ft. MSL Remarks 9 11A 602 36/60 Brown (10YR5/3), clayey SILT, little sand, trace gravel CS 60% 600 11B 11 598 12A 21 Blueish gray (5B5/1), with 30% dark yellowish brown (10YR4/6) mottles, lean CLAY, trace coal 60/60 CS 100% - 596 12B 23 594 592 60/60 CS 100% 13A 14 Very dark gray (10Y3/1), lean CLAY, trace sand and gravel 588 60/60 CS 100% 586 14 14A NOTE(S): Borehole abandoned using bentonite grout pumped from bottom of borehole.

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A DATES: Start: 5/5/2006

SAMPLE

Finish: 5/5/2006 **WEATHER:** Partly cloudy, mild (high-50's)

TESTING

CONTRACTOR: Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

TOPOGRAPHIC MAP INFORMATION:

Eng/Geo: R. Hasenyager

WATER LEVEL INFORMATION:

HANSON

624 ft. MSL

50 ft. BGS

876,410.0N

2,513,210.0E

BOREHOLE ID: SB-02

Surface Elev:

Completion:

Station:

Well ID: n/a

Œ, Quadrangle: Coffeen, IL $\mathbf{Y} = 12.80$ - While drilling Dry Den. (lb/ft3) Recov / Total (% Recovery Qu (tsf) Failure Type Township: East Fork $\nabla = 7.42 - MW02S \text{ on } 6/1/06$ Moisture (%) ∇ = 7.36 - MW02D on 6/1/06 Section 10, Tier 7N; Range 3WNumber Lithologic Borehole Elevation Description Detail ft. MSL Remarks 582 60/60CS 100% 580 15A 14 Very dark gray (10Y3/1), lean CLAY, trace sand and gravel [Continued from previous page] 578 60/60 CS 100% - 576 13 16A End of Boring = 50.0 ft. BGS

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A DATES: Start: 4/27/2006

Finish: 4/27/2006 **WEATHER:** Sunny, mild (high-50's)

CONTRACTOR: Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS sampler & 41/4" HSA overdrill

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

BOREHOLE ID: SB-03

Well ID: MW3D

 Surface Elev:
 626 ft. MSL

 Completion:
 58 ft. BGS

 Station:
 876,554.5N

HANSON

2,514,535.3E

Page 1 of 3

| SA | MPLI | E | Т | TESTING | | | TOPOGRAPHIC MAP INFORMATION: | WATER I EVEL INCORMATION. |
|-------------------|--------------------------------|------|---|--------------|-------------------|--------------------------|--|--|
| er (Total (in) | Recov / I otal (in) % Recovery | | / 6 in Ilue | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadrangle: Coffeen, IL Township: East Fork Section 11, Tier 7N; Range 3W | WATER LEVEL INFORMATION: $\underline{\Psi}$ = 14.00 - While drilling $\underline{\Psi}$ = 7.03 - MW03S on 6/1/06 $\underline{\nabla}$ = 55.40 - MW03D on 6/1/06 |
| Number | Kecov % Rec | Type | Blows / 6 in N - Value RQD | Moist | Dry D | Qu (ts: Failur | Depth Lithologic ft. BGS Description | Borehole Elevation Detail ft. MSL Remarks |
| A | | Π | | 17 | | 2.07 | Very dark grayish brown (10YR3/2), lean CLA | AY THE STATE OF TH |
| 2 | 0/24 83% | ss | 2-2 4-6 | 20 | | SP SP | Grayish brown (10YR5/2), lean CLAY, trace sa | and |
| C | | | N=6 | 26 | | 3.30 | Yellowish brown (10YR5/6), lean CLAY, trace s | sand 624 |
| | 7/24 71% | ss | 2-3 4-5 N=7 | 25 | | 3.05 B | Very dark grayish brown (10YR3/2), lean CLAY Grayish brown (10YR5/2), lean CLAY, trace so Yellowish brown (10YR5/6), lean CLAY, trace so Yellowish brown (10YR5/6) with 40% gray (N3 mottles, lean CLAY, trace gravel Yellowish brown (10YR5/6) with 40% gray (N3 mottles, sandy SILT, trace gravel Yellowish brown (10YR5/6) with 50% gray (N3 mottles, lean CLAY, trace sand and gravel Yellowish brown (10YR5/6), lean CLAY, little san gravel | 5/1) 622 |
| | 0/24 | SS | 2-3 3-5 N=6 | 16 | | 1.96 B | Yellowish brown (10YR5/6) with 40% gray (No mottles, sandy SILT, trace gravel | 5/1) 620 |
| | 4/24 | ss | 4-3 5-6 N=8 | 21 | | 2.27 B | Yellowish brown (10YR5/6) with 50% gray (N: mottles, lean CLAY, trace sand and gravel | 5/1) 618 |
| 2 A B | 1/24 | ss | 1-3 3-4 N=6 | 20 19 | | 2.18 B | Yellowish brown (10YR5/6), lean CLAY, little san gravel Dark gray (10YR4/1), sandy CLAY, trace grav | 616 |
| | 8/24 75% | ss | 1-2 2-4 N=4 | 24 | | 0.87 B | Gray (10YR6/1) with 50% yellowish brown (10Y mottles, lean CLAY, little sand, trace gravel | Snelby tube take |
| B 1 | 3/24 96% 6/24 67% | SH | 3-2 2-4 N=4 | 19 12 | | | <u>▼</u> 14 | from shallow we borehole at indicated depth. |
| A 2 | 3/24 | ss | 3-12 29-50 | 13 | | | Yellowish brown (10YR5/8), silty, fine SAND, medium sand, trace gravel, wet | little |
| 3 3 | 96% | \ | N=41 | 13 12 | | | | le clay,610 |
| | 4/24 | | 8-82 85-72 | 10 | | 6.98 B | Yellowish brown (10YR5/6), lean CLAY, little san gravel Yellowish brown (10YR5/6), silty SAND, trace g | |
| 3 | 58% | SS | 85-72 N=167 | 13 | | 6.18 <i>BSh</i> | Yellowish brown (10YRS/8), silty, fine SAND, litt wet Yellowish brown (10YRS/6), lean CLAY, little san gravel Yellowish brown (10YRS/6), silty SAND, trace g wet Yellowish brown (10YRS/4), clayey SILT, trace sa gravel | |
| | 8/24 75% | SS | 6-21 32-49 N=53 | 8 | | 11.95 Sh | Gray (10YR5/1), sandy SILT, trace gravel | 606 |

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A DATES: Start: 4/27/2006 Finish: 4/27/2006

Finish: 4/27/2006 WEATHER: Sunny, mild (high-50's) CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS sampler & 41/4" HSA overdrill

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager



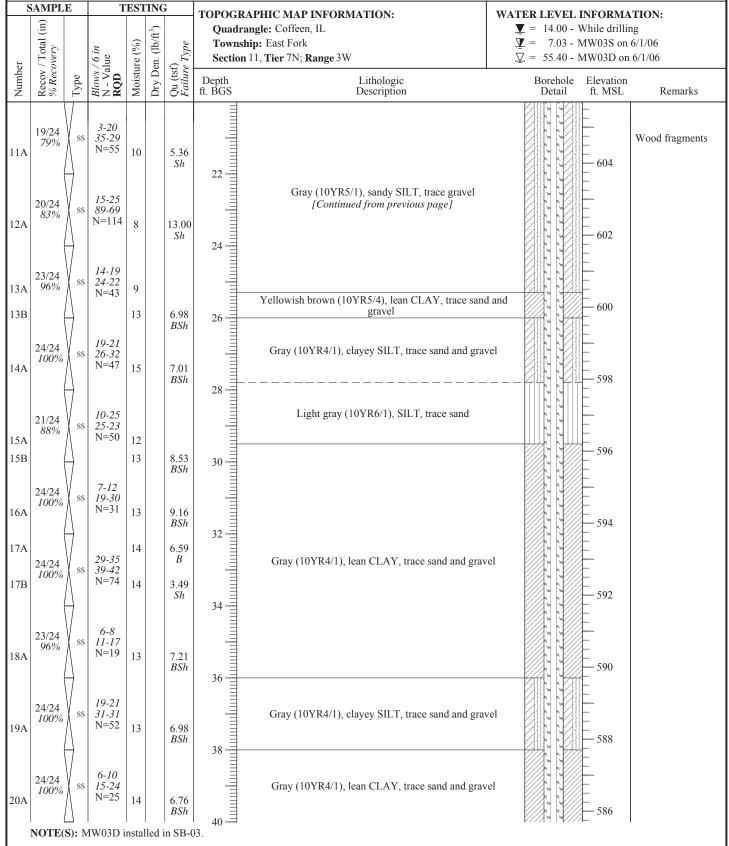
BOREHOLE ID: SB-03 Well ID: MW3D

 Surface Elev:
 626 ft. MSL

 Completion:
 58 ft. BGS

 Station:
 876,554.5N

 2,514,535.3E



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A

DATES: Start: 4/27/2006

Finish: 4/27/2006

Finish: 4/27/2006 **WEATHER:** Sunny, mild (high-50's) **CONTRACTOR:** Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS sampler & 41/4" HSA overdrill

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager



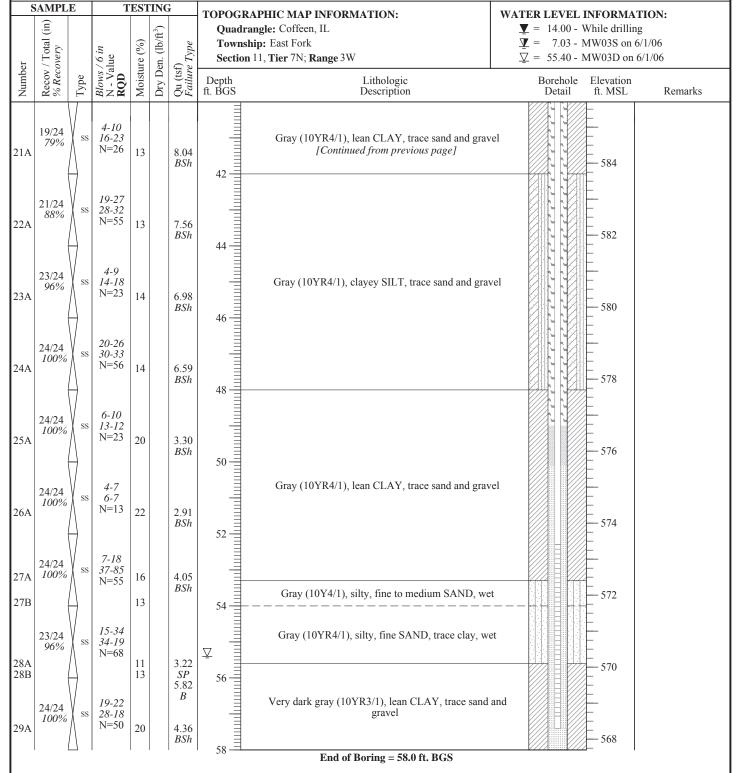
BOREHOLE ID: SB-03 Well ID: MW3D

 Surface Elev:
 626 ft. MSL

 Completion:
 58 ft. BGS

 Station:
 876,554.5N

 2,514,535.3E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A **DATES: Start:** 5/11/2006

Finish: 5/11/2006

WEATHER: Partly sunny, cool (mid-50's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig **Drilling Method:** 41/4" HSA (blind drill)

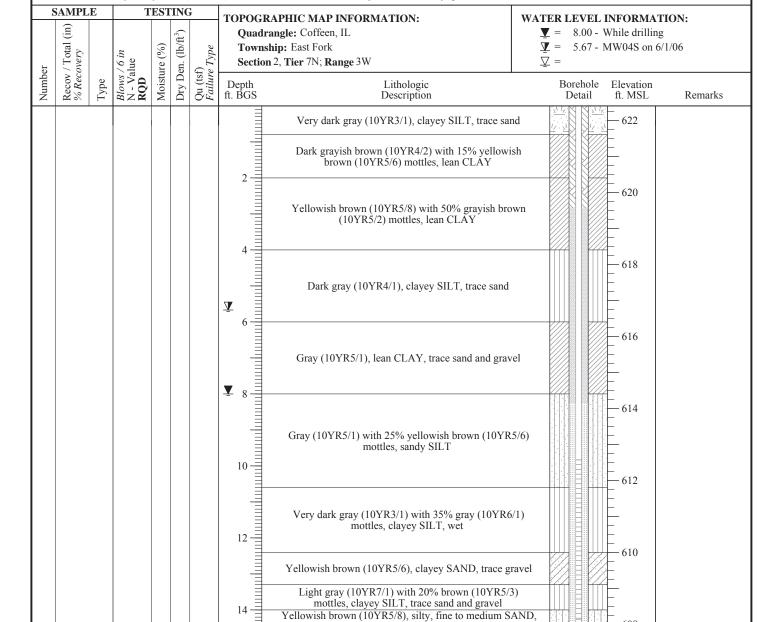
FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: SB-04a Well ID: MW4S

Surface Elev: 622 ft. MSL 15 ft. BGS **Completion: Station:** 877,999.7N 2,514,450.6E



Gray (10YR4/1), sandy SILT, trace gravel End of Boring = 14.77 ft. BGS See SB-04 for sample & testing details

trace coarse sand, wet

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A DATES: Start: 5/11/2006 Finish: 5/11/2006

WEATHER: Partly sunny, cool (mid-50's)

CONTRACTOR: Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: SB-04 **Well ID:** n/a

 Surface Elev:
 622 ft. MSL

 Completion:
 55 ft. BGS

 Station:
 878,000.0N

 2,514,445.0E

| S | SAMPLE TESTING | | | | | | TOPOGRA | APHIC MAP INFORMATION: | WATER LEVEL INFORMATION: | | | | | |
|----------|--------------------|------|---|--------------|-------------------|--------------------------|------------------|--|--------------------------|--------------------|-------------------------------|---------|--|--|
| er | Recov / Total (in) | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Townsh | ngle: Coffeen, IL ip: East Fork 2, Tier 7N; Range 3W | <u>_</u> = | 8.00 - | While drilling MW04S on 6/ | | | |
| Number | Recov % Rec | Type | Blows N - V RQD | Moist | Dry D | Qu (ts Failur | Depth ft. BGS | Lithologic Description | | Borehole Detail | Elevation ft. MSL | Remarks | | |
| Α | 21/24 | | 1-2 | 24 | | 1.09 | | Very dark gray (10YR3/1), clayey SILT, trace sar | nd 1/2 | | 622 | | | |
| 1B | 21/24 88% | ss | 2-4 N=4 | 29 | | В | 2 | Dark grayish brown (10YR4/2) with 15% yellowish brown (10YR5/6) mottles, lean CLAY | sh | | | | | |
| A | 18/24 75% | ss | 2-4 5-6 N=9 | 27 | | 2.72 BSh | 4 | Yellowish brown (10YR5/8) with 50% grayish bro (10YR5/2) mottles, lean CLAY | wn | | 620 | | | |
| A | 16/24 67% | ss | 2-3 4-6 N=7 | 23 | | 1.71 B | ₹ | Dark gray (10YR4/1), clayey SILT, trace sand | | 10000 | 618 | | | |
| ŀA | 24/24 100% | ss | 4-5 5-7 N=10 | 20 | | 1.40 BSP | ¥ 8 | Gray (10YR5/1), lean CLAY, trace sand and grav | el | | 616 | | | |
| δA | 24/24 100% | ss | 1-2 2-2 N=4 | 23 | | 0.70 B | 10- | Gray (10YR5/1) with 25% yellowish brown (10YR: mottles, sandy SILT | 5/6) | | 614 | | | |
| 6A 6B | 24/24 100% | ss | 0-1 2-3 N=3 | 24 | | 0.31 <i>BSh</i> | 12 — | Very dark gray (10YR3/1) with 35% gray (10YR6, mottles, clayey SILT, wet | /1) | 0000 | 612 | | | |
| 'A 'B | 22/24 92% | SS | 0-1 3-7 | 20 | | 0.08 B | 12 = | Yellowish brown (10YR5/6), clayey SAND, trace gr | ravel | | 610 | | | |
| C | | | N=4 | 12 | | | 14 | Light gray (10YR7/1) with 20% brown (10YR5/3 mottles, clayey SILT, trace sand and gravel Yellowish brown (10YR5/8), silty, fine to medium SA | | | | | | |
| Α | 23/24 | V | 4-9 22-25 | 14 | | 4.36 SP | | trace coarse sand, wet | шъ, | | 608 | | | |
| 8B | 96% | ss | 22-35 N=31 | 11 | | | 16- | | | | | | | |
| ЭΑ | 24/24 100% | ss | 27-38 54-50 N=92 | 7 | | | . ⊣ | Gray (10YR4/1), sandy SILT, trace gravel | | | 606 | | | |
| 0A | 24/24 100% | ss | 24-29 39-34 N=68 | 9 | | 2.18 BSh | 18 - | | | | 604 | | | |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

SAMPLE

DATES: Start: 5/11/2006 **Finish:** 5/11/2006

WEATHER: Partly sunny, cool (mid-50's)

TESTING

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

TOPOGRAPHIC MAP INFORMATION:

Eng/Geo: R. Hasenyager

2,514,445.0E WATER LEVEL INFORMATION:

HANSON

622 ft. MSL

55 ft. BGS

878,000.0N

BOREHOLE ID: SB-04

Surface Elev:

Completion:

Station:

Well ID: n/a

| ər | Recov / Total (in) % Recovery | | / 6 in Jue | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadrangl Township: | e: Coffeen, IL East Fork Cier 7N; Range 3W | WATER LEVEL Y = 8.00 - 1 Y = 5.67 - 1 Y = | | | | | |
|--------|----------------------------------|------|---|--------------|-------------------|--------------------------|------------------------|--|--|-------------------|---|--|-----|--|
| Number | Recov % Rec | Type | Blows / 6 in N - Value RQD | Moist | Dry D | Qu (ts Failur | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks | | | |
| 11A | 60/60 100% | CS | | 7 | | | 22 | | | 602 | | | | |
| | 60/60 100% | CS | | | | | 24 — | | | 596 | | | | |
| 12A | 60/60 100% | CS | | 7 | 7 | 7 | 7 | | | 30 — | Gray (10YR4/1), sandy SILT, trace gravel [Continued from previous page] | | 592 | |
| 13A | - | | | 8 | | | 34- | | | 588 | | | | |
| 14A | 60/60 100% | CS | | 13 | | | 38 — | | | 584 | | | | |

NOTE(S): Borehole abandoned using bentonite grout pumped from bottom of borehole.

Page 2 of 3

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

SAMPLE

DATES: Start: 5/11/2006 Finish: 5/11/2006

WEATHER: Partly sunny, cool (mid-50's)

TESTING

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

TOPOGRAPHIC MAP INFORMATION:

Eng/Geo: R. Hasenyager

2,514,445.0E WATER LEVEL INFORMATION:

HANSON

622 ft. MSL

55 ft. BGS

878,000.0N

BOREHOLE ID: SB-04

Surface Elev:

Completion:

Station:

Well ID: n/a

 Ψ = 8.00 - While drilling

Œ, Quadrangle: Coffeen, IL Dry Den. (lb/ft³) Recov / Total (% Recovery Qu (tsf) Failure Type Township: East Fork $\nabla = 5.67 - MW04S \text{ on } 6/1/06$ Moisture (%) Section 2, Tier 7N; Range 3WNumber Elevation Lithologic Borehole Description ft. MSL Remarks 60/60580 CS 100% Gray (10YR4/1), sandy SILT, trace gravel 15A 13 [Continued from previous page] 576 60/60 CS 100% 14 16A 16B 21 572 Greenish gray (10BG5/1) with 20% dark yellowish brown (10YR4/6) mottles, lean CLAY, trace sand 60/60 - 570 CS 100% 17A 24 End of Boring = 55.0 ft. BGS

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A **DATES:** Start: 5/12/2006

Finish: 5/17/2006 **WEATHER:** Sunny, mild (mid-60's)

CONTRACTOR: Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS sampler & 41/4" HSA overdrill

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: SB-05 Well ID: MW5D

> Surface Elev: 623 ft. MSL Completion: 54 ft. BGS Station: 878,174.8N

2,513,290.3E

Page 1 of 3

| SA | MPLI | E | Т | • | TING | 0's) } | Eng/Geo: K. Hasenyager TOPOG PARHIC MARINEORMATION. | WATED I EVEL INFORMATION. |
|------------------|-------------------------------|---------------|--|--------------|-------------------|--------------------------|--|--|
| er (Total Ga) | Recov / Total (in) % Recovery | | /6 in ılue | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | TOPOGRAPHIC MAP INFORMATION: Quadrangle: Coffeen, IL Township: East Fork Section 3, Tier 7N; Range 3W | WATER LEVEL INFORMATION: $\underline{\Psi} = 10.00$ - While drilling $\underline{\Psi} = 6.74$ - MW05S on 6/1/06 $\underline{\nabla} = 50.44$ - MW05D on 6/1/06 |
| Number | Kecov % Rec | Type | Blows / 6 in N - Value RQD | Moist | Dry D | Qu (ts: Failur | Depth Lithologic ft. BGS Description | Borehole Elevation Detail ft. MSL Remarks |
| | 9/24 79% | SS | 0-2 3-4 N=5 | 29 28 | | | Dark grayish brown (10YR4/2), clayey SILT, trace Gray (10YR5/1 with 50% yellowish brown (10YR mottles, clayey SILT Very dark brown (10YR2/2) with 20% dark gray (10YR4/1) mottles, clayey SILT, trace sand Dark gray (10YR4/1) with 30% light gray (10YR mottles, lean CLAY Gray (10YR6/1), lean CLAY, trace sand Vellowish brown (10YR5/6), clayey SAND, trace gwet Yellowish brown (10YR5/6) with 50% gray 10YR mottles, sandy CLAY Gray 10YR6/1), clayey, fine to medium SAND, trace gray 10YR6/1) | 622 |
| A 2 | 22/24 92% | SS | 2-5 5-7 N=10 | 27 | | 2.47 BSh 2.13 | Very dark brown (10YR2/2) with 20% dark gra (10YR4/1) mottles, clayey SILT, trace sand | ay = 620 |
| 2 | 24/24 100% | ss | 2-2 3-6 N=5 | 21 | | 2.33 BSP | Dark gray (10YR4/1) with 30% light gray (10YR mottles, lean CLAY | 7/1) 618 |
| | 24/24 100% | ss | 7-6 6-8 N=12 | 21 | | 1.90 BSh | Gray (10YR6/1), lean CLAY, trace sand | -616 |
| | 8/24 75% | ss | 1-3 4-5 N=7 | 22 | | 1.78 B | Gray (10YR6/1) with 50% yellowish brown (10YI mottles, lean CLAY, trace sand | R5/6) 614 |
| | 20/24 83% | SS | 0-1 3-4 N=4 | 16 22 | | 0.70 BSh | Yellowish brown (10YR5/6), clayey SAND, trace gwet Yellowish brown (10YR5/6) with 50% gray 10YF mottles, sandy CLAY | 612 |
| | 24/24 | SS | 3-6 17-20 N=23 | 19 16 | | Bon | Gray 10YR6/1), clayey, fine to medium SAND, t gravel, wet Brownish yellow (10YR6/6), silty, fine SAND, to medium sand | 610 |
| A 2 | 20/24 83% | SS | 4-16 25-25 N=41 | 20 | | | Yellowish brown (10YR5/6), silty, fine SAND, v | wet |
| B A | | $\frac{1}{2}$ | 14 10 | 11 12 | | | Brown (10YR5/3), silty SAND and GRAVEL, v | wet 606 |
| B 2 | 8/24 75% | SS | 14-18 38-62 N=56 14-39 77 N=116 | 8 | | 3.27 Sh | Dark gray (10YR4/1), sandy SILT, trace clay and g | |

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 5/12/2006 Finish: 5/17/2006 WEATHER: Sunny, mild (mid-60's) **CONTRACTOR:** Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS sampler & 41/4" HSA overdrill

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

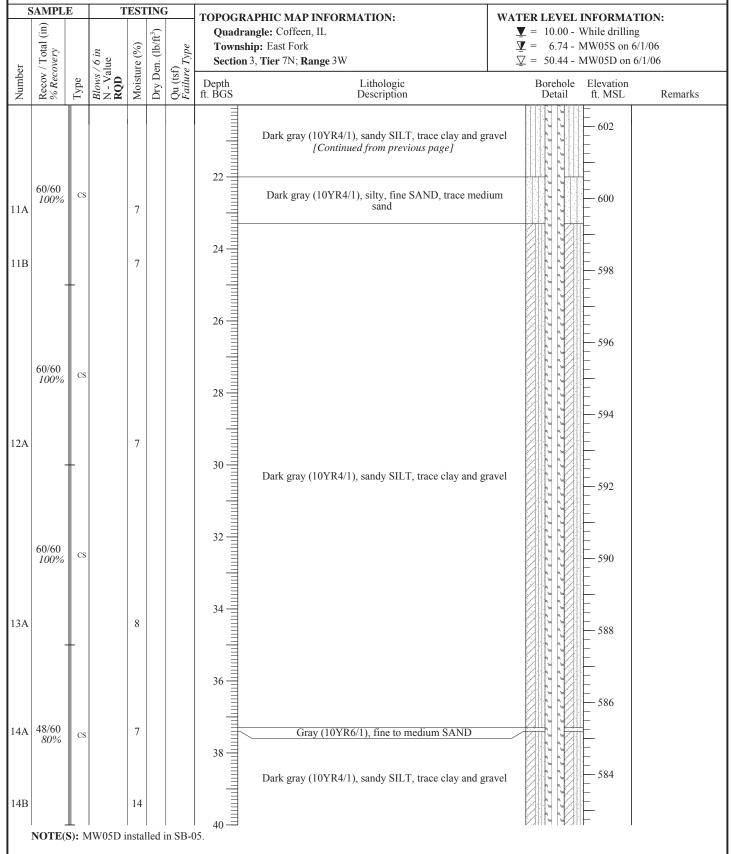
BOREHOLE ID: SB-05

Well ID: MW5D

Surface Elev: 623 ft. MSL Completion: 54 ft. BGS Station: 878,174.8N

2,513,290.3E

Page 2 of 3



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 5/12/2006 Finish: 5/17/2006 WEATHER: Sunny, mild (mid-60's) **CONTRACTOR:** Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS sampler & 41/4" HSA overdrill

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

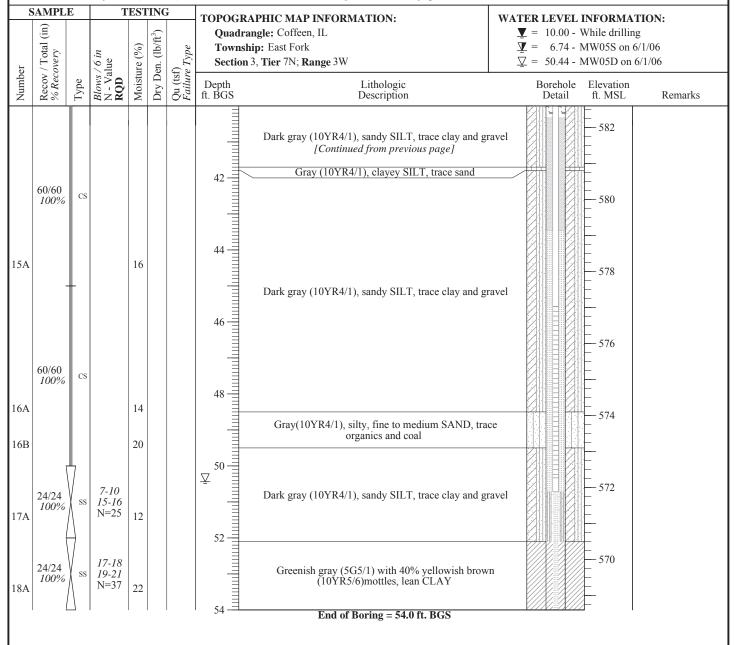
Helper: R. Keedy **Eng/Geo:** R. Hasenyager

BOREHOLE ID: SB-05

Well ID: MW5D

Surface Elev: 623 ft. MSL Completion: 54 ft. BGS Station: 878,174.8N

2,513,290.3E



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A DATES: Start: 5/17/2006

Finish: 5/17/2006
WEATHER: Sunny, mild (mid-60's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 41/4" HSA (blind drill)

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Helper: R. Keedy Eng/Geo: R. Hasenyager **HANSON**

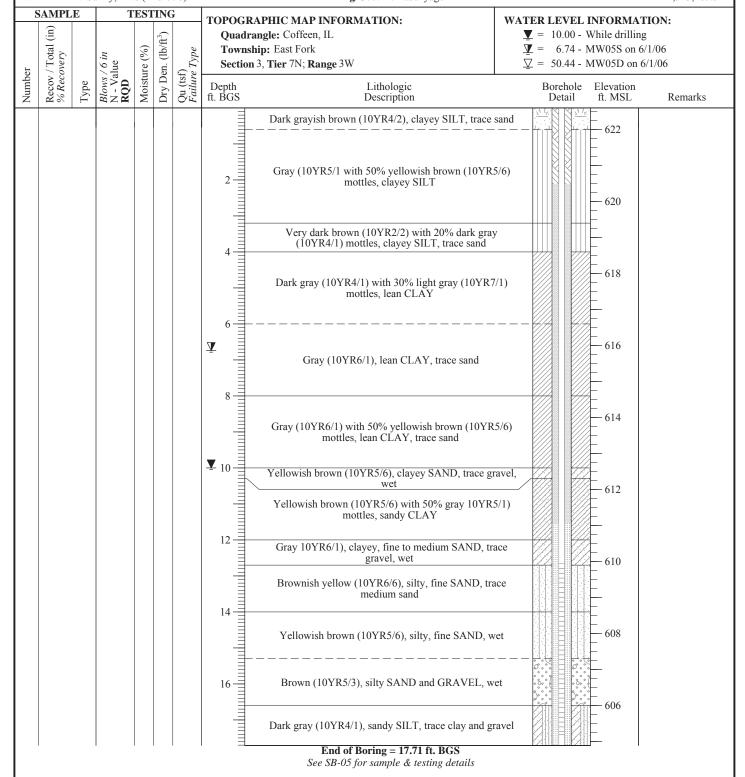
BOREHOLE ID: SB-05a **Well ID:** MW5S

 Surface Elev:
 623 ft. MSL

 Completion:
 18 ft. BGS

 Station:
 878,175.6N

 2,513,285.5E



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A **DATES:** Start: 5/12/2006

Finish: 5/17/2006 **WEATHER:** Sunny, mild (mid-60's)

CONTRACTOR: Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS sampler & 41/4" HSA overdrill

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: SB-05 Well ID: MW5D

> Surface Elev: 623 ft. MSL Completion: 54 ft. BGS Station: 878,174.8N

2,513,290.3E

Page 1 of 3

| SA | MPLI | E | Т | • | TING | 0's) } | Eng/Geo: K. Hasenyager TOPOG PARHIC MARINEORMATION. | WATED I EVEL INFORMATION. |
|------------------|-------------------------------|---------------|--|--------------|-------------------|--------------------------|--|---|
| er (Total Ga) | Recov / Total (in) % Recovery | | /6 in ılue | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | TOPOGRAPHIC MAP INFORMATION: Quadrangle: Coffeen, IL Township: East Fork Section 3, Tier 7N; Range 3W | WATER LEVEL INFORMATION: $\underline{\Psi} = 10.00$ - While drilling $\underline{\Psi} = 6.74$ - MW05S on 6/1/06 $\underline{\nabla} = 50.44$ - MW05D on 6/1/06 |
| Number | Kecov % Rec | Type | Blows / 6 in N - Value RQD | Moist | Dry D | Qu (ts: Failur | Depth Lithologic ft. BGS Description | Borehole Elevation Detail ft. MSL Remarks |
| | 9/24 79% | SS | 0-2 3-4 N=5 | 29 28 | | | Dark grayish brown (10YR4/2), clayey SILT, trace Gray (10YR5/1 with 50% yellowish brown (10YR mottles, clayey SILT Very dark brown (10YR2/2) with 20% dark gray (10YR4/1) mottles, clayey SILT, trace sand Dark gray (10YR4/1) with 30% light gray (10YR mottles, lean CLAY Gray (10YR6/1), lean CLAY, trace sand Vellowish brown (10YR5/6), clayey SAND, trace gwet Yellowish brown (10YR5/6) with 50% gray 10YR mottles, sandy CLAY Gray 10YR6/1), clayey, fine to medium SAND, trace gray 10YR6/1) | 622 |
| A 2 | 22/24 92% | SS | 2-5 5-7 N=10 | 27 | | 2.47 BSh 2.13 | Very dark brown (10YR2/2) with 20% dark gra (10YR4/1) mottles, clayey SILT, trace sand | ay = 620 |
| 2 | 24/24 100% | ss | 2-2 3-6 N=5 | 21 | | 2.33 BSP | Dark gray (10YR4/1) with 30% light gray (10YR mottles, lean CLAY | 7/1) 618 |
| | 24/24 100% | ss | 7-6 6-8 N=12 | 21 | | 1.90 BSh | Gray (10YR6/1), lean CLAY, trace sand | -616 |
| | 8/24 75% | ss | 1-3 4-5 N=7 | 22 | | 1.78 B | Gray (10YR6/1) with 50% yellowish brown (10YI mottles, lean CLAY, trace sand | R5/6) 614 |
| | 20/24 83% | SS | 0-1 3-4 N=4 | 16 22 | | 0.70 BSh | Yellowish brown (10YR5/6), clayey SAND, trace gwet Yellowish brown (10YR5/6) with 50% gray 10YF mottles, sandy CLAY | 612 |
| | 24/24 | SS | 3-6 17-20 N=23 | 19 16 | | Bon | Gray 10YR6/1), clayey, fine to medium SAND, t gravel, wet Brownish yellow (10YR6/6), silty, fine SAND, to medium sand | 610 |
| A 2 | 20/24 83% | SS | 4-16 25-25 N=41 | 20 | | | Yellowish brown (10YR5/6), silty, fine SAND, v | wet |
| B A | | $\frac{1}{2}$ | 14 10 | 11 12 | | | Brown (10YR5/3), silty SAND and GRAVEL, v | wet 606 |
| B 2 | 8/24 75% | SS | 14-18 38-62 N=56 14-39 77 N=116 | 8 | | 3.27 Sh | Dark gray (10YR4/1), sandy SILT, trace clay and g | |

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 5/12/2006 Finish: 5/17/2006 WEATHER: Sunny, mild (mid-60's) **CONTRACTOR:** Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS sampler & 41/4" HSA overdrill

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

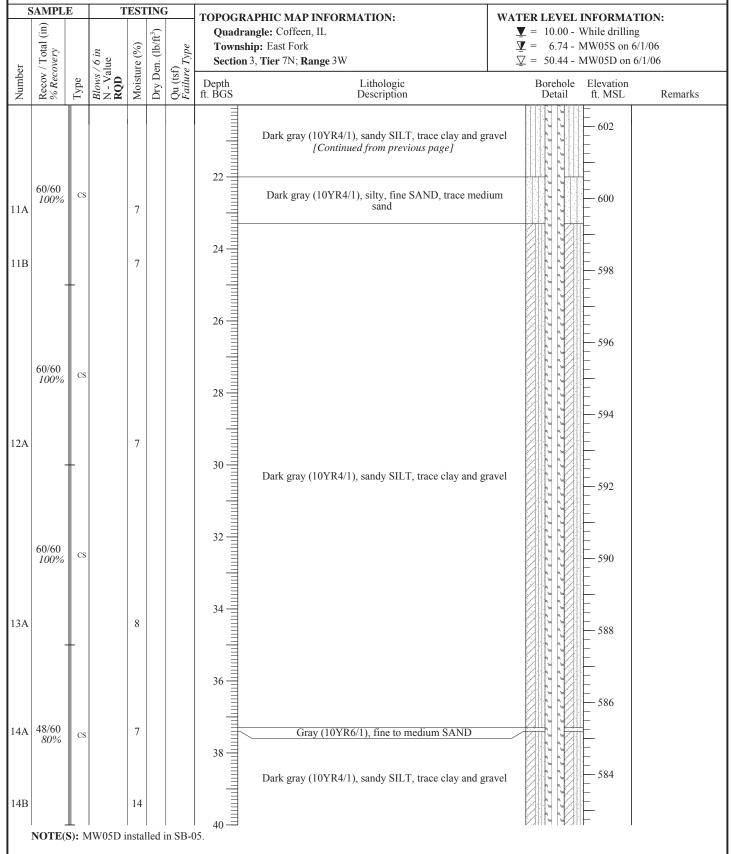
BOREHOLE ID: SB-05

Well ID: MW5D

Surface Elev: 623 ft. MSL Completion: 54 ft. BGS Station: 878,174.8N

2,513,290.3E

Page 2 of 3



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 5/12/2006 Finish: 5/17/2006 WEATHER: Sunny, mild (mid-60's) **CONTRACTOR:** Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS sampler & 41/4" HSA overdrill

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

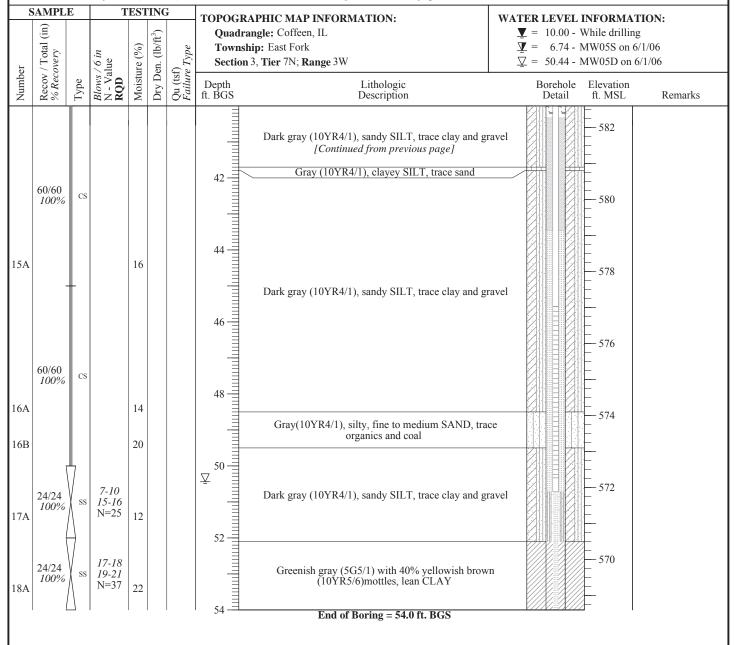
Helper: R. Keedy **Eng/Geo:** R. Hasenyager

BOREHOLE ID: SB-05

Well ID: MW5D

Surface Elev: 623 ft. MSL Completion: 54 ft. BGS Station: 878,174.8N

2,513,290.3E



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A DATES: Start: 5/4/2006 Finish: 5/4/2006

Finish: 5/4/2006 **WEATHER:** Partly sunny, cool (mid-50's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 31/4" HSA (blind drill)

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

HANSON

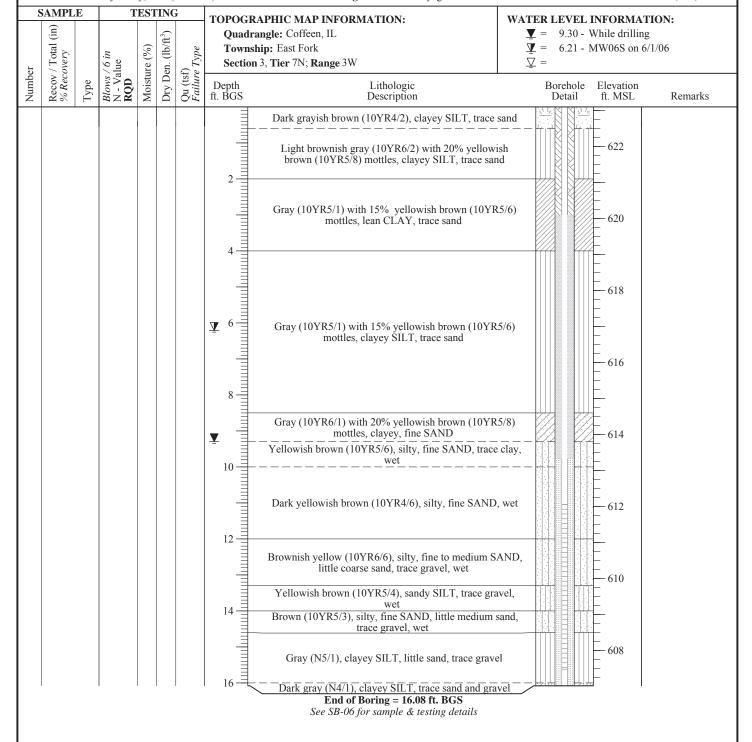
BOREHOLE ID: SB-06a Well ID: MW6S

 Surface Elev:
 623 ft. MSL

 Completion:
 16 ft. BGS

 Station:
 879,021.2N

 2,513,189.4E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility Location: Coffeen, Illinois

Project: 05S3004A **DATES: Start:** 5/4/2006

Finish: 5/4/2006 WEATHER: Partly sunny, cool (mid-50's) **CONTRACTOR:** Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 31/4" HSA w/SS sampler

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

BOREHOLE ID: SB-06 Well ID: n/a

> **Surface Elev:** 623 ft. MSL **Completion:** 60 ft. BGS Station: 879,015.0N 2,513,190.0E

SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: Ξ Ψ = 9.30 - While drilling Quadrangle: Coffeen, IL Dry Den. (lb/ft3 Recov / Total % Recovery Township: East Fork $\nabla = 6.21 - MW06S \text{ on } 6/1/06$ Qu (tsf) Failure Type Moisture (%) Blows / 6 in N - Value RQD Section 3, Tier 7N; Range 3W Number Depth ft. BGS Lithologic Borehole Elevation Description Detail Remarks Dark grayish brown (10YR4/2), clayey SILT, trace sand 25 1A 2-3 SP24/24 SS 3-5 622 100% Light brownish gray (10YR6/2) with 20% yellowish N=61B 28 1.96 brown (10YR5/8) mottles, clayey SILT, trace sand B24/24 Gray (10YR5/1) with 15% yellowish brown (10YR5/6) 2A 27 1 94 5-6 SS 620 100% mottles, lean CLAY, trace sand BShN=92B19 2.52 BSh1-3 24/24 618 100% 3A 21 1.36 В Gray (10YR5/1) with 15% yellowish brown (10YR5/6) mottles, clayey SILT, trace sand <u>1</u> 4-6 24/24 100% 616 N=1217 1.78 B5A 18 0.85 BShGray (10YR6/1) with 20% yellowish brown (10YR5/8) 22/24 3-3 mottles, clayey, fine SAND 614 92% 5B 17 0.81 Yellowish brown (10YR5/6), silty, fine SAND, trace clay, None wet 5C 21 0.31 10 None 0 - 120/24 Dark yellowish brown (10YR4/6), silty, fine SAND, wet 2-4 612 83% N=325 6A 12 Brownish yellow (10YR6/6), silty, fine to medium SAND, little coarse sand, trace gravel, wet 24/24 7-8 100% 15 7A N=11Yellowish brown (10YR5/4), sandy SILT, trace gravel, wet 7B 12 1.48 Brown (10YR5/3), silty, fine SAND, little medium sand, BShtrace gravel, wet 11-33 22/24 57-35 N=90 608 92% Gray (N5/1), clayey SILT, little sand, trace gravel 8 8B 7.18 30-39 22/24 46-55 606 92% N = 859A 11.35 Dark gray (N4/1), clayey SILT, trace sand and gravel 4-23 24/24 50-51 SS 604 100% N = 737 10A 11 64 Sh20 NOTE(S): Borehole abandoned using bentonite grout pumped from bottom of borehole.

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility Location: Coffeen, Illinois

Project: 05S3004A

WEATHER: Partly sunny, cool (mid-50's)

DATES: Start: 5/4/2006 **Finish:** 5/4/2006 **CONTRACTOR:** Testing Service Corporation Rig mfg/model: CME-650 Track Rig **Drilling Method:** 31/4" HSA w/SS sampler

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy Eng/Geo: R. Hasenyager HANSON

BOREHOLE ID: SB-06 Well ID: n/a

623 ft. MSL **Surface Elev:** 60 ft. BGS **Completion: Station:** 879,015.0N 2,513,190.0E

Page 2 of 3

| S | SAMPL | E | Т | EST | ING | 1 | ТОРОСР | APHIC MAP INFORMATION: | WATER LEVEL INFORMATION: |
|----------|-------------------------------|------|----------------------------------|--------------|-------------------|--------------------------|------------------|--|---|
| ber | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadra | ingle: Coffeen, IL nip: East Fork 3, Tier 7N; Range 3W | $\underline{\underline{\mathbf{y}}}$ = 9.30 - While drilling $\underline{\underline{\mathbf{y}}}$ = 6.21 - MW06S on 6/1/06 $\underline{\underline{\nabla}}$ = |
| Number | Reco % Re | Type | Blow N - V RQD | Mois | Dry] | Qu (1 Failu | Depth ft. BGS | Lithologic Description | Borehole Elevation Detail ft. MSL Remarks |
| 1A | 20/24 83% | ss | 6-16 33-58 N=49 | 11 | | 3.49 <i>BSh</i> | 22 | | 602 |
| 2A | 20/24 83% | ss | 45-56 54-50/3" N=110 | 9 | | 11.64 Sh | 24 | | 600 |
| 3A | 12/24 50% | ss | 26-78 | 12 | | 2.84 Sh | 26 | | 598 |
| 4A | 8/24 33% | ss | 52-48/2" | 9 | | 5.43 <i>BSh</i> | 28 | | 596 |
| 5A | 24/24 100% | ss | 10-24 30-40 N=54 | 13 | | 4.95 BSh | 30 | Dark gray (N4/1), clayey SILT, trace sand and gra [Continued from previous page] | vel |
| 6A | 21/24 88% | ss | 10-16 37-38 N=53 | 8 | | 10.91 <i>BSh</i> | 32 | | 592 |
| 7A | 17/24 71% | ss | 36-47 61/5" | 9 | | | | | 590 |
| 8A | 22/24 92% | ss | 11-36 45-60 N=81 | 9 | | 10.04 Sh | 36 | | 588 |
| 9A 9B | 22/24 92% | ss | 40-35 34-29 N=69 | 10 13 | | 9.60 Sh 8.92 | 36 | | 586 |
| 0A | 24/24 100% | ss | 3-8 12-15 N=20 | 14 | | 8.53 BSh | 40 | Very dark greenish gray (10Y3/1), lean CLAY, trace | sand 584 |

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A DATES: Start: 5/4/2006 Finish: 5/4/2006

Finish: 5/4/2006 **WEATHER:** Partly sunny, cool (mid-50's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 3¹/₄" HSA w/SS sampler

FIELD STAFF: Driller: B. Williamson **Helper:** R. Keedy

Eng/Geo: R. Hasenyager



BOREHOLE ID: SB-06 Well ID: n/a

 Surface Elev:
 623 ft. MSL

 Completion:
 60 ft. BGS

 Station:
 879,015.0N

 2,513,190.0E

| | SAMPL | E | Т | EST | ING | Ţ. | TOPOGRA | APHIC MAP INFORMATION: | WATI | WATER LEVEL INFORMATION: | | | | | |
|--------|----------------------------------|------|---|--------------|-------------------|--------------------------|-------------------|--|--------------------------|---|-------------------|---------|--|--|--|
| ber | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Townsh Section | ngle: Coffeen, IL ip: East Fork 3, Tier 7N; Range 3W | $\bar{\mathbf{\Lambda}}$ | $\underline{\Psi}$ = 9.30 - While drilling $\underline{\Psi}$ = 6.21 - MW06S on 6/1/06 $\underline{\nabla}$ = | | | | | |
| Number | Reco % Re | Type | Blow N - V RQD | Mois | Dry I | Qu (t Failu | Depth ft. BGS | Lithologic Description | | Borehole Detail | Elevation ft. MSL | Remarks | | | |
| 1A | 23/24 96% | ss | 3-5 8-12 N=13 | 15 | | 4.27 B | 44 | | | 00000 | 582 | | | | |
| 2A | 22/24 92% | ss | 6-6 7-8 N=13 | 14 | | 3.49 B | 44 | | | | 580 | | | | |
| 3A | 24/24 100% | ss | 5-7 9-12 N=16 | 16 | | 2.72 B | 46 | Very dark greenish gray (10Y3/1), lean CLAY, trace and gravel | sand | () () () () () () () () () () () () () (| 578 | | | | |
| 4A | 24/24 100% | ss | 4-8 10-11 N=18 | 15 | | 4.07 B | 48 | a 5 | | () () () () () () () () () () () () () (| 576 | | | | |
| 5A | 24/24 100% | ss | 5-6 9-13 N=15 | 15 | | 3.10 B | 50 | | | | 574 | | | | |
| 6A | 24/24 100% | ss | 5-6 8-12 N=14 | 22 | | 1.94 <i>B</i> | 52 | | | | 572 | | | | |
| 7A | 24/24 100% | ss | 5-6 8-8 N=14 | 23 | | 2.13 B | 54 | Dark greenish gray (10BG4/1), lean CLAY | | | 570 | | | | |
| 8A | 24/24 100% | ss | 3-5 6-8 N=11 | 24 | | 2.33 BSh | 54 | | | | 568 | | | | |
| 9A | 24/24 100% | ss | 12-10 12-14 N=22 | 24 | | 3.30 <i>BSh</i> | 58 | Greenish gray (5G4/1) with 10% dark yellowish bro (10YR3/4) mottles, lean CLAY, trace sand | own | | 566 | | | | |
| 0A | 24/24 100% | ss | 5-8 12-13 N=20 | 27 | | 2.13 <i>BSh</i> | 60 | Dark greenish gray (10G4/1), lean CLAY, trace sa End of Boring = 60.0 ft. BGS | nd | | 564 | | | | |

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A **DATES: Start:** 5/9/2006

Finish: 5/9/2006
WEATHER: Overcast, mild (mid-60's)

CONTRACTOR: Reynolds Drilling Corp. **Rig mfg/model:** CME-1050 ATV Rig **Drilling Method:** 4¹/₄" HSA (blind drill)

FIELD STAFF: Driller: P. McIntire Helper: S. McCartney Eng/Geo: R. Hasenyager **HANSON**

BOREHOLE ID: SB-07a **Well ID:** MW7S

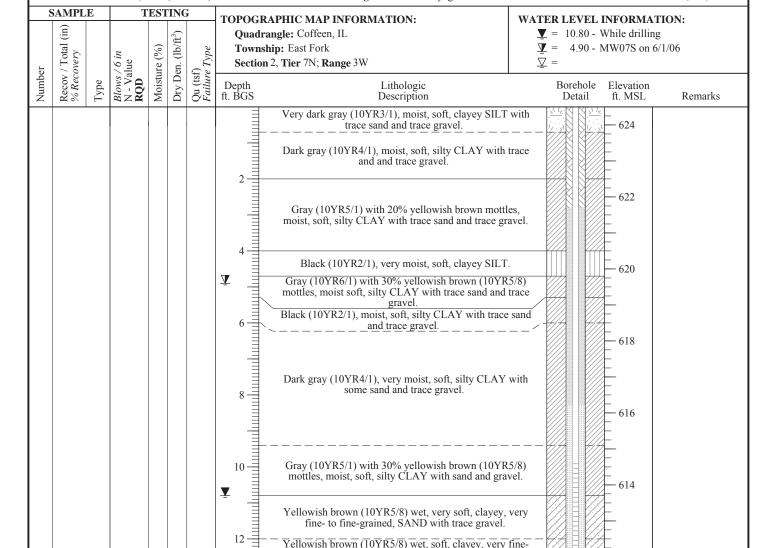
612

 Surface Elev:
 625 ft. MSL

 Completion:
 14 ft. BGS

 Station:
 879,181.1N

 2,514,397.5E



End of Boring = 14.39 ft. BGS See SB-07 for sample & testing details

to fine-grained, SAND with trace gravel.

Gray (10YR4/1), moist, very hard, sandy, clayey SILT with gravel.

NOTE(S): MW07S installed in blind-drilled borehole within 10 ft of SB-07.

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A **DATES: Start:** 5/5/2006

Finish: 5/8/2006

WEATHER: Partly cloudy, mild (mid-70s)

CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

Eng/Geo: R. Hasenyager

FIELD STAFF: Driller: P. McIntire Helper: S. McCartney **BOREHOLE ID:** SB-07 Well ID: n/a

Station:

625 ft. MSL **Surface Elev: Completion:** 54 ft. BGS

HANSON

879,180.0N 2,514,390.0E

Page 1 of 3

| | SAMPLE | | Т | EST | ING | j | TOPOGRAPHIC MAP INFORMATION: | WATER LEVEL INFORMATION: |
|----------------|----------------------------------|--------------|---|----------------|-------------------|---|--|--|
| er | Recov / Total (in) % Recovery | | /6 in alue | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadrangle: Coffeen, IL Township: East Fork Section 2, Tier 7N; Range 3W | $\underline{\Psi}$ = 10.80 - While drilling $\underline{\Psi}$ = 4.90 - MW07S on 6/1/06 $\underline{\nabla}$ = |
| Number | Recov % Rec | Type | Blows / 6 in N - Value RQD | Moist | Dry D | Qu (ts Failur | Depth Lithologic ft. BGS Description | Borehole Elevation Detail ft. MSL Remarks |
| 1A 1B | 18/24 75% | ss | 1-1 1-1 N=2 | 23 | | 2.40 B | Very dark gray (10YR3/1), moist, soft, clayey SILT trace sand and trace gravel. Dark gray (10YR4/1), moist, soft, silty CLAY with tand and trace gravel. | 624 |
| 2A | 24/24 100% | ss | 0-0 1-1 N=1 | 26 | | 2.33 B | Gray (10YR5/1) with 20% yellowish brown mottle moist, soft, silty CLAY with trace sand and trace gra | es, avel. |
| 3A 3B 3C | 24/24 100% | ss | 0-1 1-2 N=2 | 25 25 22 | | 4.33 BSh 2.52 BSh 3.05 B | Dark gray (10YR4/1), moist, soft, silty CLAY with the and and trace gravel. Gray (10YR5/1) with 20% yellowish brown mottle moist, soft, silty CLAY with trace sand and trace gravel. Black (10YR2/1), very moist, soft, clayey SILT. Gray (10YR6/1) with 30% yellowish brown (10YR: mottles, moist soft, silty CLAY with trace sand and the gravel. Black (10YR2/1), moist, soft, silty CLAY with trace and trace gravel. Dark gray (10YR4/1), very moist, soft, silty CLAY some sand and trace gravel. | 5/8) trace |
| 4A | 24/24 100% | ss | 0-1 1-2 N=2 | 22 | | 1.75 B | Dark gray (10YR4/1), very moist, soft, silty CLAY some sand and trace gravel. | with 618 |
| 5A | 24/24 100% | SS | 0-0 1-1 N=1 | 22 | | 1.24 B | | 5/8) |
| 6A | 24/24 100% | ss | 0-0 0-1 N=0 | 24 | | 0.54 B | Gray (10YR5/1) with 30% yellowish brown (10YR: mottles, moist, soft, silty CLAY with sand and grave Yellowish brown (10YR5/8) wet, very soft, clayey, fine- to fine-grained, SAND with trace gravel. | vel. 614 |
| 6B 7A | 24/24 | ss | 0-0 1-2 | 20 24 | | 1.65 B | 12 —— Yellowish brown (10YR5/8) wet, soft, clayey, very to fine-grained, SAND with trace gravel. | fine- 612 |
| 7B | 100% | \bigwedge | N=1 | 13 | | 2.89 B | 14 — | 610 |
| 8A | 24/24 100% | ss | 2-5 7-9 N=12 | 8 | | 5.04 <i>BSh</i> | Gray (10YR4/1), moist, very hard, sandy, clayey Sl | |
| 9A | 24/24 100% | ss | 3-6 6-8 N=12 | 9 | | 9.27 <i>BSh</i> | with gravel. | 608 |
| 10A | | SS | 3-6 8-11 N=14 | 9 | | 11.13 BSh | 20 | 606 |
| | NOTE(| S): B | Borehole a CME-105 | aban 0 ha | done d 280 | ed using 0# ham | bentonite grout pumped from bottom of borehole. mer for SPT. | |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A **DATES: Start:** 5/5/2006

Finish: 5/8/2006 WEATHER: Partly cloudy, mild (mid-70s) **CONTRACTOR:** Reynolds Drilling Corp. Rig mfg/model: CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: P. McIntire Helper: S. McCartney

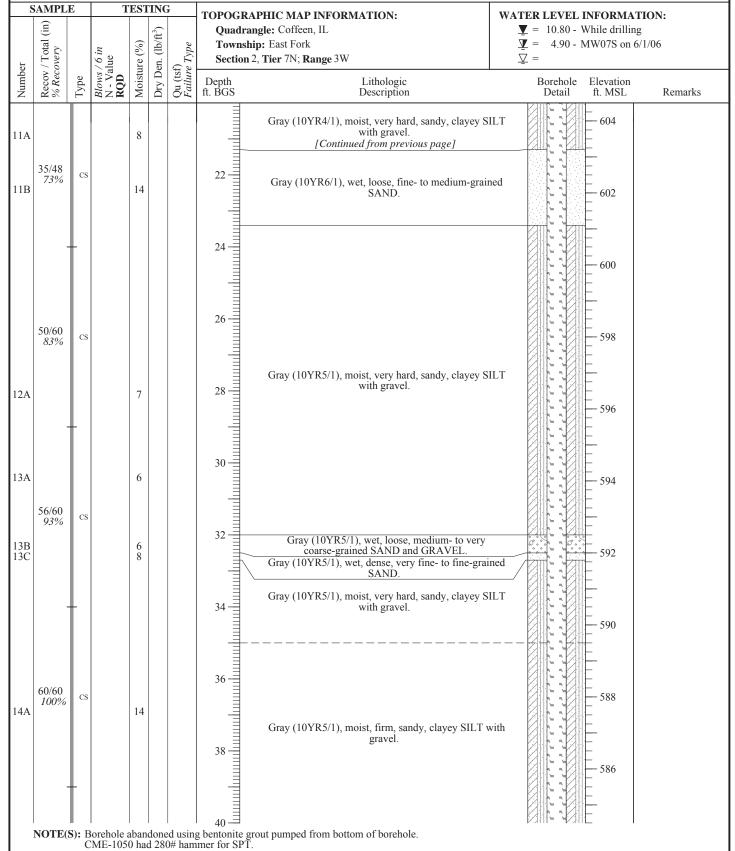
Eng/Geo: R. Hasenyager



BOREHOLE ID: SB-07 Well ID: n/a

Surface Elev: 625 ft. MSL 54 ft. BGS **Completion: Station:** 879,180.0N 2,514,390.0E

Page 2 of 3



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

DATES: Start: 5/5/2006 Finish: 5/8/2006 **CONTRACTOR:** Reynolds Drilling Corp. Rig mfg/model: CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

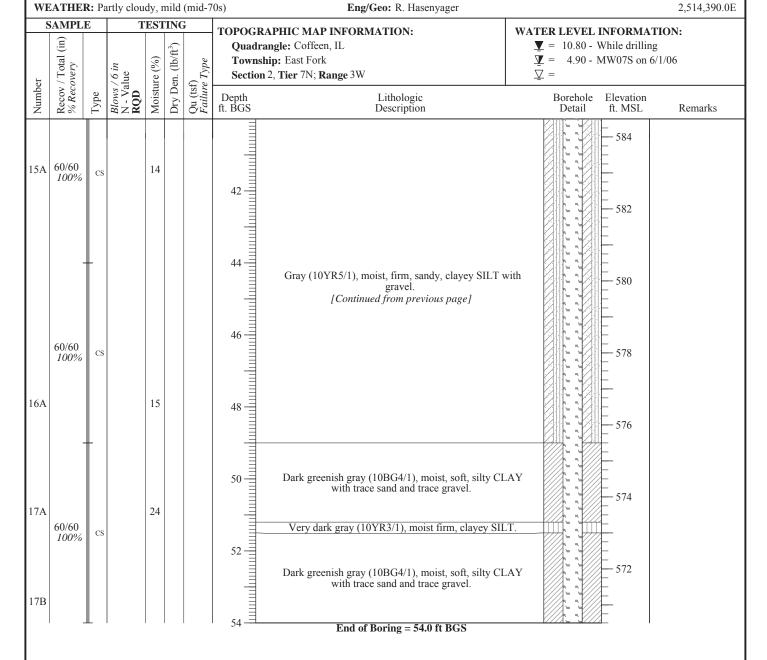
FIELD STAFF: Driller: P. McIntire Helper: S. McCartney

Eng/Geo: R. Hasenyager

BOREHOLE ID: SB-07

Well ID: n/a **Surface Elev:** 625 ft. MSL 54 ft. BGS **Completion: Station:** 879,180.0N

HANSON



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility Location: Coffeen, Illinois

Project: 05S3004A **DATES: Start:** 5/10/2006

Finish: 5/10/2006

WEATHER: Foggy to partly sunny, mild (hi-60's)

CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-1050 ATV Rig **Drilling Method:** 41/4" HSA (blind drill)

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

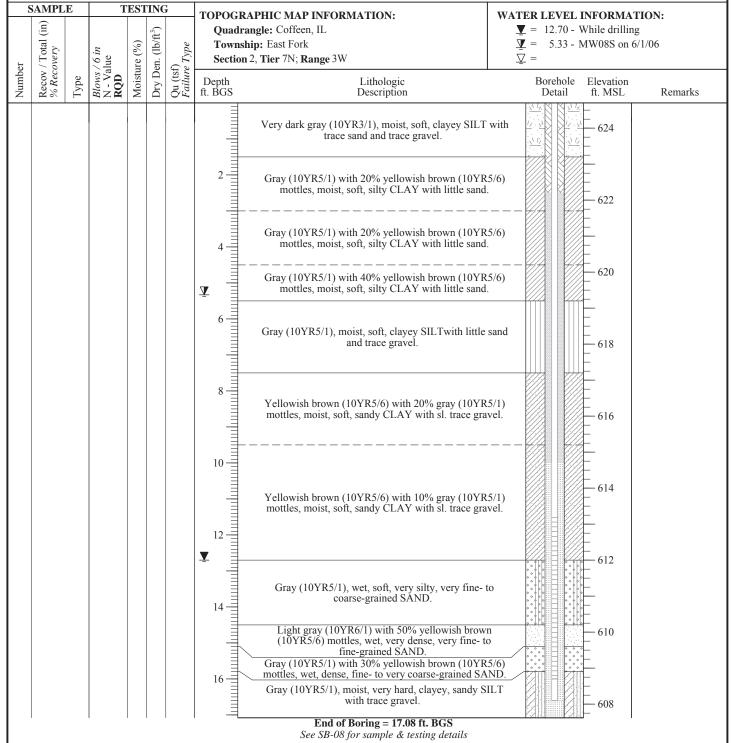
Eng/Geo: R. Hasenyager

BOREHOLE ID: SB-08a Well ID: MW8S

Surface Elev: 625 ft. MSL 17 ft. BGS **Completion: Station:** 879,776.6N

2,514,478.8E

HANSON



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A **DATES: Start:** 5/9/2006

Finish: 5/10/2006

CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

WEATHER: Foggy to partly sunny, mild (hi-60's) Eng/Geo: R. Hasenyager **SAMPLE** TESTING

WATER LEVEL INFORMATION:

HANSON

625 ft. MSL

59 ft. BGS

879,770.0N

2,514,480.0E

BOREHOLE ID: SB-08

Surface Elev:

Completion:

Station:

Well ID: n/a

TOPOGRAPHIC MAP INFORMATION: $\mathbf{V} = 12.70$ - While drilling Quadrangle: Coffeen, IL Township: East Fork Section 2, Tier 7N; Range 3W

 Ξ Dry Den. (lb/ft3 Recov / Total % Recovery $\nabla = 5.33 - MW08S \text{ on } 6/1/06$ Qu (tsf) Failure Type Moisture (%) Blows / 6 in N - Value RQD Number Depth Lithologic Borehole Elevation ft. BGS Description Detail ft. MSL Remarks Very dark gray (10YR3/1), moist, soft, clayey SILT with 624 1-1 24/24 trace sand and trace gravel. SS 100% N=2Gray (10YR5/1) with 20% yellowish brown (10YR5/6) mottles, moist, soft, silty CLAY with little sand. 622 1-1 24/24 SS 100% N=22A 25 1.59 Gray (10YR5/1) with 20% yellowish brown (10YR5/6) В mottles, moist, soft, silty CLAY with little sand. 620 1-1 Gray (10YR5/1) with 40% yellowish brown (10YR5/6) 24/24 3A 20 1.86 100% mottles, moist, soft, silty CLAY with little sand. В 3B 21 1.20 RGray (10YR5/1), moist, soft, clayey SILTwith little sand and trace gravel. 618 0-1 24/24 SS 100% 4A 25 1.01 None Yellowish brown (10YR5/6) with 20% gray (10YR5/1) mottles, moist, soft, sandy CLAY with sl. trace gravel. 0-1 616 24/24 100% N=221 5A 10 614 0 - 124/24 0.70 21 6A Yellowish brown (10YR5/6) with 10% gray (10YR5/1) 100% BShN=2mottles, moist, soft, sandy CLAY with sl. trace gravel. 31 6B 12 Y 0-1 612 20/24 7A 13 83% Gray (10YR5/1), wet, soft, very silty, very fine- to coarse-grained SAND. 7B 15 Light gray (10YR6/1) with 50% yellowish brown 7-11 610 23/24 9 5 4 5 8A (10YR5/6) mottles, wet, very dense, very fine- to 16 96% Shfine-grained SAND. N=27Gray (10YR5/1) with 30% yellowish brown (10YR5/6) 8B 8 mottles, wet, dense, fine- to very coarse-grained SAND. 16 608 24/30 CS 80% Gray (10YR5/1), moist, very hard, clayey, sandy SILT with trace gravel. 9A 5 606

NOTE(S): Borehole abandoned using bentonite grout pumped from bottom of borehole. CME-1050 had 280# hammer for SPT.

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

SAMPLE

DATES: Start: 5/9/2006 **Finish:** 5/10/2006

WEATHER: Foggy to partly sunny, mild (hi-60's)

TESTING

CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager

WATER LEVEL INFORMATION:

HANSON

625 ft. MSL

59 ft. BGS

879,770.0N

2,514,480.0E

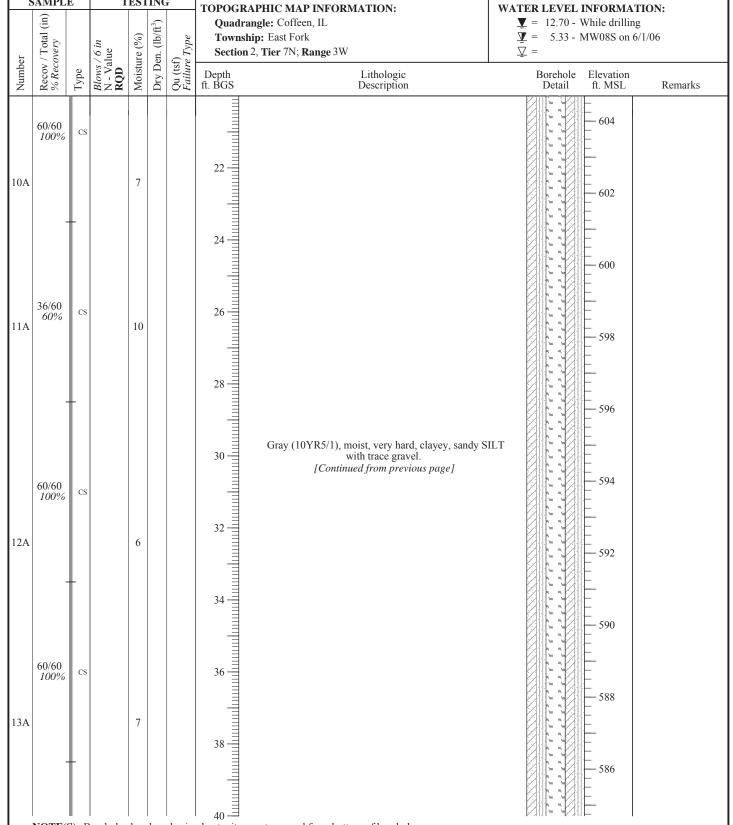
BOREHOLE ID: SB-08

Surface Elev:

Completion:

Station:

Well ID: n/a



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A **DATES: Start:** 5/9/2006

Finish: 5/10/2006

WEATHER: Foggy to partly sunny, mild (hi-60's)

CONTRACTOR: Reynolds Drilling Corp. **Rig mfg/model:** CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: SB-08

Well ID: n/a

Surface Elev: 625 ft. MSL **Completion:** 59 ft. BGS

Station: 879,770.0N 2,514,480.0E

| | SAMPLE TESTING | | | | | Eng/Geo: R. nasenyager | | | 2,314,460.0E | | |
|------------|-------------------------------|------|----------------------------------|--------------|-------------------|--------------------------|-------------------|--|--|-------------------|---------|
| | | Li . | 1 | | | | Quadra | APHIC MAP INFORMATION: ngle: Coffeen, IL | WATER LEVEL 1 $\underline{\nabla}$ = 12.70 - V | While drilling | |
| | Fotal ery | | s in | (%) | (lb/f | Fype | | ip: East Fork 2, Tier 7N; Range 3W | $\underline{\underline{\mathbf{y}}} = 5.33 - 1$ $\underline{\underline{\nabla}} =$ | MW08S on 6/1/ | /06 |
| Number | Recov / Total (in) % Recovery | Type | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks |
| | 60/60 | cs | | | | | 12 | Gray (10YR5/1), moist, very hard, clayey, sandy Sl with trace gravel. [Continued from previous page] | | 584 | |
| 14A 14B | _ | | | 14 11 | | | 42 | Greenish gray (10BG5/1) with 10% yellowish brow (10YR5/6) mottles, moist, firm, silty CLAY with li sand and trace gravel Gray (10YR5/1), moist, very hard, clayey, sandy Sl with trace gravel. | ttle | | |
| 15A | | | | 12 | | | 44 | Dark yellowish brown (10YR4/4), moist, firm, clay SILT with some sand and trace gravel. | /ey | | |
| 15B | 60/60 100% | CS | | 15 | | | 46 | Gray (10YR4/1), moist, hard, clayey, sandy SILT v trace gravel. | rith | 580 | |
| 15C | | | | 13 | | | 48 | Gray (10YR4/1) with 50% very dark grayish brow (10YR3/2), moist, firm, silty CLAY with sand and t gravel. | n race | | |
| 16A | 60/60 | CS | | 14 | | | 50 = 52 = 52 = 52 | Gray (10YR4/1), moist, hard, clayey, sandy SILT v trace gravel. | rith | 576 | |
| 16B 17A | | | | 19 24 | | | 54 — | Greenish gray (10BG4/1), moist, soft, silty CLAY v little sand and sl. trace gravel. | vith | 572 | |
| | 60/60 100% | CS | | | | | 56 | Yellowish brown (10YR5/6) with 20% Greenish g (10BG4/1) mottles, moist, soft, silty CLAY with li sand and sl. trace gravel. | ray tile | 568 | |
| 17B | _ | L | | 19 | | | 58 = | End of Boring = 58.5 ft. | | | |

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A DATES: Start: 5/3/2006 Finish: 5/3/2006

WEATHER: Overcast, mild (mid-60's)

CONTRACTOR: Reynolds Drilling Corp. **Rig mfg/model:** CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel

Helper: S. McCartney **Eng/Geo:** R. Hasenyager

HANSON

BOREHOLE ID: SB-09 **Well ID:** MW9D

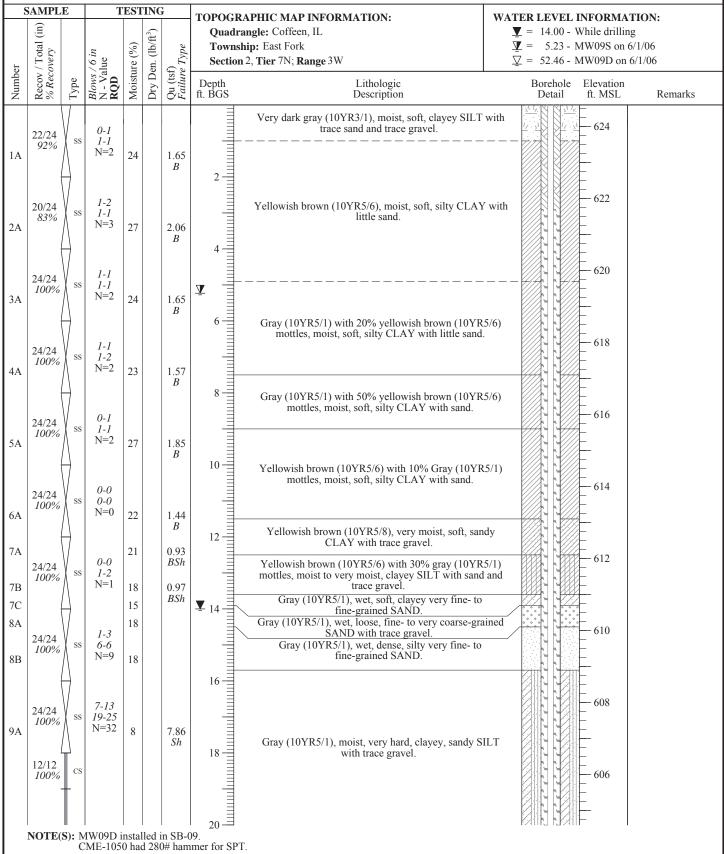
 Surface Elev:
 625 ft. MSL

 Completion:
 54 ft. BGS

 Station:
 879,679.7N

 2,515,666.3E

Page 1 of 3



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

SAMPLE

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DATES: Start: 5/3/2006 Finish: 5/3/2006

WEATHER: Overcast, mild (mid-60's)

TESTING

CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel

Helper: S. McCartney Eng/Geo: R. Hasenyager

2,515,666.3E

HANSON

625 ft. MSL

54 ft. BGS

879,679.7N

BOREHOLE ID: SB-09

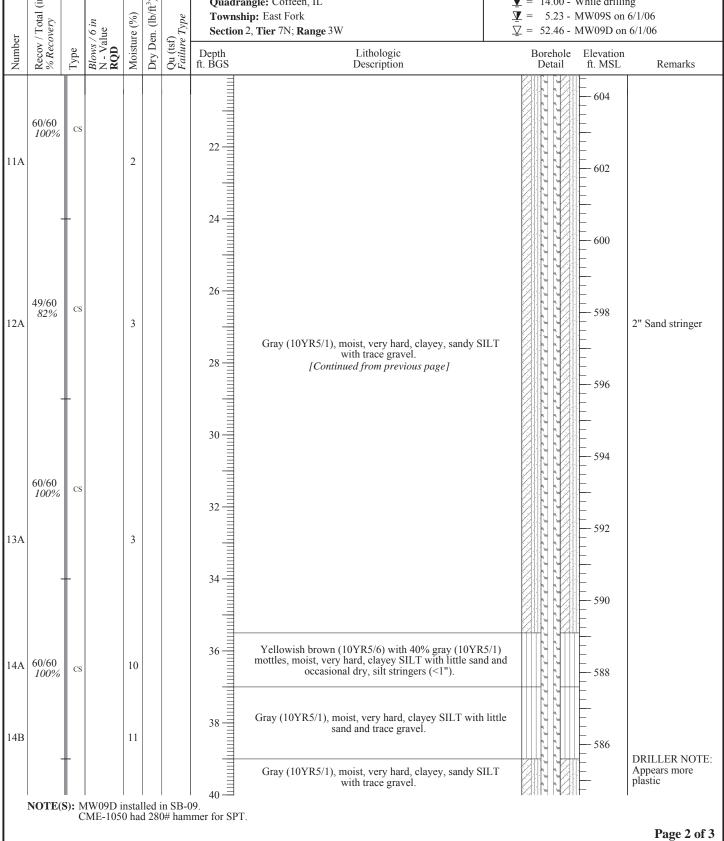
Surface Elev:

Completion:

Station:

Well ID: MW9D

TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: Quadrangle: Coffeen, IL $\mathbf{Y} = 14.00$ - While drilling Township: East Fork $\nabla = 5.23 - MW09S \text{ on } 6/1/06$ Section 2, Tier 7N; Range 3W



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A **DATES: Start:** 5/3/2006

Finish: 5/3/2006 WEATHER: Overcast, mild (mid-60's) **CONTRACTOR:** Reynolds Drilling Corp. **Rig mfg/model:** CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager



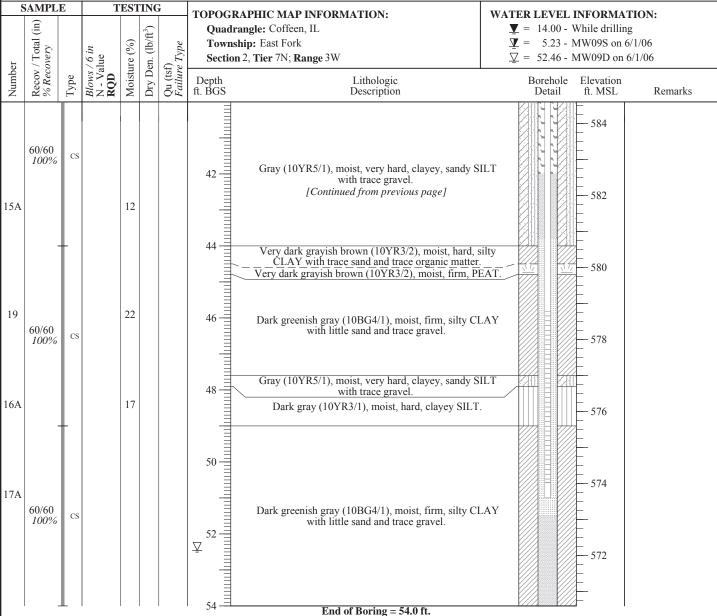
BOREHOLE ID: SB-09 Well ID: MW9D

 Surface Elev:
 625 ft. MSL

 Completion:
 54 ft. BGS

 Station:
 879,679.7N

 2,515,666.3E



NOTE(S): MW09D installed in SB-09.

CME-1050 had 280# hammer for SPT.

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A

DATES: Start: 5/3/2006

Finish: 5/2/2006

Finish: 5/3/2006 **WEATHER:** Overcast, mild (mid-60's)

CONTRACTOR: Reynolds Drilling Corp. **Rig mfg/model:** CME-1050 ATV Rig **Drilling Method:** 4¼" HSA (blind drill)

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Helper: S. McCartney Eng/Geo: R. Hasenyager **HANSON**

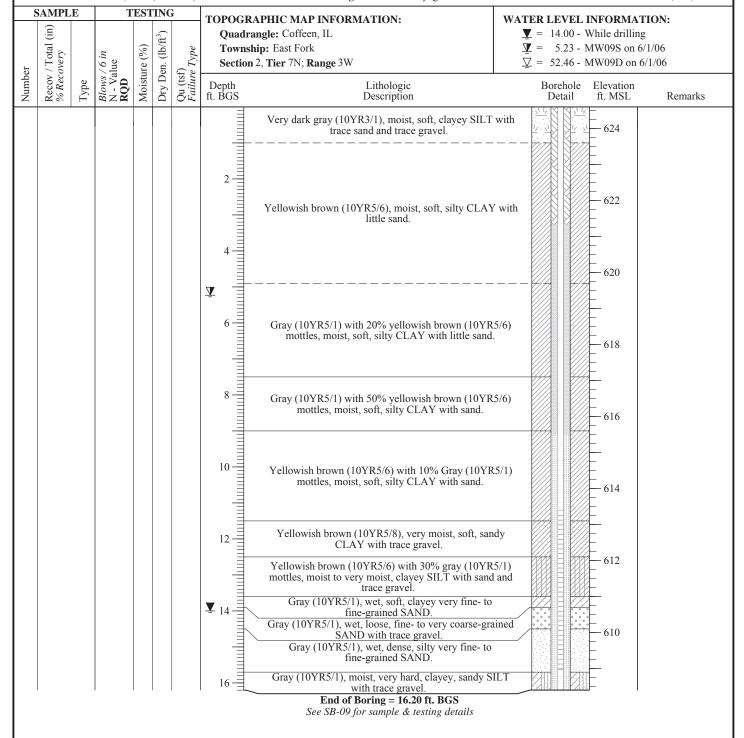
BOREHOLE ID: SB-09a **Well ID:** MW9S

 Surface Elev:
 625 ft. MSL

 Completion:
 16 ft. BGS

 Station:
 879,684.9N

 2,515,666.2E



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A DATES: Start: 5/3/2006 Finish: 5/3/2006

WEATHER: Overcast, mild (mid-60's)

CONTRACTOR: Reynolds Drilling Corp. **Rig mfg/model:** CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel

Helper: S. McCartney **Eng/Geo:** R. Hasenyager

HANSON

BOREHOLE ID: SB-09 **Well ID:** MW9D

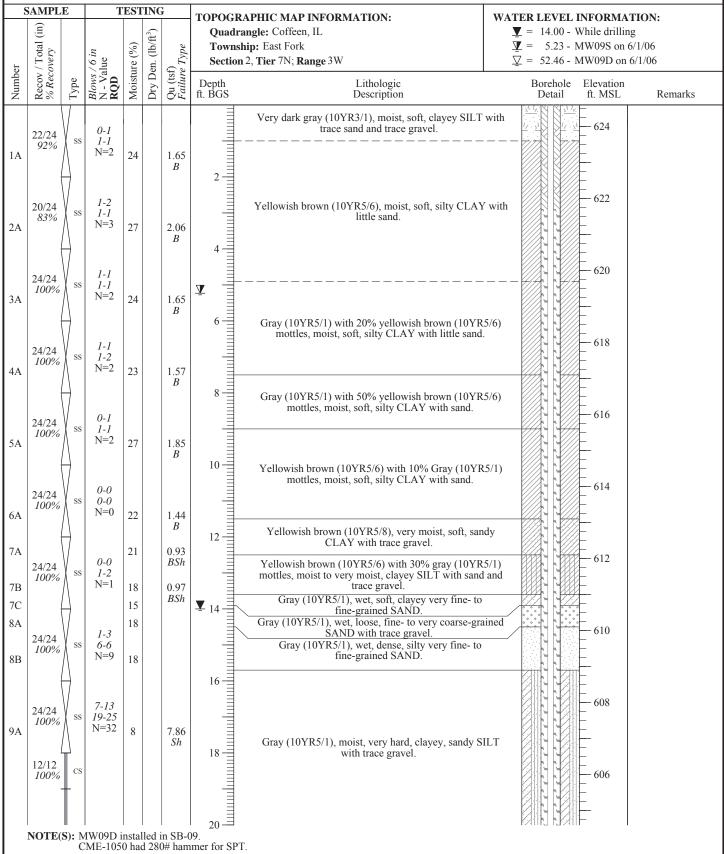
 Surface Elev:
 625 ft. MSL

 Completion:
 54 ft. BGS

 Station:
 879,679.7N

 2,515,666.3E

Page 1 of 3



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

SAMPLE

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DATES: Start: 5/3/2006 Finish: 5/3/2006

WEATHER: Overcast, mild (mid-60's)

TESTING

CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel

Helper: S. McCartney Eng/Geo: R. Hasenyager

2,515,666.3E

HANSON

625 ft. MSL

54 ft. BGS

879,679.7N

BOREHOLE ID: SB-09

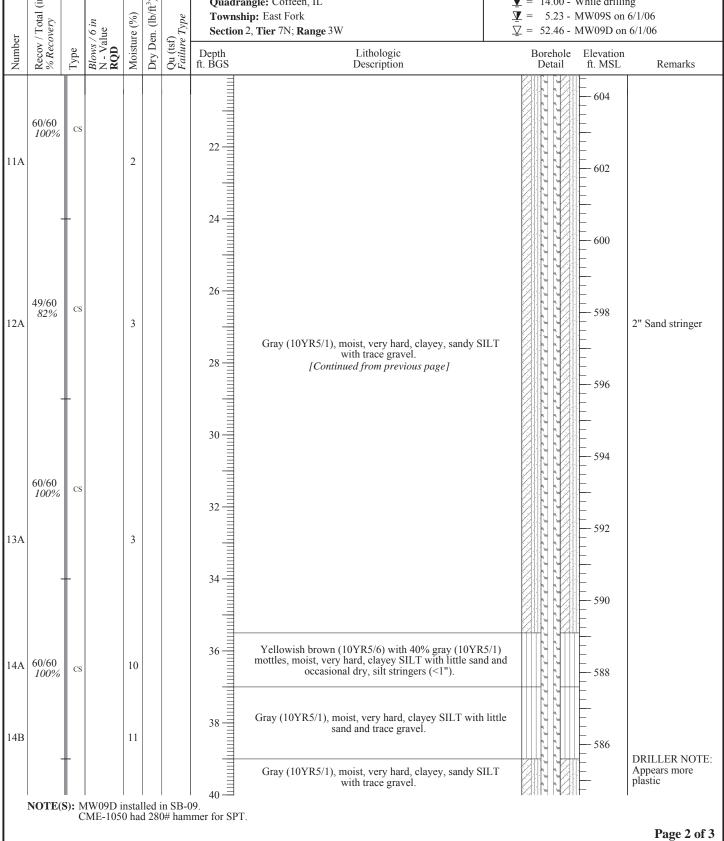
Surface Elev:

Completion:

Station:

Well ID: MW9D

TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: Quadrangle: Coffeen, IL $\mathbf{Y} = 14.00$ - While drilling Township: East Fork $\nabla = 5.23 - MW09S \text{ on } 6/1/06$ Section 2, Tier 7N; Range 3W



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A **DATES: Start:** 5/3/2006

Finish: 5/3/2006 WEATHER: Overcast, mild (mid-60's) **CONTRACTOR:** Reynolds Drilling Corp. **Rig mfg/model:** CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager



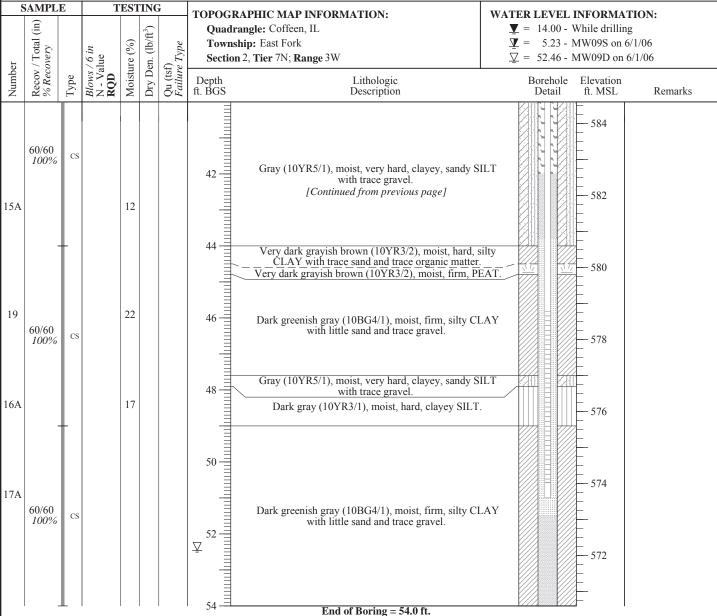
BOREHOLE ID: SB-09 Well ID: MW9D

 Surface Elev:
 625 ft. MSL

 Completion:
 54 ft. BGS

 Station:
 879,679.7N

 2,515,666.3E



NOTE(S): MW09D installed in SB-09.

CME-1050 had 280# hammer for SPT.

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A **DATES: Start:** 5/1/2006

Finish: 5/1/2006 WEATHER: Overcast, mild (mid-60's) CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

Helper: S. McCartney

FIELD STAFF: Driller: K. Doetzel

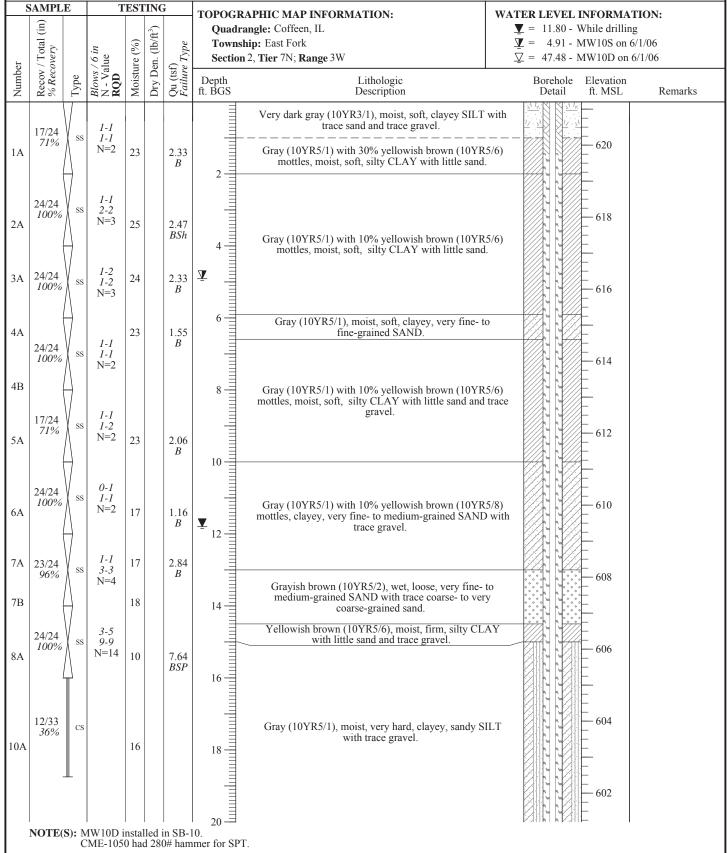
Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: SB-10 Well ID: MW10D

Surface Elev: 621 ft. MSL 49 ft. BGS **Completion:** Station: 878,245.1N 2,515,914.0E

Page 1 of 3



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A **DATES: Start:** 5/1/2006

Finish: 5/1/2006
WEATHER: Overcast, mild (mid-60's)

CONTRACTOR: Reynolds Drilling Corp. **Rig mfg/model:** CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

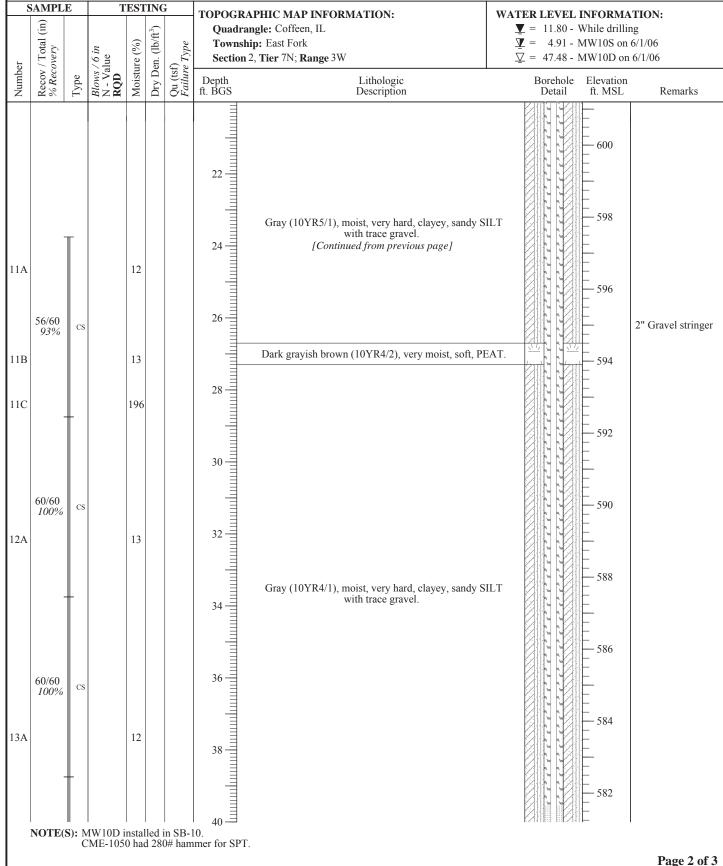
Eng/Geo: R. Hasenyager

BOREHOLE ID: SB-10

Station:

Well ID: MW10D Surface Elev: 621 ft. MSL Completion: 49 ft. BGS

> 878,245.1N 2,515,914.0E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility Location: Coffeen, Illinois

TESTING

Project: 05S3004A **DATES: Start:** 5/1/2006

SAMPLE

Finish: 5/1/2006 WEATHER: Overcast, mild (mid-60's) **CONTRACTOR:** Reynolds Drilling Corp. Rig mfg/model: CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

Eng/Geo: R. Hasenyager

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

TOPOGRAPHIC MAP INFORMATION:

WATER LEVEL INFORMATION:

HANSON

621 ft. MSL

49 ft. BGS

878,245.1N

2,515,914.0E

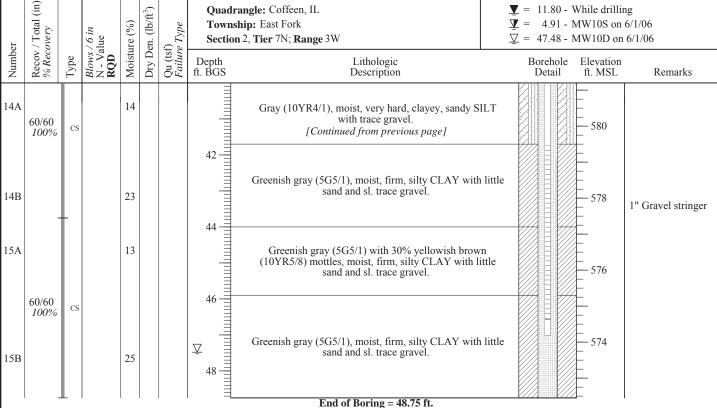
BOREHOLE ID: SB-10

Surface Elev:

Completion:

Station:

Well ID: MW10D



NOTE(S): MW10D installed in SB-10.

CME-1050 had 280# hammer for SPT.

Page 3 of 3

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A **DATES: Start:** 5/2/2006

Finish: 5/2/2006 **WEATHER:** Sunny, mild (mid-60's)

CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-1050 ATV Rig Drilling Method: 4¼" HSA (blind drill)

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney Eng/Geo: R. Hasenyager **HANSON**

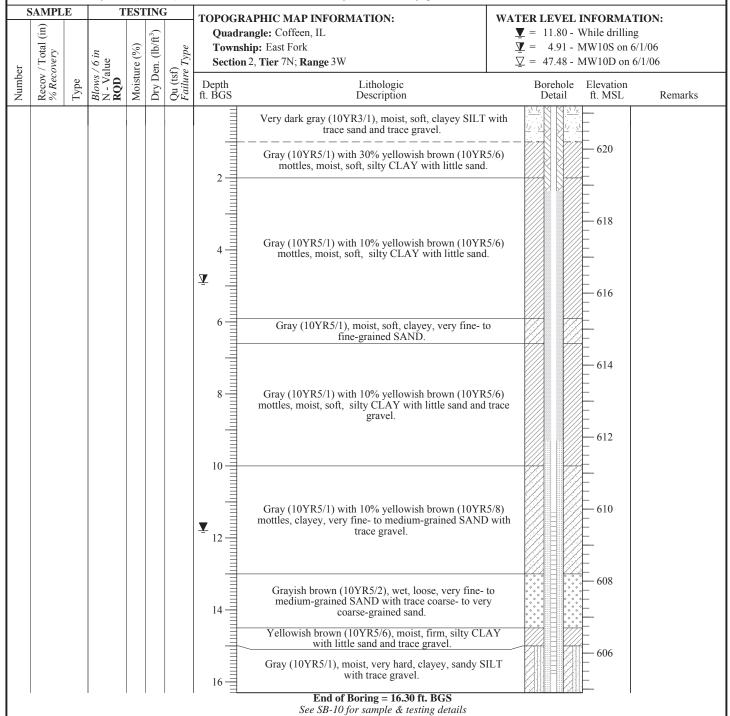
BOREHOLE ID: SB-10a **Well ID:** MW10S

 Surface Elev:
 621 ft. MSL

 Completion:
 16 ft. BGS

 Station:
 878,250.5N

 2,515,914.4E



NOTE(S): MW10S installed in blind-drilled borehole within 10 ft of SB-10.

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A **DATES: Start:** 5/1/2006

Finish: 5/1/2006 WEATHER: Overcast, mild (mid-60's) CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

Helper: S. McCartney

FIELD STAFF: Driller: K. Doetzel

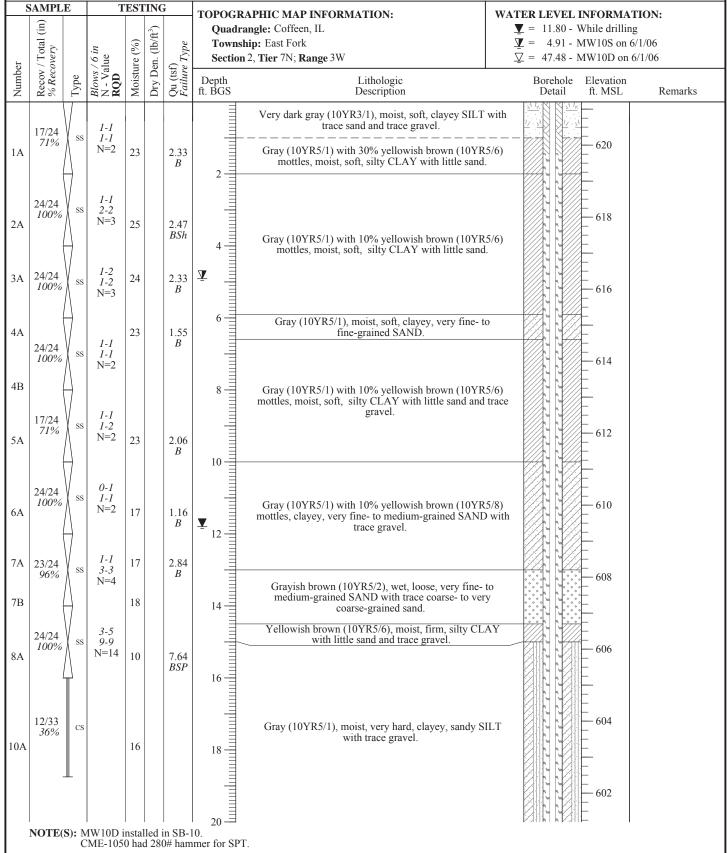
Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: SB-10 Well ID: MW10D

Surface Elev: 621 ft. MSL 49 ft. BGS **Completion:** Station: 878,245.1N 2,515,914.0E

Page 1 of 3



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A **DATES: Start:** 5/1/2006

Finish: 5/1/2006
WEATHER: Overcast, mild (mid-60's)

CONTRACTOR: Reynolds Drilling Corp. **Rig mfg/model:** CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

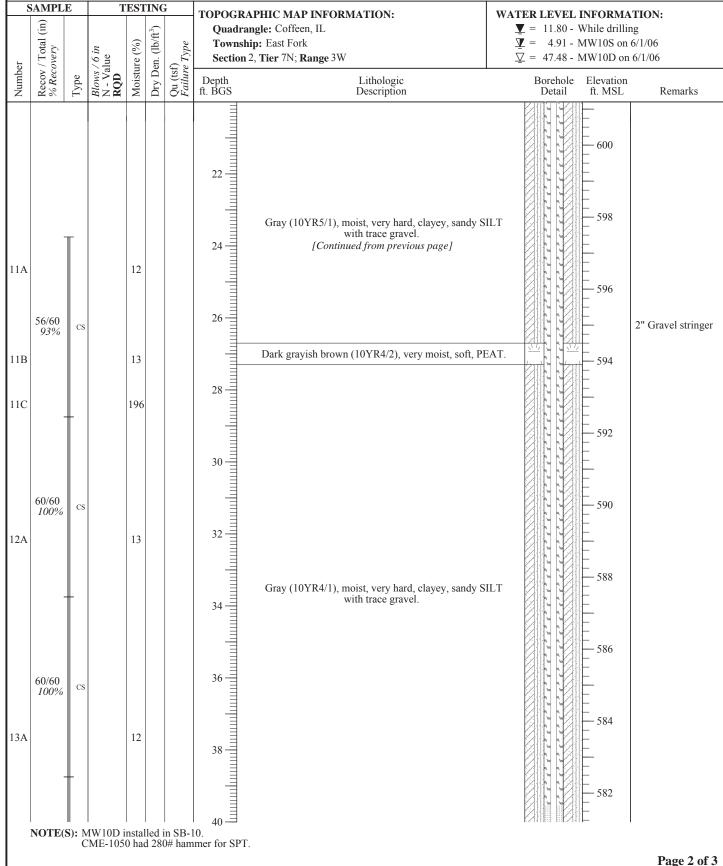
Eng/Geo: R. Hasenyager

BOREHOLE ID: SB-10

Station:

Well ID: MW10D Surface Elev: 621 ft. MSL Completion: 49 ft. BGS

> 878,245.1N 2,515,914.0E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility Location: Coffeen, Illinois

TESTING

Project: 05S3004A **DATES: Start:** 5/1/2006

SAMPLE

Finish: 5/1/2006 WEATHER: Overcast, mild (mid-60's) **CONTRACTOR:** Reynolds Drilling Corp. Rig mfg/model: CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

Eng/Geo: R. Hasenyager

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

TOPOGRAPHIC MAP INFORMATION:

WATER LEVEL INFORMATION:

HANSON

621 ft. MSL

49 ft. BGS

878,245.1N

2,515,914.0E

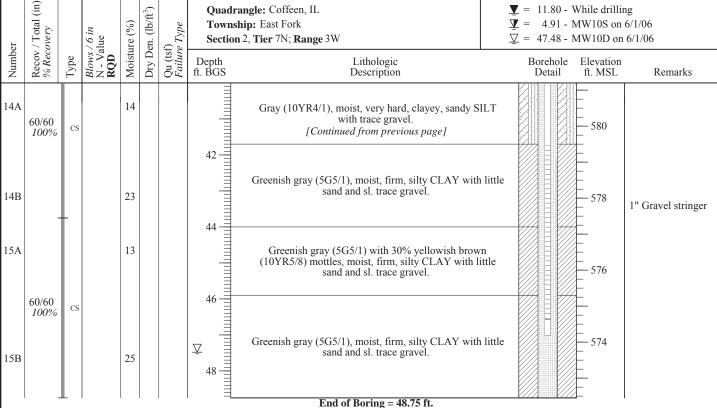
BOREHOLE ID: SB-10

Surface Elev:

Completion:

Station:

Well ID: MW10D



NOTE(S): MW10D installed in SB-10.

CME-1050 had 280# hammer for SPT.

Page 3 of 3

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A **DATES: Start: 4/27/2006** Finish: 4/28/2006

WEATHER: Partly cloudy, mild (mid-60's)

CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-850 Track Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

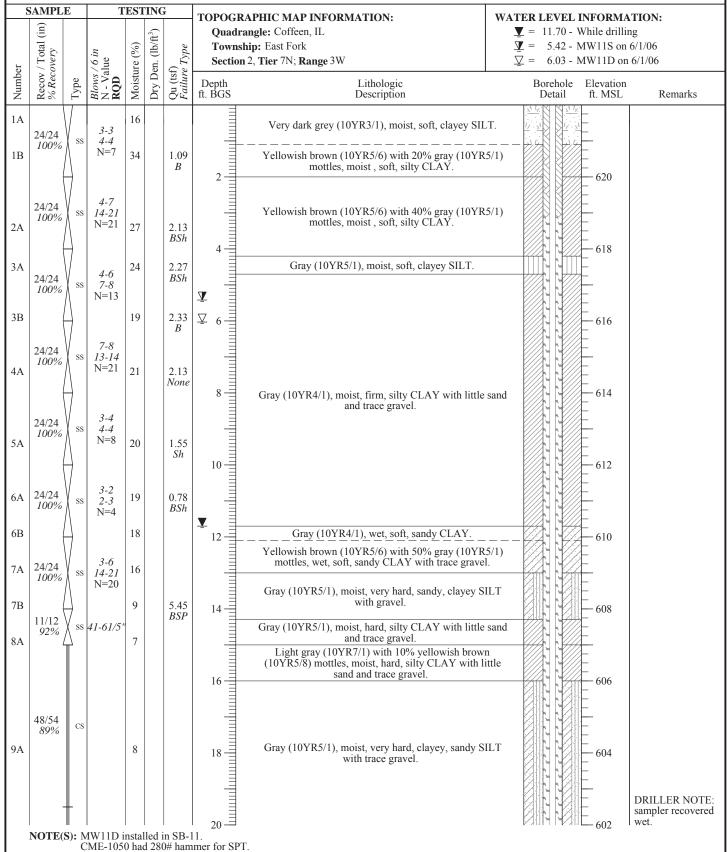
Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: SB-11 Well ID: MW11D

Surface Elev: 622 ft. MSL 36 ft. BGS **Completion:** Station: 876,749.6N 2,515,976.7E

Page 1 of 2



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois
Project: 05S3004A

DATES: Start: 4/27/2006

Finish: 4/28/2006 **WEATHER:** Partly cloudy, mild (mid-60's) **CONTRACTOR:** Reynolds Drilling Corp. **Rig mfg/model:** CME-850 Track Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager

HANSON

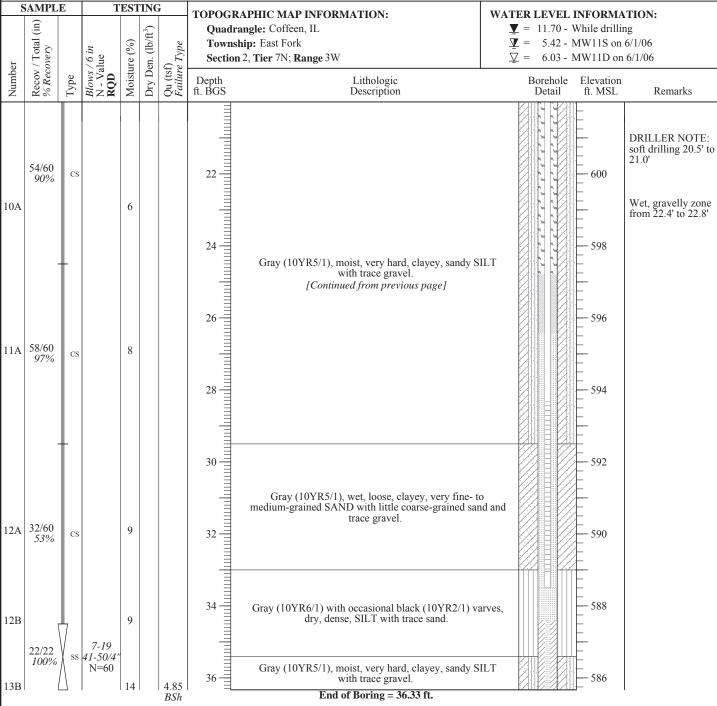
BOREHOLE ID: SB-11 Well ID: MW11D

 Surface Elev:
 622 ft. MSL

 Completion:
 36 ft. BGS

 Station:
 876,749.6N

 2,515,976.7E



NOTE(S): MW11D installed in SB-11.

CME-1050 had 280# hammer for SPT.

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A DATES: Start: 4/28/2006

DATES: Start: 4/28/2006 Finish: 4/28/2006

WEATHER: Partly cloudy, mild (mid-60's)

CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-850 Track Rig Drilling Method: 4¹/₄" HSA (blind drill)

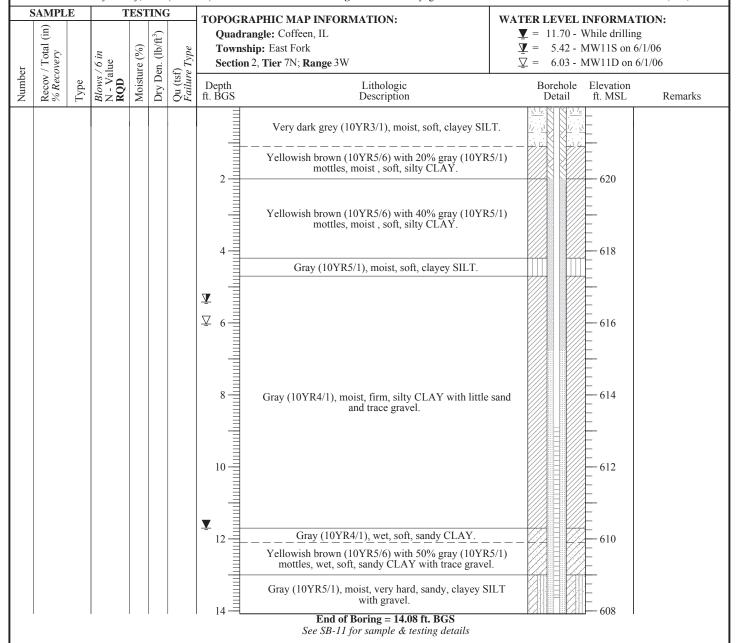
FIELD STAFF: Driller: K. Doetzel
Helper: S. McCartney
Eng/Geo: R. Hasenyager

HANSON
BOREHOLE ID: SB-11a

Station:

Well ID: MW11S
Surface Elev: 622 ft. MSL
Completion: 14 ft. BGS

876,749.4N 2,515,971.2E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A **DATES: Start: 4/27/2006** Finish: 4/28/2006

WEATHER: Partly cloudy, mild (mid-60's)

CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-850 Track Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

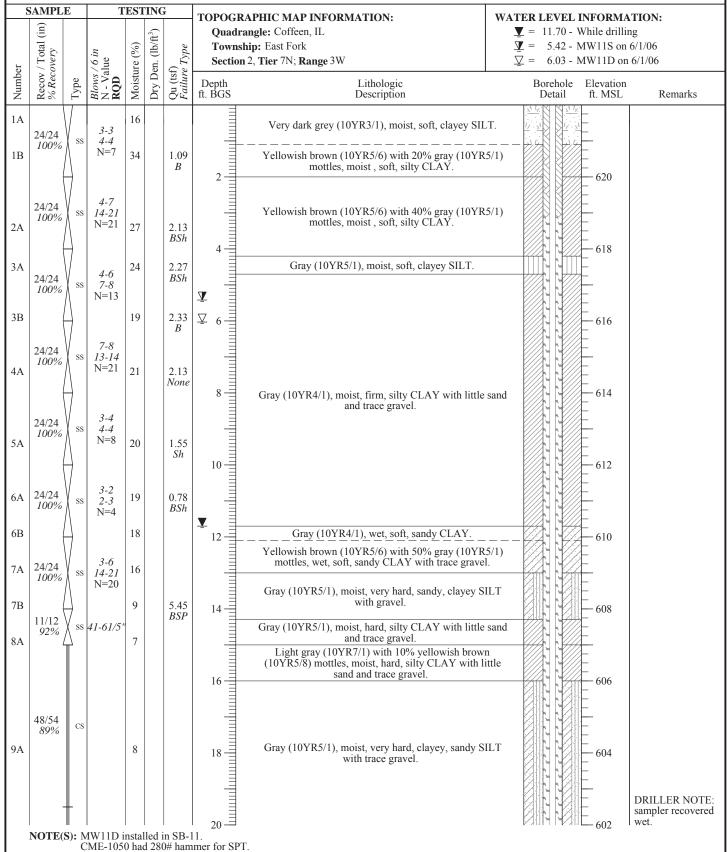
Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: SB-11 Well ID: MW11D

Surface Elev: 622 ft. MSL 36 ft. BGS **Completion:** Station: 876,749.6N 2,515,976.7E

Page 1 of 2



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois
Project: 05S3004A

DATES: Start: 4/27/2006

Finish: 4/28/2006 **WEATHER:** Partly cloudy, mild (mid-60's) **CONTRACTOR:** Reynolds Drilling Corp. **Rig mfg/model:** CME-850 Track Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager

HANSON

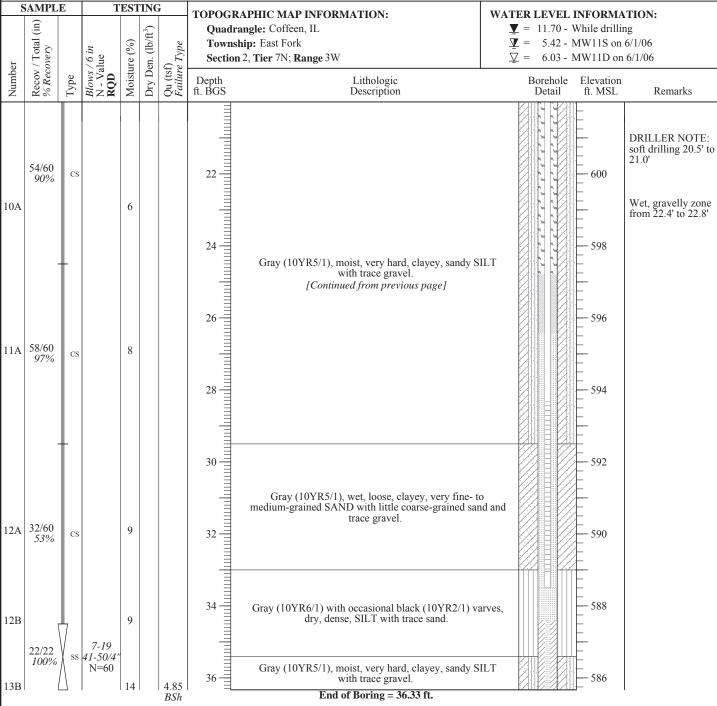
BOREHOLE ID: SB-11 Well ID: MW11D

 Surface Elev:
 622 ft. MSL

 Completion:
 36 ft. BGS

 Station:
 876,749.6N

 2,515,976.7E



NOTE(S): MW11D installed in SB-11.

CME-1050 had 280# hammer for SPT.

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 5/10/2006 **Finish:** 5/10/2006

WEATHER: Foggy to partly sunny, mild (hi-60's)

CONTRACTOR: Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

HANSON

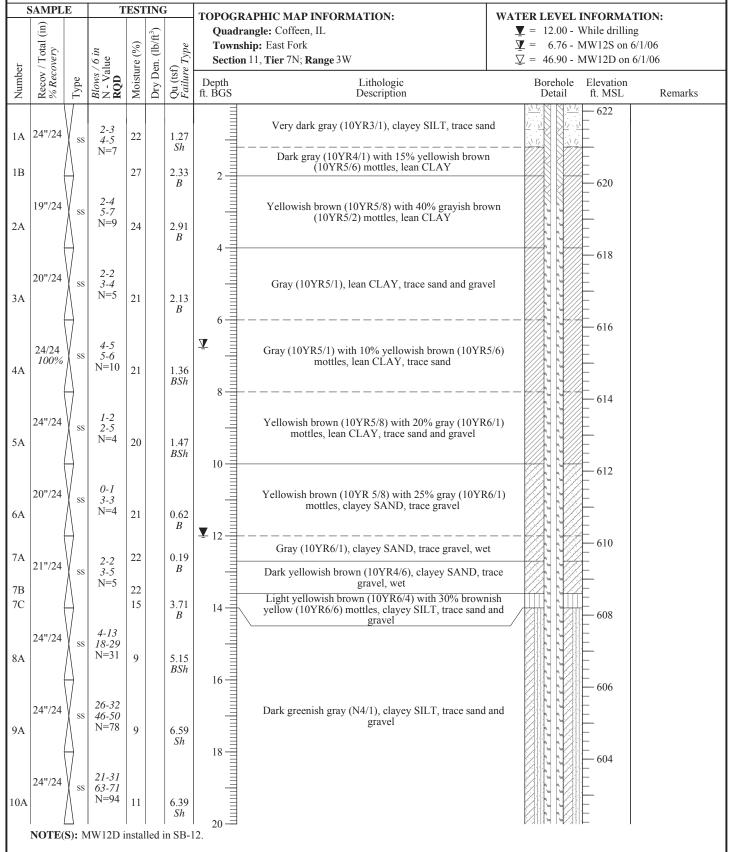
BOREHOLE ID: SB-12 Well ID: MW12D

 Surface Elev:
 622 ft. MSL

 Completion:
 50 ft. BGS

 Station:
 875,515.1N

 2,515,900.6E



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 5/10/2006 **Finish:** 5/10/2006

Finish: 5/10/2006 **WEATHER:** Foggy to partly sunny, mild (hi-60's) **CONTRACTOR:** Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager



BOREHOLE ID: SB-12 **Well ID:** MW12D

 Surface Elev:
 622 ft. MSL

 Completion:
 50 ft. BGS

 Station:
 875,515.1N

 2,515,900.6E

Page 2 of 3

| Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) Qu (tsf) Failusa Tuna | Quadra | APHIC MAP INFORMATION: ingle: Coffeen, IL ingl: East Fork 11, Tier 7N; Range 3W Lithologic Description | WATER LEVEL INFORM | rilling S on 6/1/06 O on 6/1/06 |
|----------------------------------|--------------|---|------------------|---|---|---------------------------------------|
| Blows N - Vs RQD | Moist | Dry D Qu (ts | Depth ft. BGS | Lithologic | Borehole Eleva | tion |
| | | | | Description | Detail ft. M | SL Remarks |
| 5 | 6 | | 22 — | Dark greenish gray (N4/1), clayey SILT, trace sand a gravel [Continued from previous page] | | |
| 5 | 7 | | 26 | | | |
| 5 | 12 | | 32 | Dark greenish gray (N4/1), sandy SILT, trace grav | 590 | |
| 5 | 16 | | 36 | Very dark gray (N3/1), clayey SILT, trace sand and g | ravel - 586 | ; |
| S | | 7 | 7 | 7 30 32 33 34 34 36 38 38 38 38 38 | Dark greenish gray (N4/1), sandy SILT, trace grav 32 34 Very dark gray (N3/1), clayey SILT, trace sand and g | 28 |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A **DATES: Start:** 5/10/2006

Finish: 5/10/2006

WEATHER: Foggy to partly sunny, mild (hi-60's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig

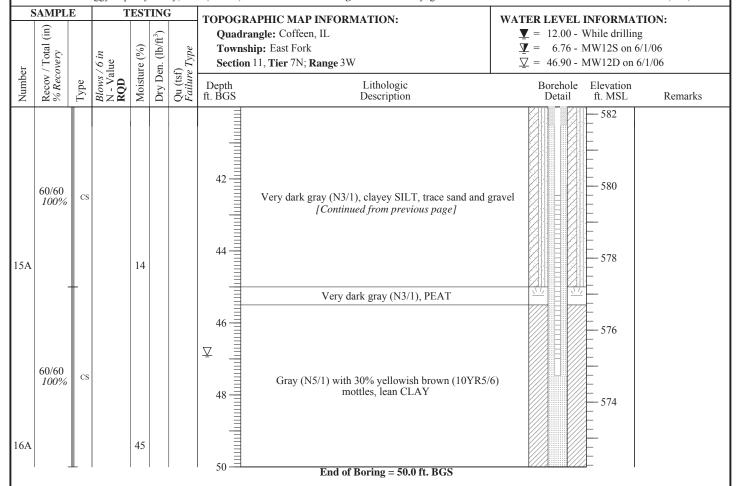
Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

BOREHOLE ID: SB-12 Well ID: MW12D

Surface Elev: 622 ft. MSL **Completion:** 50 ft. BGS **Station:** 875,515.1N 2,515,900.6E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility Location: Coffeen, Illinois

Project: 05S3004A **DATES: Start:** 5/10/2006

Finish: 5/10/2006

WEATHER: Foggy to partly sunny, mild (hi-60's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig **Drilling Method:** 31/4" HSA (blind drill)

FIELD STAFF: Driller: B. Williamson

Eng/Geo: R. Hasenyager

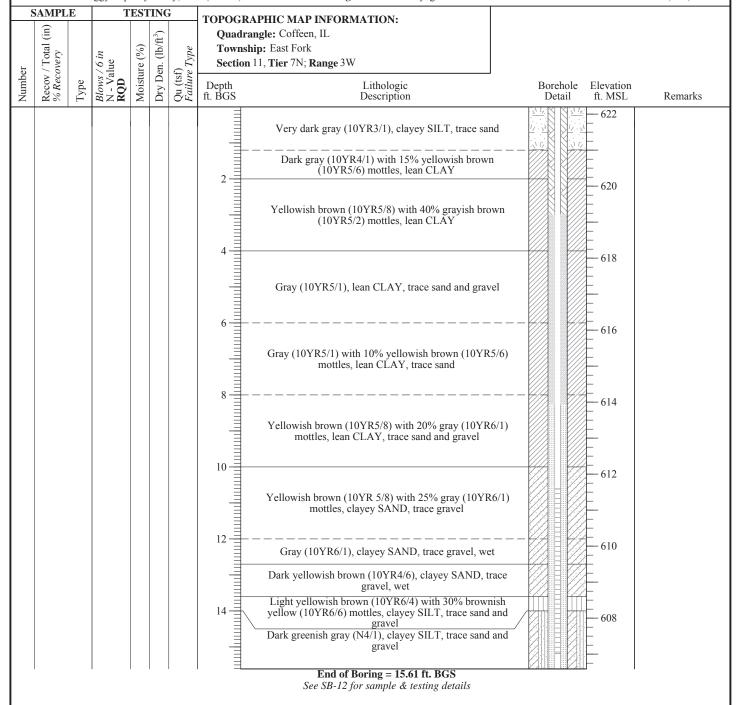
Helper: R. Keedy

Well ID: MW12S **Surface Elev:** 622 ft. MSL 16 ft. BGS **Completion:**

BOREHOLE ID: SB-12a

Station:

875,520.1N 2,515,900.5E



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 5/10/2006 **Finish:** 5/10/2006

WEATHER: Foggy to partly sunny, mild (hi-60's)

CONTRACTOR: Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

HANSON

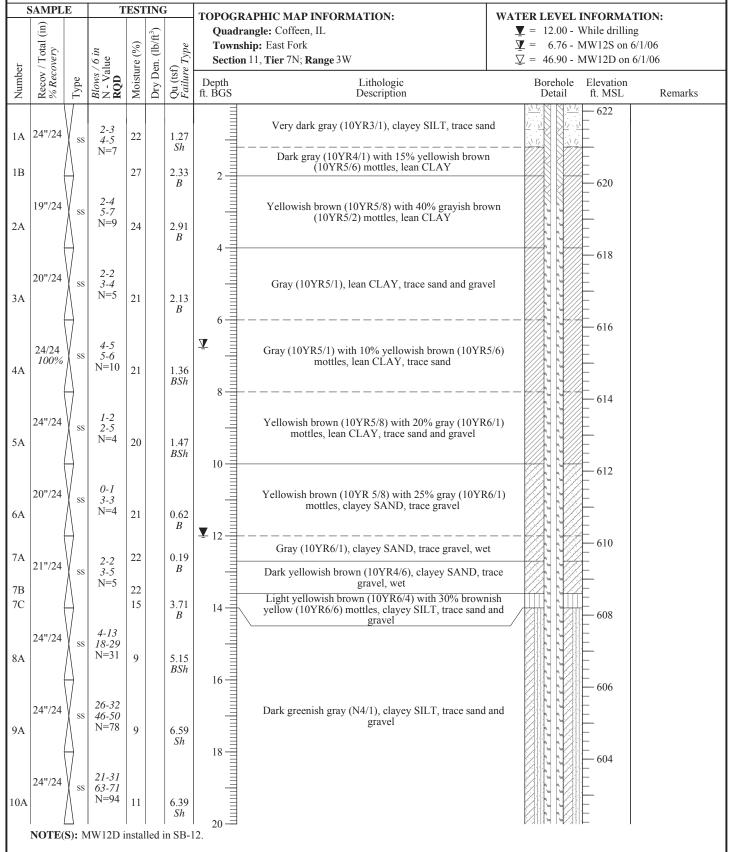
BOREHOLE ID: SB-12 Well ID: MW12D

 Surface Elev:
 622 ft. MSL

 Completion:
 50 ft. BGS

 Station:
 875,515.1N

 2,515,900.6E



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 5/10/2006 **Finish:** 5/10/2006

Finish: 5/10/2006 **WEATHER:** Foggy to partly sunny, mild (hi-60's) **CONTRACTOR:** Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager



BOREHOLE ID: SB-12 **Well ID:** MW12D

 Surface Elev:
 622 ft. MSL

 Completion:
 50 ft. BGS

 Station:
 875,515.1N

 2,515,900.6E

Page 2 of 3

| Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) Qu (tsf) Failusa Tuna | Quadra | APHIC MAP INFORMATION: ingle: Coffeen, IL ingl: East Fork 11, Tier 7N; Range 3W Lithologic Description | WATER LEVEL INFORM | rilling S on 6/1/06 O on 6/1/06 |
|----------------------------------|--------------|---|------------------|---|---|---------------------------------------|
| Blows N - Vs RQD | Moist | Dry D Qu (ts | Depth ft. BGS | Lithologic | Borehole Eleva | tion |
| | | | | Description | Detail ft. M | SL Remarks |
| 5 | 6 | | 22 — | Dark greenish gray (N4/1), clayey SILT, trace sand a gravel [Continued from previous page] | | |
| 5 | 7 | | 26 | | | |
| 5 | 12 | | 32 | Dark greenish gray (N4/1), sandy SILT, trace grav | 590 | |
| 5 | 16 | | 36 | Very dark gray (N3/1), clayey SILT, trace sand and g | ravel - 586 | ; |
| S | | 7 | 7 | 7 30 32 33 34 34 36 38 38 38 38 38 | Dark greenish gray (N4/1), sandy SILT, trace grav 32 34 Very dark gray (N3/1), clayey SILT, trace sand and g | 28 |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A **DATES: Start:** 5/10/2006

Finish: 5/10/2006

WEATHER: Foggy to partly sunny, mild (hi-60's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig

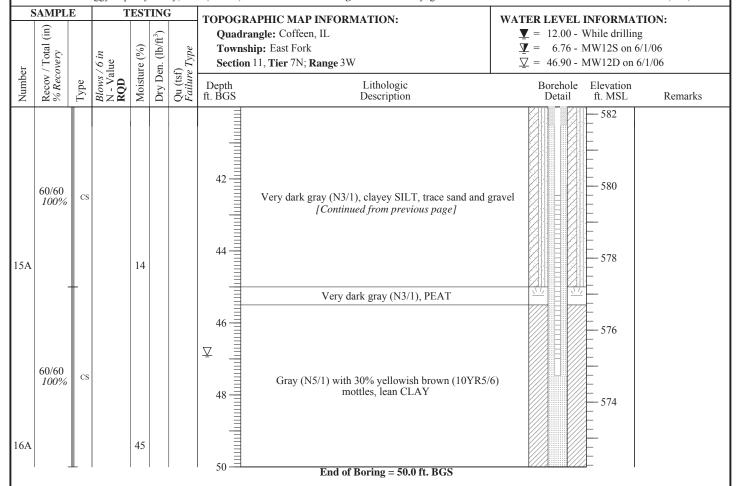
Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

BOREHOLE ID: SB-12 Well ID: MW12D

Surface Elev: 622 ft. MSL **Completion:** 50 ft. BGS **Station:** 875,515.1N 2,515,900.6E



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A **DATES:** Start: 5/9/2006

Finish: 5/9/2006
WEATHER: Overcast, mild (mid-60's)

CONTRACTOR: Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS sampler & 41/4" HSA overdrill

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Helper: R. Keedy Eng/Geo: R. Hasenyager **HANSON**

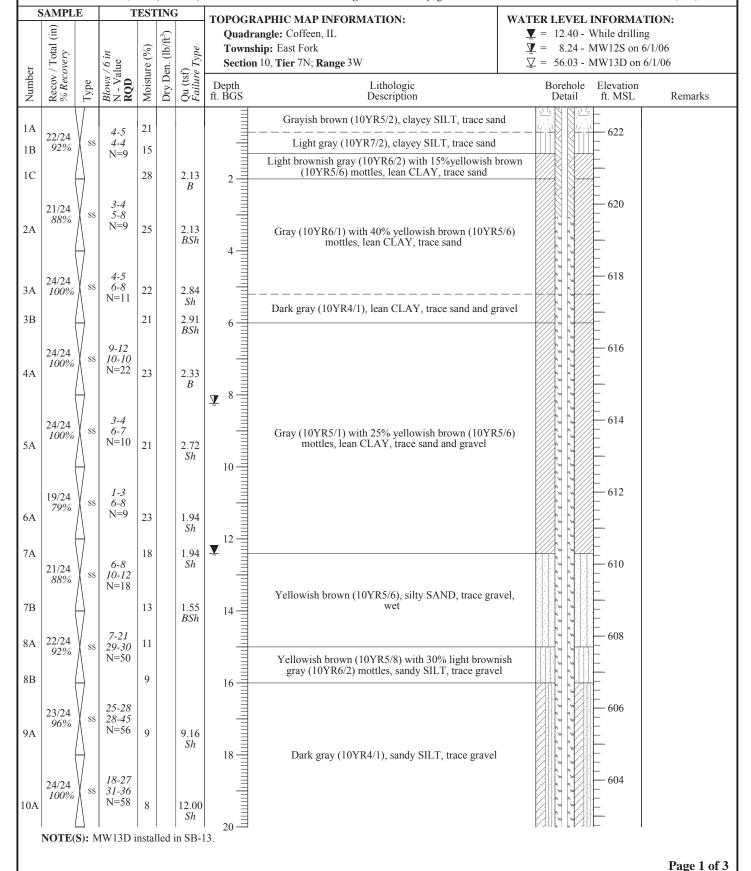
BOREHOLE ID: SB-13 Well ID: MW13D

 Surface Elev:
 623 ft. MSL

 Completion:
 55 ft. BGS

 Station:
 874,694.3N

 2,513,929.9E



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

TESTING

Location: Coffeen, Illinois
Project: 05S3004A

DATES: Start: 5/9/2006 Finish: 5/9/2006

SAMPLE

WEATHER: Overcast, mild (mid-60's)

CONTRACTOR: Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS sampler & 41/4" HSA overdrill

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

TOPOGRAPHIC MAP INFORMATION:

Eng/Geo: R. Hasenyager

WATER LEVEL INFORMATION:

BOREHOLE ID: SB-13

Surface Elev:

Completion:

Station:

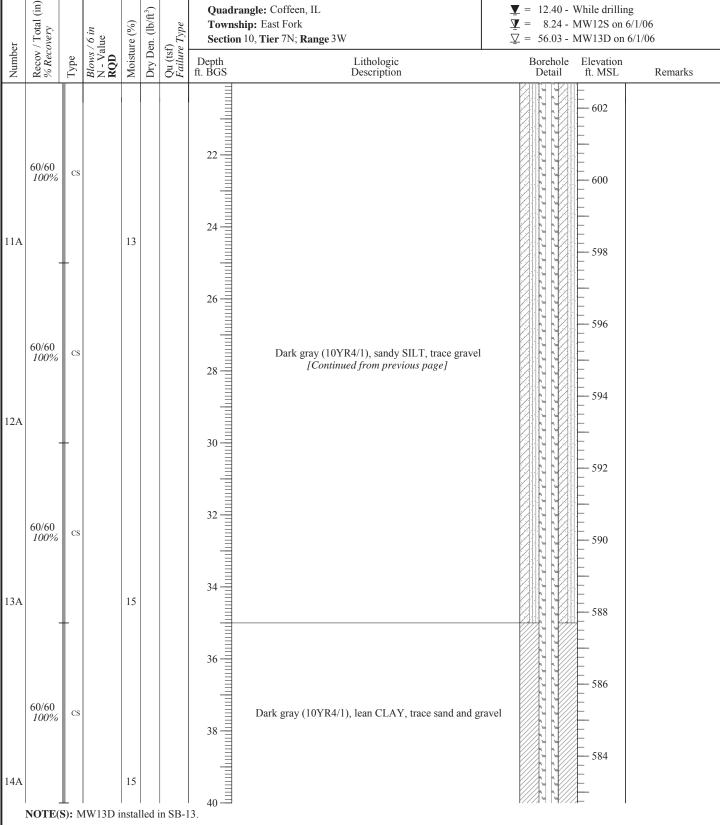
Well ID: MW13D

623 ft. MSL

55 ft. BGS

874,694.3N

2,513,929.9E



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 5/9/2006 Finish: 5/9/2006 WEATHER: Overcast, mild (mid-60's) **CONTRACTOR:** Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS sampler & 41/4" HSA overdrill

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

BOREHOLE ID: SB-13

Well ID: MW13D Surface Elev: 623 ft. MSL

Completion: 55 ft. BGS Station: 874,694.3N 2,513,929.9E

HANSON

| SAMI | DI F | | | ING | | | Eng Geo. R. Husenyager | | 2,313,727 | |
|-------------------|-------------|----------------------------------|----------------|-------------------|--------------------------|--------------------|--|---|--|---|
| Fotal (in) | covery | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadrai Townshi | PHIC MAP INFORMATION: ngle: Coffeen, IL p: East Fork 0, Tier 7N; Range 3W | $\underline{\underline{\mathbf{y}}} = 12.40 - \underline{\underline{\mathbf{y}}} = 8.24 - \underline{\mathbf{y}}$ | INFORMATION: While drilling MW12S on 6/1/06 MW13D on 6/1/06 | |
| Number Recov / 7 | Туре | Blows N - V RQD | Moist | Dry L | Qu (ts Failu | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL Remarks | ; |
| 60/6 | 50 9% cs | | | | | 42 | | | | |
| 15A | 50 | | 15 | | | 44 | Dark gray (10YR4/1), lean CLAY, trace sand and gray [Continued from previous page] | avel | 578 | |
| 100 16A | | | 15 | | | 48 | | | 574 | |
| 17A 17B 17C | 50 9% CS | | 14 20 14 | | | 52 | Gray (10YR4/1), silty, fine to medium SAND, we Gray (10YR4/1), sandy SILT Dark greenish gray (5GY4/1) with 25% yellowish bro (10YR5/6) mottles, lean CLAY | | 570 | |
| 17D | 1 | | 22 | | | | End of Boring = 55.0 ft. BGS | | 568 | |

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A **DATES: Start:** 5/9/2006

Finish: 5/9/2006
WEATHER: Overcast, mild (mid-60's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 31/4" HSA (blind drill)

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

HANSON

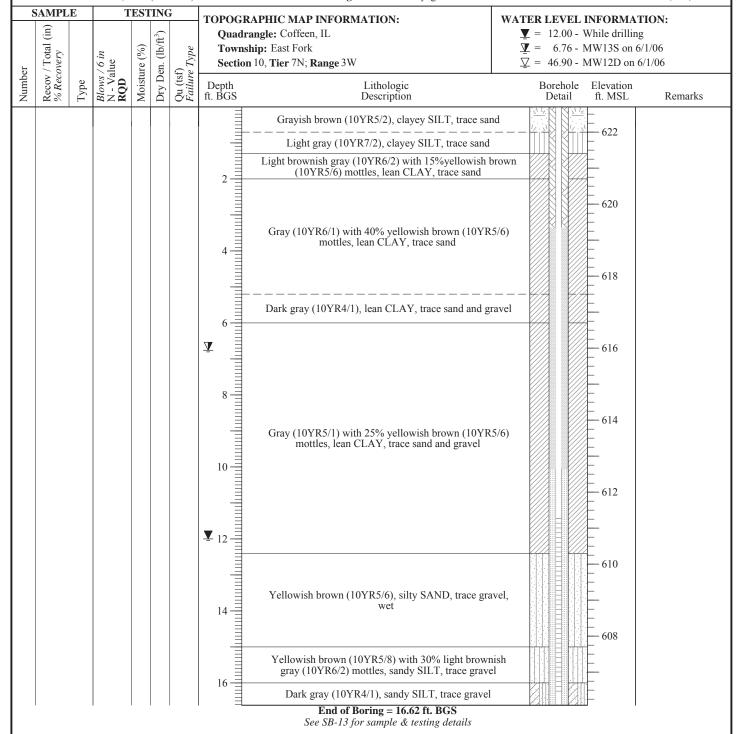
BOREHOLE ID: SB-13a **Well ID:** MW13S

 Surface Elev:
 623 ft. MSL

 Completion:
 17 ft. BGS

 Station:
 874,695.7N

 2,513,925.3E



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A **DATES:** Start: 5/9/2006

Finish: 5/9/2006
WEATHER: Overcast, mild (mid-60's)

CONTRACTOR: Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS sampler & 41/4" HSA overdrill

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Helper: R. Keedy Eng/Geo: R. Hasenyager **HANSON**

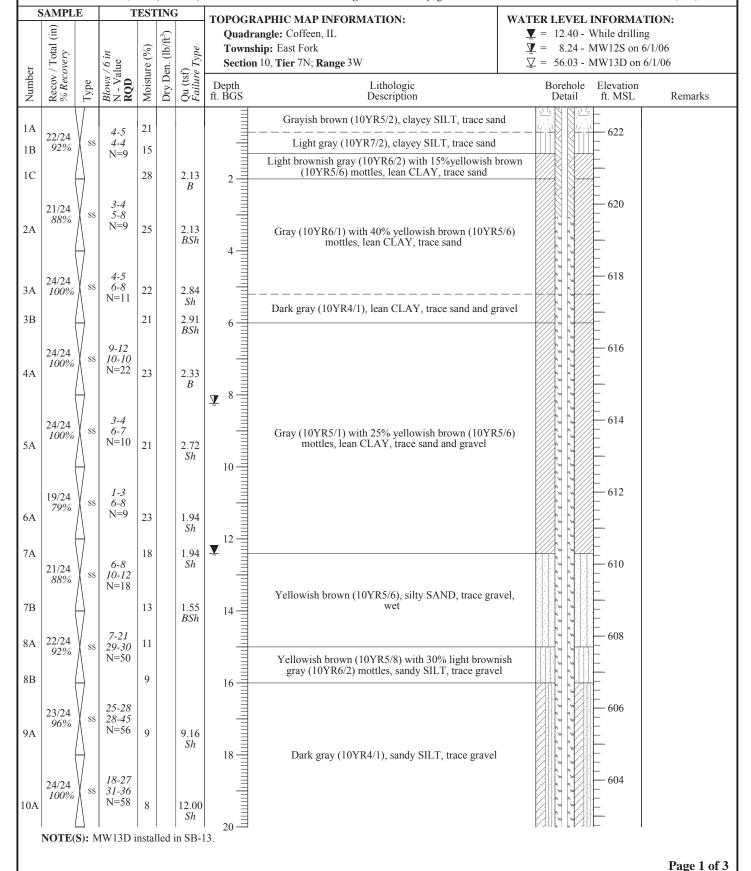
BOREHOLE ID: SB-13 Well ID: MW13D

 Surface Elev:
 623 ft. MSL

 Completion:
 55 ft. BGS

 Station:
 874,694.3N

 2,513,929.9E



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

TESTING

Location: Coffeen, Illinois
Project: 05S3004A

DATES: Start: 5/9/2006 Finish: 5/9/2006

SAMPLE

WEATHER: Overcast, mild (mid-60's)

CONTRACTOR: Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS sampler & 41/4" HSA overdrill

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

TOPOGRAPHIC MAP INFORMATION:

Eng/Geo: R. Hasenyager

WATER LEVEL INFORMATION:

BOREHOLE ID: SB-13

Surface Elev:

Completion:

Station:

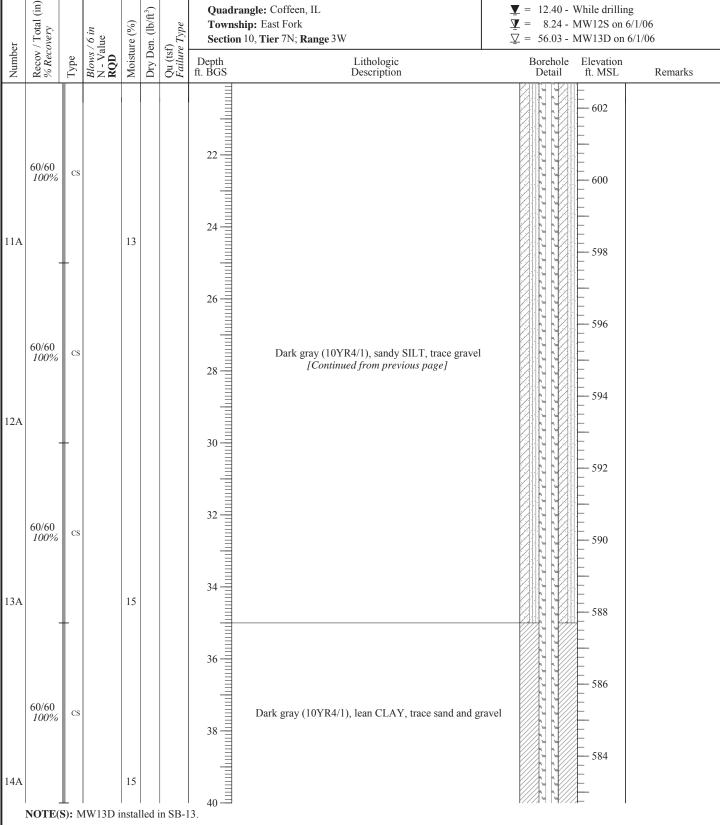
Well ID: MW13D

623 ft. MSL

55 ft. BGS

874,694.3N

2,513,929.9E



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 5/9/2006 Finish: 5/9/2006 WEATHER: Overcast, mild (mid-60's) **CONTRACTOR:** Testing Service Corporation **Rig mfg/model:** CME-650 Track Rig

Drilling Method: 31/4" HSA w/SS sampler & 41/4" HSA overdrill

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

BOREHOLE ID: SB-13

Well ID: MW13D Surface Elev: 623 ft. MSL

Completion: 55 ft. BGS Station: 874,694.3N 2,513,929.9E

HANSON

| SAMI | DI F | | | ING | | | Eng Geo. R. Husenyager | | 2,313,727 | |
|-------------------|-------------|----------------------------------|----------------|-------------------|--------------------------|--------------------|--|---|--|---|
| Fotal (in) | covery | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadrai Townshi | PHIC MAP INFORMATION: ngle: Coffeen, IL p: East Fork 0, Tier 7N; Range 3W | $\underline{\underline{\mathbf{y}}} = 12.40 - \underline{\underline{\mathbf{y}}} = 8.24 - \underline{\mathbf{y}}$ | INFORMATION: While drilling MW12S on 6/1/06 MW13D on 6/1/06 | |
| Number Recov / 7 | Туре | Blows N - V RQD | Moist | Dry L | Qu (ts Failu | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL Remarks | ; |
| 60/6 | 50 9% cs | | | | | 42 | | | | |
| 15A | 50 | | 15 | | | 44 | Dark gray (10YR4/1), lean CLAY, trace sand and gray [Continued from previous page] | avel | 578 | |
| 100 16A | | | 15 | | | 48 | | | 574 | |
| 17A 17B 17C | 50 9% CS | | 14 20 14 | | | 52 | Gray (10YR4/1), silty, fine to medium SAND, we Gray (10YR4/1), sandy SILT Dark greenish gray (5GY4/1) with 25% yellowish bro (10YR5/6) mottles, lean CLAY | | 570 | |
| 17D | 1 | | 22 | | | | End of Boring = 55.0 ft. BGS | | 568 | |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility Location: Coffeen, Illinois

Project: 05S3004A **DATES: Start:** 5/2/2006

Finish: 5/2/2006 WEATHER: Sunny, mild (mid-60's) **CONTRACTOR:** Testing Service Corporation Rig mfg/model: CME-650 Track Rig **Drilling Method:** 41/4" HSA (blind drill)

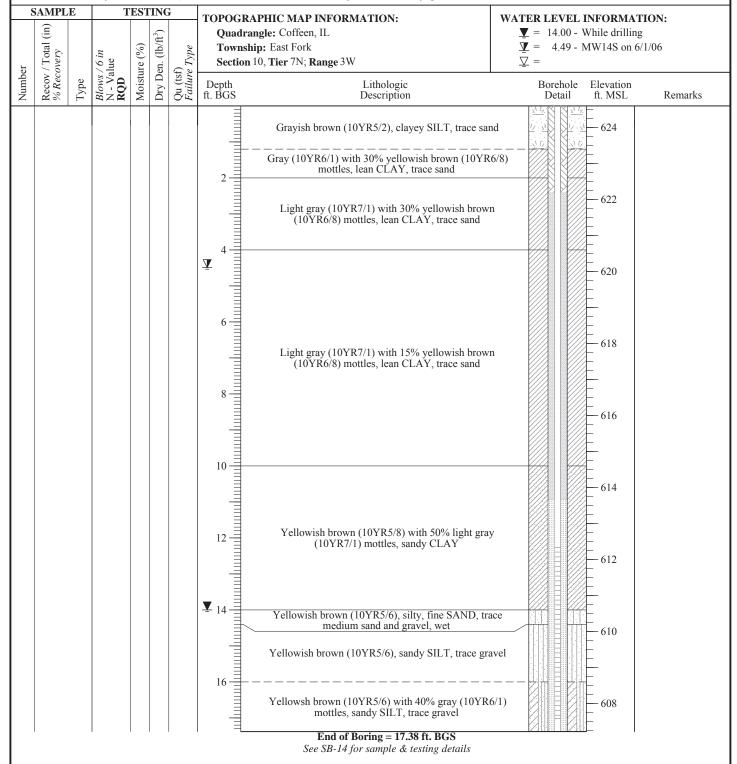
FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager



BOREHOLE ID: Sb-14a Well ID: MW14S

Surface Elev: 625 ft. MSL 17 ft. BGS **Completion: Station:** 875,737.8N 2,514,125.9E



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A DATES: Start: 5/1/2006 Finish: 5/2/2006

Finish: 5/2/2006
WEATHER: Sunny, mild (mid-60's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 3¹/₄" HSA w/SS sampler

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy Eng/Geo: R. Hasenyager **HANSON**

BOREHOLE ID: SB-14 **Well ID:** n/a

 Surface Elev:
 625 ft. MSL

 Completion:
 60 ft. BGS

 Station:
 875,740.0N

 2,514,130.0E

| i. | SAMPLE TESTING | | | | | r | TOPOGRAPHIC MAP INFORMATION: W. | | | WATER LEVEL INFORMATION: | | | | | |
|------------|----------------------------------|----------|---|--------------|-------------------|--------------------------|--|--|--------|--------------------------|----|--------------------------------|---------|--|--|
| nei | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Towns | angle: Coffeen, IL hip: East Fork 10, Tier 7N; Range 3W | | 4.49 | | While drilling AW14S on 6/1 | /06 | | |
| Number | Reco % Re | Type | Blow. N - V RQD | Mois | Dry I | Qu (t Failu | Depth ft. BGS | Lithologic Description | I | Boreho Detai | | Elevation ft. MSL | Remarks | | |
| A | 23/24 96% | ss | 2-3 2-3 | 16 | | | | Grayish brown (10YR5/2), clayey SILT, trace sar | id (2) | | 70 | 624 | | | |
| В | (| <u> </u> | N=5 | 26 | | 2.33 B | 2 = | Gray (10YR6/1) with 30% yellowish brown (10YR mottles, lean CLAY, trace sand | 6/8) | | | | | | |
| Α | 24/24 100% | ss | 3-4 5-7 N=9 | 23 | | 3.10 B | 4 | Light gray (10YR7/1) with 30% yellowish brown (10YR6/8) mottles, lean CLAY, trace sand | ı | | | 622 | | | |
| A | 23/24 96% | ss | 3-3 5-5 N=8 | 19 | | 2.33 B | Ā | | | | | | | | |
| A | 24/24 100% | ss | 5-6 5-7 N=11 | 23 | | 2.68 BSh | 8 10 10 10 10 10 10 10 1 | Light gray (10YR7/1) with 15% yellowish brown (10YR6/8) mottles, lean CLAY, trace sand | 1 | | | 618 | | | |
| iΑ | 24/24 100% | ss | 2-2 3-4 N=5 | 26 | | 1.83 B | 10 | | | | | 616 | | | |
| δA | 19/24 79% | ss | 2-2 3-5 N=5 | 17 | | 2.18 B | 12 | Yellowish brown (10YR5/8) with 50% light gray (10YR7/1) mottles, sandy CLAY | | | | 614 | | | |
| 7A | 20/24 83% | ss | 2-3 3-3 N=6 | 22 | | 1.16 B | ¥ 14 | (10 110) 1) money, sandy CEIT | | | | 612 | | | |
| A | 24/24 100% | SS | 5-14 14-20 | 16 | | 1.36 B | 14 | Yellowish brown (10YR5/6), silty, fine SAND, tra medium sand and gravel, wet | | | | 610 | | | |
| В | 100/6 | <u> </u> | N=28 | 11 | | 5.77 BSh | 16 | Yellowish brown (10YR5/6), sandy SILT, trace gra | | | | | | | |
| PΑ | 12/24 50% | SS | 57-65 | 10 | | | 18 | Yellowsh brown (10YR5/6) with 40% gray (10YR6 mottles, sandy SILT, trace gravel | 5/1) | | | 608 | | | |
| 0 A | 24/24 100% | ss | 6-8 16-18 N=24 | 12 | | 5.04 BSh | 20 | Dark gray (10YR4/1), clayey SILT, trace sand and g | ravel | | | 606 | | | |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility Location: Coffeen, Illinois

Project: 05S3004A **DATES: Start:** 5/1/2006

Finish: 5/2/2006 WEATHER: Sunny, mild (mid-60's) **CONTRACTOR:** Testing Service Corporation Rig mfg/model: CME-650 Track Rig **Drilling Method:** 31/4" HSA w/SS sampler

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: SB-14 Well ID: n/a

625 ft. MSL **Surface Elev: Completion:** 60 ft. BGS **Station:** 875,740.0N 2,514,130.0E

| 5 | SAMPLE TESTING | | | | | ì | TOPOGRAPHIC MAP INFORMATION: V | | | WATER LEVEL INFORMATION: | | | | |
|----------|-------------------------------|------|---|--------------|-------------------|--------------------------|--------------------------------|--|---------|--------------------------|--------------------------------|---------|--|--|
| IMILIDOL | Recov / Total (in) % Recovery | 0 | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Townsh Section | ngle: Coffeen, IL ip: East Fork 10, Tier 7N; Range 3W | <u></u> | 4.49 - 1 | While drilling MW14S on 6/1 | 1/06 | | |
| | Recc %Re | Type | Blow N-N | Mois | Dry | Qu (Fail | Depth ft. BGS | Lithologic Description | | Borehole Detail | Elevation ft. MSL | Remarks | | |
| A | 24/24 100% | SS | 2-7 13-30 N=20 | 13 | | 9.70 B | 22 | | | | 604 | | | |
| A | 24/24 100% | SS | 26-40 36-40 N=76 | 9 | | 13.09 BSP | 24 | | | | 602 | | | |
| A | 24/24 100% | ss | 8-18 28-34 N=46 | 9 | | 8.73 <i>BSP</i> | 26 | | | | 600 | | | |
| Α | 22/24 92% | SS | 20-18 24-30 N=42 | 9 | | 7.42 BSP | 28 | Dark gray (10YR4/1), clayey SILT, trace sand and g [Continued from previous page] | ravel | | 598 | | | |
| δA | 19/24 79% | SS | 8-27 33-67 N=60 | 9 | | | 30 | Dark gray (10YR4/1), clayey SILT, trace sand and gray [Continued from previous page] 28 30 32 | | | 596 | | | |
| δA | 24/24 100% | ss | 8-25 27-33 N=52 | 10 | | 9.60 <i>BSh</i> | 32 | | | | 594 594 | | | |
| 7A | 20/24 83% | ss | 11-15 20-24 N=35 | 14 | | 6.80 B | 34 | | | | 592 | | | |
| 3A | 24/24 100% | ss | 3-4 7-9 N=11 | 16 | | 3.88 B | | | | | 590 | | | |
| θA | 24/24 100% | SS | 8-12 13-15 N=25 | 16 | | 6.18 <i>B</i> | 36 | Dark gray (N4/1), lean CLAY, trace sand and grav | vel | | 588 | | | |
|)A | 24/24 100% | ss | 3-7 10-13 N=17 | 14 | | 3.10 B | 40 | | | | 586 | | | |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility Location: Coffeen, Illinois

Project: 05S3004A **DATES: Start:** 5/1/2006 **Finish:** 5/2/2006

WEATHER: Sunny, mild (mid-60's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 31/4" HSA w/SS sampler

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: SB-14 Well ID: n/a

> 625 ft. MSL **Surface Elev: Completion:** 60 ft. BGS **Station:** 875,740.0N 2,514,130.0E

| 5 | SAMPL | E | Т | EST | ING | 1 | TODOCDA | DILIC MAD INFORMATION. | XX A TELE | D I EXTEL | INFORMAT | ION. |
|--------|----------------------------------|------|---|--------------|-------------------|--------------------------|--------------------|---|-----------|-----------------------|----------------------------|---------|
| er | Recov / Total (in) % Recovery | | /6 in alue | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadrar Townshi | PHIC MAP INFORMATION: ngle: Coffeen, IL p: East Fork 0, Tier 7N; Range 3W | . ▼ : | = 14.00 - = 4.49 - | While drilling MW14S on 6/ | |
| Number | Recov % Rec | Type | Blows / 6 in N - Value RQD | Moist | Dry D | Qu (ts Failur | Depth ft. BGS | Lithologic Description | | Borehole Detail | Elevation ft. MSL | Remarks |
| 21A | 23/24 96% | ss | 3-6 8-13 N=14 | 15 | | 4.80 B | 42 | | | | 584 | |
| 2A | 24/24 100% | ss | 13-15 16-18 N=31 | 14 | | 5.62 B | 44 — | Dark gray (N4/1), lean CLAY, trace sand and grav | vel | | 582 | |
| 3A | 24/24 100% | ss | 4-8 11-13 N=19 | 15 | | 4.65 B | 46 — | [Continued from previous page] | | | 580 | |
| 24A | 24/24 100% | ss | 18-18 20-20 N=38 | 15 | | 4.65 B | 48 | | · — — — | | 578 | |
| 25A | 24/24 100% | SS | 4-7 9-11 N=16 | 19 | | 2.13 BSh | 50 | Dark gray (N4/1), clayey SILT, trace sand and gra Gray (N4/1), wet, loose, fine- to medium-grained SA Dark gray (N4/1), clayey SILT, trace sand and gra | AND | | 576 | |
| 26A | 22/24 92% | ss | 3-5 6-8 N=11 | 22 | | 3.30 <i>BSh</i> | 52 | Greenish gray (5BG5/1), lean CLAY | VCI | | 574 | |
| 27A | 24/24 100% | ss | 3-5 5-7 N=10 | 25 | | 2.89 <i>BSh</i> | | Greenish gray (5BG5/1) with 15% yellowish brov (10YR5/6) mottles, lean CLAY | wn | | 572 | |
| 28A | 21/24 88% 0/24 0% | SS | 4-6 7-8 N=13 | 22 | | 3.71 <i>BSh</i> | 56 | Greenish gray (5BG5/1) with 25% yellowish brow (10YR5/6) mottles, lean CLAY | vn | | 570 | |
| 29A | 14/24 58% | ss | 0-0 0-0 N=0 | 22 | | 3.09 <i>BSh</i> | 58 | Greenish gray (5BG5/1) with 50% yellowish brow (10YR5/6) mottles, lean CLAY | wn | | 568 | |
| 30A | 22/24 92% | ss | 5-6 8-12 N=14 | 19 | | 4.46 <i>BSh</i> | 60 | Yellowish brown (10YR4/6) with 10% greenish gr (5BG5/1) mottles, lean CLAY End of Boring = 60.0 ft. BGS | ray | | 566 | |

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A **DATES: Start:** 4/24/2006

Finish: 4/25/2006 WEATHER: Overcast, cool (lo-50's) CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 41/4" HSA (blind drill)

FIELD STAFF: Driller: B. Williamson **Helper:** R. Keedy

Helper: R. Keedy Eng/Geo: R. Hasenyager **HANSON**

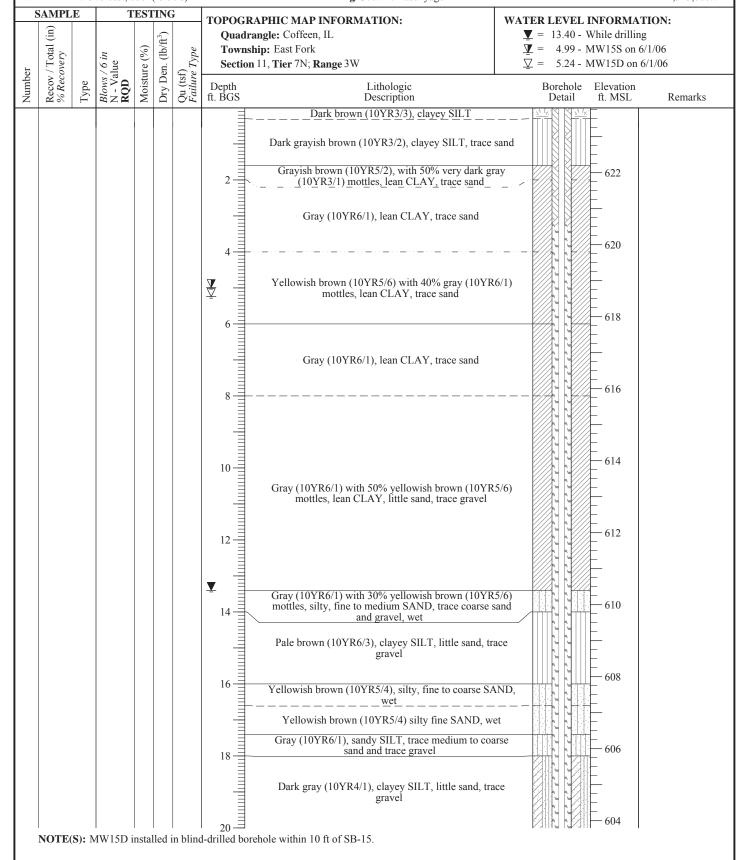
BOREHOLE ID: SB-15b **Well ID:** MW15D

 Surface Elev:
 624 ft. MSL

 Completion:
 39 ft. BGS

 Station:
 875,970.5N

 2,515,080.7E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility Location: Coffeen, Illinois

Project: 05S3004A **DATES: Start:** 4/24/2006

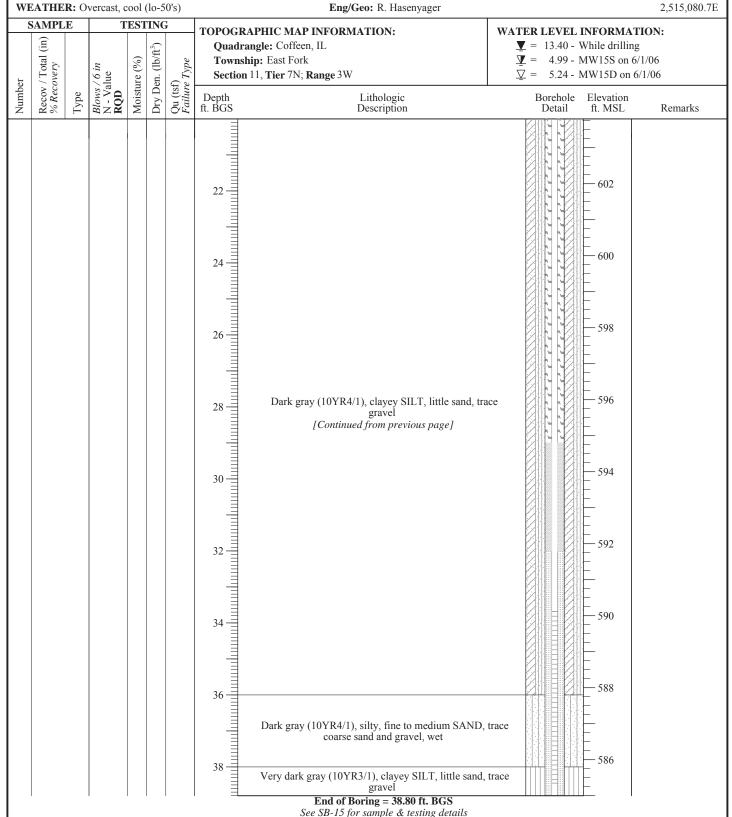
Finish: 4/25/2006 WEATHER: Overcast, cool (lo-50's) **CONTRACTOR:** Testing Service Corporation Rig mfg/model: CME-650 Track Rig **Drilling Method:** 41/4" HSA (blind drill)

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

HANSON

Well ID: MW15D **Surface Elev:** 624 ft. MSL **Completion:** 39 ft. BGS **Station:** 875,970.5N

BOREHOLE ID: SB-15b



NOTE(S): MW15D installed in blind-drilled borehole within 10 ft of SB-15.

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois
Project: 05S3004A
DATES: Start: 4/24/2006
Finish: 4/25/2006

Finish: 4/25/2006
WEATHER: Overcast, cool (lo-50's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 3¹/₄" HSA w/SS sampler

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager



BOREHOLE ID: SB-15 Well **ID:** n/a

 Surface Elev:
 624 ft. MSL

 Completion:
 84 ft. BGS

 Station:
 875,970.0N

 2,515,080.0E

| 5 | AMPLE TESTING | | | | | | TOPOGRAPHIC MAP INFORMATION: | WATER LE | VEI | INFORMA | TION: |
|----------------|----------------------------------|------|---|---------------|-------------------|--------------------------|--|--|--------------|---|-----------------------------------|
| er | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadrangle: Coffeen, IL Township: East Fork Section 11, Tier 7N; Range 3W | $\underline{\underline{\nabla}} = 13.$ $\underline{\underline{\nabla}} = 4.$ | 40 - 99 - | While drilling MW15S on MW15D on | ng 6/1/06 |
| Number | Recov % Rec | Type | Blows N - V ₈ RQD | Moist | Dry D | Qu (ts Failur | Depth Lithologic ft. BGS Description | Bore Det | | Elevation ft. MSL | Remarks |
| 1A 1B | 24/24 100% | ss | 2-2 3-4 N=5 | 19 27 | | 1.94 | Dark brown (10YR3/3), clayey SILT Dark grayish brown (10YR3/2), clayey SILT, trace sand Grayish brown (10YR5/2), with 50% very dark gray | d | | 622 | |
| 2A | 24/24 100% | ss | 2-2 4-6 N=6 | 25 | | 3.10 B | Gray (10YR6/1), lean CLAY, trace sand Gray (10YR6/1), lean CLAY, trace sand | | | 620 | |
| A | 20/24 83% | ss | 2-3 3-5 N=6 | 29 | | 2.10 B | Yellowish brown (10YR5/6) with 40% gray (10YR6/1) mottles, lean CLAY, trace sand | | | 618 | |
| A | 24/24 100% | ss | 4-6 5-5 N=11 | 24 | | 1.75 B | Gray (10YR6/1), lean CLAY, trace sand | | | 616 | |
| δA | 22/24 92% | ss | 1-2 3-4 N=5 | 26 | | 1.55 B | Gray (10YR6/1) with 50% yellowish brown (10YR5/6) mottles, lean CLAY, little sand, trace gravel | | | 614 | |
| ōΑ | 22/24 92% [19/24 79% [| SS | 2-3 3-4 N=6 | 22 | | 1.85 B | Gray (10YR6/1) with 50% yellowish brown (10YR5/6) mottles, lean CLAY, little sand, trace gravel | | | 612 | Shelby tube taker from shallow we |
| 'A 'B | 24/24 100% | ss | 4-4 5-5 N=9 | 23 17 | | 1.22 B | Gray (10YR6/1) with 30% yellowish brown (10YR5/6 mottles, silty, fine to medium SAND, trace coarse sand and gravel, wet | | | 610 | borehole at indicated depth. |
| SA | 21/24 88% | SS | 2-6 15-19 N=21 | 11 | | 3.22 BSP | Pale brown (10YR6/3), clayey SILT, little sand, trace gravel Yellowish brown (10YR5/4), silty, fine to coarse SANI | | ,,,,,,,, | - - - - - - - - - - - - - - - - - - - | |
| OA OB OC | 24/24 100% | ss | 18-29 40-50 N=69 | 20 21 9 | | | Yellowish brown (10YR5/4), silty, fine to coarse SAND wet Yellowish brown (10YR5/4) silty fine SAND, wet Gray (10YR6/1), sandy SILT, trace medium to coarse sand and trace gravel | | | 606 | |
| 0A | 17/24 71% | SS | 11-43 59/5" | 7 | | 7.42 B | Dark gray (10YR4/1), clayey SILT, little sand, trace gravel | | | — — — 604 | |

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A

DATES: Start: 4/24/2006

Finish: 4/25/2006

Finish: 4/25/2006 **WEATHER:** Overcast, cool (lo-50's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 3¹/₄" HSA w/SS sampler

FIELD STAFF: Driller: B. Williamson **Helper:** R. Keedy

Eng/Geo: R. Hasenyager



BOREHOLE ID: SB-15 **Well ID:** n/a

 Surface Elev:
 624 ft. MSL

 Completion:
 84 ft. BGS

 Station:
 875,970.0N

 2,515,080.0E

| S | AMPL | E | Т | EST | ING | ř | ГОРОGRAPHIC MAP INFOR | MATION: | WATER LEVE | L INFORM | ATION: |
|--------|----------------------------------|------|---|--------------|-------------------|--------------------------|--|--|--|--|--------------|
| er | Recov / Total (in) % Recovery | | /6 in ılue | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadrangle: Coffeen, IL Township: East Fork Section 11, Tier 7N; Range 3V | | $\underline{\underline{\mathbf{y}}} = 13.40$ $\underline{\underline{\mathbf{y}}} = 4.99$ | - While drilli - MW15S on - MW15D or | ng 6/1/06 |
| Number | Recov % Rec | Type | Blows / 6 in N - Value RQD | Moist | Dry D | Qu (ts: Failur | Depth ft. BGS | Lithologic Description | Boreho Detail | | Remarks |
| 1A | 14/24 58% | ss | 14-55 45/2" | 8 | | | 22 — 24 — 26 — 28 — Dark gray (10YR [Conting of the conting of the | | | 602 | |
| 2A | 8/24 33% | ss | 100/8" | 8 | | 6.76 SP | 24 | | | 600 | |
| 3A | 23/24 96% | ss | 12-28 43-57/5" N=71 | 5 | | | 26 | | | 598 | |
| 4A | 8/24 33% | ss | 59-41/2" | 6 | | 7.95 BSh | Dark gray (10YR | 4/1), clayey SILT, little sand, trac gravel | ce | | |
| 5A | 16/24 67% | ss | 11-26 74/4" | 12 | | 4.74 <i>BSh</i> | [Contin | ued from previous page] | | 594 | |
| 6A | 12/24 50% | ss | 39-61 | 7 | | | 32 | | | 592 | |
| 7A | 10/24 42% | ss | 49-51/4" | 9 | | 5.43 B | 34 | | | 590 | |
| 8A | 11/24 46% | ss | 100-95 | 11 | | | 34 - 36 - 36 - 36 - 36 - 36 - 36 - 36 - | | | 588 | |
| 9A | 8/24 33% | ss | 61-39/2" | 10 | | | Dark gray (10YR4/ | 1), silty, fine to medium SAND, t e sand and gravel, wet | trace | | |
| .0A | 24/24 100% | ss | 21-41 21-24 N=62 | 12 | | 16.00 <i>None</i> | Very dark gray (10) | YR3/1), clayey SILT, little sand, t gravel YR3/1) with 20% dark grayish br | own | | |
| 20B | 1 | | | 13 | | 9.38 | Very dark gray (10 ^v (10YR4/2) mottles bentonite grout pumped from bott | , clayey SILT, trace sand and gra | ivel | <u></u> | |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility Location: Coffeen, Illinois

Project: 05S3004A **DATES: Start:** 4/24/2006 Finish: 4/25/2006

WEATHER: Overcast, cool (lo-50's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 31/4" HSA w/SS sampler

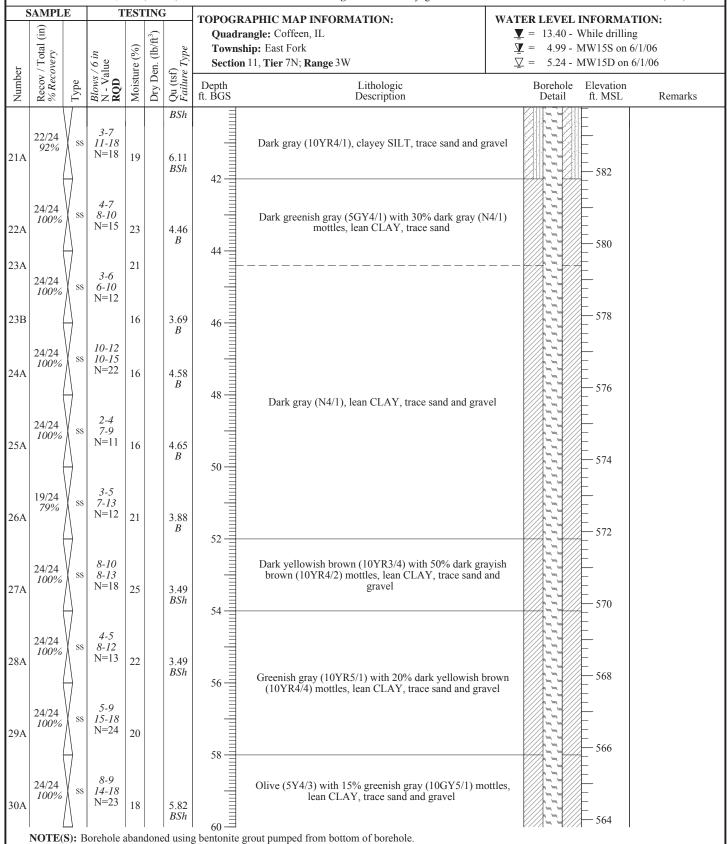
FIELD STAFF: Driller: B. Williamson Helper: R. Keedy Eng/Geo: R. Hasenyager

BOREHOLE ID: SB-15

Well ID: n/a

Surface Elev: 624 ft. MSL 84 ft. BGS **Completion:** Station: 875,970.0N 2,515,080.0E

HANSON



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A

DATES: Start: 4/24/2006

Finish: 4/25/2006 **WEATHER:** Overcast, cool (lo-50's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 31/4" HSA w/SS sampler

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: SB-15 Well **ID:** n/a

 Surface Elev:
 624 ft. MSL

 Completion:
 84 ft. BGS

 Station:
 875,970.0N

 2,515,080.0E

| 5 | SAMPL | E | Т | EST | TIN(| 3 | TOPOGR | APHIC MAP INFORMATION: | WATE | R LEVEL | INFORMAT | ION: |
|------------|-------------------------------|------|---|--------------|-------------------|--------------------------|------------------|---|---------|-----------------------|--|---------|
| er | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadra Towns | angle: Coffeen, IL hip: East Fork 11, Tier 7N; Range 3W | Ī | = 13.40 - = 4.99 - | While drilling MW15S on 6/ MW15D on 6/ | 1/06 |
| Number | Reco. % Re | Type | Blow: N - V RQD | Moist | Dry I | Qu (t Failu | Depth ft. BGS | Lithologic Description | | Borehole Detail | Elevation ft. MSL | Remarks |
| 1A | 24/24 100% | ss | 4-7 13-15 N=20 | 18 | | 5.42 BSh | 62 — | Olive (5Y4/3) with 15% greenish gray (10GY5/1) mo | ottles, | | 562 | |
| 2A | 24/24 100% | ss | 10-15 11-16 N=26 | 20 | | 4.74 BSh | 64 | lean CLAY, trace sand and gravel [Continued from previous page] | | | 560 | |
| 3A | 24/24 100% | ss | 6-10 11-13 N=21 | 16 | | 6.98 <i>BSh</i> | 66 | Greenish gray (10Y5), lean CLAY, trace sand and gr | ravel | | 558 | |
| 4A | 24/24 100% | ss | 11-14 18-31 N=32 | 18 | | 6.98 BSh | | | | | 556 | |
| 5A | 23/24 96% | ss | 9-18 27-40 N=45 | 15 | | 11.95 BSh | 68 = | | | | 554 | |
| 66A | 24/24 100% | ss | 4-12 18-24 N=30 | 16 | | 7.15 <i>BSh</i> | 72 | | | | 552 | |
| 7A | 24/24 100% | ss | 17-29 36-47 N=65 | 17 | | 8.24 <i>BSh</i> | | Dark yellowish brown (10YR4/4), lean CLAY, trace and gravel | sand | | 550 | |
| 8A | 20/24 83% | ss | 12-18 23-28 N=41 | 17 | | 6.59 <i>BSh</i> | 74 | | | | 548 | |
| 9A | 9/24 38% | ss | 29-39 48-66 N=87 | 16 | | | 78 | | | | 546 | |
| θ Α | 24/24 100% | ss | 5-9 13-18 N=22 | 18 | | 6.21 B | 80 | | | | 544 | |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility Location: Coffeen, Illinois

Project: 05S3004A **DATES: Start:** 4/24/2006

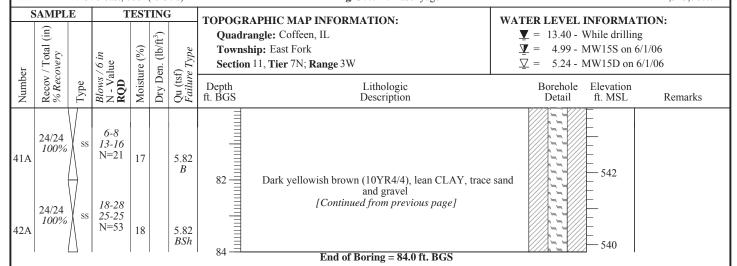
Finish: 4/25/2006 WEATHER: Overcast, cool (lo-50's) **CONTRACTOR:** Testing Service Corporation Rig mfg/model: CME-650 Track Rig **Drilling Method:** 31/4" HSA w/SS sampler

FIELD STAFF: Driller: B. Williamson

Helper: R. Keedy Eng/Geo: R. Hasenyager **HANSON**

BOREHOLE ID: SB-15 Well ID: n/a

> **Surface Elev:** 624 ft. MSL **Completion:** 84 ft. BGS **Station:** 875,970.0N 2,515,080.0E



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A DATES: Start: 4/25/2006

Finish: 4/25/2006
WEATHER: Overcast, cool (lo-50's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 41/4" HSA (blind drill)

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

HANSON

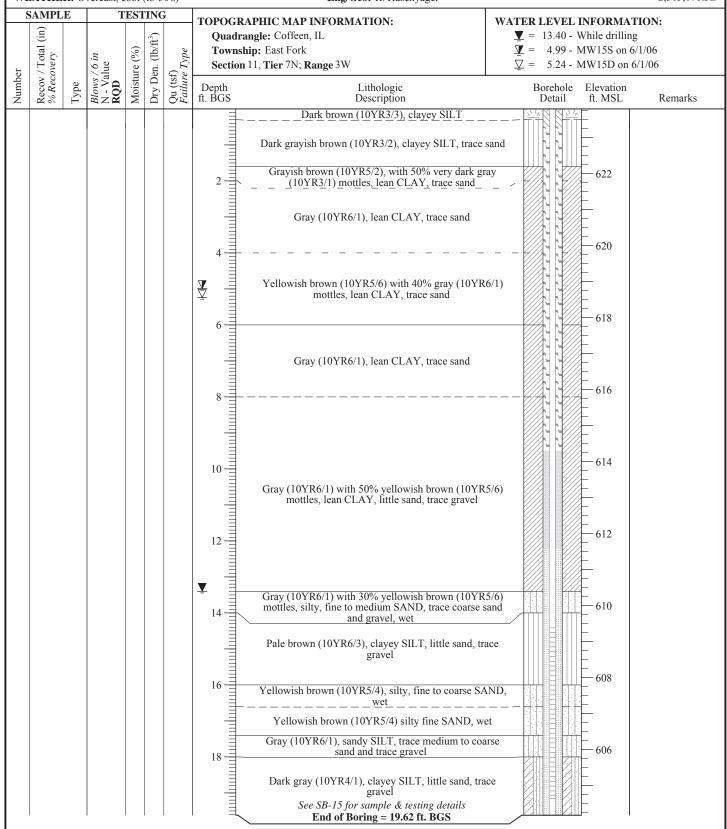
BOREHOLE ID: SB-15a **Well ID:** MW15S

 Surface Elev:
 624 ft. MSL

 Completion:
 20 ft. BGS

 Station:
 875,971.1N

 2,515,076.3E



NOTE(S): MW15S installed in blind-drilled borehole within 10 ft of SB-15.

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois
Project: 05S3004A
DATES: Start: 4/24/2006
Finish: 4/25/2006

Finish: 4/25/2006
WEATHER: Overcast, cool (lo-50's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 3¹/₄" HSA w/SS sampler

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager



BOREHOLE ID: SB-15 Well **ID:** n/a

 Surface Elev:
 624 ft. MSL

 Completion:
 84 ft. BGS

 Station:
 875,970.0N

 2,515,080.0E

| 5 | AMPLE TESTING | | | | | | TOPOGRAPHIC MAP INFORMATION: | WATER LE | VEI | INFORMA | TION: |
|----------------|----------------------------------|------|---|---------------|-------------------|--------------------------|--|--|--------------|---|-----------------------------------|
| er | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadrangle: Coffeen, IL Township: East Fork Section 11, Tier 7N; Range 3W | $\underline{\underline{\nabla}} = 13.$ $\underline{\underline{\nabla}} = 4.$ | 40 - 99 - | While drilling MW15S on MW15D on | ng 6/1/06 |
| Number | Recov % Rec | Type | Blows N - V ₈ RQD | Moist | Dry D | Qu (ts Failur | Depth Lithologic ft. BGS Description | Bore Det | | Elevation ft. MSL | Remarks |
| 1A 1B | 24/24 100% | ss | 2-2 3-4 N=5 | 19 27 | | 1.94 | Dark brown (10YR3/3), clayey SILT Dark grayish brown (10YR3/2), clayey SILT, trace sand Grayish brown (10YR5/2), with 50% very dark gray | d | | 622 | |
| 2A | 24/24 100% | ss | 2-2 4-6 N=6 | 25 | | 3.10 B | Gray (10YR6/1), lean CLAY, trace sand Gray (10YR6/1), lean CLAY, trace sand | | | 620 | |
| A | 20/24 83% | ss | 2-3 3-5 N=6 | 29 | | 2.10 B | Yellowish brown (10YR5/6) with 40% gray (10YR6/1) mottles, lean CLAY, trace sand | | | 618 | |
| A | 24/24 100% | ss | 4-6 5-5 N=11 | 24 | | 1.75 B | Gray (10YR6/1), lean CLAY, trace sand | | | 616 | |
| δA | 22/24 92% | ss | 1-2 3-4 N=5 | 26 | | 1.55 B | Gray (10YR6/1) with 50% yellowish brown (10YR5/6) mottles, lean CLAY, little sand, trace gravel | | | 614 | |
| ōΑ | 22/24 92% [19/24 79% [| SS | 2-3 3-4 N=6 | 22 | | 1.85 B | Gray (10YR6/1) with 50% yellowish brown (10YR5/6) mottles, lean CLAY, little sand, trace gravel | | | 612 | Shelby tube taker from shallow we |
| 'A 'B | 24/24 100% | ss | 4-4 5-5 N=9 | 23 17 | | 1.22 B | Gray (10YR6/1) with 30% yellowish brown (10YR5/6 mottles, silty, fine to medium SAND, trace coarse sand and gravel, wet | | | 610 | borehole at indicated depth. |
| SA | 21/24 88% | SS | 2-6 15-19 N=21 | 11 | | 3.22 BSP | Pale brown (10YR6/3), clayey SILT, little sand, trace gravel Yellowish brown (10YR5/4), silty, fine to coarse SANI | | ,,,,,,,, | - - - - - - - - - - - - - - - - - - - | |
| OA OB OC | 24/24 100% | ss | 18-29 40-50 N=69 | 20 21 9 | | | Yellowish brown (10YR5/4), silty, fine to coarse SAND wet Yellowish brown (10YR5/4) silty fine SAND, wet Gray (10YR6/1), sandy SILT, trace medium to coarse sand and trace gravel | | | 606 | |
| 0A | 17/24 71% | SS | 11-43 59/5" | 7 | | 7.42 B | Dark gray (10YR4/1), clayey SILT, little sand, trace gravel | | | — — — 604 | |

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A

DATES: Start: 4/24/2006

Finish: 4/25/2006

Finish: 4/25/2006 **WEATHER:** Overcast, cool (lo-50's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 3¹/₄" HSA w/SS sampler

FIELD STAFF: Driller: B. Williamson **Helper:** R. Keedy

Eng/Geo: R. Hasenyager



BOREHOLE ID: SB-15 **Well ID:** n/a

 Surface Elev:
 624 ft. MSL

 Completion:
 84 ft. BGS

 Station:
 875,970.0N

 2,515,080.0E

| S | AMPL | E | Т | EST | ING | ř | ГОРОGRAPHIC MAP INFOR | MATION: | WATER LEVE | L INFORM | ATION: |
|--------|----------------------------------|------|---|--------------|-------------------|--------------------------|--|--|--|--|--------------|
| er | Recov / Total (in) % Recovery | | /6 in ılue | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadrangle: Coffeen, IL Township: East Fork Section 11, Tier 7N; Range 3V | | $\underline{\underline{\mathbf{y}}} = 13.40$ $\underline{\underline{\mathbf{y}}} = 4.99$ | - While drilli - MW15S on - MW15D or | ng 6/1/06 |
| Number | Recov % Rec | Type | Blows / 6 in N - Value RQD | Moist | Dry D | Qu (ts: Failur | Depth ft. BGS | Lithologic Description | Boreho Detail | | Remarks |
| 1A | 14/24 58% | ss | 14-55 45/2" | 8 | | | 22 — 24 — 26 — 28 — Dark gray (10YR [Conting of the conting of the | | | 602 | |
| 2A | 8/24 33% | ss | 100/8" | 8 | | 6.76 SP | 24 | | | 600 | |
| 3A | 23/24 96% | ss | 12-28 43-57/5" N=71 | 5 | | | 26 | | | 598 | |
| 4A | 8/24 33% | ss | 59-41/2" | 6 | | 7.95 BSh | Dark gray (10YR | 4/1), clayey SILT, little sand, trac gravel | ce | | |
| 5A | 16/24 67% | ss | 11-26 74/4" | 12 | | 4.74 <i>BSh</i> | [Contin | ued from previous page] | | 594 | |
| 6A | 12/24 50% | ss | 39-61 | 7 | | | 32 | | | 592 | |
| 7A | 10/24 42% | ss | 49-51/4" | 9 | | 5.43 B | 34 | | | 590 | |
| 8A | 11/24 46% | ss | 100-95 | 11 | | | 34 - 36 - 36 - 36 - 36 - 36 - 36 - 36 - | | | 588 | |
| 9A | 8/24 33% | ss | 61-39/2" | 10 | | | Dark gray (10YR4/ | 1), silty, fine to medium SAND, t e sand and gravel, wet | trace | | |
| .0A | 24/24 100% | ss | 21-41 21-24 N=62 | 12 | | 16.00 <i>None</i> | Very dark gray (10) | YR3/1), clayey SILT, little sand, t gravel YR3/1) with 20% dark grayish br | own | | |
| 20B | 1 | | | 13 | | 9.38 | Very dark gray (10 ^v (10YR4/2) mottles bentonite grout pumped from bott | , clayey SILT, trace sand and gra | ivel | <u></u> | |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility Location: Coffeen, Illinois

Project: 05S3004A **DATES: Start:** 4/24/2006 Finish: 4/25/2006

WEATHER: Overcast, cool (lo-50's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 31/4" HSA w/SS sampler

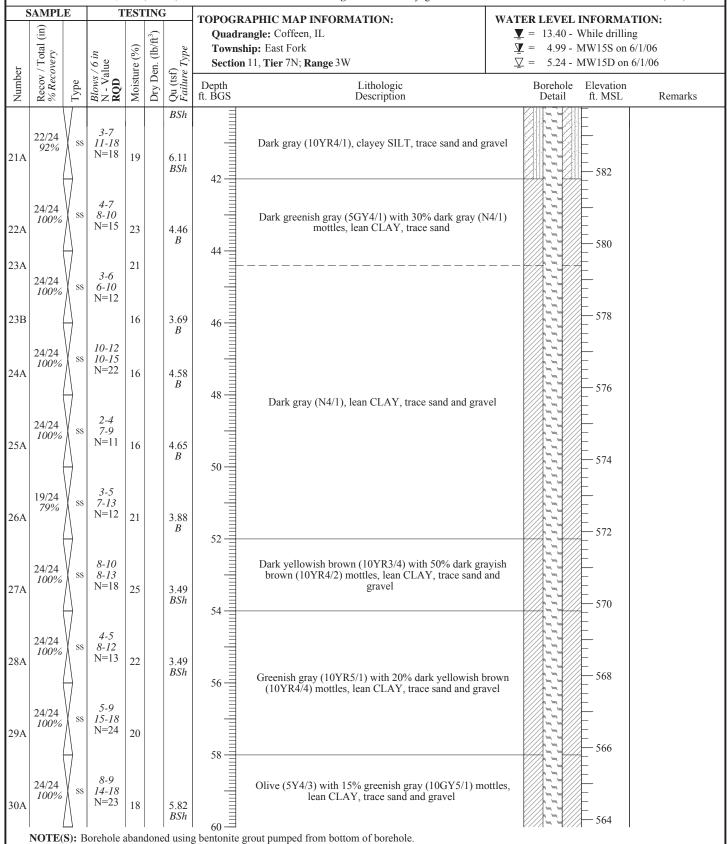
FIELD STAFF: Driller: B. Williamson Helper: R. Keedy Eng/Geo: R. Hasenyager

BOREHOLE ID: SB-15

Well ID: n/a

Surface Elev: 624 ft. MSL 84 ft. BGS **Completion:** Station: 875,970.0N 2,515,080.0E

HANSON



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility Location: Coffeen, Illinois

Project: 05S3004A **DATES: Start:** 4/24/2006 Finish: 4/25/2006

WEATHER: Overcast, cool (lo-50's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig **Drilling Method:** 31/4" HSA w/SS sampler

BOREHOLE ID: SB-15 Well ID: n/a **Surface Elev: Completion:** Station:

HANSON

624 ft. MSL

84 ft. BGS

875,970.0N

2,515,080.0E

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy Eng/Geo: R. Hasenyager

| SA | AMPLE | 1 | EST | ING | r | TOPOGRAPHIC | MAP INFORMATION: | WATER | LEVEL INFORMATION: |
|-----|--------------|--------------|---------|---------------|--------------|--|--------------------|--------------------------|--|
| | / Total (in) | /6 in Jue | ure (%) | Den. (lb/ft³) | f) e Type | Quadrangle: Co Township: East Section 11, Tier | offeen, IL Fork | <u>Ā</u> = <u>Ā</u> = | 13.40 - While drilling 4.99 - MW15S on 6/1/06 |
| ę l | ov e | 2 \$ 5 | str | Ω | tsf ure | Daniella | Tithelesia | D | arabala Elemetica |

| ı | Recov / Total (i% Recovery | | 6 in | re (%) | Dry Den. (lb/ft | Type | Townsh | ip: East Fork 11, Tier 7N; Range 3W | $\overline{\Lambda} = \overline{\Lambda}$ | 4.99 - 1 | MW15S on 6/1 MW15D on 6/ | |
|--------|----------------------------|------|---|--------------|-----------------|--------------------------|------------------|---|---|--------------------|-----------------------------|---------|
| Number | Recov % Reco | Type | Blows / 6 in N - Value RQD | Moisture (%) | Dry De | Qu (tsf) Failure Type | Depth ft. BGS | Lithologic Description | | Borehole Detail | Elevation ft. MSL | Remarks |
| 31A | 24/24 100% | SS | 4-7 13-15 N=20 | 18 | | 5.42 <i>BSh</i> | 62 — | Olive (5Y4/3) with 15% greenish gray (10GY5/1) mottl | les, | | 562 | |
| 32A | 24/24 100% | ss | 10-15 11-16 N=26 | 20 | | 4.74 BSh | 64 | lean CLAY, trace sand and gravel [Continued from previous page] | | | 560 | |
| 33A | 24/24 100% | SS | 6-10 11-13 N=21 | 16 | | 6.98 BSh | 66 | Greenish gray (10Y5), lean CLAY, trace sand and grav | vel | | 558 | |
| 34A | 24/24 100% | ss | 11-14 18-31 N=32 | 18 | | 6.98 <i>BSh</i> | 66 | | | | 556 | |
| 35A | 23/24 96% | SS | 9-18 27-40 N=45 | 15 | | 11.95 BSh | 70 — | | | | 554 | |
| 36A | 24/24 100% | ss | 4-12 18-24 N=30 | 16 | | 7.15 BSh | 72 | | | | 552 | |
| 37A | 24/24 100% | ss | 17-29 36-47 N=65 | 17 | | 8.24 <i>BSh</i> | 74- | Dark yellowish brown (10YR4/4), lean CLAY, trace sa and gravel | and | | 550 | |
| 38A | 20/24 83% | ss | 12-18 23-28 N=41 | 17 | | 6.59 BSh | 76- | | | | 548 | |
| 39A | 9/24 38% | ss | 29-39 48-66 N=87 | 16 | | | 78 — | | | | 546 | |
| 40A | 24/24 100% | ss | 5-9 13-18 N=22 | 18 | | 6.21 B | 80 | rout numbed from bottom of borehole | | | 544 | |

NOTE(S): Borehole abandoned using bentonite grout pumped from bottom of borehole.

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A **DATES: Start:** 4/24/2006

Finish: 4/25/2006
WEATHER: Overcast, cool (lo-50's)

CONTRACTOR: Testing Service Corporation Rig mfg/model: CME-650 Track Rig Drilling Method: 3¹/₄" HSA w/SS sampler

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

HANSON

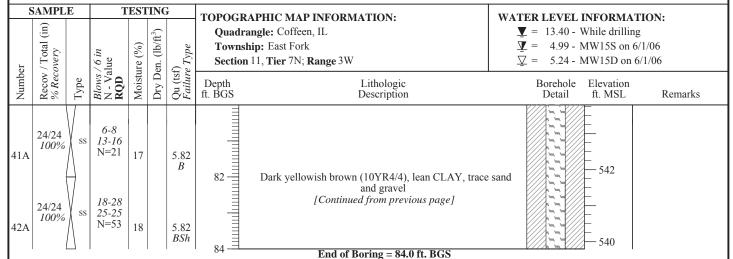
BOREHOLE ID: SB-15 **Well ID:** n/a

 Surface Elev:
 624 ft. MSL

 Completion:
 84 ft. BGS

 Station:
 875,970.0N

 2,515,080.0E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility Location: Coffeen, Illinois

Project: 05S3004A **DATES: Start: 4/21/2006**

SAMPLE

Finish: 4/25/2006 WEATHER: Overcast, cool (mid-40's)

TESTING

CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-850 Track Rig **Drilling Method:** 41/4" HSA (blind drill)

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager

WATER LEVEL INFORMATION:

BOREHOLE ID: SB-16b

Surface Elev:

Completion:

Station:

Well ID: MW16D

626 ft. MSL

51 ft. BGS

2,515,079.4E

877,354.9N

TOPOGRAPHIC MAP INFORMATION: Ξ $\mathbf{Y} = 12.80$ - While drilling Quadrangle: Coffeen, IL Dry Den. (lb/ft3 Recov / Total % Recovery Township: East Fork $\nabla = 5.74 - MW16S \text{ on } 6/1/06$ Qu (tsf) Failure Type Moisture (%) Blows / 6 in N - Value RQD Section 2, Tier 7N; Range 3W ∇ = 51.37 - MW16D on 6/1/06 Number Depth ft. BGS Lithologic Borehole Elevation Description Detail ft. MSL Remarks 626 Black (10YR2/1), sl. moist, firm, clayey SILT with trace sand and trace gravel. Brown (10YR4/3), sl. moist, firm, silty CLAY with trace sand. 624 Gray (10YR5/1) with 25% yellowish brown (10YR5/8) mottles, moist, very soft, very silty CLAY with trace sand. $\bar{\Lambda}$ 620 Gray (10YR5/1) with 15% dark yellowish brown (10YR4/6) mottles, moist, very soft, very silty CLAY with trace sand. 618 Gray (10YR5/1) with 10% yellowish brown (10YR5/8) mottles, moist, firm, silty CLAY with some sand and trace 616 gravel. \blacksquare Dark yellowish brown (10YR4/6), wet, sl. dense, silty, very fine- to fine-grained SAND. Dark yellowish brown (10YR4/6), moist, firm, silty 14 612 CLAY with sand and trace gravel. Dark yellowish brown (10YR4/6), wet, loose, silty, very fine- to fine-grained SAND. Dark yellowish brown (10YR4/6), wet, soft, silty CLAY with sand and trace gravel. 610 Yellowish brown (10YR5/6), wet, loose, very fine- to very coarse-grained SAND. Gray (10YR5/1), wet, loose, fine- to medium-grained SAND. Gray (10YR5/1), moist, hard, clayey SILT with sand and 608 trace gravel Gray (10YR5/1), wet, loose, very fine- to fine-grained SAND. Gray (10YR4/1), moist, very hard, clayey, sandy SILT 20 with trace gravel. NOTE(S): MW16D installed in blind-drilled borehole within 10 ft of SB-16.

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A **DATES: Start:** 4/21/2006

Finish: 4/25/2006 **WEATHER:** Overcast, cool (mid-40's)

CONTRACTOR: Reynolds Drilling Corp. **Rig mfg/model:** CME-850 Track Rig **Drilling Method:** 4¼" HSA (blind drill)

FIELD STAFF: Driller: K. Doetzel
Helper: S. McCartney
Eng/Geo: R. Hasenyager

Well ID: MW16D Surface Elev: 626 ft

 Surface Elev:
 626 ft. MSL

 Completion:
 51 ft. BGS

 Station:
 877,354.9N

 2,515,079.4E

BOREHOLE ID: SB-16b

HANSON

| | SAMPLE TESTING | | | | INC | j | торосра | PHIC MAP INFORMATION: | WATER LEVEL | INFORMAT | ION: |
|--------|-------------------------------|-------|---|--------------|-------------------|--------------------------|--|---|--------------------|----------------------------|---------|
| er | Recov / Total (in) % Recovery | | / 6 in alue | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadrai | ngle: Coffeen, IL p: East Fork P, Tier 7N; Range 3W | | While drilling MW16S on 6/ | 1/06 |
| Number | Recov % Rec | Type | Blows / 6 in N - Value RQD | Moist | Dry D | Qu (ts Failur | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks |
| | NOTE | S): M | ſW16D i | nsta | lled i | n bline | 22 ——————————————————————————————————— | Gray (10YR4/1), moist, very hard, clayey, sandy SI with trace gravel. [Continued from previous page] | | | |

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility Location: Coffeen, Illinois

Project: 05S3004A **DATES: Start:** 4/21/2006

Finish: 4/25/2006

WEATHER: Overcast, cool (mid-40's)

CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-850 Track Rig **Drilling Method:** 41/4" HSA (blind drill)

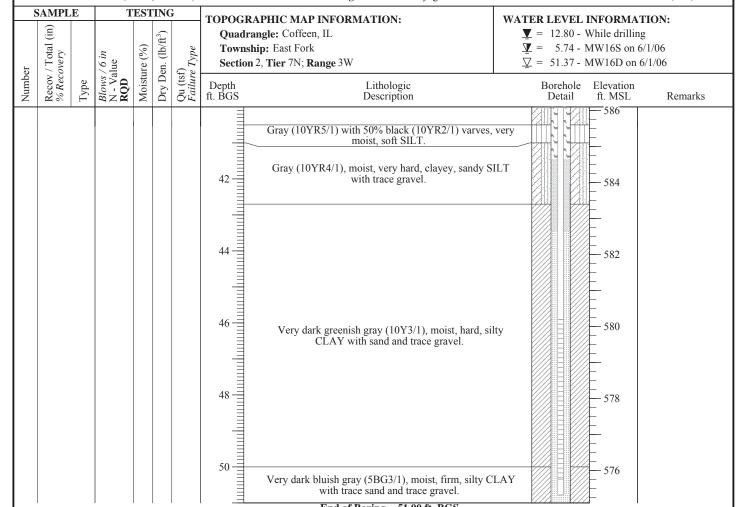
FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager

BOREHOLE ID: SB-16b Well ID: MW16D **Surface Elev:**

626 ft. MSL 51 ft. BGS **Completion:** Station: 877,354.9N 2,515,079.4E

HANSON



End of Boring = 51.00 ft. BGS See SB-16 for sample & testing details

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois
Project: 05S3004A

DATES: Start: 4/21/2006

Expire 4/05/0006

Finish: 4/25/2006 WEATHER: Overcast, cool (mid-40's) **CONTRACTOR:** Reynolds Drilling Corp. **Rig mfg/model:** CME-850 Track Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: SB-16 **Well ID:** n/a

 Surface Elev:
 626 ft. MSL

 Completion:
 92 ft. BGS

 Station:
 877,355.0N

 2,515,080.0E

| 2 | SAMPL | E | T | EST | INC | j | TOPOGR | APHIC MAP INFORMATION: | WAT | ER LI | EV. | EL I | INFORMA | TION: |
|---------|----------------------------------|-------------|---|--------------|-------------------|--------------------------|------------------|---|----------------|--------------|------|----------|---------------------------------------|--|
| er | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Towns | angle: Coffeen, IL hip: East Fork 12, Tier 7N; Range 3W | $\bar{\Delta}$ | <u>'</u> = 4 | 5.74 | 4 - 1 | While drillin MW16S on MW16D on | 6/1/06 |
| Number | Recov % Rec | Type | Blows N - Ve RQD | Moist | Dry D | Qu (ts Failur | Depth ft. BGS | Lithologic Description | | Bor De | | | Elevation ft. MSL | Remarks |
| Α | 21/24 | SS | 4-4 6-7 | 22 | | | | Black (10YR2/1), sl. moist, firm, clayey SILT with t sand and trace gravel. | race | V V | 1111 | 7/ 7/ | 626 | |
| В | 88% | 55 | N=10 | 29 | | 2.13 B | 2- | Brown (10YR4/3), sl. moist, firm, silty CLAY with sand. | race | | | | 624 | |
| A | 24/24 100% | SS | 4-6 7-9 N=13 | 25 | | 2.13 B | 4- | | | | | | 622 | |
| A | 20/24 83% | ss | 3-4 5-7 N=9 | 21 | | 2.33 B | Ā | Gray (10YR5/1) with 25% yellowish brown (10YR mottles, moist, very soft, very silty CLAY with trace | | | | | 022 | |
| A | 24/24 100% | ss | 2-3 4-6 N=7 | 25 | | 2.13 | 6- | Gray (10YR5/1) with 15% dark yellowish brown (10YR4/6) mottles, moist, very soft, very silty CLAY trace sand. | with | | | | 620 | |
| A | 24/24 100% | SS | 3-4 5-5 N=9 | 24 | | 2.33 B | 8 | Gray (10YR5/1) with 10% yellowish brown (10YR: mottles, moist, firm, silty CLAY with some sand and | 5/8) trace | | | | 618 | |
| A | 24/24 100% 24/24 100% | SS SH | 2-4 4-5 N=8 | 24 | | 1.75 B | | gravel. | | | | | | Shelby tube take from shallow we borehole at indicated depth. |
| 'A | 24/24 | SS | 4-7 7-7 | 22 | | 1.94 <i>BSh</i> | 12 | | | - | | | 614 | писаси исриг. |
| В | 100% | \[\] \[\] | N=14 | 18 | | | 14 | Dark yellowish brown (10YR4/6), wet, sl. dense, si very fine- to fine-grained SAND. Dark yellowish brown (10YR4/6), moist, firm, sil- | | - | | | | |
| A | 21/24 88% | ss | 1-2 2-4 N=4 | 20 | | | 16- | CLAY with sand and trace gravel. Dark yellowish brown (10YR4/6), wet, loose, silty, fine- to fine-grained SAND. Dark yellowish brown (10YR4/6), wet, soft, silty CI with sand and trace gravel. | very | | | | 612 | |
| A | 18/24 75% | SS | 4-3 4-10 N=7 | 14 | | | 16- | Yellowish brown (10YR5/6), wet, loose, very fine-to-coarse-grained SAND. Gray (10YR5/1), wet, loose, fine- to medium-grain | | | | | 610 | |
| B)A | + | | | 15 10 | | | 18 | SAND. Gray (10YR5/1), moist, hard, clayey SILT with sand trace gravel. | | | 1111 | <u>a</u> | 608 | |
| В | 20/24 83% | ss | 27-54 59-59 N=113 | 17 | | | 20 | Gray (10YR5/1), wet, loose, very fine- to fine-grain SAND. Gray (10YR4/1), moist, very hard, clayey, sandy SI | | | | ZIII | <u>-</u> | |
| | | | | | | | 20 ∄ | with trace gravel. | | | , | | F | |

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 4/21/2006 Finish: 4/25/2006 WEATHER: Overcast, cool (mid-40's) **CONTRACTOR:** Reynolds Drilling Corp. **Rig mfg/model:** CME-850 Track Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel

Helper: S. McCartney **Eng/Geo:** R. Hasenyager

HANSON

BOREHOLE ID: SB-16 Well **ID:** n/a

 Surface Elev:
 626 ft. MSL

 Completion:
 92 ft. BGS

 Station:
 877,355.0N

 2,515,080.0E

| S | SAMPL | E | Т | EST | ΓING | Ĭ | TOPOGRAP | PHIC MAP INFORMATION: | WAT | ER LEVEL | INFORMA | TION: |
|--------|-------------------------------|------|----------------------------------|--------------|-------------------|--------------------------|------------------------------------|--|-----|---|---------------------------------------|--------------------------------|
| ber | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadrang Township Section 2, | gle: Coffeen, IL : East Fork Tier 7N; Range 3W | Ž | Z = 12.80 - | While drillin MW16S on MW16D on | ng 6/1/06 |
| Number | Reco % Re | Type | Blow N - V RQD | Mois | Dry I | Qu (t Failu | Depth ft. BGS | Lithologic Description | | Borehole Detail | Elevation ft. MSL | Remarks |
| 1A | 10/24 42% | ss | 10-96 | 8 | | | 22 | | | | 606 | |
| 2A | 14/24 58% | ss | 84-132 | 10 | | 3.10 <i>BSh</i> | 24- | | | | 602 | |
| 3A | 20/24 83% | SS | 41-68 82 N=150 | 10 | | 7.56 B | 26 | | | | | |
| 1A | 12/24 50% | ss | 58-119 | 10 | | 9.89 B | 20 | | | | 600 | Dusky red (7.5YR3/4) staining. |
| 5A | 24/24 100% | ss | 30-48 70-71 N=118 | 9 | | 5.62 B | 22 | Gray (10YR4/1), moist, very hard, clayey, sandy SI | LT | 1111111 | 598 | |
| 6A | 24/24 100% | ss | 50-54 68-93 N=122 | 9 | | | 32 — | with trace gravel. [Continued from previous page] | | | 594 | |
| 7A | 35/36 97% | CS | | 17 | | | 34- | | | | 592 | |
| | 60/60 | CS | | | | | 36- | | | | 590 | |
| 8A | 100% | | | 10 | | | 38 = 40 | | | | 588 | Wood fragmen |

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A

DATES: Start: 4/21/2006

Finish: 4/25/2006 WEATHER: Overcast, cool (mid-40's) **CONTRACTOR:** Reynolds Drilling Corp. **Rig mfg/model:** CME-850 Track Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager

HANSON

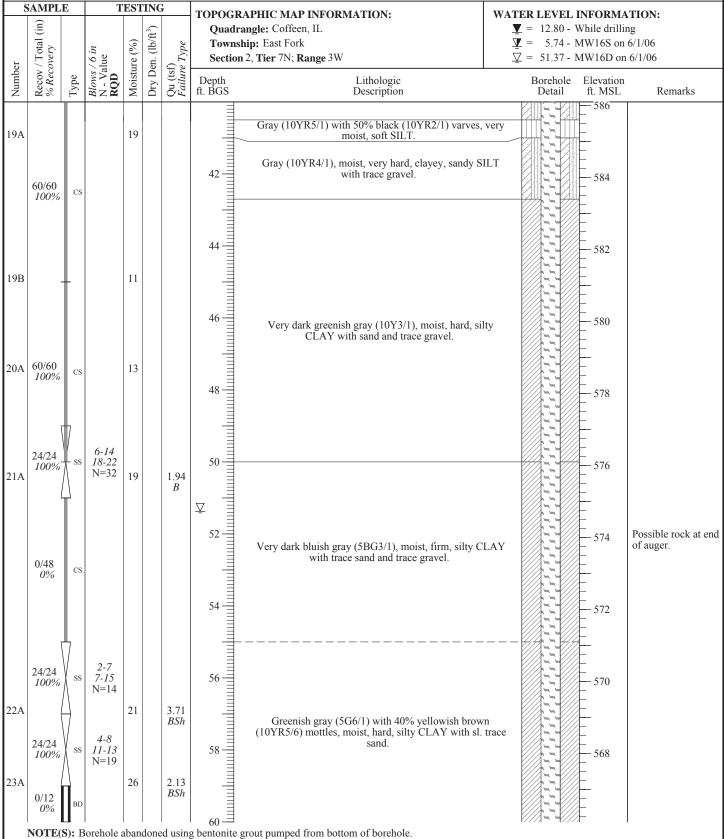
BOREHOLE ID: SB-16 **Well ID:** n/a

 Surface Elev:
 626 ft. MSL

 Completion:
 92 ft. BGS

 Station:
 877,355.0N

 2,515,080.0E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A **DATES: Start:** 4/21/2006

Finish: 4/25/2006

SAMPLE

WEATHER: Overcast, cool (mid-40's)

TESTING

CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-850 Track Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager TOPOGRAPHIC MAP INFORMATION:

HANSON

BOREHOLE ID: SB-16 Well ID: n/a

626 ft. MSL **Surface Elev: Completion:** 92 ft. BGS Station: 877,355.0N

2,515,080.0E WATER LEVEL INFORMATION:

| ber | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadra | APHIC MAP INFORMATION: ungle: Coffeen, IL uip: East Fork 2, Tier 7N; Range 3W | Ā Ā | ER LEVEL | While drillir MW16S on | ng 6/1/06 |
|--------|-------------------------------|------|---|--------------|-------------------|--------------------------|--------|--|------------|--------------------|---|--|
| Number | Reco %Re | Type | Blow N - V RQD | Mois | Dry I | Qu (t Failu | | Lithologic Description | | Borehole Detail | Elevation ft. MSL | Remarks |
| | 0/48 | RC | | | | | 62 — | Greenish gray (5G6/1) with 40% yellowish brown (10YR5/6) mottles, moist, hard, silty CLAY with sl. sand. [Continued from previous page] | n trace | | 566 | |
| 26A | 24/24 100% | SS | 32-34 42-51 N=76 | 25 | | 2.72 <i>BSh</i> | 64- | | | | 562 | |
| | 0/24 | RC | | | | | 66 | Yellowish brown (10YR5/6) with 20% greenish gr. (5G6/1) mottles, moist, hard, silty CLAY with trace s and trace coal fragments. | ay sand | | 560 | |
| 28A | 24/24 100% | SS | 15-21 21-21 N=42 | 18 | | 2.72 | 66 | | | 777777 | 558 | |
| 29A | 24/24 100% | ss | 14-17 21-25 N=38 | 20 | | 2.91 BSh | 70 | | | | 556 | 70' to 79.5' - possible oxidation rinds. |
| 30A | 24/24 100% | ss | 12-21 34-35 N=55 | 18 | | 5.04 BSh | 72 | | | | - - - - - - - - - - - - - - - - - - - | |
| 31A | 24/24 100% | ss | 16-21 27-35 N=48 | 16 | | 8.15 <i>BSh</i> | 74 | Yellowish brown (10YR5/6) with zones of gray (10YR4/1) mottles, moist, hard, clayey SILT with so sand and trace gravel. | ome | | 552 | |
| 32A | 60/60 | CS | | 19 | | | 76 | | | | | |

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A **DATES: Start:** 4/21/2006

Finish: 4/25/2006 WEATHER: Overcast, cool (mid-40's) CONTRACTOR: Reynolds Drilling Corp.

Rig mfg/model: CME-850 Track Rig

Drilling Model: 41/" USA 11/SS & CME of

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

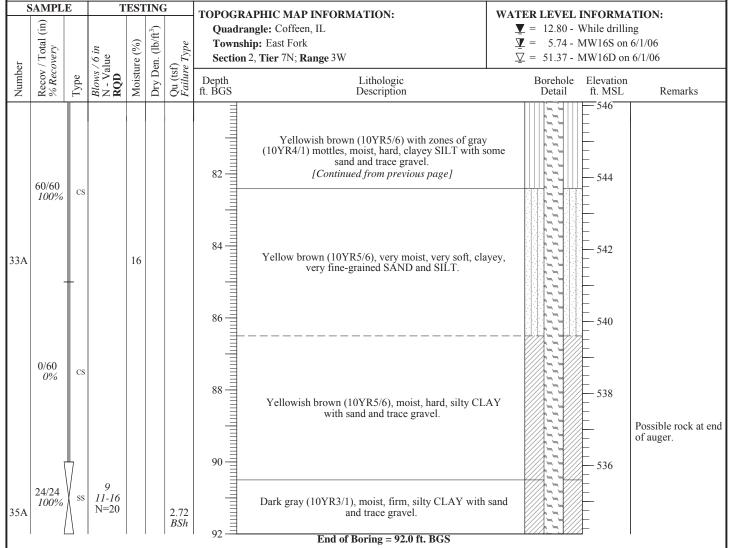
Eng/Geo: R. Hasenyager

BOREHOLE ID: SB-16

Well ID: n/a Surface Elev: 626 ft. MSL

Completion: 92 ft. BGS **Station:** 877,355.0N 2,515,080.0E

HANSON



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A

DATES: Start: 4/25/2006

Finish: 4/25/2006 **WEATHER:** Overcast, cool (mid-40's)

CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-850 Track Rig Drilling Method: 4¹/₄" HSA (blind drill)

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager

Well ID: MW16S

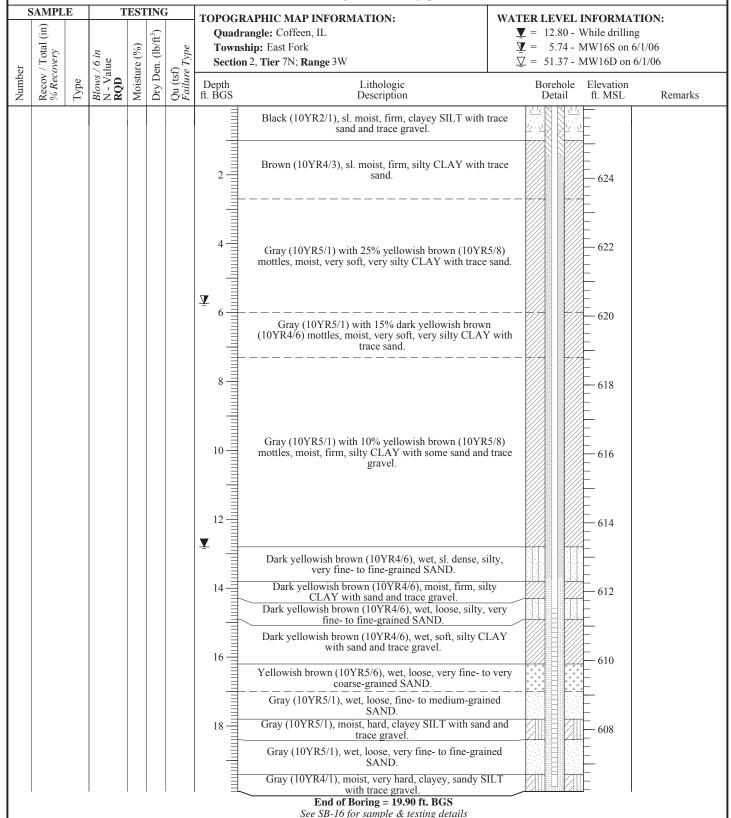
 Surface Elev:
 626 ft. MSL

 Completion:
 20 ft. BGS

 Station:
 877,355.1N

 2,515,088.0E

HANSON



NOTE(S): MW16S installed in blind-drilled borehole within 10 ft of SB-16.

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois
Project: 05S3004A

DATES: Start: 4/21/2006

Expire 4/05/0006

Finish: 4/25/2006 WEATHER: Overcast, cool (mid-40's) **CONTRACTOR:** Reynolds Drilling Corp. **Rig mfg/model:** CME-850 Track Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: SB-16 **Well ID:** n/a

 Surface Elev:
 626 ft. MSL

 Completion:
 92 ft. BGS

 Station:
 877,355.0N

 2,515,080.0E

| 2 | SAMPLE TESTING | | | | | j | TOPOGRAPHIC MAP INFORMATION: | | | WATER LEVEL INFORMATION: | | | | | |
|---------|--------------------------------|-------------|---|--------------|-------------------|--------------------------|--|---|---------------|--|--------|-------|-------------------|--|--|
| er | Recov / Total (in) % Recovery | | /6 in ılue | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadrangle: Coffeen, IL Township: East Fork Section 2, Tier 7N; Range 3W | | | $ \underline{\Psi} $ = 12.80 - While drilling $ \underline{\Psi} $ = 5.74 - MW16S on 6/1/06 $ \underline{\nabla} $ = 51.37 - MW16D on 6/1/06 | | | | | |
| Number | Recov % Rec | Type | Blows / 6 in N - Value RQD | Moist | Dry D | Qu (ts Failur | Depth ft. BGS | Lithologic Description | | Bore De | | | Elevation ft. MSL | Remarks | |
| Α | 21/24 | SS | 4-4 6-7 | 22 | | | | Black (10YR2/1), sl. moist, firm, clayey SILT with t sand and trace gravel. | race | | 1111 | 7/ 7/ | 626 | | |
| В | 88% | 55 | N=10 | 29 | | 2.13 B | 2- | Brown (10YR4/3), sl. moist, firm, silty CLAY with sand. | race | - | 11111 | | 624 | | |
| A | 24/24 100% | SS | 4-6 7-9 N=13 | 25 | | 2.13 B | 4- | | | | 111111 | | 622 | | |
| A | 20/24 83% | ss | 3-4 5-7 N=9 | 21 | | 2.33 B | Ā | Gray (10YR5/1) with 25% yellowish brown (10YR mottles, moist, very soft, very silty CLAY with trace | | | | | 022 | | |
| A | 24/24 100% | ss | 2-3 4-6 N=7 | 25 | | 2.13 | 6- | Gray (10YR5/1) with 15% dark yellowish brown (10YR4/6) mottles, moist, very soft, very silty CLAY trace sand. | with | - | | | 620 | | |
| A | 24/24 100% | SS | 3-4 5-5 N=9 | 24 | | 2.33 B | 8 | Gray (10YR5/1) with 10% yellowish brown (10YR: mottles, moist, firm, silty CLAY with some sand and | 5/8) trace | | | | 618 | | |
| A | 24/24 100% 24/24 100% | | 2-4 4-5 N=8 | 24 | | 1.75 B | | gravel. | | | | | | Shelby tube taker from shallow wel borehole at indicated depth. | |
| 'A | 24/24 | SS | 4-7 7-7 | 22 | | 1.94 <i>BSh</i> | 12 | | | | 1717 | | 614 | marcarea aepin. | |
| В | 100% | \[\] \[\] | N=14 | 18 | | | 14 | Dark yellowish brown (10YR4/6), wet, sl. dense, si very fine- to fine-grained SAND. Dark yellowish brown (10YR4/6), moist, firm, sil- | | | | | | | |
| A | 21/24 88% | ss | 1-2 2-4 N=4 | 20 | | | 16- | CLAY with sand and trace gravel. Dark yellowish brown (10YR4/6), wet, loose, silty, fine- to fine-grained SAND. Dark yellowish brown (10YR4/6), wet, soft, silty CI with sand and trace gravel. | very | - | | | 612 | | |
| A | 18/24 75% | SS | 4-3 4-10 N=7 | 14 | | | 16- | Yellowish brown (10YR5/6), wet, loose, very fine-to-coarse-grained SAND. Gray (10YR5/1), wet, loose, fine- to medium-grain | | | | | 610 | | |
| B)A | | | | 15 10 | | | 18 | SAND. Gray (10YR5/1), moist, hard, clayey SILT with sand trace gravel. | | | | | 608 | | |
| ОΒ | 20/24 83% | ss | 27-54 59-59 N=113 | 17 | | | 20 | Gray (10YR5/1), wet, loose, very fine- to fine-grain SAND. Gray (10YR4/1), moist, very hard, clayey, sandy SI | | | 1111 | Z)II | - - - | | |
| | | | | | | | 20 🗏 | with trace gravel. | i | | , | | <u> </u> | | |

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 4/21/2006 Finish: 4/25/2006 WEATHER: Overcast, cool (mid-40's) **CONTRACTOR:** Reynolds Drilling Corp. **Rig mfg/model:** CME-850 Track Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel

Helper: S. McCartney **Eng/Geo:** R. Hasenyager

HANSON

BOREHOLE ID: SB-16 Well **ID:** n/a

 Surface Elev:
 626 ft. MSL

 Completion:
 92 ft. BGS

 Station:
 877,355.0N

 2,515,080.0E

| SAMPLE TESTING | | | | | ING | j | TOPOGRAPHIC MAP INFORMATION: | WATER LEVEL INFORMATION: | | | |
|----------------|-------------------------------|------|----------------------------------|--------------|-------|--------------------------|--|--|--|------|------------------|
| ber | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | ft³) | Qu (tsf) Failure Type | Quadrangle: Coffeen, IL Township: East Fork Section 2, Tier 7N; Range 3W | $ \underline{\underline{\mathbf{y}}} = 12.80 $ - While drilling $ \underline{\underline{\mathbf{y}}} = 5.74 $ - MW16S on 6/1/06 $ \underline{\underline{\mathbf{y}}} = 51.37 $ - MW16D on 6/1/06 | | | |
| Number | Reco % Re | Type | Blow N - V RQD | Mois | Dry I | Qu (t Failu | Depth Lithologic ft. BGS Description | Borehole Elevation Detail ft. MSL Remarks | | | |
| 1A | 10/24 42% | ss | 10-96 | 8 | | | 22 — 24 — 28 — 28 — 29 — 29 — 29 — 29 — 29 — 29 | 604 | | | |
| 2A | 14/24 58% | ss | 84-132 | 10 | | 3.10 <i>BSh</i> | 24 | 602 | | | |
| 3A | 20/24 83% | SS | 41-68 82 N=150 | 10 | | 7.56 B | 26 | | | | |
| 4A | 12/24 50% | SS | 58-119 | 10 | | 9.89 B | 20 | Dusky red (7.5YR3/4) staining. | | | |
| 5A | 24/24 100% | ss | 30-48 70-71 N=118 | 9 | | 5.62 B | Gray (10YR4/1), moist, very hard, clayey, | sandy SILT | | | |
| 6A | 24/24 100% | ss | 50-54 68-93 N=122 | 9 | | | with trace gravel. [Continued from previous page] | | | | |
| 7A | 35/36 97% | CS | | 17 | | | 34 | 592 | | | |
| | 60/60 | CS | | | | | 36 | 590 | | | |
| 18A 10 | 100% | % | CS | CS | CS | | 10 | | | 38 — | 588 Wood fragmer |

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A

DATES: Start: 4/21/2006

Finish: 4/25/2006 WEATHER: Overcast, cool (mid-40's) **CONTRACTOR:** Reynolds Drilling Corp. **Rig mfg/model:** CME-850 Track Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager

HANSON

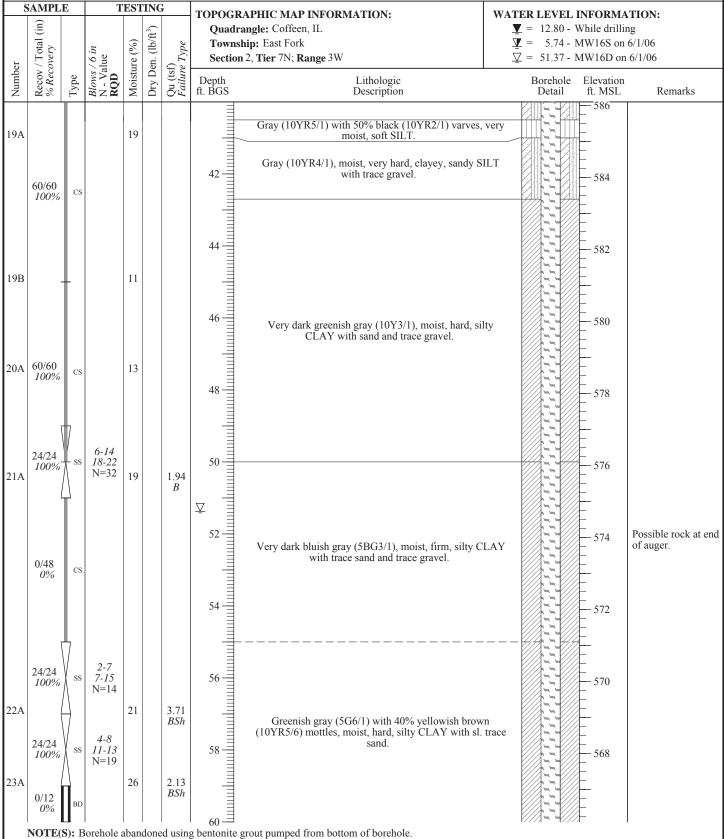
BOREHOLE ID: SB-16 **Well ID:** n/a

 Surface Elev:
 626 ft. MSL

 Completion:
 92 ft. BGS

 Station:
 877,355.0N

 2,515,080.0E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A **DATES: Start:** 4/21/2006

Finish: 4/25/2006

SAMPLE

WEATHER: Overcast, cool (mid-40's)

TESTING

CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-850 Track Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager TOPOGRAPHIC MAP INFORMATION:

HANSON

BOREHOLE ID: SB-16 Well ID: n/a

626 ft. MSL **Surface Elev: Completion:** 92 ft. BGS Station: 877,355.0N

2,515,080.0E WATER LEVEL INFORMATION:

| ber | Recov / Total (in) % Recovery | 6 | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadrangle: Coffeen, IL | | Ā Ā | WATER LEVEL INFORMATION: | | |
|--------|-------------------------------|------|---|--------------|-------------------|--------------------------|--|--|------------|---------------------------------|---|--|
| Number | Reco %Re | Type | Blow N - V RQD | Mois | Dry I | Qu (t Failu | | Lithologic Description | | Borehole Detail | Elevation ft. MSL | Remarks |
| | 0/48 | RC | | | | | 62 — | Greenish gray (5G6/1) with 40% yellowish brown (10YR5/6) mottles, moist, hard, silty CLAY with sl. sand. [Continued from previous page] | n trace | | 566 | |
| 26A | 24/24 100% | SS | N=76 | 25 | BSh | 2.72 <i>BSh</i> | Yellowish brown (10YR5/6) with 20% greenish graves (5G6/1) mottles, moist, hard, silty CLAY with trace say and trace coal fragments. | | | | 562 | |
| | 0/24 | RC | | | | | | ay sand | | 560 | | |
| 28A | 24/24 100% | ss | 15-21 21-21 N=42 | 18 | | 68 | | | 777777 | 558 | | |
| 29A | 24/24 100% | ss | 14-17 21-25 N=38 | 20 | | 2.91 BSh | 70 | | | | 556 | 70' to 79.5' - possible oxidation rinds. |
| 30A | 24/24 100% | ss | 12-21 34-35 N=55 | 18 | | 5.04 BSh | 72 | | | | - - - - - - - - - - - - - - - - - - - | |
| 31A | 24/24 100% | ss | 16-21 27-35 N=48 | 16 | | 8.15 <i>BSh</i> | 74 | Yellowish brown (10YR5/6) with zones of gray (10YR4/1) mottles, moist, hard, clayey SILT with somsand and trace gravel. | ome | | 552 | |
| 32A | 100% | CS | | 19 | | | 76 | | | | | |

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A **DATES: Start:** 4/21/2006

Finish: 4/25/2006 WEATHER: Overcast, cool (mid-40's) CONTRACTOR: Reynolds Drilling Corp.

Rig mfg/model: CME-850 Track Rig

Drilling Model: 41/" USA 11/SS & CME of

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

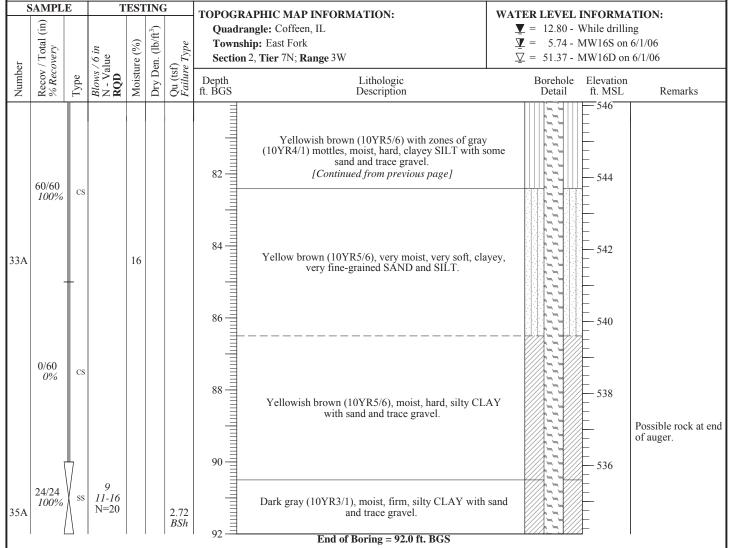
Eng/Geo: R. Hasenyager

BOREHOLE ID: SB-16

Well ID: n/a Surface Elev: 626 ft. MSL

Completion: 92 ft. BGS **Station:** 877,355.0N 2,515,080.0E

HANSON



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A DATES: Start: 5/4/2006 Finish: 5/4/2006

WEATHER: Partly sunny, cool (mid-50's)

CONTRACTOR: Reynolds Drilling Corp.
Rig mfg/model: CME-1050 ATV Rig
Drilling Method: 4¼" HSA w/SS & CME s

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney Eng/Geo: R. Hasenyager **HANSON**

 BOREHOLE ID: SB-17

 Well ID:
 MW17D

 Surface Elev:
 627 ft. MSL

 Completion:
 54 ft. BGS

 Station:
 878,659.0N

2,515,090.4E

SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: Ξ $\mathbf{V} = 11.70$ - While drilling Quadrangle: Coffeen, IL Dry Den. (lb/ft3 Recov / Total % Recovery Township: East Fork $\nabla = 6.89 - MW17S \text{ on } 6/1/06$ Qu (tsf) Failure Type Moisture (%) Blows / 6 in N - Value RQD Section 2, Tier 7N; Range 3W ∇ = 54.45 - MW17D on 6/1/06 Number Depth ft. BGS Lithologic Borehole Elevation Description Detail ft. MSL Remarks Dark grayish brown (10YR4/2), moist, soft, clayey SILT with trace sand and trace gravel. 20/24 SS 1-1 83% 626 N=21 A 29 Yellowish brown (10YR5/8), moist, soft, silty CLAY. 24/24 Gray (10YR5/1) with 40% yellowish brown (10YR5/6) 2-2 100% mottles, moist, firm, silty CLAY with little sand and trace 624 N=32A 26 1.71 gravel. 24/24 1-3 622 100% Yellowish brown (10YR5/6) with 10% gray (10YR5/1) N=23A 16 2.62 mottles, moist, firm sandy, clayey SILT. BSh1-2 1 24/24 2-3 620 100% N=418 2.33 Yellowish brown (10YR5/6) with 30% gray (10YR5/1) mottles, moist, firm sandy, clayey SILT. 24/24 2-3 100% N=318 5A 10 Yellowish brown (10YR5/6), moist, soft, very sandy, clayey SÍLT. 1-1 24/24 1-1 616 100% Gray (10YR5/1) with 30% yellowish brown (10YR5/6) N=221 0.58 6A mottles, very moist, soft, very sandy, clayey SILT. 18 6B Moderate yellowish brown (10YR5/4), wet, loose, very 12 fine- to fine-grained SAND. Yellowish brown (10YR5/6), wet, dense, silty, very fine-24/24 21 to fine-grained SAND. 3-7 100% Yellowish brown (10YR5/6), very moist, dense, silty, 7B 19 very fine-grained SAND. Yellowish brown (10YR5/6) wet, dense, fine- to 84 15 medium-grained SAND. 24/24 Moderate yellowish brown (10YR5/4), wet, dense, SILT 5-7 612 100% and very fine-grained SAND. N = 108B13 Yellowish brown (10YR5/6), moist, clayey SILT and very fine-grained SAND with trace gravel. 8C 13 0-6 Yellowish brown (10YR5/6), wet, loose, very fine- to 24/24 6-6 medium-grained SAND. 610 100% N=129A 17 Yellowish brown (10YR5/6), wet, loose, very fine- to 0-2 fine-grained SAND. 24/24 2-3 SS 608 100% Yellowish brown (10YR5/6), wet, sl. dense, SILT with N=410A 19 some very fine-grained SAND. Gray (10YR5/1), wet, sl. dense, SILT with some very 10B 23 NOTE(S): CME-1050 had 280# hammer for SPT.

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A **DATES: Start:** 5/4/2006 Finish: 5/4/2006

WEATHER: Partly sunny, cool (mid-50's)

CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

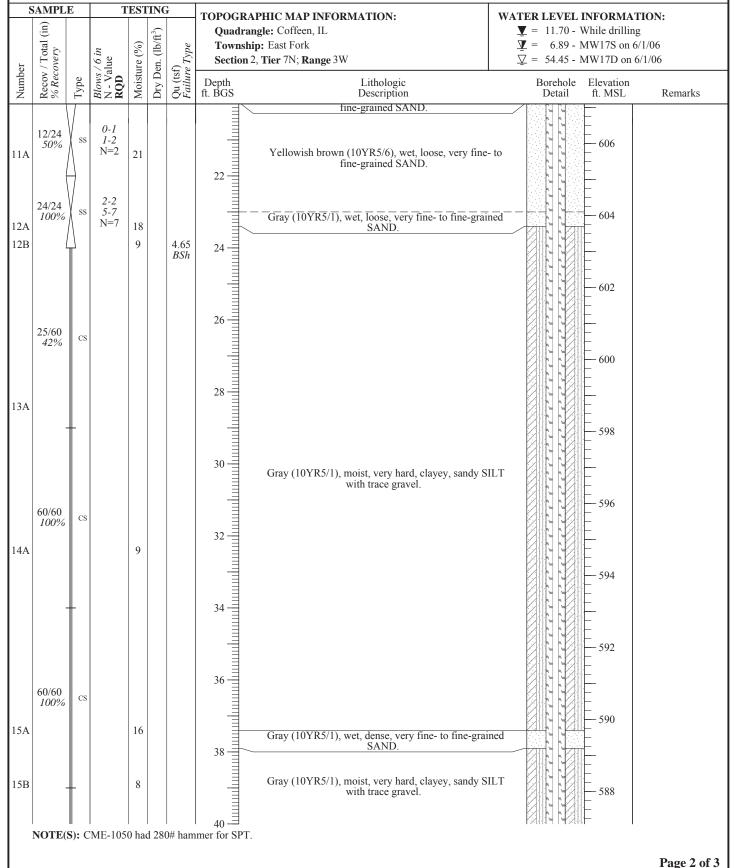
FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager



BOREHOLE ID: SB-17 Well ID: MW17D

Surface Elev: 627 ft. MSL 54 ft. BGS **Completion:** Station: 878,659.0N 2,515,090.4E



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A

DATES: Start: 5/4/2006

Finish: 5/4/2006 **WEATHER:** Partly sunny, cool (mid-50's)

CONTRACTOR: Reynolds Drilling Corp. **Rig mfg/model:** CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager



BOREHOLE ID: SB-17 Well ID: MW17D

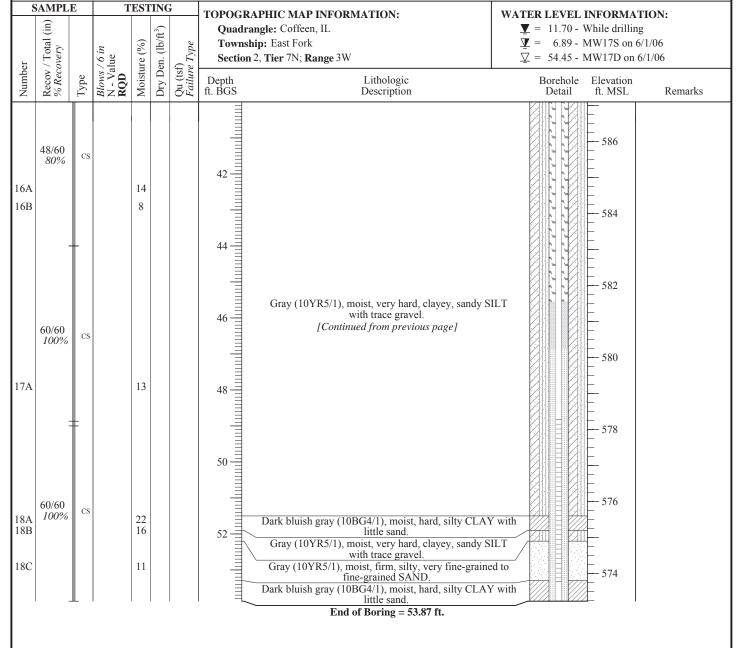
 Well ID:
 MW17D

 Surface Elev:
 627 ft. MSL

 Completion:
 54 ft. BGS

 Station:
 878,659.0N

 2,515,090.4E



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility
Location: Coffeen, Illinois

Project: 05S3004A DATES: Start: 5/4/2006 Finish: 5/4/2006

Finish: 5/4/2006 **WEATHER:** Partly sunny, cool (mid-50's) CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-1050 ATV Rig Drilling Method: 4¼" HSA (blind drill)

FIELD STAFF: Driller: K. Doetzel
Helper: S. McCartney
Eng/Geo: R. Hasenyager

HANSON

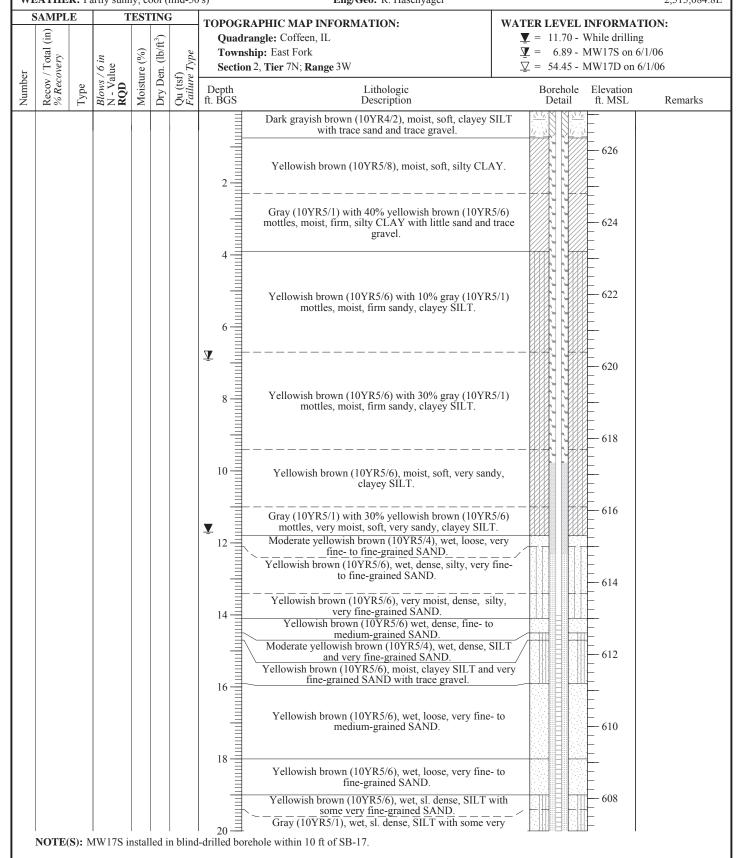
BOREHOLE ID: SB-17a **Well ID:** MW17S

 Surface Elev:
 627 ft. MSL

 Completion:
 24 ft. BGS

 Station:
 878,658.5N

 2,515,084.8E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility Location: Coffeen, Illinois

Project: 05S3004A **DATES: Start:** 5/4/2006 Finish: 5/4/2006

WEATHER: Partly sunny, cool (mid-50's)

CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-1050 ATV Rig **Drilling Method:** 41/4" HSA (blind drill)

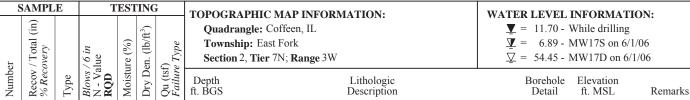
FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: SB-17a Well ID: MW17S

Surface Elev: 627 ft. MSL **Completion:** 24 ft. BGS 878,658.5N **Station:** 2,515,084.8E





End of Boring = 24.11 ft. BGS See SB-17 for sample & testing details

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A DATES: Start: 5/4/2006 Finish: 5/4/2006

WEATHER: Partly sunny, cool (mid-50's)

CONTRACTOR: Reynolds Drilling Corp.
Rig mfg/model: CME-1050 ATV Rig
Drilling Method: 4¼" HSA w/SS & CME s

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney Eng/Geo: R. Hasenyager **HANSON**

 BOREHOLE ID: SB-17

 Well ID:
 MW17D

 Surface Elev:
 627 ft. MSL

 Completion:
 54 ft. BGS

 Station:
 878,659.0N

2,515,090.4E

SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: Ξ $\mathbf{V} = 11.70$ - While drilling Quadrangle: Coffeen, IL Dry Den. (lb/ft3 Recov / Total % Recovery Township: East Fork $\nabla = 6.89 - MW17S \text{ on } 6/1/06$ Qu (tsf) Failure Type Moisture (%) Blows / 6 in N - Value RQD Section 2, Tier 7N; Range 3W ∇ = 54.45 - MW17D on 6/1/06 Number Depth ft. BGS Lithologic Borehole Elevation Description Detail ft. MSL Remarks Dark grayish brown (10YR4/2), moist, soft, clayey SILT with trace sand and trace gravel. 20/24 SS 1-1 83% 626 N=21 A 29 Yellowish brown (10YR5/8), moist, soft, silty CLAY. 24/24 Gray (10YR5/1) with 40% yellowish brown (10YR5/6) 2-2 100% mottles, moist, firm, silty CLAY with little sand and trace 624 N=32A 26 1.71 gravel. 24/24 1-3 622 100% Yellowish brown (10YR5/6) with 10% gray (10YR5/1) N=23A 16 2.62 mottles, moist, firm sandy, clayey SILT. BSh1-2 1 24/24 2-3 620 100% N=418 2.33 Yellowish brown (10YR5/6) with 30% gray (10YR5/1) mottles, moist, firm sandy, clayey SILT. 24/24 2-3 100% N=318 5A 10 Yellowish brown (10YR5/6), moist, soft, very sandy, clayey SÍLT. 1-1 24/24 1-1 616 100% Gray (10YR5/1) with 30% yellowish brown (10YR5/6) N=221 0.58 6A mottles, very moist, soft, very sandy, clayey SILT. 18 6B Moderate yellowish brown (10YR5/4), wet, loose, very 12 fine- to fine-grained SAND. Yellowish brown (10YR5/6), wet, dense, silty, very fine-24/24 21 to fine-grained SAND. 3-7 100% Yellowish brown (10YR5/6), very moist, dense, silty, 7B 19 very fine-grained SAND. Yellowish brown (10YR5/6) wet, dense, fine- to 84 15 medium-grained SAND. 24/24 Moderate yellowish brown (10YR5/4), wet, dense, SILT 5-7 612 100% and very fine-grained SAND. N = 108B13 Yellowish brown (10YR5/6), moist, clayey SILT and very fine-grained SAND with trace gravel. 8C 13 0-6 Yellowish brown (10YR5/6), wet, loose, very fine- to 24/24 6-6 medium-grained SAND. 610 100% N=129A 17 Yellowish brown (10YR5/6), wet, loose, very fine- to 0-2 fine-grained SAND. 24/24 2-3 SS 608 100% Yellowish brown (10YR5/6), wet, sl. dense, SILT with N=410A 19 some very fine-grained SAND. Gray (10YR5/1), wet, sl. dense, SILT with some very 10B 23 NOTE(S): CME-1050 had 280# hammer for SPT.

CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A **DATES: Start:** 5/4/2006 Finish: 5/4/2006

WEATHER: Partly sunny, cool (mid-50's)

CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

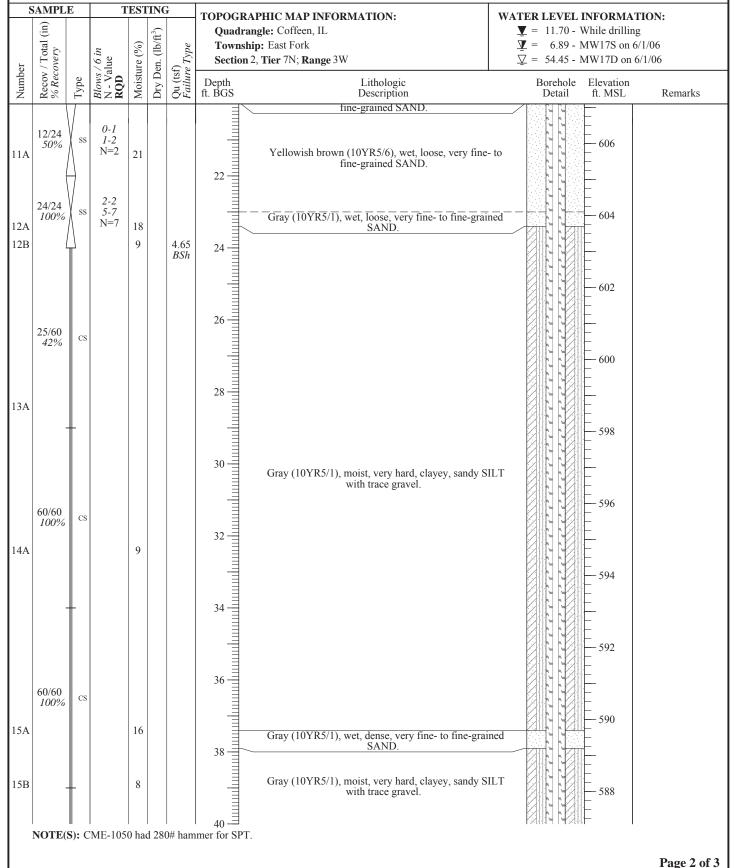
FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager



BOREHOLE ID: SB-17 Well ID: MW17D

Surface Elev: 627 ft. MSL 54 ft. BGS **Completion:** Station: 878,659.0N 2,515,090.4E



CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois
Project: 05S3004A

DATES: Start: 5/4/2006

Finish: 5/4/2006 **WEATHER:** Partly sunny, cool (mid-50's)

CONTRACTOR: Reynolds Drilling Corp. **Rig mfg/model:** CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: SB-17

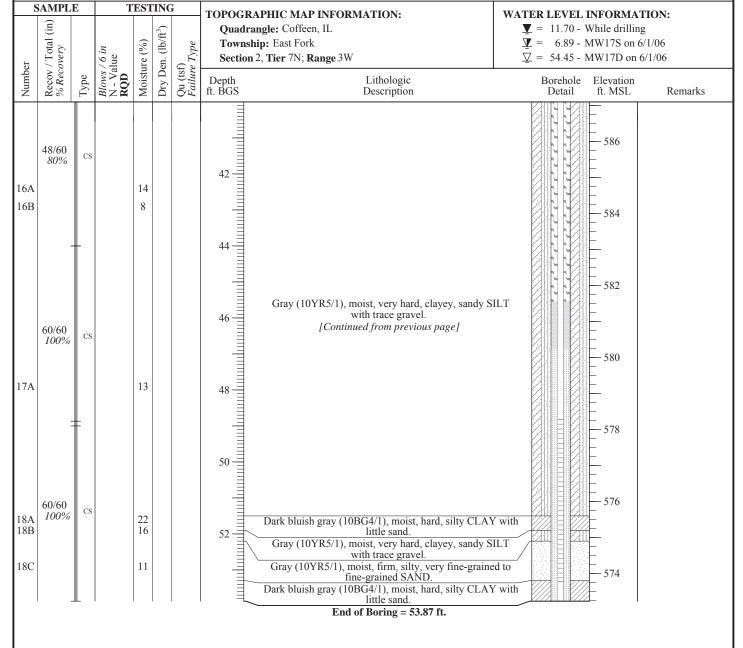
 Well ID:
 MW17D

 Surface Elev:
 627 ft. MSL

 Completion:
 54 ft. BGS

 Station:
 878,659.0N

2,515,090.4E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility Location: Coffeen, Illinois

Project: 05S3004A **DATES: Start:** 5/11/2006

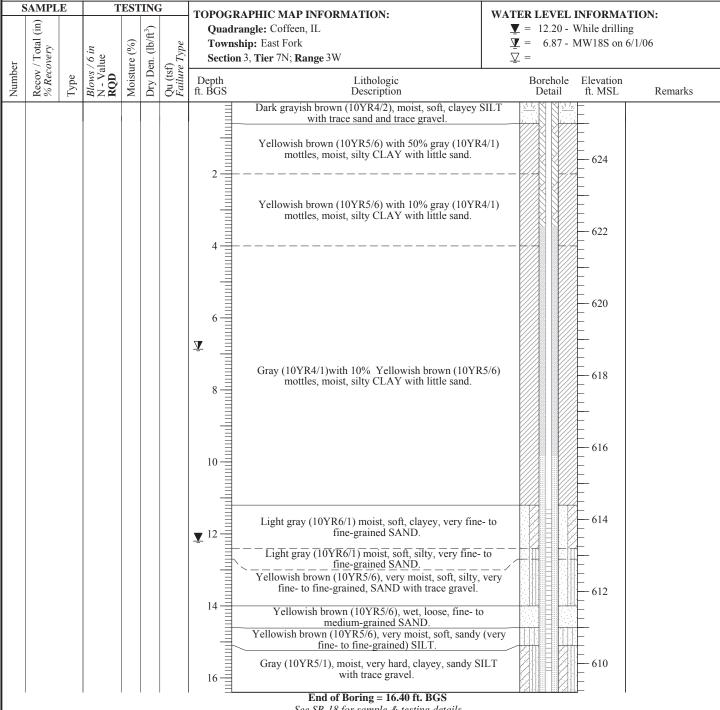
Finish: 5/11/2006 WEATHER: Partly sunny, cool (mid-50's) **CONTRACTOR:** Reynolds Drilling Corp. Rig mfg/model: CME-1050 ATV Rig **Drilling Method:** 41/4" HSA (blind drill)

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: R. Hasenyager

BOREHOLE ID: SB-18a Well ID: MW18S

Surface Elev: 626 ft. MSL 16 ft. BGS **Completion: Station:** 878,604.7N 2,513,745.2E



See SB-18 for sample & testing details

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A DATES: Start: 5/11/2006

Finish: 5/11/2006 **WEATHER:** Partly sunny, cool (mid-50's) **CONTRACTOR:** Reynolds Drilling Corp. **Rig mfg/model:** CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel
Helper: S. McCartney

Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: SB-18 **Well ID:** n/a

 Surface Elev:
 626 ft. MSL

 Completion:
 54 ft. BGS

 Station:
 878,605.0N

 2,513,750.0E

Page 1 of 3

SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: Ξ $\mathbf{V} = 12.20$ - While drilling Quadrangle: Coffeen, IL Dry Den. (lb/ft3 Recov / Total % Recovery Township: East Fork $\Psi = 6.87 - MW18S \text{ on } 6/1/06$ Qu (tsf) Failure Type Moisture (%) Blows / 6 in N - Value RQD Section 3, Tier 7N; Range 3W Number Depth ft. BGS Lithologic Borehole Elevation Description Detail Remarks Dark grayish brown (10YR4/2), moist, soft, clayey SILT with trace sand and trace gravel. 0 - 118/24 SS 1-1 75% Yellowish brown (10YR5/6) with 50% gray (10YR4/1) N=21 A 24 1 31 mottles, moist, silty CLAY with little sand. 624 BSh1-2 2-2 24/24 Yellowish brown (10YR5/6) with 10% gray (10YR4/1) 100% mottles, moist, silty CLAY with little sand. N=42A 28 1.78 622 24/24 2-2 100% 3A 23 1.32 620 BSh $\bar{\pmb{\Lambda}}$ 24/24 24 1.09 1-2 N=2 100% В Gray (10YR4/1)with 10% Yellowish brown (10YR5/6) 618 mottles, moist, silty CLAY with little sand. 5A 28 24/24 100% 616 0-0 24/24 1-2 100% N=121 0.39 6A Light gray (10YR6/1) moist, soft, clayey, very fine- to 614 **▼** 12 fine-grained SAND. 7A 17 Light gray (10YR6/1) moist, soft, silty, very fine- to 24/24 <u>fine-grained SAND.</u> 9-15 100% Yellowish brown (10YR5/6), very moist, soft, silty, very N = 14fine- to fine-grained, SAND with trace gravel. 612 7B 15 Yellowish brown (10YR5/6), wet, loose, fine- to 8A 14 medium-grained SAND. 8-9 Yellowish brown (10YR5/6), very moist, soft, sandy (very 24/24 8B 11 9-10 fine- to fine-grained) SILT. 100% N = 18610 9 8C 24/36 Gray (10YR5/1), moist, very hard, clayey, sandy SILT 608 67% with trace gravel. 9A NOTE(S): Borehole abandoned using bentonite grout pumped from bottom of borehole. CME-1050 had 280# hammer for SPT.

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 5/11/2006 **Finish:** 5/11/2006

WEATHER: Partly sunny, cool (mid-50's)

CONTRACTOR: Reynolds Drilling Corp. **Rig mfg/model:** CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager



BOREHOLE ID: SB-18 **Well ID:** n/a

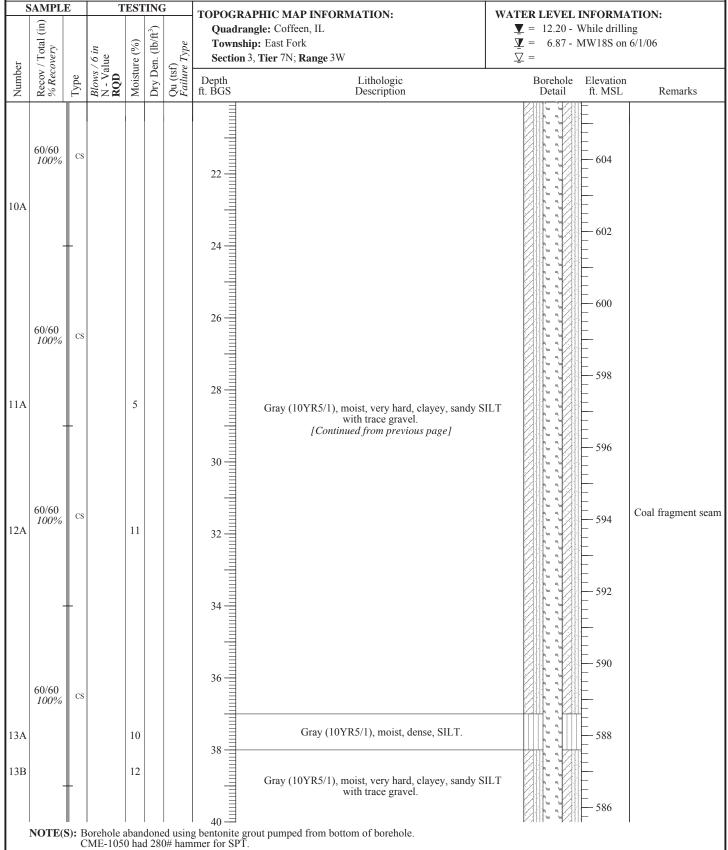
 Surface Elev:
 626 ft. MSL

 Completion:
 54 ft. BGS

 Station:
 878,605.0N

 2,513,750.0E

Page 2 of 3



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

DATES: Start: 5/11/2006 **Finish:** 5/11/2006

WEATHER: Partly sunny, cool (mid-50's)

CONTRACTOR: Reynolds Drilling Corp. Rig mfg/model: CME-1050 ATV Rig

Drilling Method: 41/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: K. Doetzel Helper: S. McCartney

Eng/Geo: R. Hasenyager TOPOGRAPHIC MAP INFORMATION:

BOREHOLE ID: SB-18 Well ID: n/a

Surface Elev: 626 ft. MSL **Completion:** 54 ft. BGS **Station:** 878,605.0N

HANSON

2,513,750.0E

| | SAMPLI | E | Т | EST | INC | j | TOPOGR | APHIC MAP INFORMATION: | WATER LEVEL INFORMATION: | | | |
|--------|----------------------------------|------|----------------------------------|--------------|-------------------|--------------------------|-----------------------------|---|--------------------------|------------------------------|--|--|
| er | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadra Townsl Section | ingle: Coffeen, IL ip: East Fork 3, Tier 7N; Range 3W | ▼ = 12.20 - | | | |
| Number | Recov % Rea | Type | Blows N - V RQD | Moist | Dry D | Qu (ts Failu | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL Remarks | | |
| 14A | 60/60 100% | CS | | 13 | | | 42 | | | Appears more clayey | | |
| 15.4 | 60/60 | CS | | 12 | | | 44 | Gray (10YR5/1), moist, very hard, clayey, sandy SI with trace gravel. [Continued from previous page] | LT | 580 | | |
| 15A | _ | | | 13 | | | 50 | | | 576 | | |
| 16B | 60/60 100% | CS | | 22 | | | 52 | Greenish gray (10BG5/1), moist, firm, silty CLAY v little sand and trace gravel. | vith | 574 | | |
| | | _ | ı | I | I | l l | 54 — | End of Boring = 54.0 ft. | V///I= \$/// | ⊿ I | | |

CLIENT: AEG Coffeen Power Station **Site:** Ash Pond Investigation

Location: Coffeen, IL Project: 05S3004B

NOTE(S):

DATES: Start: 5/1/2007 Finish: 5/1/2007 WEATHER: Partly sunny, warm **CONTRACTOR**: Reynolds Drilling Corp. **Rig mfg/model**: CME-550 ATV Drill

Drilling Method: 41/4" Hollow stem auger with split spoon

sampler

FIELD STAFF: Driller: A. Rachford Helper: M. Brown

Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID:SB20 Well ID: MW20S

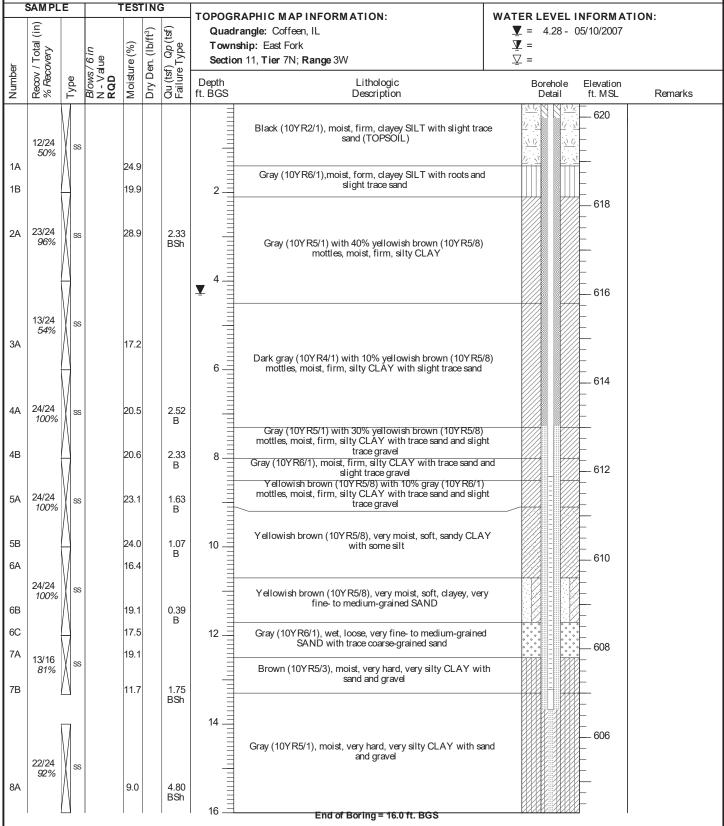
 Surface Elev:
 620.30 ft. MSL

 Completion:
 16.00 ft. BGS

 Station:
 874,226.44N

ation: 874,226.44N 2,515,867.87E

Page 1 of 1



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois Project: 05S3004A

DATES: Start: 10/8/2010 Finish: 10/8/2010

WEATHER: Sunny, mild

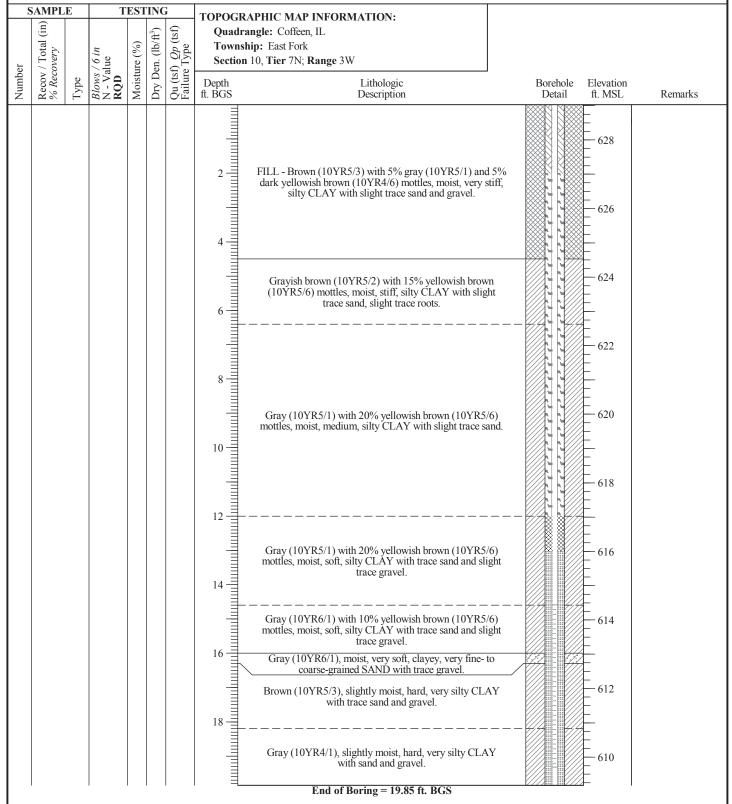
CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill **Drilling Method:** 41/4" HSA (blind drill)

FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: R. Hasenyager

BOREHOLE ID: R104 Well ID: R104

> Surface Elev: 629.03 ft. MSL Completion: 19.85 ft. BGS **Station:** 875,857.80N 2,514,503.41E



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A **DATES:** Start: 2/15/2010

Finish: 2/15/2010

WEATHER: Overcast, cold, windy (lo-20's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 4½" HSA w/SS samplers

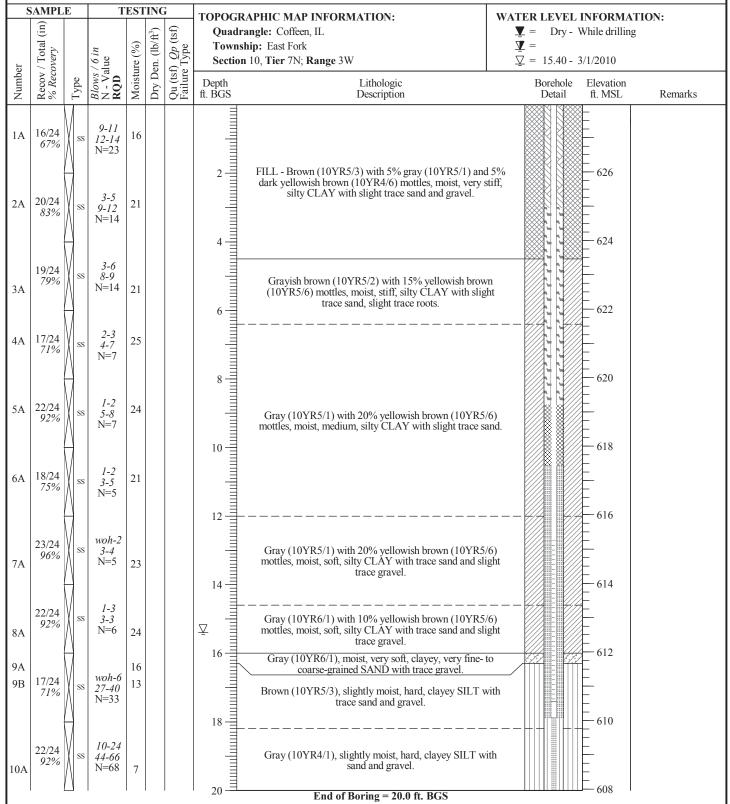
FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby **Eng/Geo:** S. Suzanna Simpson

HANSON

BOREHOLE ID: G104 **Well ID:** G104

Surface Elev: 627.96 ft. MSL Completion: 20.00 ft. BGS Station: 875,849.26N 2.514.504.98E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/15/2010

Finish: 10/15/2010 WEATHER: Sunny (mid-50's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 41/4" HSA (blind drill)

FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: R. Hasenyager

HANSON

BOREHOLE ID: R201 **Well ID:** R201

 Surface Elev:
 624.02 ft. MSL

 Completion:
 17.22 ft. BGS

 Station:
 877,925.26N

 2,514,841.96E

TESTING SAMPLE TOPOGRAPHIC MAP INFORMATION: Qu (tsf) *Qp* (tsf) Failure Type Dry Den. (lb/ft³) Quadrangle: Coffeen, IL Recov / Total (% Recovery Moisture (%) Township: East Fork Blows / 6 in N - Value RQD Section 2, Tier 7N; Range 3W Number Lithologic Borehole Elevation ft. BGS Description Detail ft. MSL Remarks Very dark grayish brown (10YR3/2), moist, soft, friable, clayey SILT, slight trace sand and gravel Dark brown (10YR3/3), moist, soft, silty CLAY 622 Yellowish brown (10YR5/8) with 20% gray (10YR5/1) mottles, moist, firm, silty CLAY, trace sand, slight trace gravel 620 Gray (10YR5/1) with 5% yellowish brown (10YR5/6) mottles, moist, firm, silty CLAY, sand and trace gravel 618 Gray (10YR5/1), moist, firm, sandy CLAY, trace silt and slight trace gravel Yellowish brown (10YR5/8) with 10% gray (10YR5/1) mottles, moist, firm, sandy CLAY, trace gravel 614 Yellowish brown (10YR5/8), wet, soft, silty SAND, trace gravel Yellowish brown (10YR5/8), moist, firm, clayey SILT Greenish gray (5GY6/1), moist, firm, interbedded clayey SILT and SILT 610 Yellowish brown (10YR5/8), wet, soft, fine-to coarse-grained SAND, slight trace gravel 608 Yellowish brown (10YR5/8), wet, firm, very fine-to __fine-grained silty SAND Gray (10YR5/1), wet, soft, SILT Gray (10YR5/1), wet, soft, fine- to coarse-grained SAND, slight trace gravel Gray (10YR5/1), moist, hard, very silty CLAY, trace sand and gravel End of Boring = 17.22 ft. BGS

CLIENT: Illinois Power Generating Co.

TESTING

Site: Coffeen Power Station - Gypsum Mgmt Facility

Quadrangle: Coffeen, IL

Location: Coffeen, IL

SAMPLE

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Project: 15E0161A **DATES: Start:** 3/20/2017

Finish: 3/20/2017 WEATHER: Sunny, mild, (mid-60s) **CONTRACTOR:** Bulldog Drilling Rig mfg/model: CME-550 ATV Drill

Drilling Method: 41/4" HSA (blind drill)

FIELD STAFF: Driller: J. Gates Helper: C. Clines

Eng/Geo: R. Hasenyager TOPOGRAPHIC MAP INFORMATION:

WATER LEVEL INFORMATION:

BOREHOLE ID: R205

Well ID: R205

Surface Elev: 621.91 ft. MSL

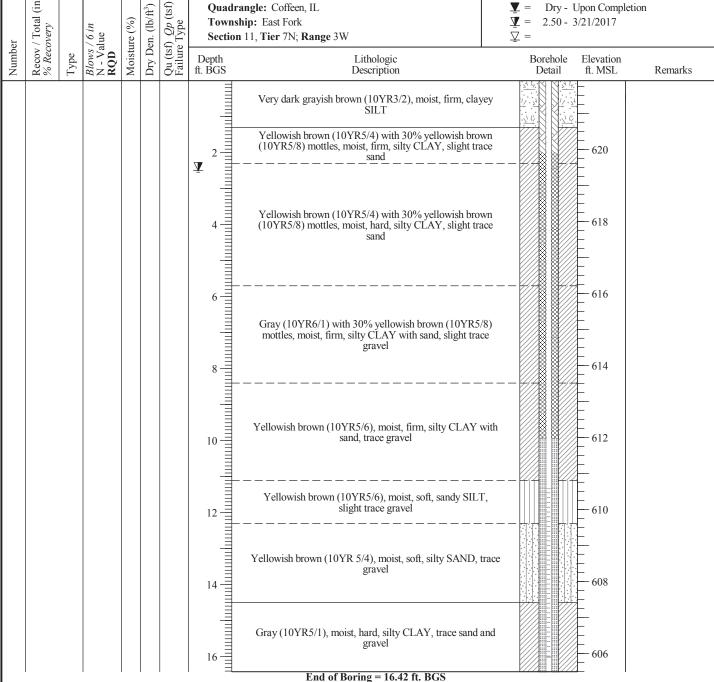
Completion: 16.42 ft. BGS

Station: 875,548.77N

2,515,910.12E

▼ = Dry - Upon Completion

 Ψ = 2.50 - 3/21/2017



CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 2/21/2008 **Finish:** 2/21/2008

WEATHER: Overcast, cold

CONTRACTOR: Testing Service Corp.
Rig mfg/model: CME-650 Track Drill

Drilling Method: 31/4" HSA w/SS & CME samplers

FIELD STAFF: Driller: B. Williamson Helper: R. Keedy

Eng/Geo: .

BOREHOLE ID: G205

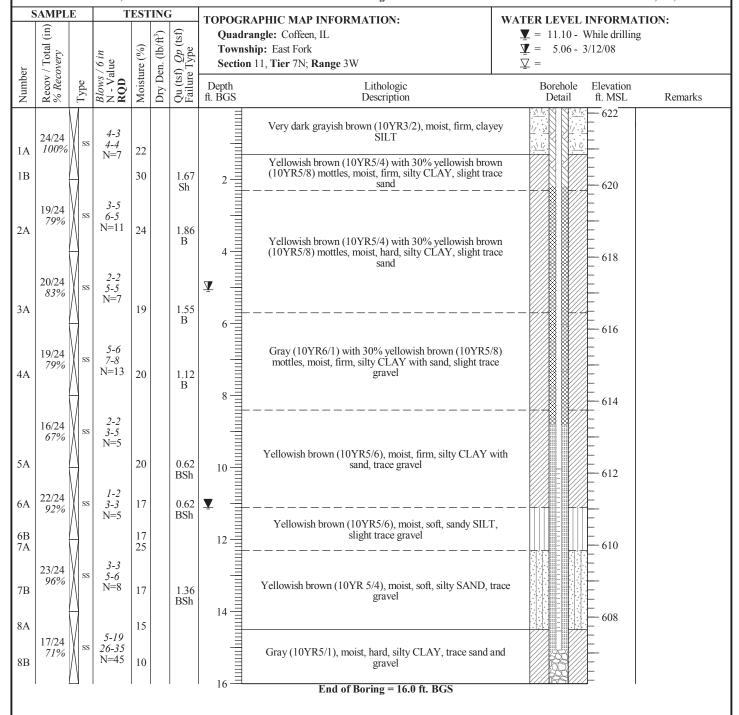
Well ID: G205

 Surface Elev:
 622.15 ft. MSL

 Completion:
 16.00 ft. BGS

 Station:
 875,550.19N

 2,515,914.87E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 2/10/2010 **Finish:** 2/10/2010

WEATHER: Overcast, wind 15mph, ~10-20F

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby

Eng/Geo: .

HANSON

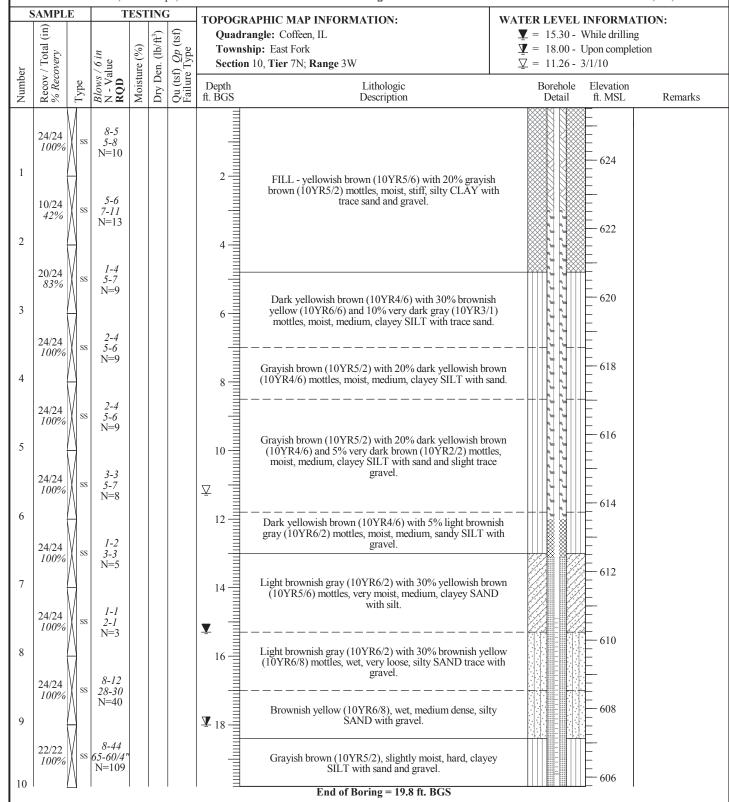
BOREHOLE ID: T127 Well ID: T127

 Surface Elev:
 625.53 ft. MSL

 Completion:
 19.80 ft. BGS

 Station:
 875,359.21N

 2.513,911.02E



CLIENT: AEG Coffeen Power Station Site: CCB Management Facility

Location: Coffeen, Illinois

Project:

DATES: Start: 2/9/2010

Finish: 2/9/2010

WEATHER: Cold, windy, snow (lo-20's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill

Drilling Method: 41/4" HSA w/SS samplers

FIELD STAFF: Driller: T. List

Helper: M. Herbst/S. Hamby

Eng/Geo: S. Simpson

HANSON

BOREHOLE ID: T128 Well ID: T128

Surface Elev: 626.27 ft. MSL **Completion:** 22.00 ft. BGS

> **Station:** 875,509.70N 2,513,909.45E

| | SAMPLE TESTING | | | | | | TOPOGRA | APHIC MAP INFORMATION: | WATER LEVEL INFORMATION: | | | | |
|------------|----------------------------------|------|----------------------------------|--------------|-------------------|--------------------------|------------------|--|---|-------------------|---------|--|--|
| er | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Moisture (%) | Dry Den. (lb/ft³) | Qu (tsf) Failure Type | Quadra Townsh | ngle: Coffeen, IL lip: East Fork 10, Tier 7N; Range 3W | $\underline{\underline{V}} = 16.84 - \underline{\underline{V}} = \underline{\underline{V}} = \underline{\underline{V}} = 12.35 - \underline{\underline{V}}$ | - | | | |
| Number | Recov % Rec | Type | Blows N - V RQD | Moist | Dry D | Qu (ts Failun | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks | | |
| 1A | 12/24 50% | SS | 37-17 15-18 N=32 | 14 | | | 2 | FILL - Brown (10YR5/3) with 5% gray (10YR5/1) and yellowish brown (10YR5/6) mottles, moist, hard (frozen silty CLAY with trace sand and slight trace gravel. FILL - Gray (10YR5/1) with 15% yellowish brown (10YR5/6) mottles, moist, hard (frozen), silty CLAY with trace sand and gravel. | en), | 626 | | | |
| 2A | 7/24 29% | SS | 4-7 7-13 N=14 | | | | 4-3 | FILL - Brown (10YR5/3) with 10% gray (10YR5/1) a 5% yellowish brown (10YR5/6) mottles, moist, stiff, s CLAY with slight trace sand and gravel. | nd ilty | 624 | | | |
| 3A | 12/24 50% | SS | 3-4 6-8 N=10 | 26 | | | 6 | Gray (10YR5/1) with 20% yellowish brown (10YR5/mottles, moist, stiff, silty CLAY with slight trace san slight trace roots. | 6) d, | 622 | | | |
| 4A | 19/24 79% | SS | 2-4 5-7 N=9 | 24 | | | | | | 620 | | | |
| 5A | 22/24 92% | SS | 1-3 4-5 N=7 | 20 | | | 8 = 10 = 10 | Gray (10YR5/1) with 20% yellowish brown (10YR5/mottles, moist, stiff, silty CLAY with trace sand and sl trace gravel. | 6) ight | 618 | | | |
| 6A | 22/24 92% | SS | <i>1-3</i> 5-5 N=8 | 20 | | | 12 | | 77 | 616 | | | |
| 7A | 22/24 92% | SS | 2-3 4-5 N=7 | 19 | | | <u> </u> | | | 614 | | | |
| 8A | 20/24 83% | SS | 2-2 3-3 N=5 | 18 | | | 16 - | Gray (10YR6/1) with 30% yellowish brown (10YR5/mottles, moist, medium, silty CLAY with trace sand a slight trace gravel. | | 612 | | | |
| 9A 9B | 22/24 92% | SS | woh-1 8-7 N=9 | 19 18 | | | ¥ 1 | Brown (10YR5/3), moist, soft, clayey SAND with sligtrace gravel. Gray (10YR6/1), wet, loose, silty, very fine- to coarse-grained SAND. Brown (10YR5/3), wet, loose, silty, very fine- to | ght | 610 | | | |
| 10A 10B | | SS | 3-10 13-11 N=23 | 17 | | | 18 - | Brown (10YR5/3), slightly moist, very stiff, clayey SI with trace sand and gravel. | LT | 608 | | | |

CLIENT: AEG Coffeen Power Station
Site: CCB Management Facility

Location: Coffeen, Illinois

Project:

DATES: Start: 2/9/2010

Finish: 2/9/2010

FIELD STAFF: Driller: T. List

CONTRACTOR: Layne-Western Co **Rig mfg/model:** CME-750 ATV Drill

Drilling Method: 4¹/₄" HSA w/SS samplers

Helper: M. Herbst/S. Hamby

HANSON

BOREHOLE ID: T128

Well ID: T128 Surface Elev: 626.27 ft. MSL

Completion: 22.00 ft. BGS Station: 875,509.70N 2,513,909.45E

| | WE | EATHEI | R: C | old, wind | y, sn | ow (| lo-20's |) | Eng/Geo: S. Simpson | 2,513,909.45E | | | |
|----|--------|----------------|------|------------------------|----------|----------|---------------------|------------------|--|---|--|--|--|
| I | S | SAMPL | E | Т | EST | ING | j | TOPOGRA | PHIC MAP INFORMATION: | WATER LEVEL INFORMATION: | | | |
| 1 | | (in) | | | | (£3) | | Quadrar | gle: Coffeen, IL | $\mathbf{\underline{V}} = 16.84$ - While drilling | | | |
| 1 | | Total ery | | in | (%) | (lb/ft³) | уре | | p: East Fork | $\bar{m{\Lambda}}$ = | | | |
| 1 | er | 3 ~ | | / 6 alue | 43 | en. | | Section 1 | 0, Tier 7N; Range 3W | $\nabla = 12.35 - 3/1/10$ | | | |
| | Number | Recov % Rec | Type | Blows N - Va RQD | Moisture | Dry Den. | Qu (tsf) Failure | Depth ft. BGS | Lithologic Description | Borehole Elevation Detail ft. MSL Remarks | | | |
| | 11A | 24/24 100% | SS | 8-16 18-25 N=34 | 16 | | | 22 | Dark gray (10YR4/1), slightly moist, hard, clayey SI with trace sand and gravel. | LT | | | |
| -1 | | | | | | | | | End of Boring = 22.0 ft. BGS | | | | |

CLIENT: AEG Coffeen Power Station **Site:** CCB Management Facility

Location: Coffeen, Illinois **Project:** 05S3004A

DATES: Start: 10/15/2010

Finish: 10/15/2010 WEATHER: Sunny (mid-50's)

CONTRACTOR: Layne-Western Co Rig mfg/model: CME-750 ATV Drill Drilling Method: 4¼" HSA w/SS samplers

FIELD STAFF: Driller: D. Mahurin Helper: J. Litsch/D. Smail

Eng/Geo: R. Hasenyager

HANSON

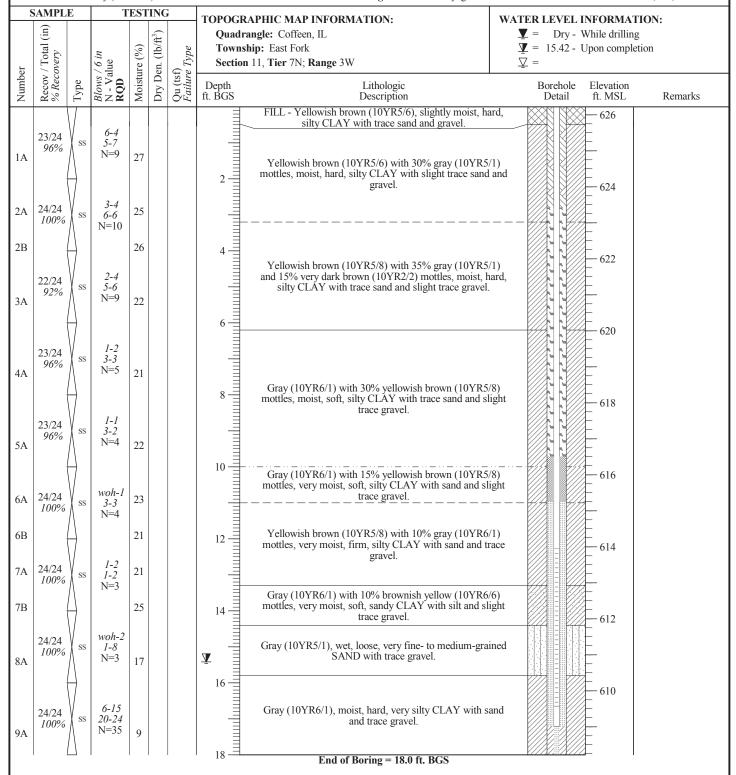
BOREHOLE ID: T202 **Well ID:** T202

 Surface Elev:
 626.22 ft. MSL

 Completion:
 18.00 ft. BGS

 Station:
 876,699.42N

 2,514,895.01E



CLIENT: Natural Resources Technology, Inc. Site: Coffeen Power Station - Ash Pond 2 Location: 134 CIPS Lane, Coffeen, IL 62017

Project: 16E0080

DATES: Start: 8/17/2016 Finish: 8/17/2016

WEATHER: Hazy, (low-80s)

CONTRACTOR: Bulldog Drilling, Inc. Rig mfg/model: CME-750 ATV Drill Drilling Method: 4 1/4" Hollow Stem Auger

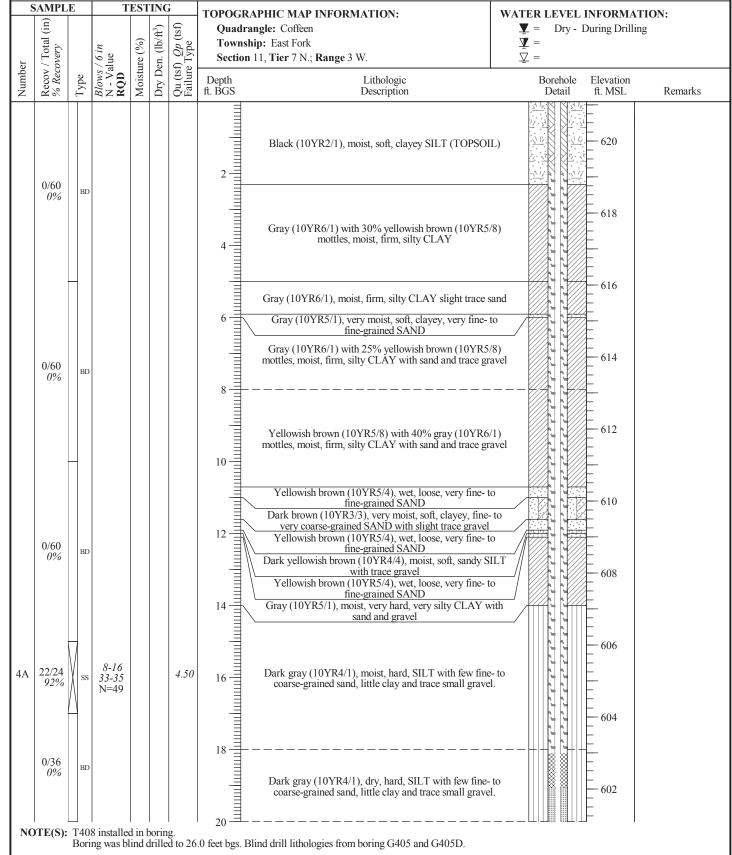
FIELD STAFF: Driller: J. Dittmaier Helper: M. Hill

Eng/Geo: K. Theesfeld



BOREHOLE ID: T408 Well ID: T408

> Surface Elev: 621.09 ft. MSL Completion: 25.92 ft. BGS **Station:** 2,515,314.91N 2,515,314.91E



CLIENT: Natural Resources Technology, Inc. Site: Coffeen Power Station - Ash Pond 2 Location: 134 CIPS Lane, Coffeen, IL 62017

Project: 16E0080

DATES: Start: 8/17/2016 Finish: 8/17/2016

WEATHER: Hazy, (low-80s)

CONTRACTOR: Bulldog Drilling, Inc. Rig mfg/model: CME-750 ATV Drill Drilling Method: 4 1/4" Hollow Stem Auger

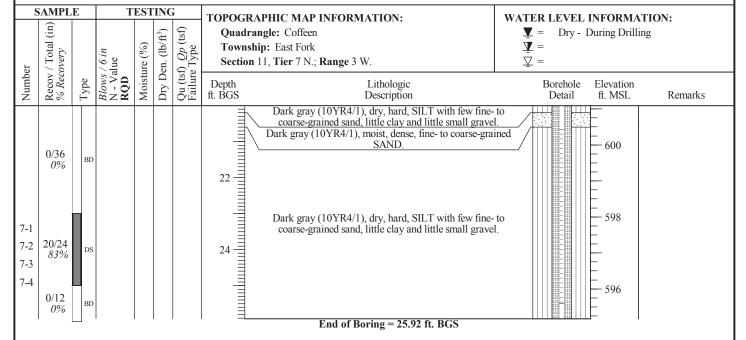
FIELD STAFF: Driller: J. Dittmaier Helper: M. Hill

Eng/Geo: K. Theesfeld



BOREHOLE ID: T408 Well ID: T408

> Surface Elev: 621.09 ft. MSL Completion: 25.92 ft. BGS **Station:** 2,515,314.91N 2,515,314.91E



CLIENT: Natural Resources Technology, Inc.
Site: Coffeen Power Station - Ash Pond 2
Location: 134 CIPS Lane, Coffeen, IL 62017

Project: 16E0080

DATES: Start: 8/19/2016 **Finish:** 8/19/2016

WEATHER: Cloudy, (70s)

CONTRACTOR: Bulldog Drilling, Inc.
Rig mfg/model: CME-750 ATV Drill
Drilling Method: 4 1/4" Hollow Stem Auger

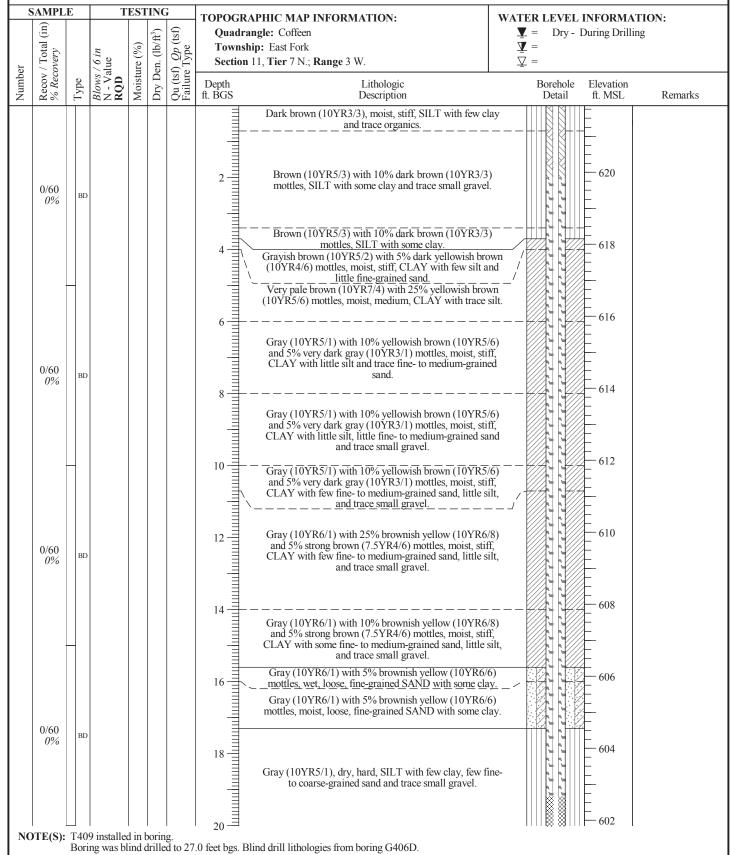
FIELD STAFF: Driller: J. Dittmaier Helper: M. Hill

Eng/Geo: K. Theesfeld



BOREHOLE ID: T409 **Well ID:** T409

Surface Elev: 621.85 ft. MSL Completion: 26.99 ft. BGS Station: 2,514,693.89N 2,514,693.89E



CLIENT: Natural Resources Technology, Inc. Site: Coffeen Power Station - Ash Pond 2 Location: 134 CIPS Lane, Coffeen, IL 62017

Project: 16E0080

DATES: Start: 8/19/2016 Finish: 8/19/2016

WEATHER: Cloudy, (70s)

CONTRACTOR: Bulldog Drilling, Inc. Rig mfg/model: CME-750 ATV Drill Drilling Method: 4 1/4" Hollow Stem Auger

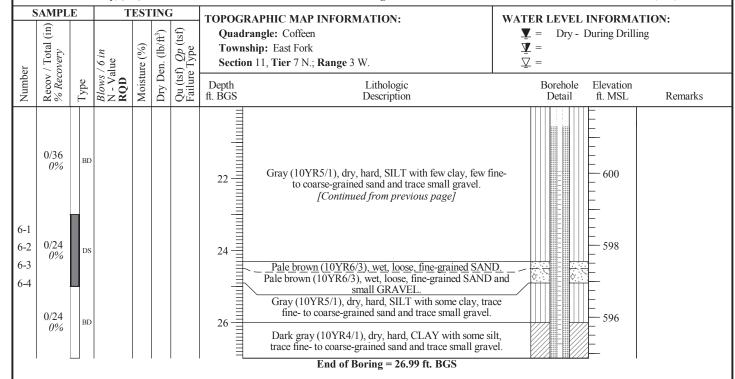
FIELD STAFF: Driller: J. Dittmaier Helper: M. Hill

Eng/Geo: K. Theesfeld



BOREHOLE ID: T409 Well ID: T409

> Surface Elev: 621.85 ft. MSL Completion: 26.99 ft. BGS **Station:** 2,514,693.89N 2,514,693.89E



CLIENT: Illinois Power Holdings **Site:** Coffeen Power Station

Location: Coffeen, Montgomery County, Illinois

NOTE(S): Monitoring well TA31 installed in borehole.

Project: 14E0078

DATES: Start: 10/28/2014 **Finish:** 10/28/2014

WEATHER: Overcast, mild - mid 50's

CONTRACTOR: Ramsey

Rig mfg/model: D-50 Turbo Tracked MST 800ATV

Drilling Method: 41/4" Hollow Stem Auger with Split spoon

FIELD STAFF: Driller: B. Williamson Helper: D. Crump

Eng/Geo: R. Hasenyager

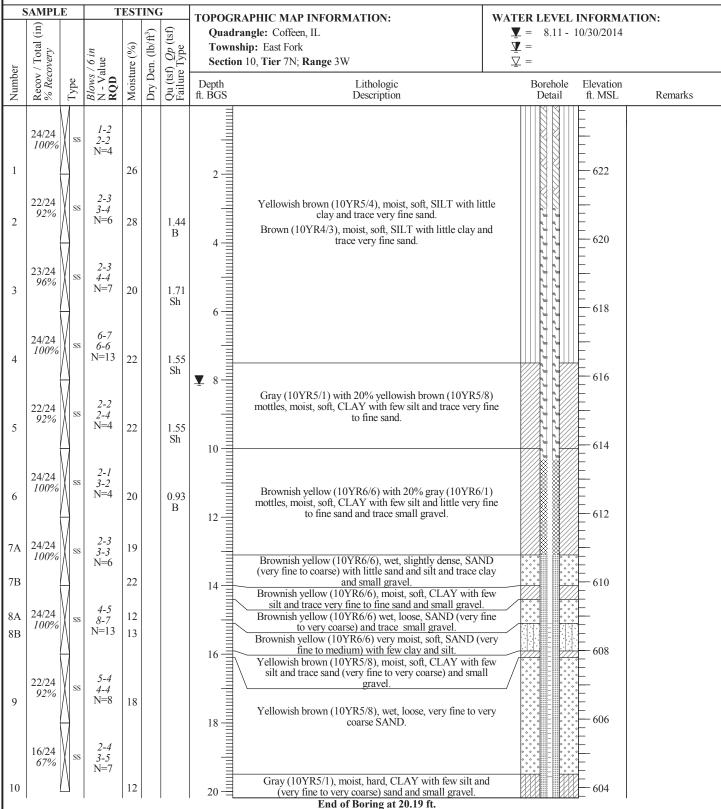
BOREHOLE ID: TA31

Well ID: TA31

Surface Elev: 623.89 ft. MSL **Completion:** 20.19 ft. BGS

Station: 876,542.25N 2,513,856.77E

Page 1 of 1



CLIENT: Illinois Power Holdings Site: Coffeen Power Station

Location: Coffeen, Montgomery County, Illinois

TESTING

Project: 14E0078

SAMPLE

DATES: Start: 10/27/2014 Finish: 10/27/2014

WEATHER: Partly sunny, mild - mid 70's

CONTRACTOR: Ramsey

TOPOGRAPHIC MAP INFORMATION:

Rig mfg/model: D-50 Turbo Tracked MST 800ATV

Drilling Method: 41/4" Hollow Stem Auger with Split spoon

FIELD STAFF: Driller: B. Williamson Helper: D. Crump

Eng/Geo: R. Hasenyager

WATER LEVEL INFORMATION:

BOREHOLE ID: TA32

Well ID: TA32

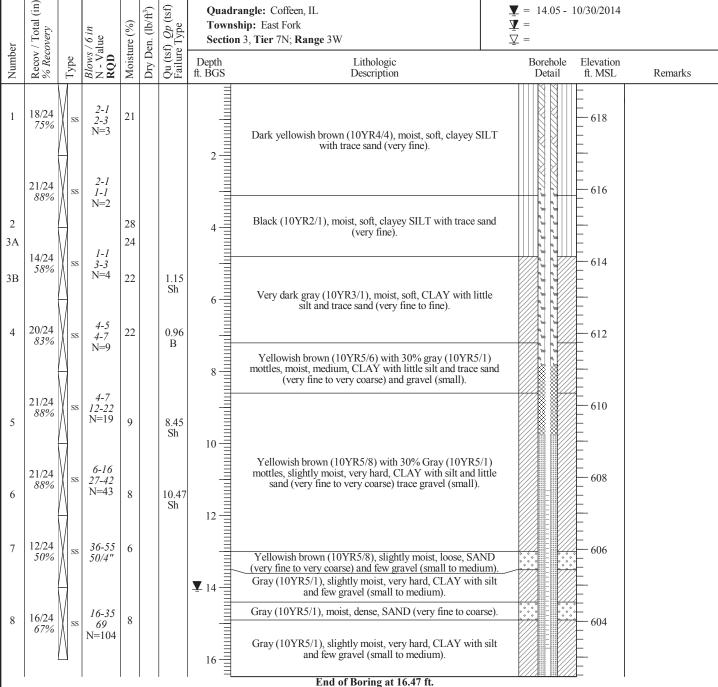
Surface Elev: 618.93 ft. MSL

Completion: 16.47 ft. BGS

Station: 877,532.57N

2,513,605.19E

 $\mathbf{V} = 14.05 - 10/30/2014$



CLIENT: Illinois Power Generating Company

Site: Coffeen Well Sealing & Assmt Well Install

Location: Coffeen, Illinois Project: 14E0078A

DATES: Start: 6/2/2015 Finish: 6/2/2015 WEATHER: Sunny, calm, hi-60s CONTRACTOR: Ramsey
Rig mfg/model: Diedrich D-50
Drilling Method: 3 ¼" HSA, blind drill

FIELD STAFF: Driller: B. Williamson

Helper: D. Crump Eng/Geo: S. Keim



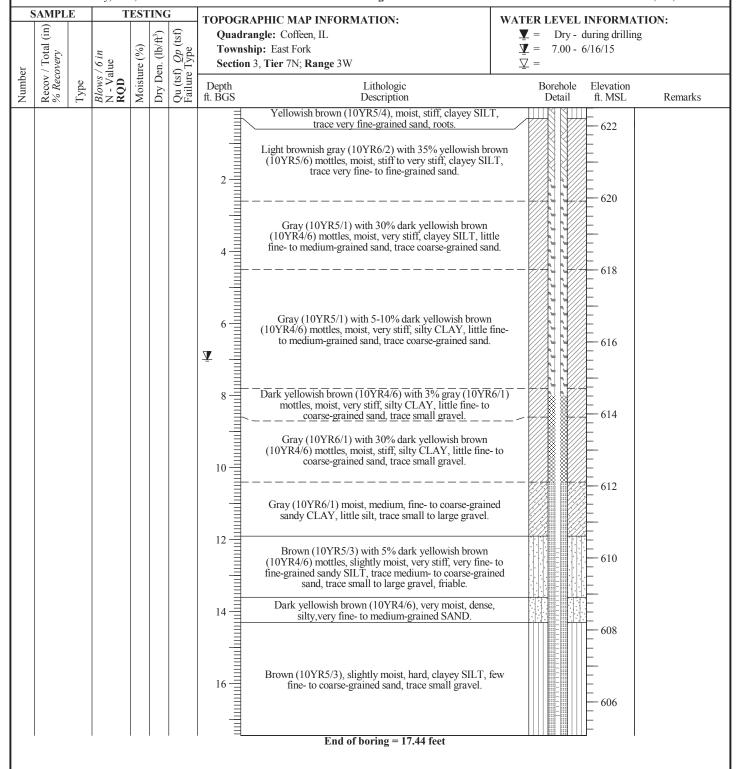
BOREHOLE ID: TA33b Well ID: TA33

 Surface Elev:
 622.51 ft. MSL

 Completion:
 17.44 ft. BGS

 Station:
 876,605.45N

 2.513,248.73E



CLIENT: Illinois Power Generating Company

Site: Coffeen Well Sealing & Assmt Well Install

Location: Coffeen, Illinois **Project:** 14E0078A

DATES: Start: 6/2/2015 **Finish:** 6/2/2015

WEATHER: Sunny, calm, hi-60s

CONTRACTOR: Ramsey **Rig mfg/model:** Diedrich D-50

Drilling Method: 3 1/4" HSA, split spoon sampler

FIELD STAFF: Driller: B. Williamson Helper: D. Crump

Eng/Geo: S. Keim

BOREHOLE ID: TA33a

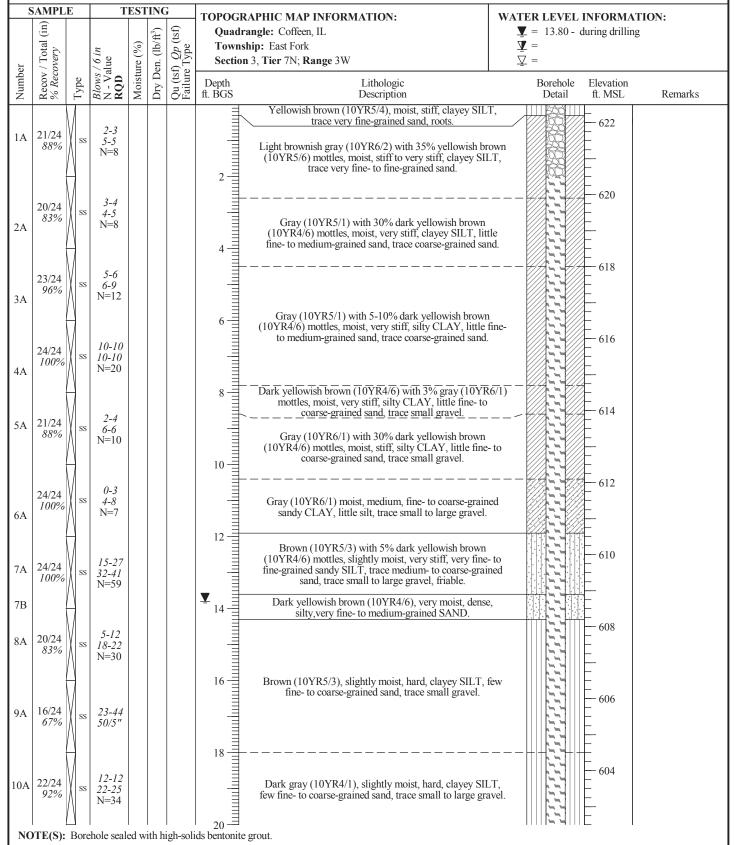
Well ID: n/a

 Surface Elev:
 622.5 ft. MSL

 Completion:
 30.0 ft. BGS

 Station:
 876,610.00N

 2.513,248.00E



CLIENT: Illinois Power Generating Company

Site: Coffeen Well Sealing & Assmt Well Install

Location: Coffeen, Illinois Project: 14E0078A

DATES: Start: 6/2/2015 **Finish:** 6/2/2015

WEATHER: Sunny, calm, hi-60s

CONTRACTOR: Ramsey **Rig mfg/model:** Diedrich D-50

Drilling Method: 3 ¹/₄" HSA, split spoon sampler

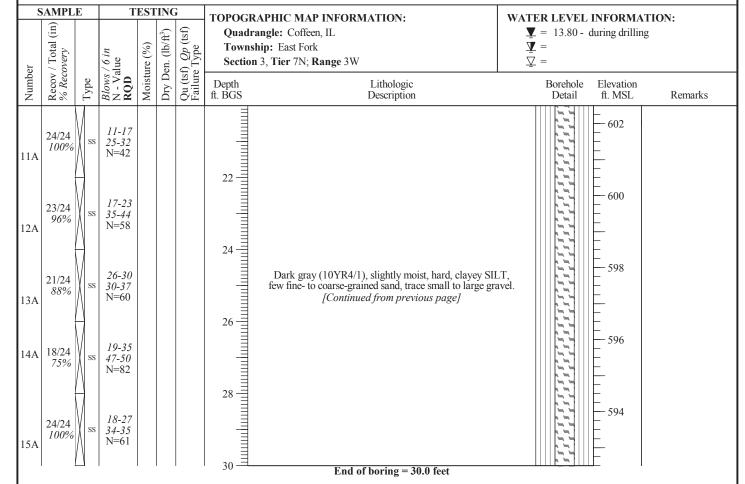
FIELD STAFF: Driller: B. Williamson Helper: D. Crump

Eng/Geo: S. Keim

BOREHOLE ID: TA33a
Well ID: n/a

Surface Elev: 622.5 ft. MSL Completion: 30.0 ft. BGS Station: 876,610.00N 2,513,248.00E

HANSON



CLIENT: Illinois Power Generating Company

Site: Coffeen Well Sealing & Assmt Well Install

Location: Coffeen, Illinois Project: 14E0078A DATES: Start: 6/3/2015

Finish: 6/3/2015 **WEATHER:** Mostly cloudy, windy, mid-60s

CONTRACTOR: Ramsey **Rig mfg/model:** Diedrich D-50

Drilling Method: 3 1/4" HSA, split spoon sampler

FIELD STAFF: Driller: B. Williamson Helper: D. Crump

Eng/Geo: S. Keim

HANSON

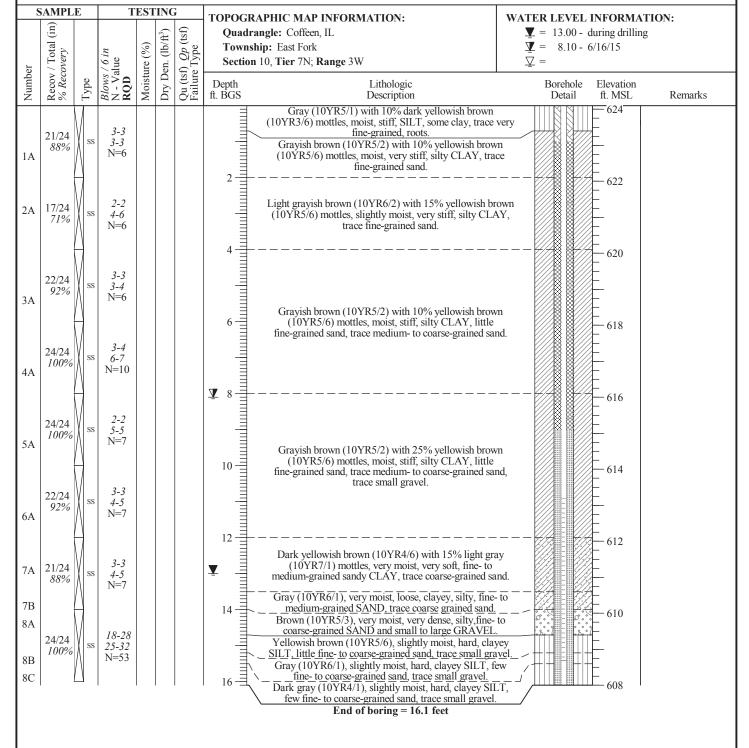
BOREHOLE ID: TA34 **Well ID:** TA34

 Surface Elev:
 624.10 ft. MSL

 Completion:
 16.10 ft. BGS

 Station:
 875,906.10N

 2.513,466.73E



| Illinois Enviro | nmental Protect | ion Agen | ıcy | | Wel | l Comple | etion | Report |
|--|--|-------------------|-----------|-------------------|-------------------|-------------------|--------------|---------------|
| Site #: | Co | ounty: | | | | Well #: | TF | R32 |
| Site Name: <u>Coffeen Power S</u> | tation | | | | | Borehole # | : <i>'</i> | ГR32 |
| State Plan€oordinate: X_2,513,605 | .0 Y <u>877,523.7</u> (oi | r) Latitude: | 39° | <u>4'</u> 266 | 63.000"Long | gitude: 89° | 24 | <u>8.070"</u> |
| Surveyed By: Kyle J. Nolan | | | IL Reg | istration #: | 035-00391 | 9 | | |
| Drilling Contractor: Ramsey | Geotechnical Engineerin | ng, LLC | Driller | : B. Willian | nson | | | |
| Consulting Firm: Hanson Pro | ofessional Services Inc. | | Geolog | ist: <u>Rhona</u> | ld W. Haser | nyager, LPG | #196-0 | 000246 |
| Drilling Method: Hollow Ster | m Auger | | Drillin | g Fluid (Type) | : <u>none</u> | | | |
| Logged By: Rhonald W. Has | enyager | | Date S | tarted:7/ | 2/2019 | Date Finishe | d: <u>7/</u> | 2/2019 |
| Report Form Completed By:F | Rhonald W. Hasenyager | | Date: | 7/3/20 |)19 | | | |
| ANNULAR SPAC | CE DETAILS | | | Elevation (MSL) | ons Dept | | 0.01 ft.) |) |
| | | | | 621.9 | | 9 Top of P | rotectiv | e Casing |
| | | T | | | _ | | | |
| | | | | 621.6 | 82.40 | <u>0</u> Top of F | liser Pip | e |
| Type of Surface Seal: <u>Concrete</u> | | | | 619.2 | 8 0.00 | Cround | Surface | |
| Type of Annular Sealant: Bent | onite | | | 616.2 | 3.00 | Top of A | nnular S | Sealant |
| Installation Method: Grav | | - | 14 | | | | | |
| Setting Time: 30 min. | | - _ <u>\</u> | 7 | | | Static W | ater Lev | rel |
| Setting Time | | - - | - | | _ | | mpletion) | |
| Type of Bentonite Seal Grand | ular Pellet Slurry | | | | | | | |
| Installation Method: | | - | \bowtie | n/a | n/a | Top of S | eal | |
| Setting Time: | | - | | 609.7 | 7 9.51 | L Top of S | and Pac | k |
| | | | | | | 10F 010 | | |
| Type of Sand Pack: Quartz San | | - | | 608.2 | 8 11.0 | 0 Top of S | creen | |
| Grain Size: <u>10/20</u> (sie | • | | | | | <u> </u> | | |
| Installation Method: <u>Grav</u> | ity | - | | 603.6 | 0 15.6 | 8 Bottom | of Scree | n |
| Type of Backfill Material: <u>n/a</u> | (if applicable) | | | 603.1 | | | | |
| Installation Method: | | | | 603.1 | 1 16.1 | 7 Bottom | of Borek | nole |
| instantion rection. | | _ | | | ced to a National | | or borer | ioic |
| | | | | | CASING M | EASUREME | NTS | |
| | | | | Diameter of | | | (inches) | 8.0 |
| | TRUCTION MATERIALS type of material for each area) | | | ID of Riser P | ipe | | (inches) | 2.0 |
| | | | | Protective Ca | asing Length | | (feet) | 5.0 |
| D. d. di . C. d | 00004 00047 5555 | UC 2007 (F | | Riser Pipe Le | | | | 13.40 |
| Protective Casing Riser Pipe Above W.T. | | VC OTHER: St | teei | | | Сар | | 0.49 |
| Riser Pipe Above W.T. Riser Pipe Below W.T. | | VC OTHER: | | | | ast slot) | | 4.68 |
| raser ripe below w.r. | 1111 (1 | | | Total Length | of Casing | | (feet) | 18.57 |

PTFE PVC OTHER:

SS304

Well Completion Form (revised 02/06/02)

SS316

Total Length of Casing

**Hand-Slotted Well Screens Are Unacceptable

Screen Slot Size **

0.010

(inches)

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 1/28/2021 **Finish:** 2/3/2021

WEATHER: Clear, cold (20s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig **Drilling Method:** 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

HANSON

BOREHOLE ID: G275D

Well ID: G275 Surface Elev: 617.52 ft. MSL

Completion: 99.70 ft. BGS **Station:** 874,285.30N

2,516,366.50E

| , | SAMPLE | | 1 | EST | ING | i | TOPOGRA | APHIC MAP INFORMATION: | WATER LEVEL INFORMATION: | | | |
|----------------|----------------------------------|------|--|-------------------|----------------------|-----------------------------------|---------|--|---|--|--|--|
| er Jer | Recov / Total (in) % Recovery | | <i>Blows / 6 in</i> N - Value RQD | Water Content (%) | Dry Density (lb/ft³) | Qu (tsf) Qp (tsf) Failure Type | | angle: Coffeen, IL hip: East Fork Township n 11, Tier 7N; Range 3W | $\underline{\underline{Y}}$ = 10.90 - During Drilling $\underline{\underline{Y}}$ = $\underline{\underline{Y}}$ = | | | |
| Number | Reco % Re | Туре | Blows N - V | Water | Dry D | Qu (ts Failur | | Lithologic Description | Borehole Elevation Detail ft. MSL Remarks | | | |
| 1A | 21/24 88% | ss | 3-4 5-10 N=9 | | | | 2 | Dark yellowish brown (10YR4/4), moist, stiff, lean CLAY, some silt, few very fine- to fine-grained sand and small grace roots. [FILL] | with avel, 616 | | | |
| 2A | 22/24 92% | ss | 3-4 6-9 N=10 | | | | | Gray (10YR5/1) with 15% yellowish brown (10YR5/6) mot moist, very stiff, lean CLAY, with some silt, few very fine fine-grained sand, trace small gravel. | ttles, - to | | | |
| ВА | 19/24 79% | ss | 2-4 6-8 N=10 | | | | 6 = | Gray (10YR5/1) with 10% yellowish brown (10YR5/6) mot moist, very stiff, lean CLAY, with some silt, few very fine fine-grained sand, trace small gravel. | | | | |
| ‡A | 23/24 96% | ss | 2-5 5-6 N=10 | | | | 8 | Gray (10YR5/1) with 20% yellowish brown (10YR5/6) and yellowish red (5YR4/6) mottles, moist, very stiff, lean CL with some silt, few very fine- to fine-grained sand, trace s | AY. /// \\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ | | | |
| 5A 5B 6A | 24/24 100% | ss | 2-3 5-6 N=8 | | | | 10 | gravel. Dark yellowish brown (10YR3/6), moist, stiff, SILT, with svery fine- to medium-grained sand, few clay and small gra | ome avel. | | | |
| 6B 7A | 24/24 100% | ss | 0-1 2-2 N=3 | | | | 6 | Gray (10YR6/1) with 10% dark yellowish brown (10YR3, mottles, moist, stiff, lean CLAY, with some silt, little very to to fine-grained sand, few small gravel. Dark yellowish brown (10YR3/6), wet, loose, SILT, with sovery fine- to fine-grained sand, few clay and small grave. | ome 606 | | | |
| | 18/24 75% | SH | | | | | | Gray (10YR6/1) with 20% yellowish brown (10YR5/6) mot moist, hard, SILT, with some very fine- to fine-grained sa few clay and small gravel. | | | | |
| ВА | 14/14 100% | ss | 26-43 50/2" | | | | 16 | Grayish brown (10YR5/2) with 10% yellowish brown (10YR mottles, moist, hard, SILT, with some very fine- to fine-grasand, few clay and small gravel. | R5/6) | | | |
| 9A | 24/24 100% | ss | 5-12 18-22 N=30 | | | | 18 | Brown (10YR5/3) with 10% yellowish brown (10YR5/6) mc | ttles, | | | |
| I0A | 24/24 100% | ss | 4-11 13-20 N=24 | | | | 20 | moist, hard, SILŤ, with somé clay and very fine- to finé-gra sand, few small gravel. | ained | | | |

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 1/28/2021

Finish: 2/3/2021 WEATHER: Clear, cold (20s) FIELD STAFF: Driller: Matt Helper: Corey

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig

Drilling Method: 4.25" HSA w/SS sampler

Eng/Geo: C. Colin Winter



BOREHOLE ID: G275D

Well ID: G275

 Surface Elev:
 617.52 ft. MSL

 Completion:
 99.70 ft. BGS

 Station:
 874,285.30N

2,516,366.50E

| | SAMPLE | | Т | ES1 | ΓING | | TOPOGRA | PHIC MAP INFORMATION: | WATE | R LEVEL IN | FORMATIO | | |
|------------|----------------------------------|-----------|----------------------------------|-------------------|----------------------|-----------------------------------|------------------|--|-----------------|--------------------|-------------------|--|--|
| ler ler | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Water Content (%) | Dry Density (lb/ft³) | Qu (tsf) Qp (tsf) Failure Type | Quadra Townsl | ngle: Coffeen, IL nip: East Fork Township 11, Tier 7N; Range 3W | | | | | |
| Number | Reco % Re | Туре | Blows N - Vs RQD | Water | Dry D | Qu (ts Failur | Depth ft. BGS | Lithologic Description | | Borehole Detail | Elevation ft. MSL | Remarks | |
| 11A 12A | 24/24 100% | ss | 3-9 13-22 N=22 | | | | 22 | Brown (10YR5/3) with 10% yellowish brown (10YR5/6) mo moist, hard, SILT, with some clay and very fine- to fine-grasand, few small gravel. [Continued from previous page] | ttles, ained | 00000 | | Vertical fractures with oxidation from 22 to | |
| | 24/24 100% | ss | 7-14 20-24 N=34 | | | | 24 | | | | 594 | 24 ft, no oxidation below 24 ft. | |
| 13A | 24/24 100% | ss | 6-11 15-21 N=26 | | | | 26 | | | | 592 | Occasional thin SILT and SAND lenses from 25.3 to 25.8 ft. | |
| 14A | 18/24 75% | ss | 4-8 12-10 N=20 | | | | 28 — | | | | 590 | Trace wood | |
| 15A | 24/24 100% | ss | 5-7 13-17 N=20 | | | | 30 | | | | 588 | fragments below 28 ft. | |
| 16A | 23/24 96% | ss | 4-7 12-16 N=19 | | | | | Dark gray (10YR4/1) with frequent dark yellowish brow (10YR3/6) oxidation along fractures, moist, hard, lean CL with some silt, few very fine- to fine-grained sand and sn gravel. | AY, | | 586 | | |
| 17A | 2/24 8% | ss | 4-10 13-17 N=23 | | | | 32 | | | | 584 | | |
| 18A | 21/24 88% | SH | | | | | 34 | | | | 582 | | |
| 19A | 24/24 100% | ss | 3-6 10-14 N=16 | | | | 36 | | | | 580 | | |
| 20A | 4/24 17% | ss | 3-8 11-17 N=19 | | | | 38 | | | | 578 | | |
| NO | TE(S): (| _ G275 | installed | in a | djac | ent blir | nd drill boreh | ole. | , | | | | |

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois Project: 20E0111A

DATES: Start: 1/28/2021 Finish: 2/3/2021

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt

Helper: Corey

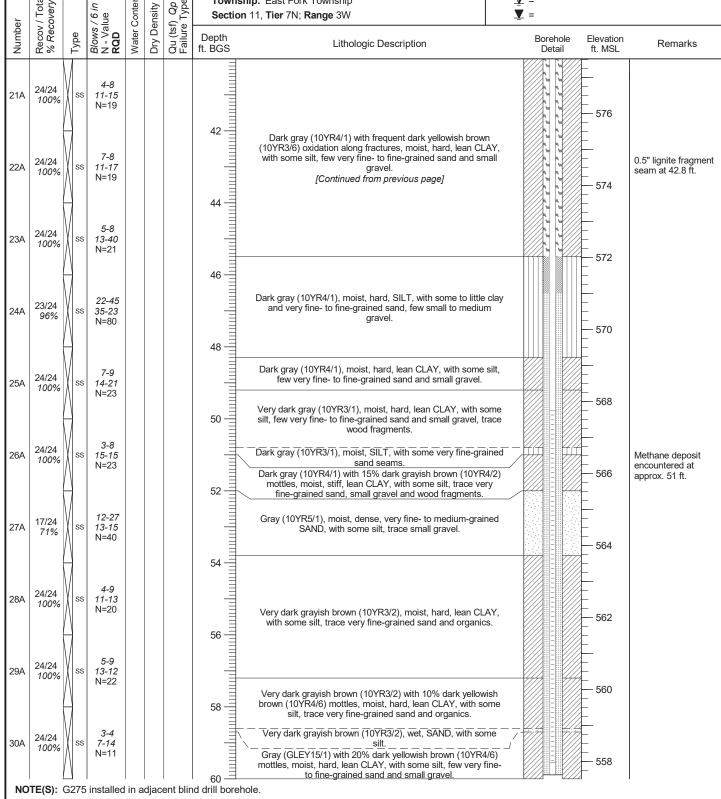
Eng/Geo: C. Colin Winter

BOREHOLE ID: G275D

Well ID: G275 Surface Elev: 617.52 ft. MSL

Completion: 99.70 ft. BGS 874,285.30N Station:

WEATHER: Clear, cold (20s) 2.516.366.50E SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: (lb/ft³ Ξ Water Content (%)) Qp (tsf) Type Quadrangle: Coffeen, IL Recov / Total (% Recovery <u>v</u> = Township: East Fork Township ▼ = Section 11, Tier 7N; Range 3W Depth Borehole Elevation Remarks



CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 1/28/2021 **Finish:** 2/3/2021

WEATHER: Clear, cold (20s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter



BOREHOLE ID: G275D Well ID: G275

 Surface Elev:
 617.52 ft. MSL

 Completion:
 99.70 ft. BGS

 Station:
 874,285.30N

2,516,366.50E

| | | | | | | | TOPOGRAPHIC MAP INFORMATION: | WATER LEVEL INFORMATION: |
|------------|----------------------------------|------|---------------------------------|-------------------|----------------------|-----------------------------------|---|--|
| e | Recov / Total (in) % Recovery | | / 6 <i>in</i> Ilue | Water Content (%) | Dry Density (lb/ft³) | Qu (tsf) Qp (tsf) Failure Type | Quadrangle: Coffeen, IL Township: East Fork Township Section 11, Tier 7N; Range 3W | ▼ = 10.90 - During Drilling ▼ = ▼ = |
| Number | Recov % Rec | Type | Blows / 6 i N - Value RQD | Water | Dry De | Qu (ts Failure | Depth Lithologic Des | scription Borehole Elevation Remarks Detail ft. MSL |
| 31A | 24/24 100% | ss | <i>0-4</i> <i>5-7</i> N=9 | | | | Gray (GLEY15/) with 30% dark y mottles, moist, hard, lean CLAY, w to fine-grained sand a | with some silt, few very fine- |
| 32A 33A | 24/24 100% | SS | 4-6 8-11 N=14 | | | | Greenish gray (GLEY15/1) with 15 mottles, moist, hard, lean CLAY, v | 5% very dark gray (10YR3/1) |
| 34A | 24/24 100% 24/24 100% | SH | 5-10 22-41 | | | | mottles, moist, hard, lean CLAY, v to fine-grained sand a | nd small gravel. |
| 35A | 24/24 100% | ss | N=32 12-24 33-45 N=57 | | | | 68 | 550 |
| 36A | 23/24 96% | SS | 6-14 25-30 N=39 | | | | 70 — Yellowish brown (10YR5/4) with or (GLEY15/1) seams, moist, hard, few small gravel, trace ver | lean CLAY, with some silt, at 70 ft. |
| 37A | 24/24 100% | ss | 8-18 24-32 N=42 | | | | 74 | 544 |
| 38A | 24/24 100% | ss | 7-16 25-29 N=41 | | | | 76 Yellowish brown (10YR5/4) with 19 moist, hard, lean CLAY, with some very fine-graine | 5% gray (10YR6/1) mottles, |
| 39A | 24/24 100% | ss | 7-15 20-21 N=35 | | | | moist, hard, lean CLAY, with some very fine-grains | e silt, few small gravel, trace |
| 40A | 19/24 79% | ss | 3-5 7-10 N=12 | | | | Greenish gray (GLEY15/1) with 5% mottles, moist, stiff, lean CLAY, | 6 yellowish brown (10YR5/6) with some silt, trace very |

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois Project: 20E0111A

DATES: Start: 1/28/2021 Finish: 2/3/2021

WEATHER: Clear, cold (20s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig Drilling Method: 4.25" HSA w/SS sampler

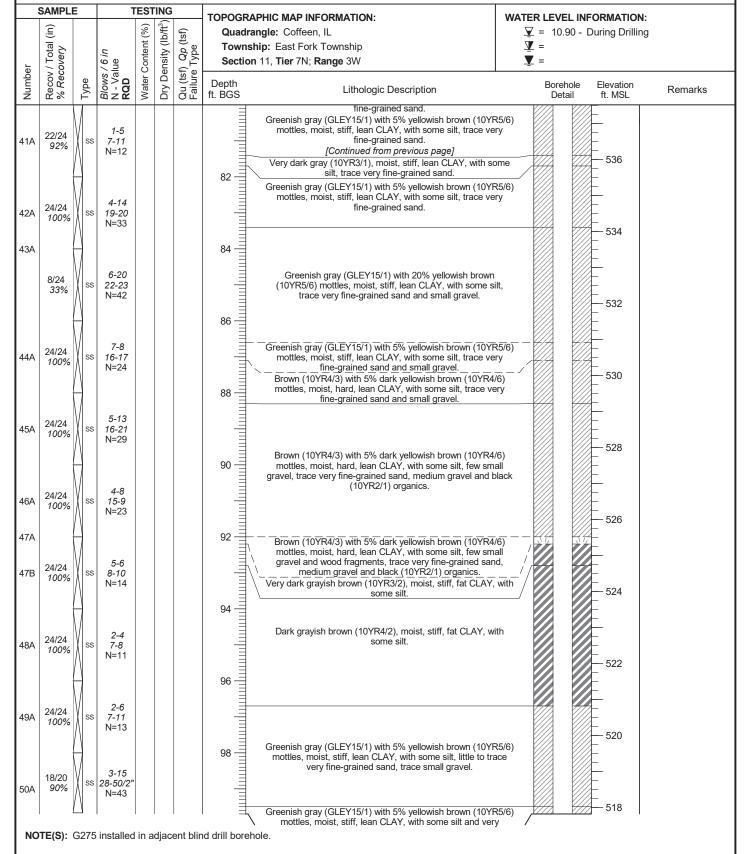
FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

BOREHOLE ID: G275D Well ID: G275

Surface Elev: 617.52 ft. MSL Completion: 99.70 ft. BGS 874,285.30N Station:

2.516.366.50E



CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 1/28/2021 **Finish:** 2/3/2021

WEATHER: Clear, cold (20s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

HANSON

BOREHOLE ID: G275D

Well ID: G275

Surface Elev: 617.52 ft. MSL Completion: 99.70 ft. BGS

npletion: 99.70 π. BGS Station: 874,285.30N

2,516,366.50E

| SA | AMPLE | Ξ | 7 | TES1 | ING | i | TOPOGRAPH | IC MAP INFORMATION: | WATER LEVEL IN | JEORMATION: | |
|-------|----------------|------|-------------------------------|-------------|-----------------|---------------------|----------------------|--|--------------------|-------------------|---------|
| : | / Iotal (in) | | / 6 <i>in</i> lue | Content (%) | ensity (lb/ft³) | f) Qp (tsf) Type | Quadrang Township | le: Coffeen, IL : East Fork Township , Tier 7N; Range 3W | | During Drilling | |
| 윤 경 | Kecov % Rec | Type | Blows N - Va RQD | Water | Dry De | Qu (tsf) Failure | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks |

fine-grained sand, trace small gravel.

End of boring = 99.7 feet

NOTE(S): G275 installed in adjacent blind drill borehole.

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

WEATHER: Rain, cold (30s)

DATES: Start: 1/25/2021 **Finish:** 1/25/2021

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig **Drilling Method:** 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

HANSON

BOREHOLE ID: G282D Well ID: 282D

Surface Elev: ft. MSL
Completion: 60.00 ft. BGS

Station: N E

| | SAMPLE TESTING | | | | | | TOPOGRA | APHIC MAP INFORMATION: | WATER LEVEL INFORMATION: | | | | |
|----------|----------------------------------|------|--|-------------------|----------------------|-----------------------------------|------------------|--|---|--|--|--|--|
| ber | Recov / Total (in) % Recovery | | <i>Blows / 6 in</i> N - Value RQD | Water Content (%) | Dry Density (lb/ft³) | Qu (tsf) Qp (tsf) Failure Type | Quadra Towns | ingle: Coffeen, IL hip: East Fork Township n 11, Tier 7N; Range 3W | | | | | |
| Number | Reco % Re | Туре | <i>Blow</i> . N - V RQD | Wate | Dry [| Qu (t Failu | Depth ft. BGS | Lithologic Description | Borehole Elevation Remarks Detail ft. MSL | | | | |
| | 45/04 | M | 3-3 | | | | | Gray (10YR6/1), wet, loose, GRAVEL, with some sand. [F | FILL] | | | | |
| 1A | 15/24 63% | ss | 3-4 N=6 | | | | 2 | Brown (10YR5/3), moist, stiff, lean CLAY, with some silt, t very fine- to fine-grained sand. [FILL] | trace | | | | |
| 2A | 17/24 71% | ss | 3-4 4-5 N=8 | | | | 4- | Yellowish brown (10YR5/4) with 10% gray (10YR6/1) mot moist, stiff, lean CLAY, with some silt, trace very fine- t fine-grained sand and small gravel. [FILL] | ttles, to | | | | |
| 3A | 22/24 92% | ss | 2-3 5-6 N=8 | | | | 6 | Grayish brown (10YR5/2), moist, stiff, lean CLAY, with so silt, trace small gravel. | ome | | | | |
| 4A | 20/24 83% | ss | 3-4 4-5 N=8 | | | | 8 | Grayish brown (10YR5/2) with 10% yellowish brown (10YF mottles, moist, stiff, lean CLAY, with some silt, trace sm gravel. | | | | | |
| 5A | 22/24 92% | ss | 2-3 5-7 N=8 | | | | 10 = | Grayish brown (10YR5/2) with 10% yellowish brown (10YF and 5% gray (10YR5/1) mottles, moist, stiff, lean CLAY, some silt, trace small gravel. | R5/4) with | | | | |
| 6A | 20/24 83% | ss | 3-4 4-7 N=8 | | | | 12 - | Grayish brown (10YR5/2) with 20% yellowish brown (10YF and 5% gray (10YR5/1) mottles, moist, stiff, lean CLAY, some silt, trace small gravel. | R5/4) with | | | | |
| 7A | 20/24 83% | ss | 2-3 4-5 N=7 | | | | 14 - | Gray (10YR6/1) with 20% yellowish brown (10YR5/6) mot moist, stiff, lean CLAY, with some silt, little very fine- to fine-grained sand, trace small gravel. | | | | | |
| 8A | 20/24 83% | ss | 1-2 3-4 N=5 | | | | 16 — | Dark gray (10YR4/1), moist, stiff, lean CLAY, with some Gray (10YR6/1) with 20% yellowish brown (10YR5/6) mot moist, stiff, lean CLAY, with some silt, little very fine-to fine-grained sand, trace small gravel. | itles, | | | | |
| 9A 0A | 21/24 88% | ss | 1-2 2-3 N=4 | | | | 18 - | Gray (10YR6/1) with 30% yellowish brown (10YR5/6) mot moist, stiff, lean CLAY, with some silt, little very fine- to fine-grained sand, trace small gravel. | | | | | |
| 0B | 24/24 100% | ss | 0-1 1-0 N=2 | | | | 20 | Yellowish brown (10YR5/6) with 10% gray (10YR6/1) mot wet, very loose, SILT, with some very fine- to fine-grain sand, few small gravel, trace clay. | ttles, ed | | | | |

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 1/25/2021 **Finish:** 1/25/2021

WEATHER: Rain, cold (30s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

HANSON

BOREHOLE ID: G282D

Well ID: 282D

Surface Elev: ft. MSL Completion: 60.00 ft. BGS

Station: N

Ε

SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: Ξ Dry Density (Ib/ft³ ▼ = 18.80 - During Drilling Water Content (%)) Qp (tsf) Type Quadrangle: Coffeen, IL Recov / Total (% Recovery Ψ = 55.90 - During Drilling Township: East Fork Township Blows / 6 in N - Value **RQD** ▼ = Section 11, Tier 7N; Range 3W Qu (tsf) Failure T Number Borehole Elevation Lithologic Description Remarks Detail ft. MSL Yellowish brown (10YR5/4) with 20% yellowish brown (10YR5/6) and 5% yellowish red (5YR4/6) mottles, moist, hard, 3-7 24/24 SS 11-16 11A SILT, with some very fine- to fine-grained sand, little clay, few 100% N=18 small gravel. Yellowish brown (10YR5/4), wet, fine- to medium-grained 22 SAND Yellowish brown (10YR5/4) with 20% yellowish brown (10YR5/6) and 5% yellowish red (5YR4/6) mottles, moist, hard, 7-12 24/24 SILT, with some very fine- to fine-grained sand, little clay, few 12A 17-24 100% small gravel, trace medium gravel. N=29 9-15 24/24 13A 22-22 100% N=37 26 8-17 Dark gray (10YR4/1), moist, hard, SILT, with some very fine-22/24 to fine-grained sand, little clay, few small gravel, trace medium 14A SS 16-22 92% N = 33gravel. 5-11 21/24 15A 15-19 88% 30 Dark gray (10YR4/1), moist, SAND, little silt and clay. 5-25 22/22 SS 33-50/4 16A 100% Dark gray (10YR4/1), moist, hard, SILT, with some very fine-N=58 to fine-grained sand, little clay, few small gravel, trace medium gravel. 7-10 22/24 15-20 17A 92% N=25 4-8 24/24 18A 10-16 100% N=18 Dark gray (10YR4/1), moist, hard, lean CLAY, with some silt, few very fine- to fine-grained sand, little small gravel. 5-8 24/24 19A 13-15 100% N=21 2-4 21/24 20A SS 8-11 88% N=12 NOTE(S): G282D installed in borehole.

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 1/25/2021

Finish: 1/25/2021 WEATHER: Rain, cold (30s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

HANSON

BOREHOLE ID: G282D

Well ID: 282D

Surface Elev: ft. MSL
Completion: 60.00 ft. BGS

Station: N E

Page 3 of 4

| • | SAMPLE TESTING | | | | | | TOPOGRAF | PHIC MAP INFORMATION: | WATER LEVEL INFORMATION: | | | | | |
|------------|----------------------------------|------|----------------------------------|-------------------|----------------------|-----------------------------------|-------------------|---|--------------------------|---------------------------------------|-------------------|---------------------------------|--|--|
| oer . | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Water Content (%) | Dry Density (lb/ft³) | Qu (tsf) Qp (tsf) Failure Type | Quadran Townsh | igle: Coffeen, IL ip: East Fork Township 11, Tier 7N; Range 3W | | ▼ = 18.80 - E ▼ = 55.90 - E ▼ = | During Drilli | ng | | |
| Number | Reco % Re | Type | Blow N - V RQD | Water | Dry D | Qu (t Failur | Depth ft. BGS | Lithologic Description | | Borehole Detail | Elevation ft. MSL | Remarks | | |
| 21A | 24/24 100% | ss | 4-8 11-14 N=19 | | | | 42 | | | | | | | |
| 22A | 22/24 92% | ss | 3-7 8-12 N=15 | | | | 44 | | | | | | | |
| 23A | 24/24 100% | ss | 3-6 9-13 N=15 | | | | 46 | | | 77777 | | Trace wood fragments below 45 | | |
| 24A | 24/24 100% | ss | 4-6 9-12 N=15 | | | | 46 | Dark gray (10YR4/1), moist, hard, lean CLAY, with some few very fine- to fine-grained sand, little small gravel. [Continued from previous page] | silt, | | | ft. | | |
| 25A | 24/24 100% | ss | 4-6 12-13 N=18 | | | | | | | | | 0.5" gravel seam at 48.5 ft. | | |
| 26A | 24/24 100% | ss | 2-7 9-13 N=16 | | | | 50 | | | | | | | |
| 27A | 24/24 100% | ss | 4-7 11-14 N=18 | | | | 54 | | | | | | | |
| 28A 28B | 24/24 100% | ss | 6-12 9-18 N=21 | | | | ¥ 56 | Light yellowish brown (10YR6/5), moist, very fine- to medium-grained SAND, with some silt, little small to medi gravel. Dark gray (10YR4/1), moist, hard, lean CLAY, with some few very fine- to fine-grained sand, little small gravel, tra | silt, | | | | | |
| 29A | 24/24 100% | ss | 6-10 11-11 N=21 | | | | | Wood fragments. Light yellowish brown (10YR6/5), wet, medium dense, ve fine- to coarse-grained SAND, little small gravel, few sil | ery lt. | | | | | |
| 30A | 24/24 100% | ss | 4-5 8-9 N=13 | | | | 58 | Dark gray (10YR4/1) with 5% dark yellowish brown (10YR mottles, moist, stiff, lean CLAY, with some silt. | R3/6) | | | | | |

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

TESTING

Water Content (%)

Dry Density (lb/ft³
Qu (tsf) Qp (tsf)
Failure Type

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 1/25/2021 **Finish:** 1/25/2021

WEATHER: Rain, cold (30s)

SAMPLE

Œ)

Recov / Total (% Recovery **CONTRACTOR:** Roberts

Rig mfg/model: CME-75 Track Rig

Drilling Method: 4.25" HSA w/SS sampler

Eng/Geo: C. Colin Winter

FIELD STAFF: Driller: Matt Helper: Corey

TOPOGRAPHIC MAP INFORMATION:

Quadrangle: Coffeen, IL Township: East Fork Township Section 11, Tier 7N; Range 3W

Depth
RGS
Lithologic Description

End of boring = 60.0 feet

HANSON

BOREHOLE ID: G282D

Well ID: 282D

Surface Elev: ft. MSL Completion: 60.00 ft. BGS

Station: N

WATER LEVEL INFORMATION: ▼ = 18.80 - During Drilling

 $\underline{\underline{Y}}$ = 55.90 - During Drilling $\underline{\underline{Y}}$ =

Borehole Elevation Detail ft. MSL

Remarks

Ε

NOTE(S): G282D installed in borehole.

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 1/18/2021 **Finish:** 1/18/2021

NOTE(S): G283 installed in borehole.

WEATHER: Overcast, cold (30s)

CONTRACTOR: Roberts

Rig mfg/model: GeoProbe 8040DT

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

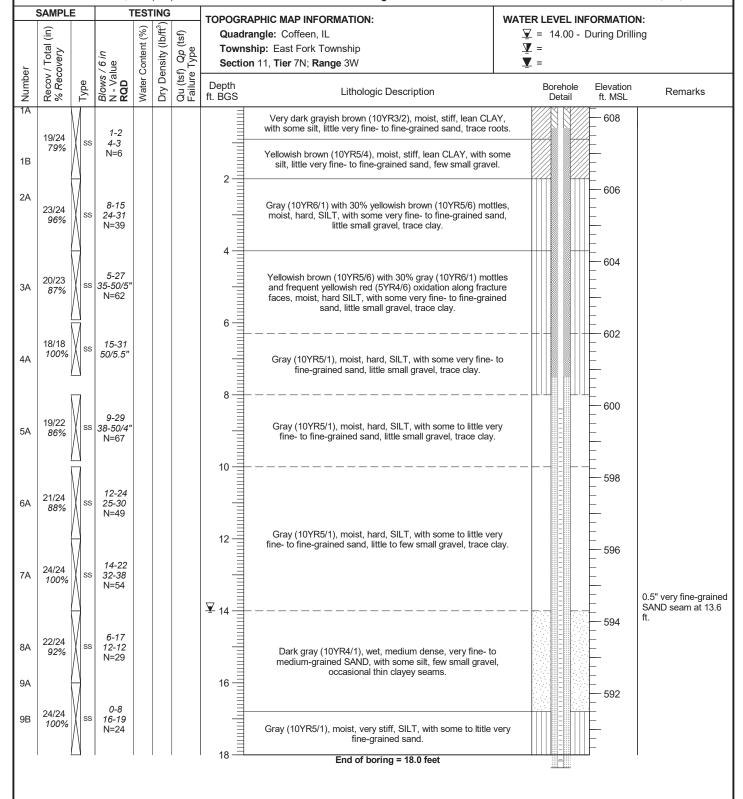
HANSON

BOREHOLE ID: G283

Well ID: G283

Surface Elev: 608.30 ft. MSL Completion: 18.00 ft. BGS

Station: 874,113.00N 2.516.503.00E



CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois
Project: 20E0111A

DATES: Start: 1/20/2021 **Finish:** 1/20/2021

Finish: 1/20/2021 **WEATHER:** Clear, cool (40s)

CONTRACTOR: Roberts

Rig mfg/model: GeoProbe 8040DT **Drilling Method:** 4.25" HSA w/SS sampler

Drilling Metriod: 4.25 FIGA W/55 sa

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter



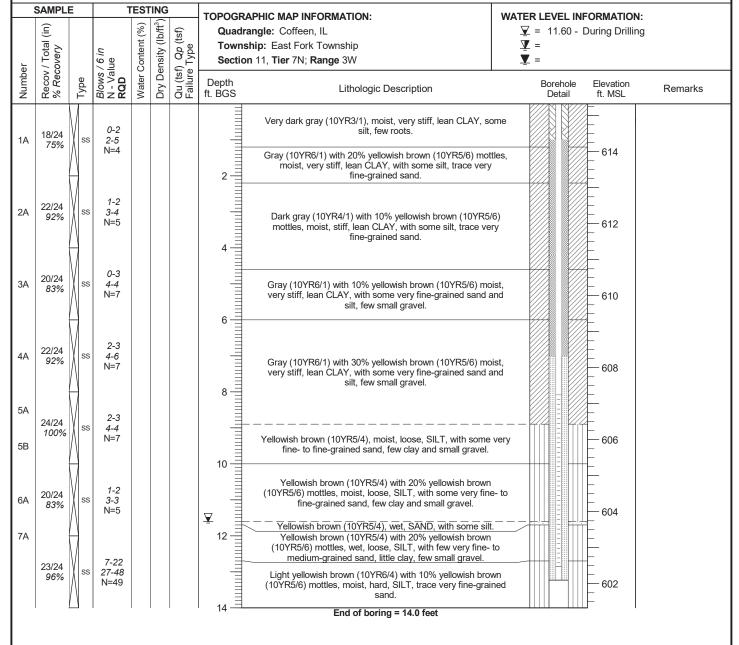
Well ID: G284

 Surface Elev:
 615.33 ft. MSL

 Completion:
 14.00 ft. BGS

 Station:
 874,423.60N

2,516,922.90E



CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 1/19/2021 **Finish:** 1/19/2021

WEATHER: Clear, cold (20s)

CONTRACTOR: Roberts

Rig mfg/model: GeoProbe 8040DT

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter



BOREHOLE ID: G285 Well ID: G285

 Surface Elev:
 610.54 ft. MSL

 Completion:
 26.00 ft. BGS

 Station:
 874.795.00N

2.516.680.40E

SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: (lb/ft³ Ξ Water Content (%) ▼ =) Qp (tsf) Type Quadrangle: Coffeen, IL **Dry During Drilling** Recov / Total (% Recovery **V** = Township: East Fork Township **Dry Density** *Blows / 6 ir* N - Value **RQD** ▼ = Section 11, Tier 7N; Range 3W Qu (tsf) Failure T Number Depth Borehole Elevation Lithologic Description Remarks ft. MSL 610 0-2 20/24 Yellowish brown (10YR5/4), moist, stiff, lean CLAY, with some SS 3-3 1A 83% silt, few fine-grained sand. N=5 608 1-3 18/24 Gray (10YR5/1) with 20% yellowish brown (10YR5/6) mottles, 2A SS 4-6 moist, very stiff, lean CLAY, with some silt, few very N=7fine-grained sand, trace small gravel. Yellowish brown (10YR5/6) with 20% gray (10YR5/1) mottles, 606 2-5 moist, very stiff, lean CLAY, with some silt, few very 22/24 ЗА SS 8-9 fine-grained sand, trace small gravel. 92% N=13 Gray (10YR5/1) with 15% yellowish brown (10YR5/6) mottles, hard, lean CLÁY, with some silt, few very fine-grained sand and small gravel. 604 3-8 22/24 4A SS 12-15 92% N = 20Yellowish brown (10YR5/6) with 20% gray (10YR5/1) mottles, hard, lean CLAY, with some silt, few very fine-grained sand and small gravel. 602 4-11 21/24 5A 16-18 88% N=27 10 600 3-8 23/24 SS 6A 13-17 96% N=21 Grayish brown (10YR5/2) with 15% yellowish brown (10YR5/6) mottles, hard, lean CLAY, with some silt, few very fine-grained sand and small gravel. 598 4-9 23/24 7A 12-17 96% N=21 596 5-14 23/24 Grayish brown (10YR5/2) with 15% yellowish brown (10YR5/6) 88 SS 21-33 N=35 96% mottles and 15% dark reddish brown (5YR3/4) oxidation along vertical fracture, hard, lean CLAY, with some silt, few very fine-grained sand and small gravel. 16 594 23/24 SS 10-15 96% N=17 Dark gray (10YR4/1), moist, hard, lean CLAY, with some silt, 10A Sampler pushing few very fine-grained sand and small gravel. gravel in Run 10. 592 4-6 4/24 SS 12-14 17% N=18 NOTE(S): G285 installed in borehole.

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois Project: 20E0111A

DATES: Start: 1/19/2021

Finish: 1/19/2021

CONTRACTOR: Roberts

Rig mfg/model: GeoProbe 8040DT

Drilling Method: 4.25" HSA w/SS sampler

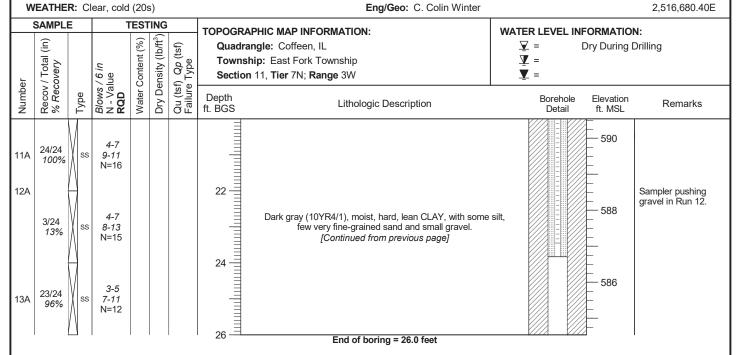
FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

BOREHOLE ID: G285 Well ID: G285

Surface Elev: 610.54 ft. MSL

Completion: 26.00 ft. BGS Station: 874,795.00N



CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 1/19/2021 **Finish:** 1/19/2021

WEATHER: Clear, cold (30s)

CONTRACTOR: Roberts

Rig mfg/model: GeoProbe 8040DT

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

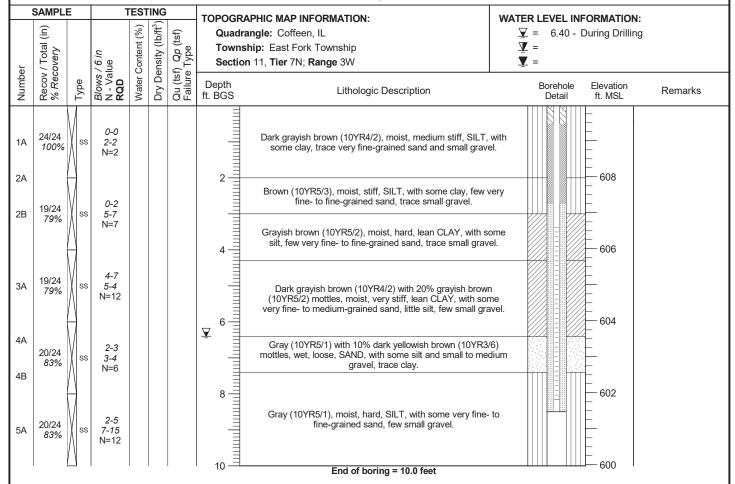
Eng/Geo: C. Colin Winter



BOREHOLE ID: G286 Well ID: G286

Surface Elev: 609.97 ft. MSL Completion: 10.00 ft. BGS

Station: 875,072.20N 2.516.561.80E



CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois Project: 20E0111A

DATES: Start: 1/18/2021 Finish: 1/18/2021

WEATHER: Overcast, cold (30s)

CONTRACTOR: Roberts

Rig mfg/model: GeoProbe 8040DT

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

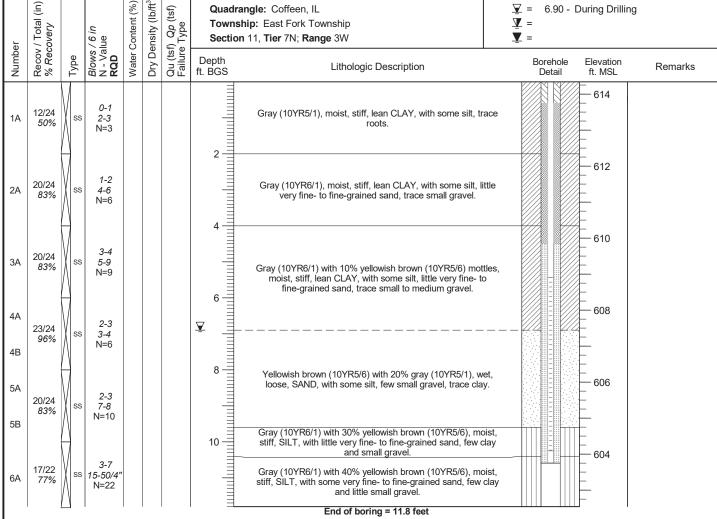
Eng/Geo: C. Colin Winter

BOREHOLE ID: G287 Well ID: G287

Surface Elev: 614.34 ft. MSL Completion: 11.80 ft. BGS

> Station: 875,442.80N 2.516.415.50E





NOTE(S): G287 installed in borehole.

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 1/21/2021

Finish: 1/21/2021 WEATHER: Clear, cold (30s)

CONTRACTOR: Roberts

Rig mfg/model: GeoProbe 8040DT

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter



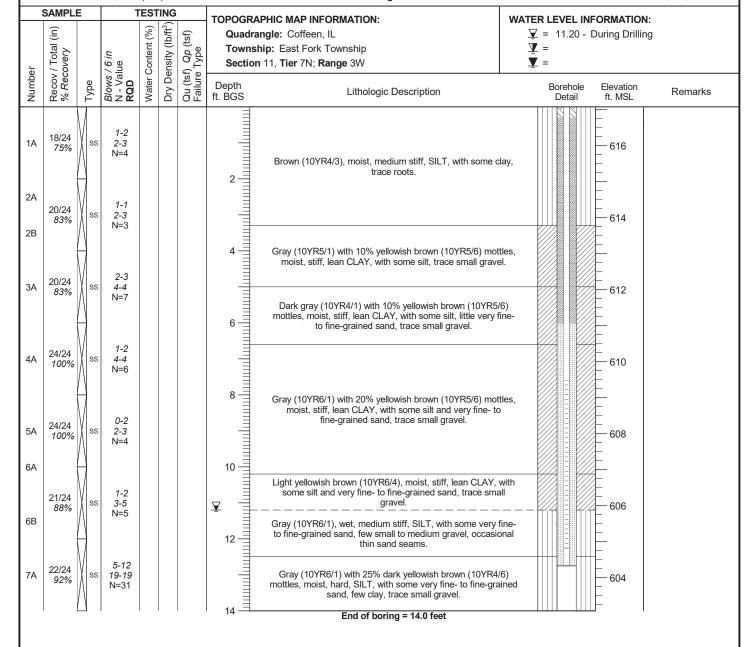
BOREHOLE ID: G288 Well ID: G288

 Surface Elev:
 617.08 ft. MSL

 Completion:
 14.00 ft. BGS

 Station:
 875.279.60N

2,517,071.40E



CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois Project: 20E0111A

DATES: Start: 1/26/2021 Finish: 1/27/2021

WEATHER: Overcast, cold (30s)

CONTRACTOR: Roberts

Rig mfg/model: GeoProbe 8040DT

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter



BOREHOLE ID: G289 Well ID: n/a

Surface Elev: ft. MSL Completion: 60.0 ft. BGS

Station: Ν

Ε

| A 17/24 71% 2A 19/24 79% | as ss | ## Blows / 6 in Signature Blows / 6 in Signa | Water Content (%) | Dry Density (Ib/ft³) | Qu (tsf) Qp (tsf) Failure Type | Quadra Towns | APHIC MAP INFORMATION: Ingle: Coffeen, IL hip: East Fork Township 111, Tier 7N; Range 3W Lithologic Description Brown (10YR4/3) with 10% gray (10YR6/1) and 10% yellow brown (10YR5/6) mottles, moist, stiff, SILT, with some clay trace very fine- to fine-grained sand. Dark gray (10YR4/1) with 20% yellowish brown (10YR5/6 mottles, moist, stiff, lean CLAY, with some silt, few very fine- grained sand, trace small gravel. | | 18.60 - I | Elevation ft. MSL | |
|---|------------------|--|-------------------|----------------------|-------------------------------------|------------------|---|---------|---------------|-------------------|---------|
| A 17/24 71% 2A 19/24 79% BA 19/24 79% 21/24 88% | SS | 2-2 4-4 N=6 3-5 6-8 N=11 | Water Con | Dry Densi | Qu (tsf) C Failure Ty | Depth ft. BGS | Lithologic Description Brown (10YR4/3) with 10% gray (10YR6/1) and 10% yellow brown (10YR5/6) mottles, moist, stiff, SILT, with some clay trace very fine- to fine-grained sand. Dark gray (10YR4/1) with 20% yellowish brown (10YR5/6 mottles, moist, stiff, lean CLAY, with some silt, few very fine- | E E | | | Remarks |
| A 19/24 79% A 19/24 79% A 19/24 79% A 21/24 88% A | SS | 2-2 4-4 N=6 3-5 6-8 N=11 | \$ | | OL | 2 — | Brown (10YR4/3) with 10% gray (10YR6/1) and 10% yellow brown (10YR5/6) mottles, moist, stiff, SILT, with some clay trace very fine- to fine-grained sand. Dark gray (10YR4/1) with 20% yellowish brown (10YR5/6 mottles, moist, stiff, lean CLAY, with some silt, few very fine. |) | Detail | II. MSL | |
| 79% | SS | 6-8 N=11 3-4 4-10 | | | | | mottles, moist, stiff, lean CLAY, with some silt, few very fin | | | | |
| 21/24 88% | | 4-10 | | | | | to mile granica sana, trace siliali gravel. | /// | a <i>VIII</i> | | |
| A 88% | ss | | | | | 6 | Dark gray (10YR4/1) with 20% yellowish brown (10YR5/6 | | | | |
| PA | $\setminus \mid$ | 2-2 4-6 N=6 | | | | | mottles, moist, stiff, lean CLAY, with some silt, little very fin to fine-grained sand, trace small gravel. Dark gray (10YR4/1), SILT, with some clay. | e- | | | |
| 18/24 75% | SH | | | | | ¥ 8 = | Dark gray (10YR4/1) with 20% yellowish brown (10YR5/6) a 5% very pale brown (10YR7/3) mottles, moist, stiff, lean CL with some silt, little very fine- to fine-grained sand, trace sm gravel. | AY, /// | | | |
| 22/24 92% | SS | 3-4 4-6 | | | | 10 | Dark grayish brown (10YR4/3), moist, stiff, lean CLAY, wit some silt. | h | | | |
| 6B | | N=8 | | | | 12 | Gray (10YR6/1) with 20% dark grayish brown (10YR4/2) at 10% yellowish brown (10YR5/6) mottles, moist, stiff, lean CLAY, with some silt, few very fine- to fine-grained sand, transmall gravel. | | | | |
| 'A 19/24 79% | ss | 3-4 6-6 N=10 | | | | 14 | Gray (10YR6/1) with 30% dark yellowish brown (10YR4/6) a 20% dark grayish brown (10YR4/2) mottles, moist, stiff, lea CLAY, with some silt, few very fine- to fine-grained sand, transmall gravel. | ın /// | | | |
| 3A 22/24 92% | ss | 3-4 5-6 N=9 | | | | | Very dark gray (10YR3/1), moist, stiff, lean CLAY, with son silt, few very fine- to fine-grained sand, trace small gravel | ne . | | | |
| 9A 24/24 100% | ss | 2-3 4-4 N=7 | | | | 16 | Gray (10YR6/1) with 10% yellowish brown (10YR5/6) mottle moist, medium stiff, lean CLAY, with some silt and very fine fine-grained sand, few small gravel. | | | | |
| 0A 24/24 100% 0B | ss | 2-2 1-2 N=3 | | | | 18 20 20 | Gray (10YR6/1) with 10% yellowish brown (10YR5/6) mottle moist to wet, SILT, with some very fine- to fine-grained sar and clay, few small gravel. Strong brown (7.5YR5/8), moist to wet, SILT, with some ve | nd | | | |

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 1/26/2021

Finish: 1/27/2021 WEATHER: Overcast, cold (30s)

CONTRACTOR: Roberts

Rig mfg/model: GeoProbe 8040DT

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

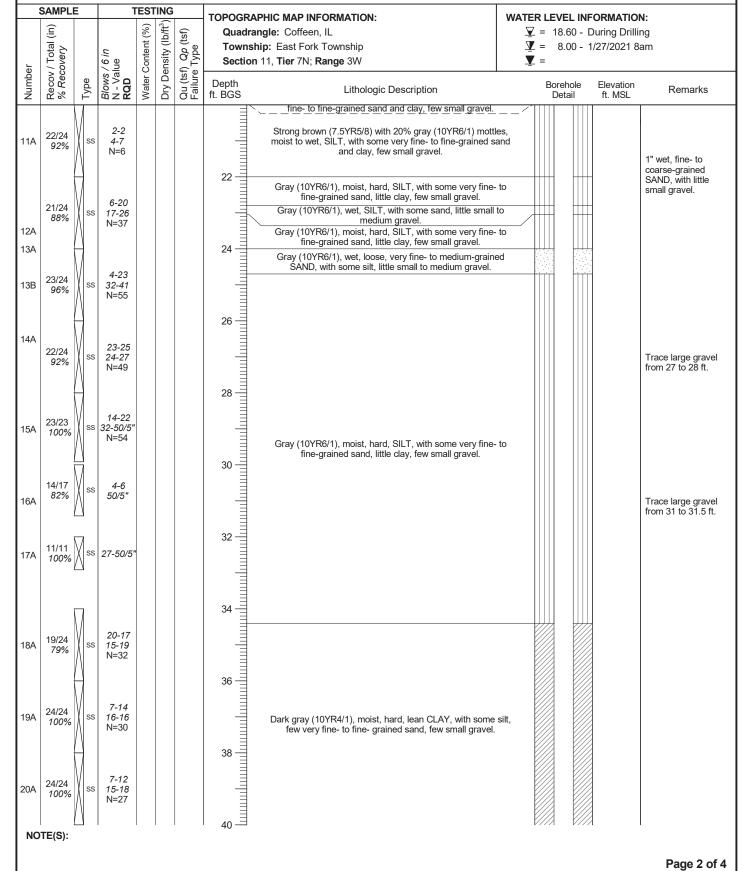
HANSON

BOREHOLE ID: G289 Well ID: n/a

Surface Elev: ft. MSL

Completion: 60.0 ft. BGS
Station: N

Station: N



CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 1/26/2021

Finish: 1/27/2021 WEATHER: Overcast, cold (30s)

CONTRACTOR: Roberts

Rig mfg/model: GeoProbe 8040DT

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter



Well ID: n/a

Surface Elev: ft. MSL Completion: 60.0 ft. BGS

Station: N E

Page 3 of 4

| | SAMPLE | | 1 | EST | ING | | TOPOGRA | PHIC MAP INFORMATION: | WATER I EVE | L INFORMATIO | N· |
|--------|----------------------------------|------|--|-------------------|----------------------|-----------------------------------|------------------------------|--|-----------------|---------------------------------------|---|
| ber | Recov / Total (in) % Recovery | | <i>Blows / 6 in</i> N - Value RQD | Water Content (%) | Dry Density (lb/ft³) | Qu (tsf) Qp (tsf) Failure Type | Quadrai Townsh Section | ngle: Coffeen, IL ip: East Fork Township 11, Tier 7N; Range 3W | <u>▼</u> = 18.6 | 60 - During Drill 00 - 1/27/2021 8 | ing |
| Number | Reco % Re | Туре | Blow N - V RQD | Wate | Dry [| Qu (t Failu | Depth ft. BGS | Lithologic Description | Boreh Deta | | Remarks |
| 21A | 24/24 100% | SH | | | | | 42 — | | | | Trace wood fragments below 42 |
| 2A | 24/24 100% | ss | 5-13 20-22 N=33 | | | | 44 | | | | ft. |
| ЗА | 22/24 92% | ss | 3-7 11-14 N=18 | | | | 46 — | | | | |
| 4A | 24/24 100% | ss | 4-9 10-14 N=19 | | | | 46 | Dark gray (10YR4/1), moist, hard, lean CLAY, with some si few very fine- to fine- grained sand, few small gravel. [Continued from previous page] | lt, | | |
| 5A | 23/24 96% | ss | 2-5 7-10 N=12 | | | | 50 | | | | |
| 6A | 24/24 100% | ss | 4-10 12-18 N=22 | | | | 50 | | | | |
| 7A | 24/24 100% | ss | 5-9 11-15 N=20 | | | | | | | | |
| 8A | 24/24 100% | ss | 3-5 7-8 N=12 | | | | 54 | Gray (10YR5/1) with 15% dark brown (10YR3/6) mottles, moist, stiff, lean CLAY, with some silt. | | | |
| 9A | 24/24 100% | ss | 3-5 9-9 N=14 | | | | 58 — | Gray (10YR5/1) with 20% dark brown (10YR3/6) and 10% days | | | |
| 0A | 24/24 100% | ss | <i>0-4</i> 8-9 N=12 | | | | 50 == | gray (10YR4/1) mottles, moist, stiff, lean CLAY, with some s | | | Few fine- to medium-grained sand below 59 ft. |

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 1/26/2021

Finish: 1/27/2021 WEATHER: Overcast, cold (30s)

CONTRACTOR: Roberts

Rig mfg/model: GeoProbe 8040DT

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

HANSON

BOREHOLE ID: G289

Well ID: n/a

Surface Elev: ft. MSL
Completion: 60.0 ft. BGS

Station: N

E

| | SAMPL | Ε | 1 | EST | ING | | TOPOGRAPH | IIC MAP INFORMATION: | WATER LEVEL INFORMATION: | | | | |
|-------|----------------|------|-------------------------|---------|----------|---------------------|------------------|------------------------------------|--------------------------|-------------------|---------|--|--|
| | (Ē | | | (%) | (lb/ft³) | (tsf) | Quadrang | le: Coffeen, IL | <u>▼</u> = 18.60 - | During Drilling | | | |
| | otal ery | | u | ent | (E) | Qp (t ype | Township | : East Fork Township | <u>▼</u> = 8.00 - | 1/27/2021 8am | | | |
| ē | /Tc | | / 6 <i>i</i> | Content | ensity | l | Section 1 | I, Tier 7N; Range 3W | ▼ = | | | | |
| Numbe | Recov % Rec | Type | Blows N - Val RQD | Water (| Dry De | Qu (tsf) Failure | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks | | |

End of boring = 60.0 feet

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 2/9/2021 **Finish:** 2/9/2021

WEATHER: Overcast, very cold (10s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter



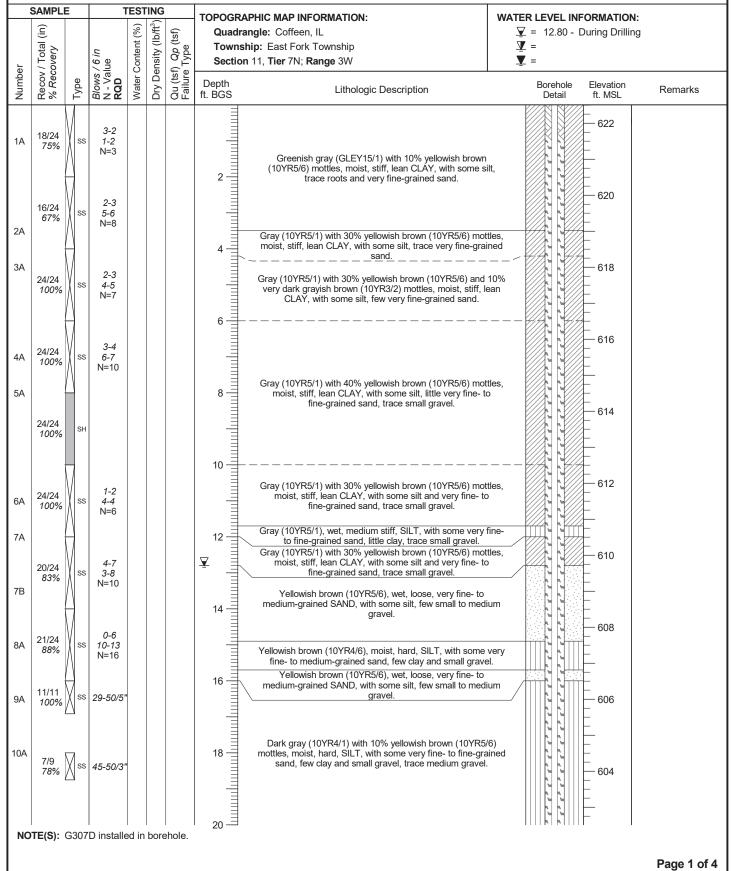
BOREHOLE ID: G307D Well ID: G307D

 Surface Elev:
 622.51 ft. MSL

 Completion:
 60.00 ft. BGS

 Station:
 871,397.20N

2,515,560.30E



CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois Project: 20E0111A

DATES: Start: 2/9/2021 Finish: 2/9/2021

WEATHER: Overcast, very cold (10s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

HANSON

BOREHOLE ID: G307D Well ID: G307D

Surface Elev: 622.51 ft. MSL

Completion: 60.00 ft. BGS **Station:** 871,397.20N

2,515,560.30E

| | SAMPLI | | vercasi, v | | ING | | TOPOGR | APHIC MAP INFORMATION: | WATER | OLEVEL IN | FORMATIO | 2,515,500.50E |
|-------------------|----------------------------------|------------|--|-------------------|----------------------|---|--|---|-------|--|---|--|
| er | Recov / Total (in) % Recovery | | /6 in | Water Content (%) | Dry Density (lb/ft³) | Qu (tsf) Q <i>p</i> (tsf) Failure Type | Quadra Towns | ingle: Coffeen, IL hip: East Fork Township 11, Tier 7N; Range 3W | l | = 12.80 - = | During Drilli | |
| Number | Recov % Rec | Туре | Blows / 6 in N - Value RQD | Water | Dry De | Qu (ts Failure | Depth ft. BGS | Lithologic Description | | Borehole Detail | Elevation ft. MSL | Remarks |
| 11A 12A 13A | 8/8 100% 8/9 89% | | 35-50/2" 30-50/3" 23-39 | | | | 22 24 26 28 30 32 34 36 38 38 38 38 38 39 30 30 30 30 30 30 30 | | | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | | ft. |
| 14A | 9/9 | ss ss | 50/5" | | | | 26 | | | 7,0,0,0,0,0 | | |
| 15A 16A | 23/23 100% 15/15 100% | ss | 31-44 34-50/5" N=78 3-44 50/3" | | | | 30 | Dark gray (10YR4/1) with 10% yellowish brown (10YR5 mottles, moist, hard, SILT, with some very fine- to fine-grasand, few clay and small gravel, trace medium gravel [Continued from previous page] | ained | ,,,,,,,,,,,,,,, | - - - - - - - - - - - - - - - - - - - | 1" dark gray (10YR4/1), fine- to medium-grained sand, with some silt, little small gravel. |
| 17A | 10/10 100% | ss | 34-50/4" | | | | 32 | | | 00000 | | |
| 18A | 11/11 100% | ss | 31-50/5" | | | | 34 | | | 00000 | 588 | |
| 19A | 17/17 100% | ss | 28-44 50/5" | | | | 36 | | | (, (, (, (, (, (, (, (, (, (, (, (, (, (| 586 | |
| 20A | 24/24 100% | ss G307 | 14-19 13-24 N=32 D installe | ed in | bore | ehole. | 40 | Dark gray (10YR4/1), moist, hard, lean CLAY, with some little to few very fine- to fine-grained sand, few small gra | | | 584 | |
| | . , | | | | | | | | | | | Page 2 of 4 |

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 2/9/2021 **Finish:** 2/9/2021

WEATHER: Overcast, very cold (10s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig **Drilling Method:** 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt

Helper: Corey

Eng/Geo: C. Colin Winter

HANSON

BOREHOLE ID: G307D Well ID: G307D

 Surface Elev:
 622.51 ft. MSL

 Completion:
 60.00 ft. BGS

 Station:
 871,397.20N

Page 3 of 4

2,515,560.30E

| Number Number Recov / Total (in) % Recovery 100% | Туре | <i>Blows / 6 in</i> N - Value RQD | Water Content (%) | Dry Density (lb/ft³) |) <i>Qp</i> (tsf) Type | Quadran | HIC MAP INFORMATION: | 1 | R LEVEL IN 2 = 12.80 - | | |
|--|------|--|-------------------|----------------------|---------------------------|------------------|--|-----------------|-------------------------------|-------------------------|---|
| 24/24 | Туре | 8 % | 101 | ens | e Typ | | p: East Fork Township 1, Tier 7N; Range 3W | $\bar{\Lambda}$ | <u>'</u> = <u>'</u> = | During Driii | <u>.</u> |
| | | Blow N - \ | Water | Dry D | Qu (tsf) Failure T | Depth ft. BGS | Lithologic Description | | Borehole Detail | Elevation ft. MSL | Remarks |
| 22A | ss | 7-8 12-15 N=20 | | | | 42 | | | | 582 | Trace medium gravel below 40 ft. |
| 20/24 83% | SH | | | | | 44 | | | | — 580 — | |
| 24/24 100% | ss | 6-8 10-12 N=18 | | | | 46 | | | | 578 - - - - | |
| 24/24 100% | ss | 5-6 10-12 N=16 | | | | 48 | Dark gray (10YR4/1), moist, hard, lean CLAY, with some little to few very fine- to fine-grained sand, few small gra [Continued from previous page] | silt, vel. | 22.2 | 576 | |
| 24/24 100% | ss | 3-6 11-11 N=17 | | | | 50 | | | | 574 | Trace wood fragments below 48.5 ft. |
| 26A 24/24 100% | ss | 3-7 9-10 N=16 | | | | 52 — | | | | | Gravel plugged shoe |
| 27A 16/24 67% | ss | 4-7 11-9 N=18 | | | | 52 | | | | 570 | in Run 27. Large lignite fragment at 52.4 ft. |
| 24/24 100% | SS | 3-6 10-9 N=16 | | | | 54 | Greenish gray (GLEY15/1) with 15% yellowish brown (10YR5/6) mottles, moist, stiff, lean CLAY, with some strace small gravel. | ilt, | | 568 | |
| 29A 24/24 100% | ss | 4-6 8-12 N=14 | | | | | Yellowish brown (10YR5/6) with 30% greenish gray (GLEY15/1) and 5% very dark grayish brown (10YR3/mottles, moist, stiff, lean CLAY, with some silt, trace sn gravel. | | | 566 | |
| 30A 24/24 100% | SS | 2-5 8-10 N=13 | | | | 58 | Yellowish brown (10YR5/6) with 20% greenish gray (GLEY15/1) and 5% very dark grayish brown (10YR3/mottles, moist, stiff, lean CLAY, with some silt, trace sn gravel. | 2) nall | | 564 | Large wood fragment |

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois Project: 20E0111A

DATES: Start: 2/9/2021

Finish: 2/9/2021

WEATHER: Overcast, very cold (10s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

BOREHOLE ID: G307D

Station:

Well ID: G307D

Surface Elev: 622.51 ft. MSL Completion: 60.00 ft. BGS

> 871,397.20N 2,515,560.30E

> > Remarks

| | SAMPL | E | 1 | TES1 | TING | | TOPOGR | APHIC MAP INFORMATION: | WATER LEVEL IN | FORMATION: |
|-------|-----------------------|------|------------------------|-------------|-----------------|---------------------|------------------|---|--------------------|----------------------|
| Ē | / Total (in) overy | | / 6 <i>in</i> lue | Content (%) | ensity (lb/ft³) | f) Qp (tsf) Type | Quad Town | rangle: Coffeen, IL ship: East Fork Township on 11, Tier 7N; Range 3W | | During Drilling |
| Numbe | Recov % Rec | Type | Blows N - Va RQD | Water (| Dry De | Qu (tsf) Failure | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL |

End of boring = 60.0 feet

at 59.8 ft.

NOTE(S): G307D installed in borehole.

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

WEATHER: Clear, cold (30s)

DATES: Start: 1/13/2021 **Finish:** 1/13/2021

CONTRACTOR: Roberts

Rig mfg/model: GeoProbe 8040DT **Drilling Method:** 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt
Helper: Corey

Eng/Geo: C. Colin Winter



BOREHOLE ID: G308 Well ID: G308

 Surface Elev:
 621.59 ft. MSL

 Completion:
 15.80 ft. BGS

 Station:
 871,454.70N

2,515,101.40E

SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: (lb/ft³ Ξ Water Content (%) ∇ = 13.00 - During Drilling) Qp (tsf) Type Quadrangle: Coffeen, IL Recov / Total (% Recovery **V** = Township: East Fork Township **Dry Density** *Blows / 6 ir* N - Value **RQD** Section 11, Tier 7N; Range 3W ▼ = Qu (tsf) Failure T Number Depth Borehole Elevation Lithologic Description Remarks ft. BGS ft. MSL 2-2 16/24 Grayish brown (10YR5/2), moist, stiff, lean CLAY, with some SS 2-3 1A 67% silt, trace roots. 620 0-2 19/24 2A SS 3-5 Brown (10YR5/3) with 20% yellowish brown (10YR5/6) mottles, 79% N=5moist, stiff, lean CLAY, with some silt, trace roots. 618 17/24 3A SS 5-6 71% 616 Gray (10YR5/1) with 20% yellowish brown (10YR5/6) mottles, moist, stiff, lean CLAY, with some silt, trace very fine-grained sand and small gravel. 23/24 4A SS 5-6 96% N=9614 Gray (10YR5/1) with 30% yellowish brown (10YR5/6) mottles, 22/24 moist, very stiff, lean CLAY, with some silt, trace very 5A 6-7 92% fine-grained sand and small to medium gravel. N=10 612 10 2-3 21/24 4-5 6A 88% Gray (10YR5/1) with 40% yellowish brown (10YR5/6) mottles, N=7 moist, stiff to very stiff, lean CLAY, with some silt, little to trace 610 very fine-grained sand, trace small to medium gravel. 7A 12 2-3 24/24 \mathbf{V} 4-6 100% N=7 Gray (10YR5/1) with 20% yellowish brown (10YR5/6) mottles, 608 wet, stiff, lean CLAY, with some very fine- to fine-grained 14 sand, little silt, trace small gravel. 4-12

Light yellowish brown (10YR6/4) wet, hard, SILT, with some

very fine-grained sand, few clay and small to medium gravel.

End of boring = 15.8 feet

NOTE(S): G308 installed in borehole.

19/22

8A

86%

ss 33-50/4

N=45

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 1/12/2021 **Finish:** 1/12/2021

WEATHER: Clear, cold (30s)

CONTRACTOR: Roberts

Rig mfg/model: GeoProbe 8040DT

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt
Helper: Corey

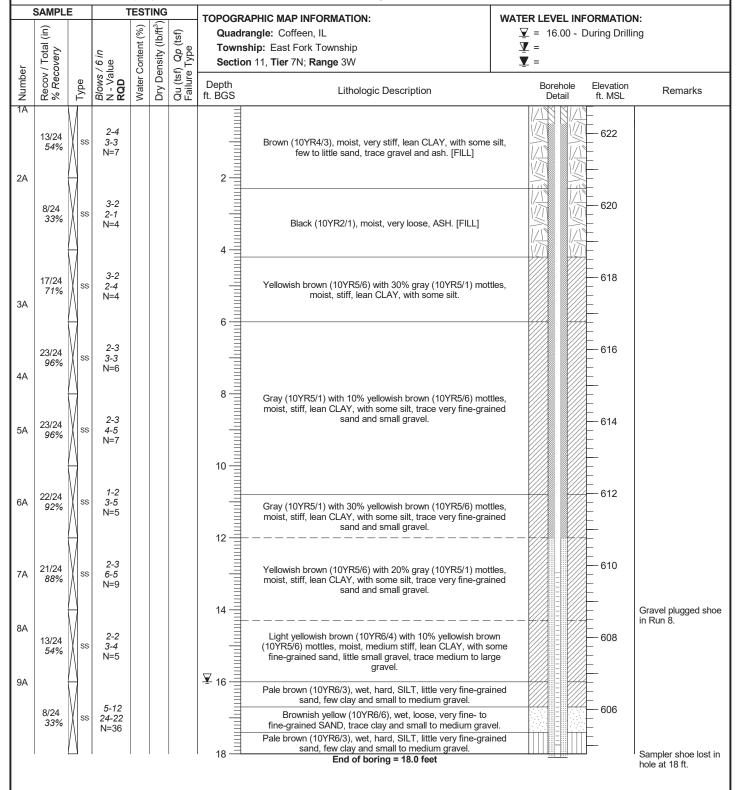
Eng/Geo: C. Colin Winter

HANSON

BOREHOLE ID: G309 Well ID: G309

Surface Elev: 622.77 ft. MSL Completion: 18.00 ft. BGS

Station: 871,865.80N 2,515,067.10E



CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois Project: 20E0111A

DATES: Start: 1/15/2021 Finish: 1/15/2021

WEATHER: Clear, light snow, cold (30s)

CONTRACTOR: Roberts

Rig mfg/model: GeoProbe 8040DT

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

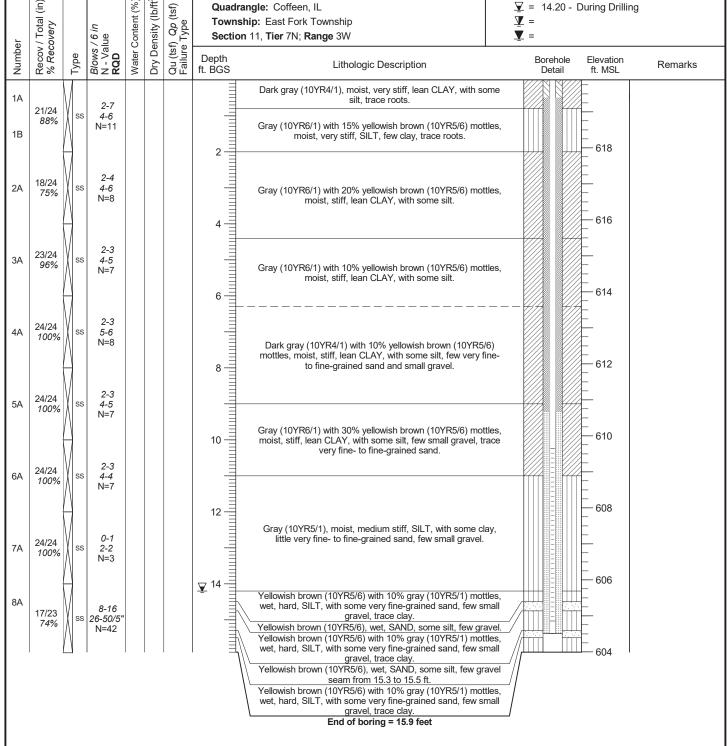
Eng/Geo: C. Colin Winter

BOREHOLE ID: G310 Well ID: G310

> Surface Elev: 619.89 ft. MSL Completion: 15.90 ft. BGS 872,239.40N Station:

> > 2.515.159.40E

SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: (lb/ft³ Ξ ∇ = 14.20 - During Drilling) Qp (tsf) Type Quadrangle: Coffeen, IL **V** = Township: East Fork Township ▼ = Section 11, Tier 7N; Range 3W



CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois

Project: 20E0111A

DATES: Start: 2/5/2021

Finish: 2/5/2021 WEATHER: Clear, cold (20s) **CONTRACTOR:** Roberts

Rig mfg/model:

Drilling Method: 4.25" HSA w/SS sampler

BOREHOLE ID: G311 Well ID: G311

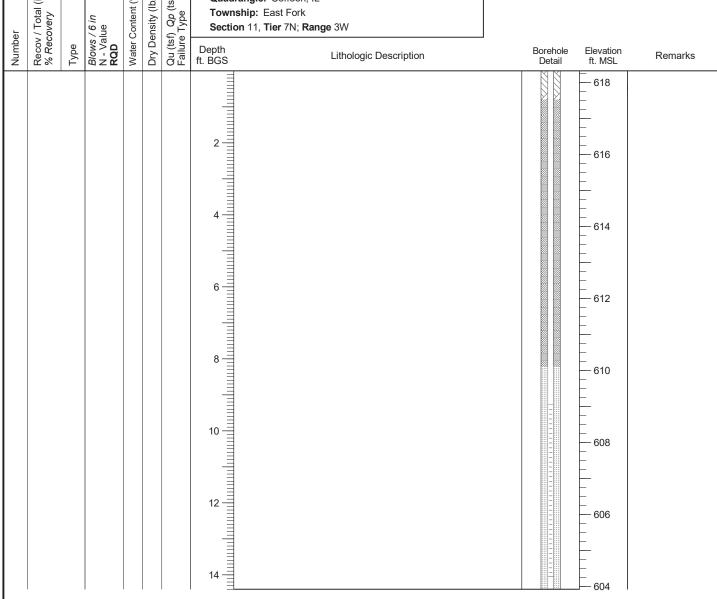
Surface Elev: 618.32 ft. MSL

Completion: 14.40 ft. BGS 872,238.70N Station:

2,515,881.80E

FIELD STAFF: Driller: Matt Helper: Corey Eng/Geo: C. Colin Winter

SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: Dry Density (lb/ft3 Qu (tsf) Q*p* (tsf) Failure Type Œ) Water Content (%) Quadrangle: Coffeen, IL Township: East Fork Section 11, Tier 7N; Range 3W Depth



CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 2/5/2021 **Finish:** 2/5/2021

WEATHER: Clear, cold (20s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig

Drilling Method: 3.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt
Helper: Corey

Eng/Geo: C. Colin Winter



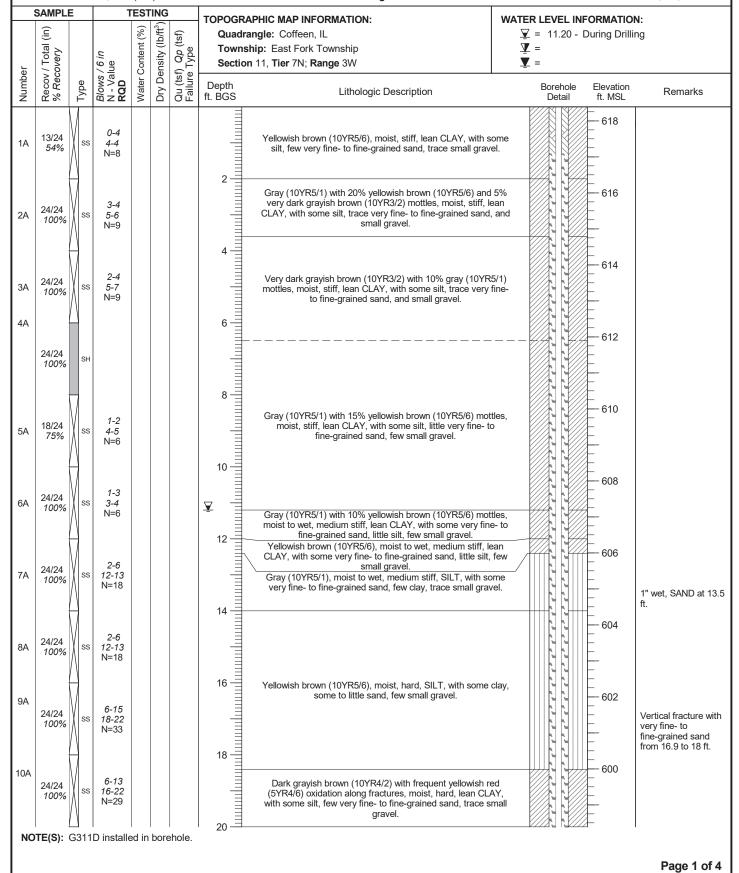
BOREHOLE ID: G311D Well ID: G311D

 Surface Elev:
 618.39 ft. MSL

 Completion:
 60.00 ft. BGS

 Station:
 872,238.70N

 2.515.881.80E



CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 2/5/2021

Finish: 2/5/2021 WEATHER: Clear, cold (20s) CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig

Drilling Method: 3.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

HANSON

BOREHOLE ID: G311D Well ID: G311D

Surface Elev: 618.39 ft. MSL Completion: 60.00 ft. BGS

Station: 872,238.70N 2,515,881.80E

| 0, | LE | | ΓEST | ING | | TOPOGRAF | PHIC MAP INFORMATION: | WATER LEVEL INF | ORMATIO | N· |
|--|-------------|----------------------------------|-------------------|----------------------|-----------------------------------|------------------|---|---|-------------------|--|
| Number Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Water Content (%) | Dry Density (lb/ft³) | Qu (tsf) Qp (tsf) Failure Type | | igle: Coffeen, IL ip: East Fork Township 11, Tier 7N; Range 3W | ∑ = 11.20 - I ∑ = ∑ = ∑ = | | |
| Number Recov / % Reco | Type | Blows N - V | Water | Dry D | Qu (ts Failur | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks |
| 11A 24/24 1009 | 4 % s | 5-15 | | | | | | | 598 | |
| 12/24 50% | 4 s | 2-3 5 14-17 N=17 | | | | 22 | | 22222 | 596 | No oxidation below 22 ft. |
| 13A 24/24 1009 | 4 % S | 6-11 14-20 N=25 | | | | 24 - | | | 594 594 | Trace medium grave below 24 ft. |
| 24/24 1009 | 4 % \ S | 4-8 11-16 N=19 | | | | 26 | | | 592 592 | |
| 5A 24/24 1009 | 4 % s | 4 | | | | 22 | Dark gray (10YR4/1) with frequent yellowish red (5YR4/ | | 590 | |
| 6A 24/24 1009 | 4 8 S | 0-3 5-8 N=8 | | | | 30 | oxidation along fractures, moist, hard, lean CLAY, with so silt, few very fine- to fine-grained sand, trace small grave | me //// 🖫 | 588 | |
| 7A 24/24 1009 | 4 % S | 2-4 6-8 N=10 | | | | | | | 586 | |
| 8A 24/24 1009 | 4 % S | 2-5 7-7 N=12 | | | | 34 | | | | Gravel plugged shoe in Run 18. Trace large gravel from 35 to 36 ft. |
| 13/24 54% | 4 S | 2-7 8-11 N=15 | | | | 36 | | | 582 | Trace lignite and wood fragments below 36 ft. |
| 20A 24/24 1009 | 4 8 S | 2-6 10-8 N=16 | | | | 38 | | 17.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7. | 580 | |

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 2/5/2021 **Finish:** 2/5/2021

WEATHER: Clear, cold (20s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig

Drilling Method: 3.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter



BOREHOLE ID: G311D Well ID: G311D

 Surface Elev:
 618.39 ft. MSL

 Completion:
 60.00 ft. BGS

 Station:
 872,238.70N

2,515,881.80E

Page 3 of 4

| - | SAMPLE | | 1 | EST | ING | | TOPOGRAPHIC MAP INFORMATION: | WATER LEVEL IN | IFORMATIO | N: |
|--------|-------------------------------|------|----------------------------------|-------------------|---------------------------------|-----------------------------------|--|--------------------|----------------------|----------------------------------|
| | (ii) | | | (%) | 2/ft ³) | sf) | Quadrangle: Coffeen, IL | <u>▼</u> = 11.20 - | | |
| | Z al | | 2 | ent |) E | <i>p</i> (ts | Township: East Fork Township | <u></u> | | |
| | , To | | 6 in Je | out | ısit | ΔŽ | Section 11, Tier 7N; Range 3W | ▼ = | | |
| Number | Recov / Total (% Recovery | Туре | Blows / 6 i. N - Value RQD | Water Content (%) | Dry Density (lb/ft ³ | Qu (tsf) Qp (tsf) Failure Type | Depth Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks |
| 1A | 16/24 67% | SS | 3-3 6-8 N=9 | | | | Dark gray (10YR4/1) with frequent yellowish red (5 oxidation along fractures, moist, hard, lean CLAY, we silt, few very fine- to fine-grained sand, trace small [Continued from previous page] | ith some | 578 | |
| 2A | | 1 | | | | | 42 Greenish gray (GLEY15/1) with 20% dark reddish | | ¥ | |
| 2B | 24/24 100% | ss | 3-4 7-8 N=11 | | | | (10YR3/2) mottles, moist, medium stiff, lean CLAY, v silt. | vith some | 576 | |
| A | 24/24 100% | ss | 1-3 5-7 N=8 | | | | *** | | 574 | |
| -A | 20/24 83% | ss | 3-4 10-8 N=14 | | | | Dark grayish brown (10YR4/1) with frequent yellow (5YR4/6) oxidation along fractures, moist, hard, lea with some silt, few very fine- to fine-grained sand, trato large gravel. | rish red | 572 | |
| iΑ | 24/24 100% | ss | 3-5 8-13 N=13 | | | | (5YR4/6) oxidation along fractures, moist, hard, lea with some silt, few very fine- to fine-grained sand, tra to large gravel. | n CLAY. | | |
| ŝΑ | 24/24 100% | ss | 2-5 10-12 N=15 | | | | 50 | | 568 | |
| 'Α | 24/24 100% | ss | 2-6 10-14 N=16 | | | | 52 | | 566 | |
| ВА | 24/24 100% | ss | 4-7 7-11 N=14 | | | | Dark gray (10YR4/1) with 20% greenish gray (GLEY 5% yellowish brown (10YR5/6) mottles, moist, very schaff clay, with some silt, trace very fine-grained sand a gravel. | stiff, lean | | Trace small grave below 54.3 ft. |
| 9A | 24/24 100% | ss | 2-5 9-11 N=14 | | | | Greenish gray (GLEY16/1) with 40% yellowish b (10YR5/6) mottles, moist, very stiff, lean CLAY, with trace very fine-grained sand and small grave | some silt, | 562 | |
| Α | 24/24 100% | ss | 3-7 10-13 N=17 | | | | Yellowish brown (10YR5/6) with 30% greenish (GLEY16/1) mottles, moist, very stiff, lean CLAY, w silt, trace very fine-grained sand and small gra | th some | 560 | 0.5" small to med GRAVEL. |

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois Project: 20E0111A

DATES: Start: 2/5/2021

Finish: 2/5/2021

WEATHER: Clear, cold (20s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig

Drilling Method: 3.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

HANSON

BOREHOLE ID: G311D Well ID: G311D

Surface Elev: 618.39 ft. MSL Completion: 60.00 ft. BGS **Station:** 872,238.70N

2,515,881.80E

| SAI | MPLE | | Т | EST | | | TOPOGRAPH | IC MAP INFORMATION: | WATER LEVEL IN | FORMATION | |
|--------------------|-------|------|------------------------|-------------|-----------------|-----------------------------|------------------------|---|--|----------------------|---------|
| er //Total (in) | overy | | <i>/ 6 in</i> lue | Content (%) | ensity (lb/ft³) | f) Q <i>p</i> (tsf) Type | Quadrangl Township: | e: Coffeen, IL East Fork Township , Tier 7N; Range 3W | <u>▼</u> = 11.20 - <u>▼</u> = <u>▼</u> = | | = |
| | % Rec | Туре | Blows N - Va RQD | Water (| Dry De | Qu (tsf) Failure | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks |

End of boring = 60.0 feet

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 2/4/2021 **Finish:** 2/4/2021

WEATHER: Rain, cold (30s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig **Drilling Method:** 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt

Eng/Geo: C. Colin Winter

Helper: Corey

HANSON

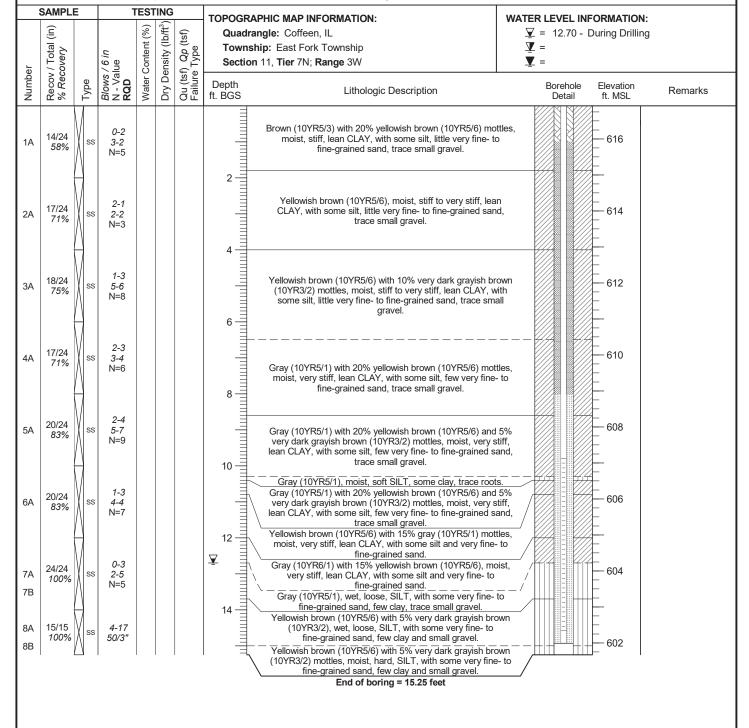
BOREHOLE ID: G312 **Well ID:** G312

 Surface Elev:
 616.92 ft. MSL

 Completion:
 15.25 ft. BGS

 Station:
 872,260.90N

2,516,557.40E



CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 1/14/2021 **Finish:** 1/14/2021

WEATHER: Overcast, cool (40s)

CONTRACTOR: Roberts

Rig mfg/model: GeoProbe 8040DT

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter



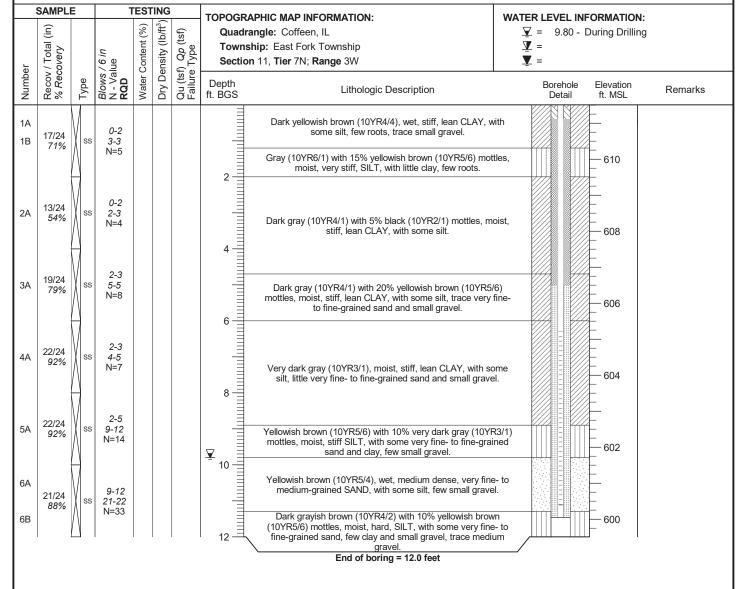
BOREHOLE ID: G313 Well ID: G313

 Surface Elev:
 611.51 ft. MSL

 Completion:
 12.00 ft. BGS

 Station:
 871.976.80N

2,516,803.70E



CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

WEATHER: Clear, mild (40s)

DATES: Start: 2/26/2021

DATES: Start: 2/26/2021 **Finish:** 2/26/2021

CONTRACTOR: Holcomb Foundation Engineering Co.

Rig mfg/model:

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Steve Helper: Jeff

Eng/Geo: C. Colin Winter

HANSON

BOREHOLE ID: G314

Well ID: G314

 Surface Elev:
 611.11 ft. MSL

 Completion:
 20.05 ft. BGS

 Station:
 871,630.20N

2,516,852.10E

| | SAMPLI | E | 1 | EST | ING | | | | | | |
|--------|-------------------------------|------|----------------------------------|-------------------|------|---|--|------------------------|--------------------|----------------------|-------------|
| Number | Recov / Total (in) % Recovery | | Blows / 6 in N - Value RQD | Water Content (%) | | Qu (tsf) Q <i>p</i> (tsf) Failure Type | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks |
| NGO | DTE(S): | G314 | installed | l in b | oreh | ole. | 2 4 4 6 8 10 12 14 14 16 18 18 18 20 1 | | 7//AV//AV/ | | Pero 1 of 2 |

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 2/26/2021

Finish: 2/26/2021

WEATHER: Clear, mild (40s)

CONTRACTOR: Holcomb Foundation Engineering Co.

Rig mfg/model:

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Steve Helper: Jeff

Eng/Geo: C. Colin Winter

HANSON

BOREHOLE ID: G314

Well ID: G314

Surface Elev: 611.11 ft. MSL Completion: 20.05 ft. BGS

Station: 871,630.20N 2,516,852.10E

| SAMPLE | TESTING | | | | | |
|---|---|------------------|------------------------|--------------------|----------------------|---------|
| Number Recov / Total (in) % Recovery Type | Blows / 6 in N - Value RQD Water Content (%) Dry Density (Ib/ft²) Qu (tsf) Qp (tsf) Failure Type | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks |

NOTE(S): G314 installed in borehole.

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 2/10/2021 **Finish:** 2/12/2021

WEATHER: Overcast, very cold (10s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt
Helper: Corey

Eng/Geo: C. Colin Winter

HANSON

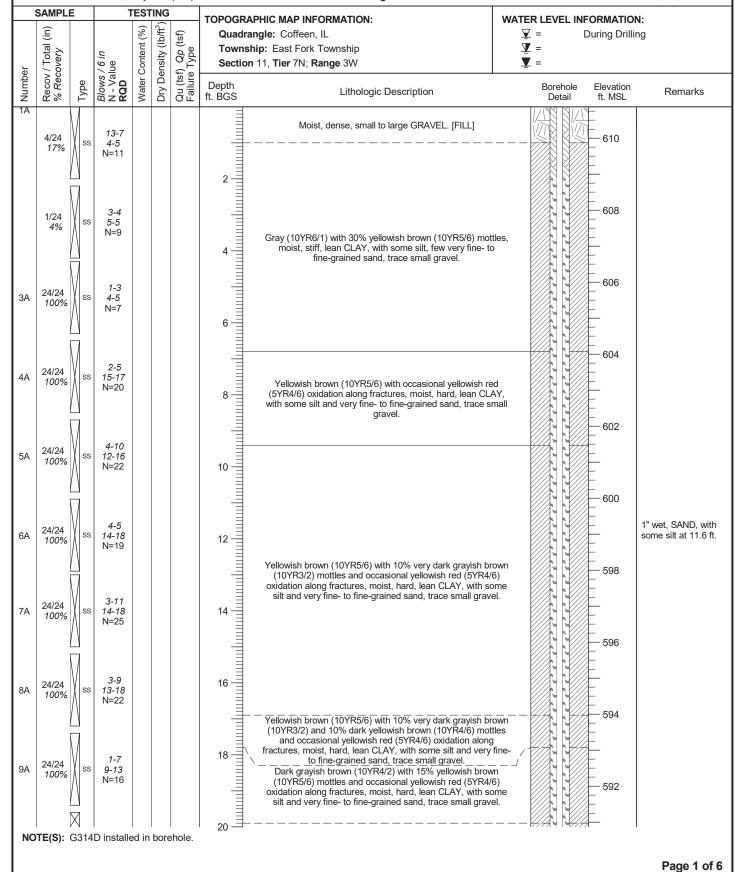
BOREHOLE ID: G314D **Well ID**: G314D

 Surface Elev:
 610.87 ft. MSL

 Completion:
 100.30 ft. BGS

 Station:
 871,642.00N

2.516.853.90E



CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois Project: 20E0111A

DATES: Start: 2/10/2021 Finish: 2/12/2021

WEATHER: Overcast, very cold (10s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter



BOREHOLE ID: G314D Well ID: G314D

> Surface Elev: 610.87 ft. MSL Completion: 100.30 ft. BGS Station: 871,642.00N

2.516.853.90E SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: Ξ Dry Density (lb/ft³ Water Content (%) Quadrangle: Coffeen, IL ▼ = **During Drilling**) Qp (tsf) Type Recov / Total (% Recovery **V** = Township: East Fork Township Blows / 6 in N - Value **RQD** Section 11, Tier 7N; Range 3W ▼ = Qu (tsf) Failure T Number Borehole Elevation Lithologic Description Remarks Detail ft. MSL 1" wet, SAND, with 1-5 some silt at 20 ft. 24/24 10A 10-13 100% N=15 590 Dark grayish brown (10YR4/2) with 15% yellowish brown (10YR5/6) and 5% dark yellowish brown (10YR4/6) mottles and occasional yellowish red (5YR4/6) oxidation along fractures, moist, hard, lean CLAY, with some silt and very fine-to fine-grained sand, trace small gravel. Frequent oxidation below 21 7 ft 1-6 24/24 11A 9-12 100% [Continued from previous page] 588 N=15 4-7 24/24 10-13 586 12A 100% 26 3-7 584 24/24 13A 10-13 100% N=17 1 ft vertical fracture with yellowish red (5YR4/6) oxidation at 582 4-6 24/24 28.3 ft. 14A 10-10 Dark grayish brown (10YR4/2), moist, hard, lean CLAY, with 100% N=16 some silt and very fine- to fine-grained sand, trace small gravel. 30 580 3-9 24/24 15A 10-12 100% N=19 - 578 2-3 24/24 16A 7-8 100% N=10 Trace roots below 34 17A 576 Gray (GLEY15/), moist, stiff, lean CLAY, with some silt. 24/24 7-9 100% 36 N=11 574 18A Dark grayish brown (10YR4/2), moist, hard, lean CLAY, with some silt and very fine- to fine-grained sand, trace small gravel 21/24 and roots. 88% 572 2-5 NOTE(S): G314D installed in borehole.

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois Project: 20E0111A

DATES: Start: 2/10/2021 Finish: 2/12/2021

WEATHER: Overcast, very cold (10s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

BOREHOLE ID: G314D Well ID: G314D

Surface Elev: 610.87 ft. MSL Completion: 100.30 ft. BGS 871,642.00N Station:

2.516.853.90E SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: (lb/ft³ **During Drilling** Ξ Water Content (%) ▼ =) Qp (tsf) Type Quadrangle: Coffeen, IL Recov / Total (% Recovery **V** = Township: East Fork Township **Dry Density** *Blows / 6 ir* N - Value **RQD** Section 11, Tier 7N; Range 3W ▼ = Qu (tsf) Failure T Number Depth Borehole Elevation Lithologic Description Remarks ft. BGS ft. MSL 19A 24/24 N=12 100% 570 Trace medium gravel below 41.3 ft. 42 4-8 24/24 20A SS 10-14 100% Dark grayish brown (10YR4/2), moist, hard, lean CLAY, with N=18 some silt and very fine- to fine-grained sand, trace small gravel 568 and roots. [Continued from previous page] 3-9 24/24 21A 13-16 100% N=22 566 46 22A Gray (10YR5/1), wet, dense, SAND, with some silt, few small 12-31 24/24 gravel. 14-11 100% 564 N=45 22B 48 1" SILT, with some sand at 48.2 ft. 24/24 Gray (GLEY15/) with 10% yellowish brown (10YR5/6) mottles. 6-9 23A 562 100% moist, stiff, lean CLAY, with some silt, trace very fine-grained N=10 50 5-11 24/24 560 24A 14-17 100% N=25 52 Yellowish brown (10YR5/6) with 20% gray (GLEY15/) mottles, 558 4-6 24/24 11-15 moist, stiff, lean CLAY, with some silt, trace very fine-grained 100% N=17 556 4-5 20/24 26A 18-30 83% N = 2356 Yellowish brown (10YR5/6), moist, hard, lean CLAY, with some silt, little very fine- to fine-grained sand and small gravel. 554 9-22 20/24 27A 33-33 83% N=55 Yellowish brown (10YR5/6) with 20% gray (GLEY15/) mottles, moist, hard, lean CLAY, with some silt, little very fine- to fine-grained sand and small gravel. Yellowish brown (10YR5/6) with 10% gray (GLEY15/) and 5% dark yellowish brown (10YR4/6) mottles, moist, hard, lean CLAY, with some silt, little very fine- to fine-grained sand and 552 7-19 24/24 28A SS 29-43 small gravel. 100% 60 NOTE(S): G314D installed in borehole.

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 2/10/2021 **Finish:** 2/12/2021

WEATHER: Overcast, very cold (10s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt
Helper: Corey

Eng/Geo: C. Colin Winter

HANSON

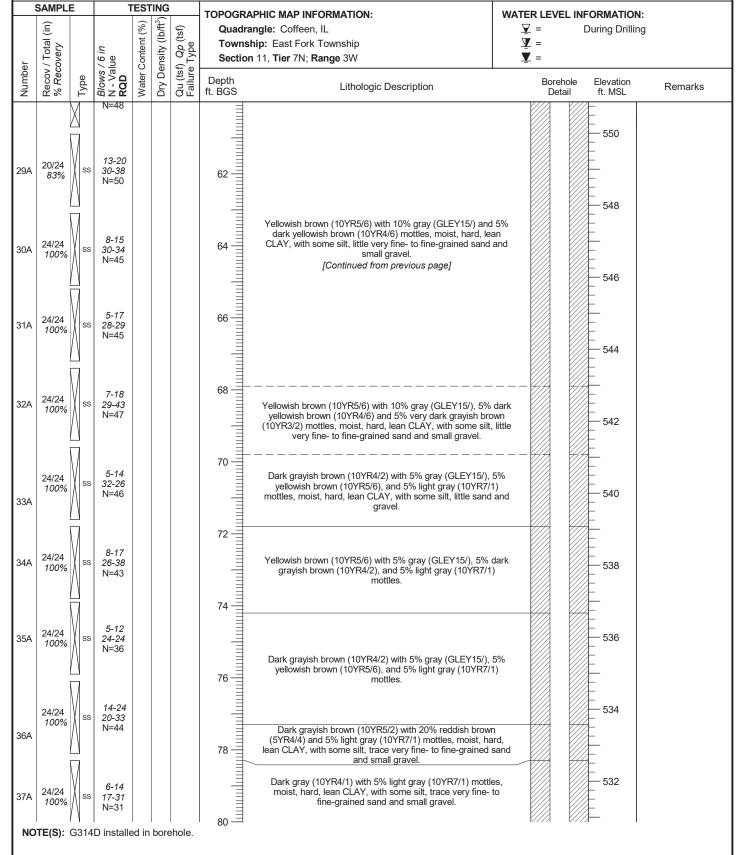
BOREHOLE ID: G314D Well ID: G314D

 Surface Elev:
 610.87 ft. MSL

 Completion:
 100.30 ft. BGS

 Station:
 871.642.00N

2.516.853.90E



CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 2/10/2021 **Finish:** 2/12/2021

WEATHER: Overcast, very cold (10s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig **Drilling Method:** 4.25" HSA w/SS sampler

2.20 110/1 W/00 3d

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

HANSON

BOREHOLE ID: G314D Well ID: G314D

 Surface Elev:
 610.87 ft. MSL

 Completion:
 100.30 ft. BGS

 Station:
 871,642.00N

2,516,853.90E

| | SAMPL | E | 1 | EST | ING | | TOPOGR | APHIC MAP INFORMATION: | WATER | I EVEL IN | FORMATIO | M• |
|------------|----------------------------------|------|----------------------------------|-------------------|----------------------|-----------------------------------|-------------------|---|-------------|--------------------|--|--|
| | (ii) | | | (%) | b/ft³) | (st) | Quadra | angle: Coffeen, IL | : | = | During Drilli | |
| | otal ery | | in | tent | <u> ₹</u> | 3 <i>p</i> (t | Towns | hip: East Fork Township | <u> </u> | | | |
| er | V / T | | s / 6 alue | S | ensi | sf) (s e T) | Section | n 11, Tier 7N; Range 3W | Ţ: | = | | |
| Number | Recov / Total (in) % Recovery | Туре | Blows / 6 in N - Value RQD | Water Content (%) | Dry Density (lb/ft³) | Qu (tsf) Qp (tsf) Failure Type | Depth ft. BGS | Lithologic Description | | Borehole Detail | Elevation ft. MSL | Remarks |
| 38A | 24/24 100% | ss | 7-17 21-29 N=38 | | | | 82 — | Dark gray (10YR4/1) with 5% light gray (10YR7/1) mottl moist, hard, lean CLAY, with some silt, trace very fine- fine-grained sand and small gravel. [Continued from previous page] | es, to | | 530 | Trace roots at 82 ft. |
| 39A | 24/24 100% | ss | 8-24 26-27 N=50 | | | | 84 - | Very dark gray (10YR3/1), moist, hard, lean CLAY, with s silt. | ome | | | |
| 40A | 24/24 100% | ss | 5-9 10-13 N=19 | | | | 86 | Dark gray (10YR4/1) with 5% black (10YR2/1) mottles, m hard, lean CLAY, with some silt. | oist, | | 526 - - - - - - - - - - - - - - - - - - - | |
| 41A | 24/24 100% | SS | 6-10 25-33 N=35 | | | | 88 - | Dark greenish gray (GLEY14/1) with 5% yellowish brov (10YR5/6) mottles, moist, hard, lean CLAY, with some | vn silt. | | 522 | Few very fine- to fine-grained sand below 88 ft. |
| 42A 43A | 11/11 100% 5/5 100% | | 3-50/5" | | | | 90 | Light reddish brown (2.5YR6/3) with 10% gray (GLEY15/) hard, SILT, with few clay and very fine-grained sand. | | | 520 | |
| 44A | 5/5 100% | ∑ ss | 50/5" | | | | 94 — | | | | | |
| 45A | 8/8 100% | ss | 49-50/2" | | | | 96 | | | | | |
| 46A | 11/11 100% | ss | 25-50/5" | | | | 96 98 98 98 | Light reddish brown (2.5YR6/3) with 10% gray (GLEY15/ 5% dark yellowish brown (10YR4/6) mottles, dry, hard, S with few clay and very fine-grained sand. | and ILT, | | | |
| NC | TE(S): | G314 | D installe | ed in | bore | ehole. | 100 | | | | F | |
| | | | | | | | | | | | | Page 5 of 6 |

 $\begin{tabular}{ll} \textbf{CLIENT:} & \textbf{Illinois Power Generating Co.} \\ \end{tabular}$

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 2/10/2021 **Finish:** 2/12/2021

WEATHER: Overcast, very cold (10s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

HANSON

BOREHOLE ID: G314D Well ID: G314D

 Surface Elev:
 610.87 ft. MSL

 Completion:
 100.30 ft. BGS

 Station:
 871,642.00N

2,516,853.90E

| | SAMPL | TESTING | | | | TOPOGRAPHIC MAP INFORMATION: | | WATER LEVEL IN | FORMATION: | | |
|--------|----------------|---------|----------------------------------|-------------------|-----------------|-----------------------------------|--|-------------------------------------|---------------------|-------------------|---------|
| Number | (in) | | Blows / 6 in N - Value RQD | Water Content (%) | ensity (lb/ft³) | Qu (tsf) Qp (tsf) Failure Type | Quadrangle: Coffeen, IL Township: East Fork Township | | ▼ = During Drilling | | |
| | otal ery | | | | | | | | <u>Ā</u> = | | |
| | - % | | | | | | Section | 11, Tier 7N; Range 3W | ▼ = | | |
| | Recov % Rec | Type | | | Dry De | | Depth ft. BGS | Lithologic Description | Borehole Detail | Elevation ft. MSL | Remarks |
| 47 | A 3/3 | ∑ ss | 50/3" | | | | | | | | |
| 4000/ | | | | | | | | | | | |

100% End of boring = 100.3 feet

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 1/13/2021 **Finish:** 1/13/2021

WEATHER: Overcast, cool (40s)

CONTRACTOR: Roberts

Rig mfg/model: GeoProbe 8040DT

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

HANSON

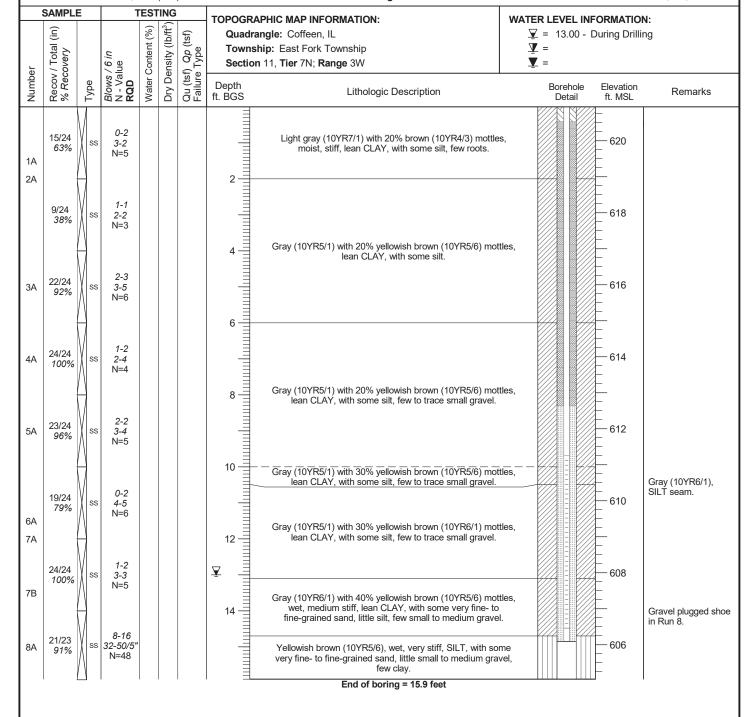
BOREHOLE ID: G315 Well ID: G315

 Surface Elev:
 620.94 ft. MSL

 Completion:
 15.90 ft. BGS

 Station:
 871,385.00N

2.516.086.60E



CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 1/14/2021 **Finish:** 1/14/2021

WEATHER: Overcast, cold (30s)

CONTRACTOR: Roberts

Rig mfg/model: GeoProbe 8040DT

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

HANSON

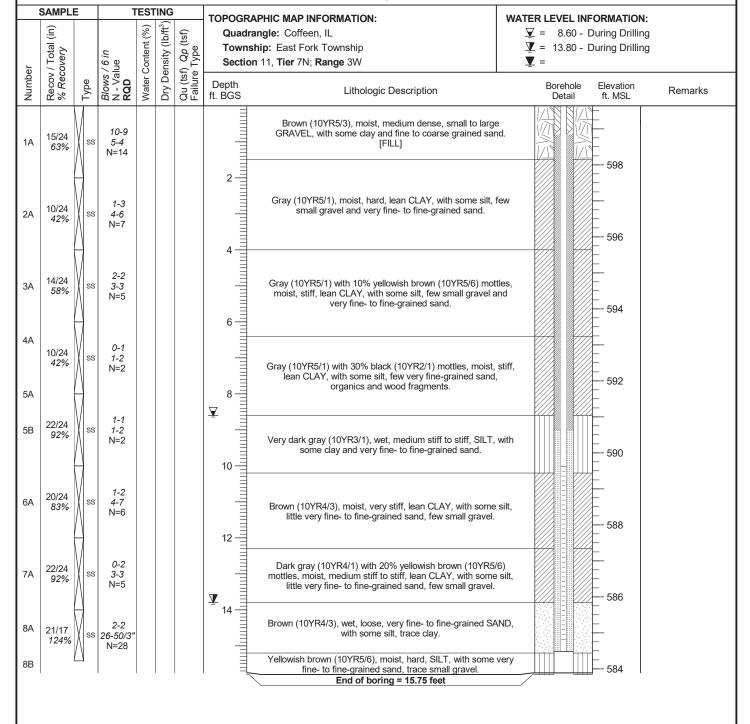
BOREHOLE ID: G316 Well ID: G316

 Surface Elev:
 599.64 ft. MSL

 Completion:
 15.75 ft. BGS

 Station:
 871,643.10N

2,517,211.60E



CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois Project: 20E0111A

DATES: Start: 1/13/2021 Finish: 1/14/2021

WEATHER: Overcast, cold (30s to 40s)

CONTRACTOR: Roberts

Rig mfg/model: GeoProbe 8040DT Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter



BOREHOLE ID: G317 Well ID: G317

Surface Elev: 638.85 ft. MSL Completion: 36.00 ft. BGS 871,234.20N Station:

Page 1 of 2

2,517,087.40E SAMPLE TESTING TOPOGRAPHIC MAP INFORMATION: WATER LEVEL INFORMATION: (lb/ft³ Ξ Water Content (%) ∇ = 34.00 - During Drilling) Qp (tsf) Type Quadrangle: Coffeen, IL Recov / Total (% Recovery **V** = Township: East Fork Township Dry Density *Blows / 6 ir* N - Value **RQD** ▼ = Section 11, Tier 7N; Range 3W Qu (tsf) Failure T Number Borehole Elevation Lithologic Description Remarks ft. MSL 2-2 17/24 638 SS 5-3 1A 71% Light yellowish brown (10YR6/4) with 20% yellowish brown (10YR5/6) mottles, moist, stiff, lean CLAY, with some silt, little 3-5 fine-grained sand and small to medium gravel, trace to no 12/24 636 2A SS 4-4 50% N=91-2 15/24 634 3A 3-4 63% N=5 Gray (10YR6/1) with 20% yellowish brown (10YR5/6) mottles, moist, stiff, lean CLAY, with some silt, few fine-grained sand and small gravel. 3-5 632 11/24 SS 5-4 46% N = 104A Brownish yellow (10YR6/8) with 20% gray (10YR6/1) mottles, moist, stiff, SILT, with little fine-grained sand and small gravel. 12/24 630 4-4 50% N=8 5A 6A 10 Wood fragment plugged shoe in Run 2-2 4/24 628 Gray (10YR5/1) with 30% very dark gray (20YR3/1) mottles, moist, very stiff, lean CLAY, with some silt, trace lignite fragments and organics. SS 3-4 17% N=5 Gravel plugged shoe in Run 7. 626 14/24 7A 4-3 58% N=7 7B Gray (10YR5/1) with 10% yellowish brown (10YR5/4) mottles, moist, stiff, SILT, with some fine-grained sand, little small gravel. 2-2 20/24 624 88 SS 3-4 Gray (10YR5/1) with 10% yellowish brown (10YR5/4) and 10% 83% N=5 very dark gray (10YR3/1) mottles, moist, very stiff, lean CLAY, with some silt, few fine-grained sand and small gravel. 16 17/24 622 3-4 71% N=5 Gray (10YR5/1) with 10% very dark gray (10YR3/1) mottles, moist, medium stiff, lean CLAY, with some silt, little small gravel, trace lignite fragments and organics. 0-2 16/24 620 10A SS 5-5 67% N=7 Thin wood fragment seam at 19.4 ft. NOTE(S): G317 installed in borehole.

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois Project: 20E0111A

DATES: Start: 1/13/2021 **Finish:** 1/14/2021

WEATHER: Overcast, cold (30s to 40s)

CONTRACTOR: Roberts

Rig mfg/model: GeoProbe 8040DT **Drilling Method:** 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt
Helper: Corey

Eng/Geo: C. Colin Winter

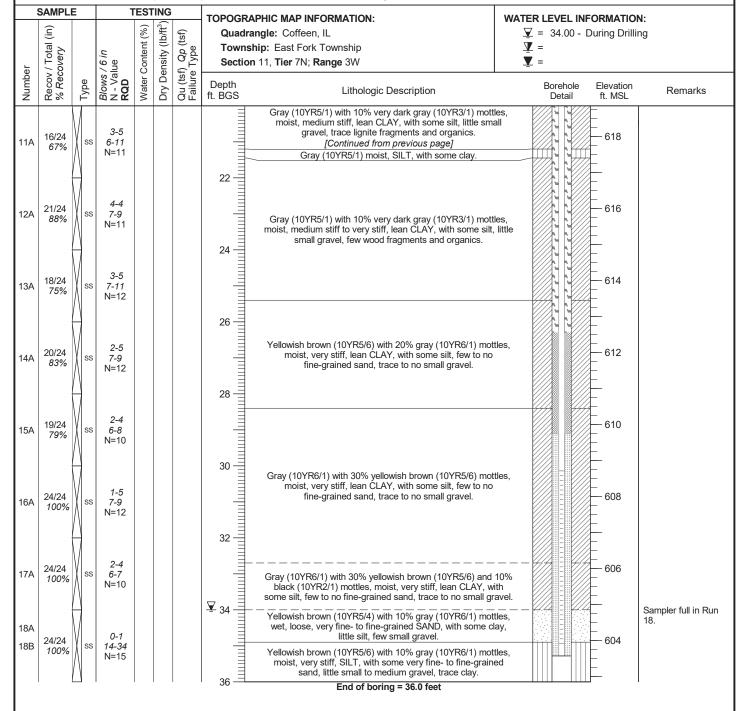
HANSON

Well ID: G317

Surface Elev: 638.85 ft. MSL

Completion: 36.00 ft. BGS **Station:** 871,234.20N

2,517,087.40E



FIELD BORING LOG

CLIENT: Illinois Power Generating Co.

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 2/8/2021 **Finish:** 2/8/2021

WEATHER: Overcast, very cold (10s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig

Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt Helper: Corey

Eng/Geo: C. Colin Winter

HANSON

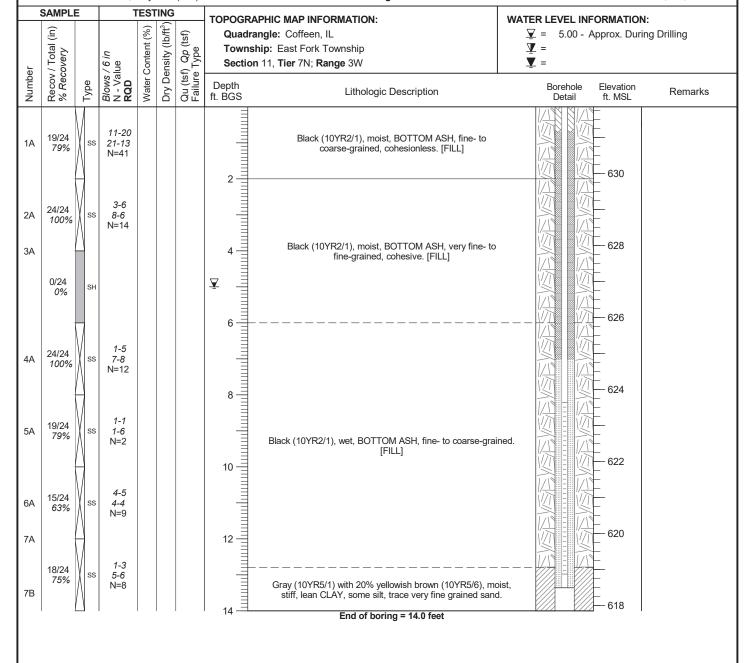
BOREHOLE ID: XPW01
Well ID: XPW01

 Surface Elev:
 631.85 ft. MSL

 Completion:
 14.00 ft. BGS

 Station:
 871,638.70N

2.515.366.30E



FIELD BORING LOG

 $\begin{tabular}{ll} \textbf{CLIENT:} & \textbf{Illinois Power Generating Co.} \\ \end{tabular}$

Site: Coffeen Part 845 Groundwater

Location: Coffeen, Illinois **Project:** 20E0111A

DATES: Start: 2/8/2021 **Finish:** 2/8/2021

WEATHER: Overcast, very cold (10s)

CONTRACTOR: Roberts

Rig mfg/model: CME-75 Track Rig Drilling Method: 4.25" HSA w/SS sampler

FIELD STAFF: Driller: Matt
Helper: Corey

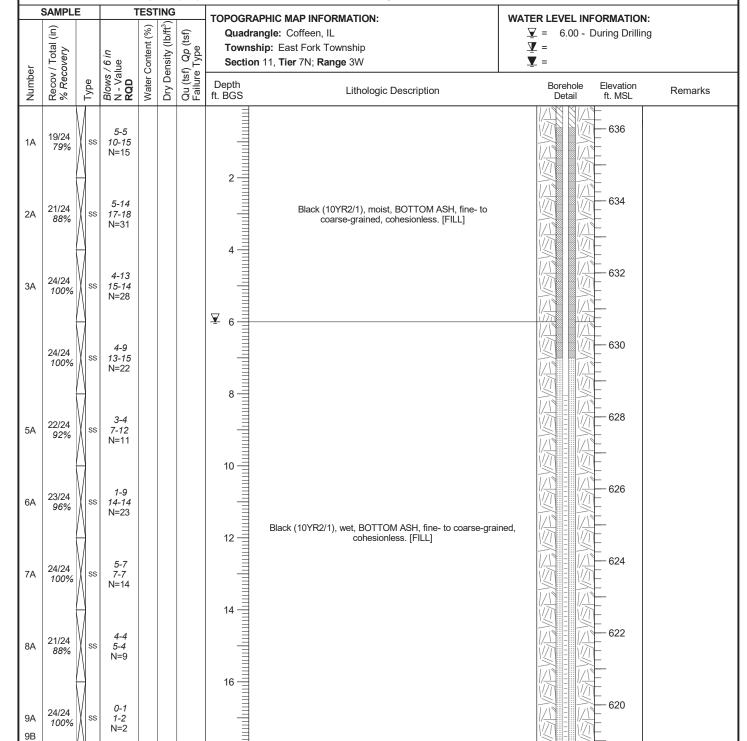
Eng/Geo: C. Colin Winter

HANSON

BOREHOLE ID: XPW02 Well ID: XPW02

Surface Elev: 636.64 ft. MSL Completion: 18.00 ft. BGS

Station: 871,987.10N 2,515,627.30E



Dark gray (10YR4/1), moist, very soft, SILT, some clay.

End of boring = 18.0 feet



| Illinois Environ | mental Protection Ag | gency | | | | Well | Completi | on Report |
|---|---|-----------|-----------|-----------|----------------------------|-----------------|------------------------------------|-------------------------|
| Site #: | Coun | ty: Mon | tgomery | 7 | | W | Vell #: | G45D |
| Site Name:Coffeen Power Sta | ation - Ash Pond 2 | | | | | В | orehole #: | G405D |
| State Plane Coordinate: X 2,515,322 | 2.2 Y 873,998.0 (or) | Latitude: | 39 | 3! | 51.657Ä | Longitud | e:89 | 23! 46.612Ä |
| Surveyed By: <u>Gary C. Rogers</u> | | | IL Regi | stration | #: <u>035-00</u> | 02957 | | |
| Drilling Contractor: Bulldog D | | | Driller: | J. D | ittmaier | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | | Geologi | ist: R | honald W. | Hasenyage | r, LPG #196-0 | 000246 |
| Drilling Method: Hollow stem | auger | | Drilling | g Fluid (| Гуре):no | ne | | |
| Logged By: Kristen L. Theesf | èld | | Date St | arted: _ | 8/16/20 | 16 Dat | e Finished: | 8/17/2016 |
| Report Form Completed By: Su | | | | | /24/2016 | | | |
| ANNULAR SPA | | | _ | El | evations (MSL)* | Depths (BGS) | (0.01 | ft.) |
| | | | | | 624.16_ | 3.22_ | Top of Protec | tive Casing |
| | | | | _ | 623.81 | 2.87 | Top of Riser I | Pipe |
| Type of Surface Seal: Concrete | | | | × | 620.94 | 0.00 | Ground Surfa | ce |
| | | | | 7 | 618.94 | 2.00 | Top of Annula | ar Sealant |
| Type of Annular Sealant: High- | | | | | | | • | |
| Installation Method: Tremic | <u>e</u> | | 7 | | | | Ct-ti- W-t I | 1 |
| Setting Time:>24 hours | | | <u>/-</u> | _ | | | Static Water I (After Completic | |
| Type of Bentonite Seal Gran | Pellet Slurry (choose one) | | | | | | | |
| Installation Method: Gravit | ` , | | | _ | 590.59 | 30.35 | Top of Seal | |
| Setting Time: <u>38 minutes</u> | | | | | 589.62 | 31.32 | Top of Sand I | Pack |
| The CC III I | | | V | | | | 1 | |
| Type of Sand Pack: Quartz San Grain Size: 10-20 (six | | | | _ | 589.06_ | _31.88_ | Top of Screen | |
| Installation Method: Gravit | | | | | | | | |
| installation victiod. Oravic | <u>y</u> | | | _ | 579.42 | 41.52 | Bottom of Scr | reen |
| Type of Backfill Material: <u>n/a</u> | (if applicable) | | _ | _ | 579.02 | 41.92 | Bottom of We | 211 |
| Installation Method: | | | | _ | 578.94 | 42.00 | Bottom of Bo | rehole |
| | | | | * | Referenced to a | National Geodet | ic Datum | |
| | | | | | CAS | ING MEA | SUREMENTS | S |
| WELL COM | | | | Diame | ter of Boreho | ole | (inch | nes) 8.0 |
| | STRUCTION MATERIALS type of material for each area) | | | | Riser Pipe | | (inch | |
| | | | | | ive Casing L | ength | • | eet) 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC | OTHER: St | teel | | ipe Length of Screen to | Fnd Can | | eet) 34.75 eet) 0.40 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC | OTHER: | | | Length (1s | • | | eet) 9.64 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC | OTHER: | | | ength of Cas | | | eet) 44.79 |

PTFE PVC OTHER:

SS304

Well Completion Form (revised 02/06/02)

SS316

Total Length of Casing

**Hand-Slotted Well Screens Are Unacceptable

Screen Slot Size **

| Illinois Environ | nmental Protection Agency | 7 | | Well | Completion | Report |
|--|------------------------------------|-----------------------|--|-----------------|-------------------------|-------------------|
| Site #: | County: N | Montgomery | | W | Vell #:G4 | 6D |
| Site Name: Coffeen Power St | ation - Ash Pond 2 | | | В | orehole #:G | 406D |
| State Plane Coordinate: X 2,514,69 | 7.8 Y 872,519.7 (or) Latitud | de: <u>39</u> _ | 3! <u>37.098</u> Ä | Longitud | e: <u>-89</u> <u>23</u> | <u>! 54.687</u> Ä |
| Surveyed By: Gary C. Rogers | | IL Registra | ation #:035-00 | 02957 | | |
| Drilling Contractor: Bulldog I | Orilling, Inc. | _ Driller: _ | J. Dittmaier | | | |
| Consulting Firm: Hanson Prof | fessional Services Inc. | Geologist: | Rhonald W. | Hasenyager | , LPG #196-0002 | 246 |
| Drilling Method: Hollow stem | n auger | Drilling Fl | uid (Type): <u>no</u> | ne | | |
| Logged By: Kristen L. Thees | feld | Date Start | ed: 8/19/20 | 16 Date | e Finished: 8/1 | 9/2016 |
| Report Form Completed By: Su | uzanna L. Keim | Date: | 8/24/2016 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | _625.53_ | -3.62 | Top of Protective | Casing |
| | | | 625.24 | -3.33 | Top of Riser Pipe | _ |
| Type of Surface Seal: Concrete | | | 621.91_ | 0.00 | Ground Surface | |
| | | | 619.91 | 2.00 | Top of Annular S | ealant |
| Type of Annular Sealant: High- | , J | | | | | |
| Installation Method:Tremi Setting Time: _ >24 hours | e | | | | Static Water Leve | 5 1 |
| Setting Time. 224 flours | | $ \overline{\Delta} $ | | | (After Completion) | a · |
| Type of Bentonite Seal Gran | nular Pellet Slurry (choose one) | | | | | |
| Installation Method: Gravit | , , | | 582.34 | 39.57 | Top of Seal | |
| Setting Time:>12 hours | | 1 🔼 | 581.21 | 40.70 | Top of Sand Pack | (|
| Towns of Court Doubles Court of | | | | | • | |
| Type of Sand Pack: Quartz San Grain Size: 10-20 (si | | | 580.30 | 41.61 | Top of Screen | |
| Installation Method: Gravin | · · | | | | | |
| | ., | | 570.65 | 51.26 | | |
| Type of Backfill Material:n/a | (if applicable) | | 570.26 | _51.65_ | Bottom of Well | |
| Installation Method: | | | 569.91 | 52.00 | Bottom of Boreho | ole |
| | | | * Referenced to a | National Geodet | ic Datum | |
| | | | CAS | ING MEAS | SUREMENTS | |
| WELL CON | STRUCTION MATERIALS | | riameter of Boreho | | (inches) | 8.0 |
| | ne type of material for each area) | | O of Riser Pipe | | (inches) | 5.0 |
| | | | rotective Casing L iser Pipe Length | engtn | | 44.94 |
| Protective Casing | SS304 SS316 PTFE PVC OTHE | - @ | ottom of Screen to | | (feet) | 0.39 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHE | | creen Length (1s | | ` | 9.65 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHE | _ | otal Length of Cas | | (feet) | 54.98 |

PTFE PVC OTHER:

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

SS304

Well Completion Form (revised 02/06/02)

SS316

| Illinois Environ | mental Protection Agency | | | Well | Completion | Report |
|--|--|------------------|------------------------|------------|---|------------------|
| Site #: | County: Mo | ntgomery | | W | Vell #: G1 | 01 |
| Site Name: CCB Management | t Facility | | | В | orehole #: | G101 |
| State Plane Coordinate: X 2,514,214 | 4.3 Y 876,551.8 (or) Latitude: | 39 | 4! <u>17.000</u> Ä | Longitud | e: <u>-89</u> <u>2</u> 4 | <u>1! 0.400Ä</u> |
| Surveyed By: | ck | IL Registi | ration #: <u>035-0</u> | 03507 | | |
| Drilling Contractor: <u>Layne-We</u> | stern Co | Driller: _ | T. List | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | Geologist | : Rhonald W. | Hasenyager | r, LPG #196-000 | 246 |
| Drilling Method: Hollow stem | auger | Drilling F | luid (Type):n/a | ì | | |
| Logged By: Suzanna Simpson | - I | Date Star | ted: 2/2/201 | 10 Dat | e Finished: 2/ | 2/2010 |
| | zanna Simpson | | 2/4/2010 | | | |
| ANNULAR SPA | - | | Elevations | | (0.01 ft.) | |
| | | | (MSL)* | (BGS) | | |
| | | | 627.89 | 2.62_ | Top of Protective | Casing |
| | | | 627.60 | -2.33 | Top of Riser Pipe | ; |
| Type of Surface Seal: Concrete | | | 625.27_ | 0.00 | Ground Surface | |
| T CA L C L 4 HT L | | | 622.27 | 3.00 | Top of Annular S | ealant |
| Type of Annular Sealant: High-s | 7 | | | | | |
| Installation Method: Tremie | | | 617.06 | 7.31 | Statio Water I ave | -1 |
| Setting Time: >24 hr. | | $raket{\square}$ | 617.96 | | Static Water Leve (After Completion) | |
| Type of Bentonite Seal Grant | | | | | | |
| Installation Method: Gravit | (choose one) | | 614.27 | 11.00 | Top of Seal | |
| Setting Time: 20 min | | | (12.14 | | | |
| | | | 612.14 | 13.13 | Top of Sand Pack | <u> </u> |
| Type of Sand Pack: Quartz sand | <u>i</u> | | 600.50 | 15 60 | Tf.C | |
| Grain Size:10/20 (sie | eve size) | | 609.59 | _15.68_ | Top of Screen | |
| Installation Method: Gravity | y | | 604.95 | 20.32 | Bottom of Screen | |
| Type of Backfill Material:Quar | | | 604.38 | 20.89 | Bottom of Well | |
| Installation Method: Gravit | (if applicable) | | 603.35 | 21.92 | Bottom of Boreho | ale |
| mountain mounds. <u>Starts</u> | | | * Referenced to a | | | <i>,</i> 10 |
| | | | CAS | SING MEAS | SUREMENTS | |
| | | Ι | Diameter of Boreho | ole | (inches) | 8.0 |
| | STRUCTION MATERIALS e type of material for each area) | I | D of Riser Pipe | | (inches) | 2.0 |
| | | P | Protective Casing L | ength | (feet) | 5.0 |
| D + +: C : | GG204 GG216 PURE PURE 1 | | Riser Pipe Length | | (feet) | 18.01 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER: (SS304 SS316 PTFE (PVC) OTHER: | | Bottom of Screen to | | (feet) | 0.57 |
| Riser Pipe Above W.T. Riser Pipe Below W.T. | SS304 SS316 PTFE (PVC) OTHER: SS304 SS316 PTFE (PVC) OTHER: | | Screen Length (1s | | | 4.64 |
| | The state of the s | _1 | Total Length of Ca | sing | (feet) | 23.22 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | mental Protection Agency | 7 | | Well (| Completion | Report |
|---------------------------------------|-----------------------------------|---------------------------------------|--|---------------------|---|--------|
| Site #: | County: N | Montgomery_ | | Wel | II #: <u>G102 (</u> N | MW3S) |
| Site Name: CCB Management | t Facility | | | Bor | ehole #:SI | 3-03a |
| State Plane Coordinate: X 2,514,531 | 1.5 Y 876,554.8 (or) Latitud | de: | | Longitude: | | |
| Surveyed By: <u>Darren E. Forgy</u> | 7 | IL Regist | tration #: <u>035-0</u> | 03637 | | |
| Drilling Contractor: Testing Se | ervice Corp. | _ Driller: _ | B. Williamson | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | Geologis | t: Rhonald W. | Hasenyager, | LPG #196-0002 | 246 |
| Drilling Method: Hollow stem | auger | Drilling I | Fluid (Type): Po | table water | | |
| Logged By: Testing Services (| Corp. | Date Star | rted: 4/28/20 | 006 Date I | Finished: 4/2 | 8/2006 |
| Report Form Completed By: Rh | onald W. Hasenyager | Date: | 6/7/2006 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | _ | | 629.45 | , , | Γop of Protective | Casing |
| | | | 628.96 | 3.26 | Γop of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 625.70 | 0.00 | Ground Surface | |
| | | | 623.70 | | Γop of Annular Se | -alant |
| Type of Annular Sealant: Benton | nite chips | | 023.70 | | rop or rumular so | zarant |
| Installation Method: Gravity | <u>y</u> | | | | | |
| Setting Time: +24 hr. | | $\mid \overline{\triangle} \mid \mid$ | 618.67 | | Static Water Leve (After Completion) 6 | |
| Type of Bentonite Seal Gran | ular Pellet Slurry (choose one) | | | | | |
| Installation Method: Gravit | v | | 623.70 | | Γop of Seal | |
| Setting Time:+24 hr. | | | 616.20 | 9.50 | Гор of Sand Pack | |
| Type of Sand Pack: Quartz sanc | | | | | | |
| Grain Size: #5 (sie | | | 613.68 | 12.02 | Γop of Screen | |
| Installation Method: Gravit | | | | | | |
| | , | | 608.92 | | Bottom of Screen | |
| Type of Backfill Material: <u>n/a</u> | (if applicable) | | _608.55_ | 17.15 I | Bottom of Well | |
| Installation Method:n/a | | | 608.55 | | Bottom of Boreho | le |
| | | | * Referenced to a | National Geodetic 1 | Datum | |
| | | | CAS | SING MEASU | JREMENTS | |
| WELL CONS | STRUCTION MATERIALS | | Diameter of Boreho | ole | (inches) | 8.0 |
| | e type of material for each area) | | ID of Riser Pipe | anath | (inches) | 5.0 |
| | | | Protective Casing L Riser Pipe Length | zingun | (feet) | 15.28 |
| Protective Casing | SS304 SS316 PTFE PVC OTHE | | Bottom of Screen to | o End Can | (feet) | 0.37 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHE | | Screen Length (1s | | (feet) | 4.76 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHE | _ | Total Length of Cas | | (feet) | 20.41 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

| Illinois Enviro | onmental Protection Agenc | e y | | Well | Completion | Report |
|---|---|----------------------------|--|------------------------------|---|---------------|
| Site #: | County: N | Iontgomery | I | V | Vell #: G1 | 03 |
| Site Name: AEG Coffeen Po | ower Station CCB Management Facili | ity | | В | orehole #: | G103 |
| State- Plant Plane Coordinate: X 2,514,50 | 01.2 Y 876,199.5 (or) Latitud | le: | · | Longitud | e:° | _'" |
| Surveyed By: | rick | _ IL Regi | istration #:035-0 | 03507 | | |
| Drilling Contractor: <u>Layne-W</u> | Vestern Co | _ Driller: | T. List | | | |
| Consulting Firm: Hanson Pro | ofessional Services Inc. | _ Geolog | ist: Rhonald W. | Hasenyage | r, LPG #196-000 | 246 |
| Drilling Method: Hollow ster | m auger | _ Drilling | g Fluid (Type):n/a | ı | | |
| Logged By: Suzanna L. Sim | pson | _ Date St | arted: 2/15/20 | 10 Dat | e Finished: 2/1 | 5/2010 |
| Report Form Completed By:S | uzanna L. Simpson | _ Date: _ | 2/18/2010 | | | |
| ANNULAR SPA | ACE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | <u></u> | | _634.07_ | 3.08 | Top of Protective | Casing |
| | | | 633.80 | 2.81 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 630.99 | 0.00 | Ground Surface | |
| Type of Annular Sealant: High | -solids bentonite | | 624.93 | 6.06 | Top of Annular S | ealant |
| Installation Method:Trem | ie J | | | | | |
| Setting Time: >24 hr. | | $ \underline{\nabla} $ | 614.00 | 16.99 | Static Water Leve (After Completion) | |
| Type of Bentonite Seal Gra | | | | | | |
| Installation Method: Gravi | (choose one) | | 618.51 | 12.48 | Top of Seal | |
| Setting Time: 8 min | | | 617.35 | _13.64_ | Top of Sand Pack | : |
| Type of Sand Pack: Quartz sar | nd | | | | | |
| | sieve size) | | 615.11 | 15.88 | Top of Screen | |
| Installation Method: Gravi | ity | | | | | |
| Type of Backfill Material:n/a | | | 610.32 609.90 | <u>20.67</u> <u>21.09</u> | Bottom of Screen Bottom of Well | |
| Installation Mathed: n/o | (if applicable) | | 609.90 | 21.09 | Dattam of Daroha | Jo. |
| Installation Method: <u>n/a</u> | | | * Referenced to a | | Bottom of Boreho | ne |
| | | | CAS | ING MEA | SUREMENTS | |
| WELL CON | | | Diameter of Boreho | ole | (inches) | 8.0 |
| | STRUCTION MATERIALS one type of material for each area) | | ID of Riser Pipe | | (inches) | 2.0 |
| | | | Protective Casing L | ength | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | R: (Steel) | Riser Pipe Length Bottom of Screen to | End Con | (feet) | 18.69 0.42 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | | Screen Length (1s | | (feet) | 4.79 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | R: | Total Length of Cas | | (feet) | 23.90 |
| Screen | SS304 SS316 PTFE PVC OTHE | R: | Screen Slot Size ** | | (inches) | 0.010 |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | nmental Protection Agency | y | | Well | Completion | Report |
|--|------------------------------------|------------|-------------------------------------|------------------------|---|--------|
| Site #: | County: | ontgomery | | W | Vell #:G1 | 04 |
| Site Name: AEG Coffeen Pov | wer Station CCB Management Facilit | у | | В | orehole #: | 104 |
| State- Plant Plane Coordinate: X 2,514,505 | 5.0 Y 875,849.3 (or) Latitude | ::° | | Longitud | e:° | |
| Surveyed By:Jeffrey D. Emri | ck | IL Regis | tration #:035-0 | 03507 | | |
| Drilling Contractor: <u>Layne-We</u> | estern Co | Driller: | T. List | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | Geologis | et: Rhonald W. | Hasenyage | er, LPG #196-000 | 246 |
| Drilling Method: Hollow stem | auger | Drilling l | Fluid (Type):n/a | a | | |
| Logged By: Suzanna L. Simp | son | _ Date Sta | rted: 2/15/20 | 010 Dat | e Finished: 2/1 | 5/2010 |
| Report Form Completed By: Su | zanna L. Simpson | Date: | 2/18/2010 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | _633.29_ | ` / | Top of Protective | Casing |
| | | | 632.94 | -2.82 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 630.12 | 0.00 | Ground Surface | |
| Type of Annular Sealant: High-s | solids bentonite | | 624.92 | 5.20 | Top of Annular So | ealant |
| Installation Method:Tremie | ; | | | | | |
| Setting Time:>24 hr. | | ∇ | 614.72 | _15.40_ | Static Water Leve (After Completion) | |
| Type of Bentonite Seal Gran | | | | | | |
| Installation Method: <u>Gravity</u> | (choose one) | × | 619.17 | _10.95_ | Top of Seal | |
| Setting Time: 10 min | | | 617.42 | _12.70_ | Top of Sand Pack | |
| Type of Sand Pack: Quartz sand | <u> </u> | | | | | |
| Grain Size:10/20 (sie | eve size) | | 615.21 | 14.91 | Top of Screen | |
| Installation Method: Gravity | <u>/</u> | | 610.51 | 19.61 | Bottom of Screen | |
| Type of Backfill Material: Quart | tz sand (if applicable) | | 610.04 | 20.08 | Bottom of Well | |
| Installation Method: <u>Gravity</u> | <u> </u> | | 607.92 * Referenced to a | 22.20 National Geodeti | Bottom of Boreho | le |
| | | | | | | |
| | | Г | | | SUREMENTS | |
| | TRUCTION MATERIALS | | Diameter of Boreho ID of Riser Pipe | ole | (inches) | 2.0 |
| (Choose on | ne type of material for each area) | | Protective Casing I | enoth | (inches) | 5.0 |
| | | | Riser Pipe Length | 20115011 | (feet) | 17.73 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | | Bottom of Screen to | o End Cap | (feet) | 0.47 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | : | Screen Length (1: | st slot to last slo | ot) (feet) | 4.70 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | : [] | Total Length of Ca | sino | (feet) | 22 90 |

PTFE PVC OTHER:

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

(inches)

SS304

Well Completion Form (revised 02/06/02)

SS316

ILLINOIS DEPARTMENT OF PUBLIC HEALTH DIVISION OF ENVIRONMENTAL HEALTH 525 W. JEFFERSON ST. SPRINGFIELD, IL 62761

WATER WELL SEALING FORM

TYPE OR PRESS FIRMLY

RETURN ALL COPIES TO IDPH OR LOCAL HEALTH DEPARTMENT

This form shall be submitted to this Department or the local health department not more than 30 days after a water well, boring or monitoring well is sealed. Such wells are to be sealed not more than 30 days after they are abandoned in accordance with the sealing requirements in the Water Well Construction Code. THE LOCAL HEALTH DEPARTMENT OR REGIONAL PUBLIC HEALTH DEPARTMENT MUST BE NOTIFIED AT LEAST 48 HOURS PRIOR TO SEALING.

| Ownership (Name of Controlling Party) AEG C | offeen Power Stat | tion | | | (G104) | |
|---|-------------------|----------|-------------|-----------------|-----------|----|
| Well Location 134 CIPS Trail | | Co | offeen | | Montgome | ry |
| Address - Lot Number | | | City | | County | |
| General Description Township 7 (N) | Range_ | 3 | _(K)(W) | | Section _ | 1 |
| SEQuarter of theNE | Quarter of the | NI | E(| Quarter | | |
| Year Drilled 2010 | | | | | | |
| Drilling Permit Number (and date, if known)n/a | | | | | | |
| Type of Well Bored Drilled_ ✓ | Other | | | | | |
| Total Depth 20.0 ft. Diam | eter (inches) | 2 | | | | |
| Formation clear of obstruction _ ✓ Yes | | | | | | |
| DETAILS OF PLUGGING | | | | | | |
| | | 0.5 | , | | | |
| Filled with Bentonite grout (cement or other materials) | from | 0.5 | to² | 20.0 ft. | | |
| | | | | | | |
| Kind of plug Random soil | from | 0 | to' | J.5ft. | | |
| Filled with | from | | to | ft. | | |
| Kind of plug | from | | to | ft. | | |
| Filled with | from | | to | ft. | | |
| Kind of plug | from | | to | ft. | | |
| CASING RECORD Upper 2 feet of casing remove | ed <u>√</u> Y€ | es | No | | | |
| Date well was sealed Month October Da | ay8 | Year_ | 2010 | _· | | |
| Licensed water well driller or other person approve | ed by the Depart | ment pe | erforming v | vell sealing | | |
| Rhonald W. Hasenyager, L.P.G. | 196-000 | 246 | | | | |
| Name | Complete | e Licens | se Number | | | |
| Hanson Professional Services Inc., 1525 S. 6th St. | Springfi | eld | | IL 62 | 2703 | |
| Address | City | | | State | e/ZIP | |

This state agency is requesting disclosure of information that is necessary to accomplish the statutory purpose as outlined under Public Act 85-0863. Disclosure of this information is mandatory. This form has been approved by the Forms Management Center.

IL 482-0631

| Illinois Environmental Protection Agency | Well Completion Report |
|--|--|
| Site #: County: Mon | ontgomery Well #: G105 |
| Site Name: AEG Coffeen Power Station CCB Management Facility | Borehole #: G105 |
| State- Plant Plane Coordinate: X 2,514,509.2 Y 875,499.7 (or) Latitude: | |
| Surveyed By: | IL Registration #:035-003507 |
| Drilling Contractor: <u>Layne-Western Co</u> | Driller: T. List |
| Consulting Firm: Hanson Professional Services Inc. | Geologist: Rhonald W. Hasenyager, LPG #196-000246 |
| Drilling Method: Hollow stem auger | Drilling Fluid (Type): <u>n/a</u> |
| Logged By: Suzanna L. Simpson | Date Started: 2/16/2010 Date Finished: 2/16/2010 |
| Report Form Completed By: Suzanna L. Simpson | Date:2/18/2010 |
| ANNULAR SPACE DETAILS | Elevations Depths (0.01 ft.) (MSL)* (BGS) |
| | 632.40 -3.14 Top of Protective Casing |
| | |
| Type of Surface Seal: Concrete | 629.26 0.00 Ground Surface |
| Type of Annular Sealant: High-solids bentonite | |
| Installation Method: Tremie | |
| | |
| | (After Completion) 3/1/2010 |
| Type of Bentonite Seal Granular Pellet Slurry (choose one) | |
| Installation Method: Gravity | 616.55 12.71 Top of Seal |
| Setting Time: 10 min | |
| Type of Sand Pack: Quartz sand | |
| Grain Size: 10/20 (sieve size) | 613.15 16.11 Top of Screen |
| Installation Method: <u>Gravity</u> | (00.26 20.00 D. 11 |
| Type of Backfill Material: Quartz sand | 608.36 20.90 Bottom of Screen 607.89 21.37 Bottom of Well |
| (if applicable) Installation Method: Gravity | 606.80 22.46 Bottom of Borehole |
| | * Referenced to a National Geodetic Datum |
| | CASING MEASUREMENTS |
| WELL CONCEDUCATION MATTERIALS | Diameter of Borehole (inches) 8.0 |
| WELL CONSTRUCTION MATERIALS (Choose one type of material for each area) | ID of Riser Pipe (inches) 2.0 |
| | Protective Casing Length (feet) 5.0 |
| D + 1 C : 2000 2000 2000 | Riser Pipe Length (feet) 18.93 |
| Protective Casing SS304 SS316 PTFE PVC OTHER: Riser Pipe Above W.T. SS304 SS316 PTFE PVC OTHER: | Bottom of Scient to End Cap (leet) 0.47 |
| Riser Pipe Below W.T. SS304 SS316 PTFE PVC OTHER: Riser Pipe Below W.T. SS304 SS316 PTFE PVC OTHER: | Screen Length (1st slot to last slot) (feet) 4.79 Total Length of Casing (feet) 24.19 |

PTFE PVC OTHER:

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

(inches)

SS304

Well Completion Form (revised 02/06/02)

SS316

| Illinois Environ | mental Protection Ag | ency | | Wel | l Completio | n Report |
|--------------------------------------|--|--------------|------------------|---------------------------------------|--|--------------------|
| Site #: | County | y: Montgome | ry | | Well #: | 106 |
| Site Name: CCB Management | t Facility | | | E | Borehole #: | G106 |
| State Plane Coordinate: X 2,514,512 | 2.8 Y 875,149.8 (or) | Latitude: 39 | | 00 <u>Ä</u> Longitud | de: <u>-89</u> <u>2</u> | 3! <u>56.800</u> Ä |
| Surveyed By: <u>Jeffrey D. Emric</u> | :k | IL Re | gistration #: _0 | 35-003507 | | |
| Drilling Contractor: <u>Layne-We</u> | stern Co | Drille | r: T. List | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | Geold | ogist: Rhonald | l W. Hasenyage | er, LPG #196-000 |)246 |
| Drilling Method: Hollow stem | auger | Drillii | ng Fluid (Type): | n/a | | |
| Logged By: Suzanna Simpson | | | | | te Finished: 2 | |
| Report Form Completed By: Su | | | 2/18/20 | | | |
| ANNULAR SPA | - | Butc. | Elevation | | (0.01 ft. | |
| ANNULAKSIA | CE DETAILS | | (MSL) | | (0.01 11. |) |
| | | | 631.45 | -3.06 | Top of Protectiv | e Casing |
| | | | 631.15 | -2.76 | Top of Riser Pip | e |
| Type of Surface Seal: Concrete | | | 628.39 | 0.00 | Ground Surface | |
| | \ | | 622.94 | 1 5.45 | Top of Annular | Sealant |
| Type of Annular Sealant: High-s | | | | | | |
| Installation Method: Tremie | | | 615 77 | 12.62 | Statio Water I o | val. |
| Setting Time: >24 hr. | | | 615.77 | 12.62 | Static Water Lev (After Completion) | |
| Type of Bentonite Seal Grant | | | = | | | |
| Installation Method:Gravit | (choose one) | | _617.44 | 10.95 | Top of Seal | |
| Setting Time:10 min | | | 616.10 | 12.20 | T f C 1 D | 1- |
| | | | 616.10 | 12.29 | Top of Sand Pag | CK. |
| Type of Sand Pack: Quartz sand | 1 | | 614.0 |) 14.27 | Ton of Saraan | |
| Grain Size:10/20 (sie | ve size) | | 614.02 | 2 14.37 | Top of Screen | |
| Installation Method: <u>Gravit</u> | У | | 609.43 | 3 18.96 | Bottom of Scree | n |
| Type of Backfill Material:Quart | | | 608.95 | | Bottom of Well | 11 |
| Installation Method: Gravit | (if applicable) | | 607.94 | 1 20.45 | Bottom of Borel | nole |
| | | | | ed to a National Geode | • | |
| | | | | CASING MEA | SUREMENTS | |
| WELL CONO | TENLICTION MATERIAL C | | Diameter of B | orehole | (inches) | 8.0 |
| | TRUCTION MATERIALS e type of material for each area) | | ID of Riser Pi | | (inches) | |
| | | | Protective Cas | | (feet) | |
| Protective Casing | SS304 SS316 PTFE PVC | OTHER: | Riser Pipe Lei | _ | (feet) | |
| Riser Pipe Above W.T. | SS304 SS316 PTFE (PVC) | | | een to End Cap (1st slot to last slo | (feet) | 4.60 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC | | Total Length | | ot) (feet) (feet) | 22.20 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviro | onmental Protection Agenc | y | | Well | Completion | Report |
|---|-------------------------------------|------------|--------------------------------------|---------------------|---|--------|
| Site #: | County:M | ontgomery | V | W | Vell #: G1 | .07 |
| Site Name: AEG Coffeen Po | ower Station CCB Management Facili | ty | | В | orehole #: | 3107 |
| State- Plant Plane Coordinate: X 2,514,35 | 58.3 Y 874,994.3 (or) Latitud | e: | · | Longitud | e:° | _'" |
| Surveyed By: | rick | _ IL Reg | istration #:035-0 | 03507 | | |
| Drilling Contractor: <u>Layne-W</u> | Vestern Co | _ Driller: | T. List | | | |
| Consulting Firm: Hanson Pro | ofessional Services Inc. | _ Geolog | ist: Rhonald W. | Hasenyage | r, LPG #196-000 | 246 |
| Drilling Method: Hollow ster | m auger | _ Drilling | g Fluid (Type): <u>n/a</u> | ı | | |
| Logged By: Suzanna L. Sim | pson | _ Date St | tarted: 2/17/20 | 10 Dat | e Finished: 2/1 | 7/2010 |
| Report Form Completed By:S | uzanna L. Simpson | _ Date: _ | 2/18/2010 | | | |
| ANNULAR SPA | ACE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | 630.60 | 2.81 | Top of Protective | Casing |
| | | | 630.23 | 2.44 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 627.79 | 0.00 | Ground Surface | |
| Type of Annular Sealant: High | -solids bentonite | | 624.08 | 3.71 | Top of Annular S | ealant |
| Installation Method:Trem | ie J | | | | | |
| Setting Time: >24 hr. | | ∇ | 617.39 | _10.40_ | Static Water Leve (After Completion) | |
| Type of Bentonite Seal Gra | nular Pellet Slurry (choose one) | | | | | |
| Installation Method: Grave | ` ' | | 617.41 | _10.38_ | Top of Seal | |
| Setting Time: 8 min | | | 616.24 | 11.55 | Top of Sand Pack | [|
| Type of Sand Pack: Quartz san | nd | | | | | |
| Grain Size:10/20 (s | sieve size) | | 613.92 | 13.87 | Top of Screen | |
| Installation Method: Gravi | ity | | (00.20 | 10.50 | D. // C.C. | |
| Type of Backfill Material: Qua | | | 609.29 608.82 | 18.50 18.97 | Bottom of Screen Bottom of Well | |
| Installation Method: Gravi | (if applicable) | | 607.08 | _20.71_ | Bottom of Boreho | ole |
| | | | * Referenced to a | National Geodet | ic Datum | |
| | | | CAS | ING MEA | SUREMENTS | |
| WELL CON | ISTRUCTION MATERIALS | | Diameter of Boreho | ole | (inches) | 8.0 |
| (Choose | one type of material for each area) | | ID of Riser Pipe Protective Casing L | ength | (inches) | 5.0 |
| | | | Riser Pipe Length | Migui | (feet) | 16.31 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | R: Steel | Bottom of Screen to | End Cap | (feet) | 0.47 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | ₹: | Screen Length (1s | st slot to last slo | ot) (feet) | 4.63 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | | Total Length of Cas | sing | (feet) | 21.41 |
| Screen | SS304 SS316 PTFE PVC OTHER | K: | Screen Slot Size ** | | (inches) | 0.010 |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviro | onmental Protection Agend | ey . | | Well | Completion | Report |
|---|---|--|--|------------------------------|---|---------------|
| Site #: | County: N | Iontgomery | V | W | Vell #: G1 | .08 |
| Site Name: AEG Coffeen Po | ower Station CCB Management Facil | ity | | В | orehole #: | 3108 |
| State- Plant Plane Coordinate: X 2,514,24 | 18.3 Y 874,948.8 (or) Latitud | le: | · | Longitud | e:° | |
| Surveyed By: <u>Jeffrey D. Emr</u> | rick | IL Reg | istration #:035-0 | 03507 | | |
| Drilling Contractor: <u>Layne-W</u> | estern Co | Driller: | T. List | | | |
| Consulting Firm: Hanson Pro | ofessional Services Inc. | Geolog | ist: Rhonald W. | Hasenyage | r, LPG #196-000 | 246 |
| Drilling Method: Hollow ster | n auger | _ Drilling | g Fluid (Type): <u>n/a</u> | ı | | |
| Logged By: <u>Diane M. Lamb</u> | | _ Date St | tarted: 2/12/20 | 10 Dat | e Finished: 2/1 | 2/2010 |
| Report Form Completed By: | piane M. Lamb | _ Date: _ | 2/19/2010 | | | |
| ANNULAR SPA | ACE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | 630.52 | | Top of Protective | Casing |
| | | | 630.22 | -2.72 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 627.50 | 0.00 | Ground Surface | |
| Type of Annular Sealant: High | -solids bentonite | | 622.50 | 5.00 | Top of Annular S | ealant |
| Installation Method:Trem | ie J | | | | | |
| Setting Time: _ >24 hr. | | \sqrt{\sq}}\sqrt{\sq}}}}}}}\sqrt{\sqrt{\sq}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}} | 618.57 | 8.93 | Static Water Leve (After Completion) | |
| Type of Bentonite Seal Gra | nular Pellet Slurry (choose one) | | | | | |
| Installation Method: Granu | ılar | | 614.00 | _13.50_ | Top of Seal | |
| Setting Time: 10 min | | 1 1 | 612.80 | _14.70_ | Top of Sand Pack | |
| Type of Sand Pack: Quartz san | nd | | | | | |
| Grain Size:10/20 (s | sieve size) | | 610.68 | 16.82 | Top of Screen | |
| Installation Method: <u>Gravi</u> | ty | | 606.00 | 21.50 | 2.0 | |
| Type of Backfill Material:n/a_ | | | 606.00 605.50 | <u>21.50</u> <u>22.00</u> | Bottom of Screen Bottom of Well | |
| Installation Method: n/a | (if applicable) | | 605.50 | 22.00 | Bottom of Boreho | ale. |
| instantation rection. <u>II/a</u> | | | * Referenced to a | | | iic |
| | | | CAS | ING MEA | SUREMENTS | |
| WELL COM | CTDLICTION MATERIAL C | | Diameter of Boreho | ole | (inches) | 8.0 |
| | STRUCTION MATERIALS one type of material for each area) | | ID of Riser Pipe | | (inches) | 2.0 |
| | | | Protective Casing L | ength | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC OTHE | R: Steel | Riser Pipe Length Bottom of Screen to | End Can | (feet) | 19.54 0.50 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHE | | Screen Length (1s | | ` | 4.68 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHE | R: | Total Length of Cas | | (feet) | 24.72 |
| Screen | SS304 SS316 PTFE PVC OTHE | R: | Screen Slot Size ** | | (inches) | 0.010 |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environmental Protection Agency | Well Completion Report |
|--|--|
| Site #: County:Mon | atgomery Well #: G109 |
| Site Name: AEG Coffeen Power Station CCB Management Facility | Borehole #: G109 |
| State- Plant Plane Coordinate: X 2,514,137.8 Y 874,970.1 (or) Latitude: | |
| Surveyed By: | IL Registration #:035-003507 |
| Drilling Contractor: Layne-Western Co | Driller: T. List |
| Consulting Firm: Hanson Professional Services Inc. | Geologist: Rhonald W. Hasenyager, LPG #196-000246 |
| Drilling Method: Hollow stem auger | Drilling Fluid (Type):n/a |
| Logged By: Diane M. Lamb | Date Started:2/11/2010 Date Finished:2/11/2010 |
| Report Form Completed By: <u>Diane M. Lamb</u> | Date:2/19/2010 |
| ANNULAR SPACE DETAILS | Elevations Depths (0.01 ft.) (MSL)* (BGS) |
| | |
| | |
| Type of Surface Seal: Concrete | |
| Type of Annular Sealant: High-solids bentonite | |
| Installation Method: Tremie | |
| Setting Time: >24 hr. | 618.35 8.85 Static Water Level |
| Type of Bentonite Seal Granular Pellet Slurry | (After Completion) 3/1/2010 |
| (choose one) Installation Method: Granular | |
| Setting Time:10 min | |
| Type of Sand Pack: Quartz sand | |
| Grain Size: 10/20 (sieve size) | |
| Installation Method: Gravity | |
| Type of Backfill Material: (if applicable) | 607.27 19.93 Bottom of Screen 606.70 20.50 Bottom of Well |
| Installation Method: n/a | 606.70 20.50 Bottom of Borehole |
| | * Referenced to a National Geodetic Datum |
| | CASING MEASUREMENTS |
| WELL CONCEDITORION ALTERNAL | Diameter of Borehole (inches) 8.0 |
| WELL CONSTRUCTION MATERIALS (Choose one type of material for each area) | ID of Riser Pipe (inches) 2.0 |
| | Protective Casing Length (feet) 5.0 |
| Dutation Carina | Riser Pipe Length (feet) 17.95 |
| Protective Casing SS304 SS316 PTFE PVC OTHER: (Riser Pipe Above W.T. SS304 SS316 PTFE PVC OTHER: | Bottom of Screen to End Cap (leet) 0.57 |
| Riser Pipe Below W.T. SS304 SS316 PTFE PVC OTHER: | Screen Length (1st slot to last slot) (feet) 4.54 Total Length of Casing (feet) 23.06 |

PTFE PVC OTHER:

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

(inches)

SS304

Well Completion Form (revised 02/06/02)

SS316

| Illinois Environ | | Well Completion Report | | | | |
|--------------------------------------|---|------------------------|--|----------------|---|---------------|
| Site #: | County: Mo | ntgomery | | W | /ell #:G1 | 10 |
| Site Name: CCB Management | t Facility | | | Во | orehole #:C | i110 |
| State Plane Coordinate: X 2,514,057 | 7.7 Y 875,015.4 (or) Latitude | :39 | 4! <u>1.800Ä</u> | | e: <u>-89</u> <u>24</u> | |
| Surveyed By:Jeffrey D. Emric | ek | IL Registra | ation #:035-00 | 03507 | | |
| Drilling Contractor: <u>Layne-We</u> | stern Co | Driller: _ | T. List | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | Geologist: | Rhonald W. | Hasenyager | , LPG #196-0002 | 246 |
| Drilling Method: Hollow stem | auger | Drilling Fl | uid (Type):n/a | l | | |
| Logged By: | | Date Start | ed: 2/11/20 | 10 Date | e Finished: 2/1 | 1/2010 |
| | | | 2/19/2010 | | | |
| ANNULAR SPA | | | Elevations | Depths | (0.01 ft.) | |
| | | | (MSL)* 629.96 | (BGS) -2.94 | Top of Protective | Casina |
| | T | | | | _ | _ |
| | | | 629.65 | 2.63 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 627.02 | 0.00 | Ground Surface | |
| | | | 621.86 | 5.16 | Top of Annular Se | ealant |
| Type of Annular Sealant: High-s | 7 | | | | | |
| Installation Method: Tremie | | | 617.50 | 9.50 | Static Water Lave | 1 |
| Setting Time:>24 nr. | | $\overline{\Delta}$ | 617.52 | 9.30 | Static Water Leve (After Completion) | |
| Type of Bentonite Seal Gran | | | | | | |
| Installation Method: Granu | (choose one) | | 615.46 | 11.56 | Top of Seal | |
| Setting Time: 10 min | | | | | | |
| | | | 614.06 | _12.96_ | Top of Sand Pack | |
| Type of Sand Pack: Quartz sand | 1 | | 611.07 | 15.05 | T | |
| Grain Size: 10/20 (sie | ve size) | | 611.97 | 15.05 | Top of Screen | |
| Installation Method: <u>Gravit</u> | У | | 607.43 | 19.59 | Bottom of Screen | |
| Type of Backfill Material:n/a | (if any limite) | | 606.86 | 20.16 | Bottom of Well | |
| Installation Method: n/a | (if applicable) | | 606.86 | 20.16 | Bottom of Boreho | le |
| | | | * Referenced to a | | | |
| | | | CAS | ING MEAS | SUREMENTS | |
| WELL COM | | D | iameter of Boreho | le | (inches) | 8.0 |
| | STRUCTION MATERIALS e type of material for each area) | | of Riser Pipe | | (inches) | 2.0 |
| | | | rotective Casing L | ength | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER: | | iser Pipe Length ottom of Screen to | End Con | (feet) | 17.68 0.57 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER: | | creen Length (1s | • | (feet) | 4.54 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER: | | otal Length of Cas | | (feet) | 22.79 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

| Illinois Enviro | onmental Protection Agenc | e y | | Well | Completion | Report |
|---|--|------------|--|-----------------|---|--------|
| Site #: | County: N | Iontgomery | Į. | W | Vell #: G1 | .11 |
| Site Name: AEG Coffeen Po | ower Station CCB Management Facili | ty | | В | orehole #: | G111 |
| State- Plant Plane Coordinate: X 2,513,98 | 81.7 Y 875,058.7 (or) Latitud | le: | · ' '' | Longitud | e:° | _'" |
| Surveyed By: | rick | _ IL Reg | istration #:035-0 | 03507 | | |
| Drilling Contractor: <u>Layne-W</u> | Vestern Co | _ Driller: | T. List | | | |
| Consulting Firm: Hanson Pro | ofessional Services Inc. | _ Geolog | ist: Rhonald W. | Hasenyage | r, LPG #196-000 | 246 |
| Drilling Method: Hollow stem auger Dril | | | g Fluid (Type):n/a | ı | | |
| Logged By:Diane M. Lamb | | _ Date St | tarted: 2/10/20 | 10 Dat | e Finished: 2/1 | 1/2010 |
| Report Form Completed By: | Diane M. Lamb | _ Date: _ | 2/19/2010 | | | |
| ANNULAR SPA | ACE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | <u></u> | | 630.19 | 2.95 | Top of Protective | Casing |
| | | | 629.90 | -2.66 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 627.24 | 0.00 | Ground Surface | |
| Type of Annular Sealant: High | e-solids bentonite | | 622.52 | 4.72 | Top of Annular S | ealant |
| Installation Method:Trem | ie J | | | | | |
| Setting Time: >24 hr. | | $ \nabla $ | 616.74 | 10.50 | Static Water Leve (After Completion) | |
| Type of Bentonite Seal Gra | | | | | | |
| Installation Method: Grant | (choose one) | | 616.41 | 10.83 | Top of Seal | |
| Setting Time: 10 min | | | 614.52 | 12.72 | Top of Sand Pack | |
| Type of Sand Pack: Quartz sar | nd | | | | | |
| Grain Size:10/20 (s | sieve size) | | 612.63 | _14.61_ | Top of Screen | |
| Installation Method: Gravi | ity | | | | | |
| Type of Backfill Material: <u>n/a</u> | | | 608.09 607.52 | | Bottom of Screen Bottom of Well | |
| Installation Method: n/a | (if applicable) | | 607.52 | 10.72 | Bottom of Boreho | ala. |
| ilistaliation Method. <u>II/a</u> | | | * Referenced to a | | | ЛС |
| | | | CAS | ING MEA | SUREMENTS | |
| WELL CON | | | Diameter of Boreho | ole | (inches) | 8.0 |
| | ISTRUCTION MATERIALS one type of material for each area) | | ID of Riser Pipe | | (inches) | 2.0 |
| | | | Protective Casing L | ength | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | R: Steel | Riser Pipe Length Bottom of Screen to | End Can | (feet) | 0.57 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | R: | Screen Length (1s | | ` | 4.54 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | R: | Total Length of Cas | | (feet) | 22.38 |
| Screen | SS304 SS316 PTFE PVC OTHER | R: | Screen Slot Size ** | | (inches) | 0.010 |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviro | onmental Protection Agenc | e y | | Well | Completion | Report |
|---|---|----------------------------|---------------------------------------|------------------------------|---|---------------|
| Site #: | County: N | Iontgomery | Į. | V | Vell #: G1 | 19 |
| Site Name: AEG Coffeen Po | ower Station CCB Management Facili | ity | | В | orehole #: | G119 |
| State- Plant Plane Coordinate: X 2,513,90 | 07.7 Y 875,675.0 (or) Latitud | le: | · ' '' | Longitud | e:° | _'" |
| Surveyed By: <u>Jeffrey D. Emr</u> | rick | _ IL Reg | istration #:035-0 | 03507 | | |
| Drilling Contractor: <u>Layne-W</u> | estern Co | _ Driller: | T. List | | | |
| Consulting Firm: Hanson Pro | fessional Services Inc. | _ Geolog | ist: Rhonald W. | Hasenyage | r, LPG #196-000 | 246 |
| Drilling Method: Hollow ster | _ Drilling | g Fluid (Type): <u>n/a</u> | ı | | | |
| Logged By: Suzanna L. Simp | pson | _ Date St | tarted: 2/9/201 | 0 Dat | e Finished: 2/ | 9/2010 |
| Report Form Completed By: S | uzanna L. Simpson | _ Date: _ | 2/18/2010 | | | |
| ANNULAR SPA | ACE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | = | | 631.85 | 3.00 | Top of Protective | Casing |
| | | | 631.55 | 2.70_ | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 628.85 | 0.00 | Ground Surface | |
| Type of Annular Sealant: High- | -solids bentonite | | 623.57 | 5.28 | Top of Annular S | ealant |
| Installation Method:Tremi | ie J | | | | | |
| Setting Time: >24 hr. | | $ \underline{\nabla} $ | 617.59 | _11.26_ | Static Water Leve (After Completion) | |
| Type of Bentonite Seal Gra | nular Pellet Slurry | | | | | |
| Installation Method: Gravi | (choose one) | | 614.87 | 13.98 | Top of Seal | |
| Setting Time:15 min | | | 613.57 | | Top of Sand Pack | |
| Type of Sand Book | | | | | • | |
| Type of Sand Pack: Quartz san Grain Size: 10/20 (s | ieve size) | | 611.56 | 17.29 | Top of Screen | |
| Installation Method: Gravi | | | | | | |
| Type of Backfill Material: n/a | | | 607.02 606.47 | <u>21.83</u> <u>22.38</u> | Bottom of Screen Bottom of Well | |
| Type of Backini Material. <u>—I/a</u> | (if applicable) | | _000.47_ | | Bottom of wen | |
| Installation Method: <u>n/a</u> | | | 606.47 * Referenced to a | 22.38 National Geodet | Bottom of Boreho | ole |
| | | | CAS | ING MEA | SUREMENTS | |
| | | | Diameter of Boreho | | (inches) | 8.0 |
| | STRUCTION MATERIALS one type of material for each area) | | ID of Riser Pipe | | (inches) | 2.0 |
| • | , | | Protective Casing L | ength | (feet) | 5.0 |
| n | 00004 00015 00000 | | Riser Pipe Length | | (feet) | 19.99 |
| Protective Casing Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHE SS304 SS316 PTFE PVC OTHE | R: Steel | Bottom of Screen to | | (feet) | 0.55 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE (PVC) OTHE | | Screen Length (1s Total Length of Cas | | | 4.54 25.08 |
| Screen | SS304 SS316 PTFE PVC OTHE | | Screen Slot Size ** | | (feet) | 0.010 |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environmental Protection Agency | Well Completion Report |
|--|--|
| Site #: County: Mor | ntgomery Well #: G120 |
| Site Name: CCB Management Facility | 912 0 |
| State Plane Coordinate: X 2,513,905.8 Y 875,854.4 (or) Latitude: | 39 4! 10.100Ä Longitude: -89 24! 4.400Ä |
| Surveyed By: | IL Registration #:035-003507 |
| Drilling Contractor: Layne-Western Co | Driller: T. List |
| Consulting Firm: Hanson Professional Services Inc. | Geologist: Rhonald W. Hasenyager, LPG #196-000246 |
| Drilling Method: Hollow stem auger | Drilling Fluid (Type):n/a |
| Logged By: Suzanna Simpson | Date Started:2/8/2010 Date Finished:2/8/2010 |
| Report Form Completed By: Suzanna Simpson | Date:2/18/2010 |
| ANNULAR SPACE DETAILS | Elevations Depths (0.01 ft.) (MSL)* (BGS) |
| | 632.18 -2.88 Top of Protective Casing |
| | |
| Type of Surface Seal: Concrete | 629.30 0.00 Ground Surface |
| | 624.22 5.08 Top of Annular Sealant |
| Type of Annular Sealant: High-solids bentonite | |
| Installation Method: Tremie | |
| Setting Time: _>24 hr | |
| Type of Bentonite Seal Granular Pellet Slurry (choose one) | |
| Installation Method: Gravity | |
| Setting Time: 8 min | 616.22 13.08 Top of Sand Pack |
| Time of Sand Backs | |
| Type of Sand Pack: Quartz sand Grain Size: 10/20 (sieve size) | |
| Installation Method: Gravity | |
| | 609.68 19.62 Bottom of Screen |
| Type of Backfill Material: Quartz sand (if applicable) | |
| Installation Method: Gravity | 607.22 22.08 Bottom of Borehole * Referenced to a National Geodetic Datum |
| | |
| | CASING MEASUREMENTS |
| WELL CONSTRUCTION MATERIALS | Diameter of Borehole (inches) 8.0 |
| (Choose one type of material for each area) | ID of Riser Pipe (inches) 2.0 Protective Casing Length (feet) 5.0 |
| | Riser Pipe Length (feet) 17.67 |
| Protective Casing SS304 SS316 PTFE PVC OTHER: (| Bottom of Screen to End Cap (feet) 0.59 |
| Riser Pipe Above W.T. SS304 SS316 PTFE PVC OTHER: | Screen Length (1st slot to last slot) (feet) 4.52 |
| Riser Pipe Below W.T. SS304 SS316 PTFE PVC OTHER: | Total Length of Casing (feet) 22.78 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

| Illinois Enviro | onmental Protection Agenc | · y | | Well | Completion | Report |
|---|---|----------------------------|--|------------------------------|---|--------------|
| Site #: | County:M | lontgomery | 7 | W | Vell #: G1 | 21 |
| Site Name: AEG Coffeen Po | ower Station CCB Management Facili | ty | | В | orehole #: | §121 |
| State- Plant Plane Coordinate: X 2,513,90 | 04.4 Y 875,964.6 (or) Latitud | e: | · ' " | Longitud | e:° | _'" |
| Surveyed By:Jeffrey D. Emi | rick | _ IL Regi | istration #:035-0 | 03507 | | |
| Drilling Contractor: <u>Layne-W</u> | Vestern Co | _ Driller: | T. List | | | |
| Consulting Firm: Hanson Pro | ofessional Services Inc. | _ Geolog | ist: Rhonald W. | Hasenyage | r, LPG #196-000 | 246 |
| Drilling Method: Hollow ster | _ Drilling | g Fluid (Type): <u>n/a</u> | ı | | | |
| Logged By: Suzanna L. Sim | pson | _ Date St | arted: 2/4/201 | 10 Dat | e Finished: 2/ | 4/2010 |
| Report Form Completed By:S | uzanna L. Simpson | _ Date: _ | 2/18/2010 | | | |
| ANNULAR SPA | ACE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | 633.14 | | Top of Protective | Casing |
| | | | 632.83 | 3.26_ | Top of Riser Pipe | |
| Type of Surface Seal: <u>Concrete</u> | | | 629.57 | 0.00 | Ground Surface | |
| Type of Annular Sealant: High | -solids bentonite | | 624.41 | 5.16 | Top of Annular S | ealant |
| Installation Method:Trem | ie | | | | | |
| Setting Time: _ >24 hr. | | ∇ | 615.13 | _14.44 | Static Water Leve (After Completion) | |
| Type of Bentonite Seal Gra | nular Pellet Slurry (choose one) | | | | | |
| Installation Method: Gravi | ity | V V | 616.81 | 12.76 | Top of Seal | |
| Setting Time: 7 min | | | 615.49 | _14.08_ | Top of Sand Pack | |
| Type of Sand Pack: Quartz sar | nd | | | | | |
| Grain Size:10/20 (s | sieve size) | = | 612.78 | _16.79_ | Top of Screen | |
| Installation Method: Gravi | ity | | | | | |
| Type of Backfill Material:Qua | | | 608.10 607.62 | <u>21.47</u> <u>21.95</u> | Bottom of Screen Bottom of Well | |
| Installation Mathada Cravi | (if applicable) | | 605.41 | 24.16 | Dattam of Daroha | .lo |
| Installation Method: <u>Gravi</u> | lty | | * Referenced to a | | Bottom of Boreho | ne |
| | | | CAS | ING MEA | SUREMENTS | |
| WELL COM | COTPLICATION MATERIAL C | | Diameter of Boreho | | (inches) | 8.0 |
| | STRUCTION MATERIALS one type of material for each area) | | ID of Riser Pipe | | (inches) | 2.0 |
| | | | Protective Casing L | ength | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | R: (Steel) | Riser Pipe Length | End C | (feet) | 20.05 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | | Bottom of Screen to Screen Length (1s | | (feet) | 0.48 4.68 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | ₹: | Total Length of Cas | | (feet) | 25.21 |
| Screen | SS304 SS316 PTFE PVC OTHER | ₹: | Screen Slot Size ** | | (inches) | 0.010 |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | nmental Protection Agenc | y | | Well | Completion | Report | | |
|--|-------------------------------------|------------|-------------------------------------|------------------------------|---|--------|--|--|
| Site #: | County: M | ontgomery | | W | Vell #:G1 | 22 | | |
| Site Name: AEG Coffeen Pov | wer Station CCB Management Facility | У | | В | orehole #:G | 122 | | |
| State- Plant Plane Coordinate: X 2,513,902 | 2.8 Y 876,080.1 (or) Latitude | e:° | | Longitud | e:° | | | |
| Surveyed By: | ck | _ IL Regis | stration #: <u>035-0</u> | 03507 | | | | |
| Drilling Contractor: <u>Layne-We</u> | stern Co | _ Driller: | T. List | | | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | _ Geologis | st: Rhonald W. | Hasenyage | er, LPG #196-000 | 246 | | |
| Drilling Method: Hollow stem auger Drilli | | | Orilling Fluid (Type):n/a | | | | | |
| Logged By: Diane M. Lamb | | Date Sta | arted: 2/4/20 | 10 Dat | e Finished: 2/4 | 4/2010 | | |
| Report Form Completed By: Di | ane M. Lamb | Date: | 2/9/2010 | | | | | |
| ANNULAR SPA | | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | | | |
| | | | 632.98 | ` ′ | Top of Protective | Casing | | |
| | | | 632.69 | | Top of Riser Pipe | | | |
| Type of Surface Seal: Concrete | | | 629.86 | 0.00 | Ground Surface | | | |
| Type of Annular Sealant: High-s | solids bentonite | | 625.01 | 4.85 | Top of Annular So | ealant | | |
| Installation Method:Tremie | : | | | | | | | |
| Setting Time: >24 hr. | | ∇ | 617.02 | _12.84_ | Static Water Leve (After Completion) | | | |
| Type of Bentonite Seal Gran | ular Pellet Slurry (choose one) | | | | | | | |
| Installation Method: Gravity | / | \bowtie | 617.01 | 12.85 | Top of Seal | | | |
| Setting Time: 10 min | | | 615.41 | _14.45_ | Top of Sand Pack | | | |
| Type of Sand Pack: Quartz sand | <u> </u> | | | | | | | |
| Grain Size: 10/20 (sie | ve size) | | 613.35 | _16.51_ | Top of Screen | | | |
| Installation Method: Gravity | / | | COO 01 | 21.05 | D // CG | | | |
| Type of Backfill Material: Quart | tz sand (if applicable) | | 608.81 608.20 | <u>21.05</u> <u>21.66</u> | Bottom of Screen Bottom of Well | | | |
| Installation Method: <u>Gravity</u> | . 22 | | 608.01 * Referenced to a | 21.85 National Geodet | Bottom of Boreho | le | | |
| | | | | | | | | |
| | | Γ | | | SUREMENTS | 0.0 | | |
| | TRUCTION MATERIALS | | Diameter of Boreho ID of Riser Pipe | oie | (inches) | 2.0 | | |
| (Choose on | the type of material for each area) | | Protective Casing I | ength | (feet) | 5.0 | | |
| | | | Riser Pipe Length | | (feet) | 19.34 | | |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | : Steel | Bottom of Screen to | o End Cap | (feet) | 0.61 | | |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | | Screen Length (1 | st slot to last slo | ot) (feet) | 4.54 | | |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | : [] | Total Length of Ca | sino | (feet) | 24 49 | | |

PTFE PVC OTHER:

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

(inches)

SS304

Well Completion Form (revised 02/06/02)

SS316

| Illinois Enviro | onmental Protection Agend | ey . | | Well | Completion | Report | |
|---|---|--------------|--|------------------------------|---|--------|--|
| Site #: | County: N | Iontgomery | ý | W | Vell #: G1 | 23 | |
| Site Name: AEG Coffeen Po | ower Station CCB Management Facili | ity | | В | orehole #: | 3123 | |
| State- Plant Plane Coordinate: X 2,513,90 | 01.5 Y 876,189.6 (or) Latitud | le: | o | Longitud | e:° | _'" | |
| Surveyed By: | rick | IL Reg | istration #:035-0 | 03507 | | | |
| Drilling Contractor: <u>Layne-W</u> | Vestern Co | Driller: | T. List | | | | |
| Consulting Firm: Hanson Pro | ofessional Services Inc. | Geolog | ist: Rhonald W. | Hasenyage | r, LPG #196-000 | 246 | |
| Drilling Method: Hollow stem auger Drilli | | | g Fluid (Type): <u>n/a</u> | | | | |
| Logged By: <u>Diane M. Lamb</u> | | _ Date St | tarted: 2/3/201 | 10 Dat | e Finished: 2/4 | 4/2010 | |
| Report Form Completed By: | Diane M. Lamb | _ Date: _ | 2/9/2010 | | | | |
| ANNULAR SPA | ACE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | | |
| | <u> </u> | | 633.29 | 3.16 | Top of Protective | Casing | |
| | | | 632.96 | -2.83 | Top of Riser Pipe | | |
| Type of Surface Seal: <u>Concrete</u> | | | 630.13 | 0.00 | Ground Surface | | |
| Type of Annular Sealant: High | -solids bentonite | | 625.06 | 5.07 | Top of Annular S | ealant | |
| Installation Method:Trem | ie J | | | | | | |
| Setting Time: _ >24 hr. | | $ \Sigma $ | 614.15 | _15.98_ | Static Water Leve (After Completion) | | |
| Type of Bentonite Seal Gra | nular Pellet Slurry (choose one) | | | | | | |
| Installation Method: Gravi | ity | | 612.31 | 17.82 | Top of Seal | | |
| Setting Time: 10 min | | 1 1 | 611.14 | _18.99_ | Top of Sand Pack | | |
| Type of Sand Pack: Quartz sar | nd | | | | | | |
| Grain Size:10/20 (s | sieve size) | | 609.19 | _20.94_ | Top of Screen | | |
| Installation Method: Gravi | ity | | | | | | |
| Type of Backfill Material: <u>n/a</u> | | | 604.67 604.06 | <u>25.46</u> <u>26.07</u> | Bottom of Screen Bottom of Well | | |
| Installation Method: n/a | (if applicable) | | 604.06 | 26.07 | Bottom of Boreho | la | |
| ilistaliation Method. <u>II/a</u> | | | * Referenced to a | | | ile. | |
| | | | CAS | SING MEA | SUREMENTS | | |
| WELL CON | CTDI ICTIONI MATERIAL C | | Diameter of Boreho | ole | (inches) | 8.0 | |
| | STRUCTION MATERIALS one type of material for each area) | | ID of Riser Pipe | | (inches) | 2.0 | |
| | | | Protective Casing L | ength | (feet) | 5.0 | |
| Protective Casing | SS304 SS316 PTFE PVC OTHE | R: Steel | Riser Pipe Length Bottom of Screen to | n End Can | (feet) | 0.61 | |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHE | | Screen Length (1s | | ` | 4.52 | |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHE | R: | Total Length of Cas | | (feet) | 28.90 | |
| Screen | SS304 SS316 PTFE PVC OTHE | R: | Screen Slot Size ** | | (inches) | 0.010 | |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviro | onmental Protection Agenc | · y | | Well | Completion | Report |
|---|---|----------------------------|--|------------------------------|---|--------------|
| Site #: | County: M | lontgomery | ý | W | Vell #: G1 | 24 |
| Site Name: <u>AEG Coffeen Po</u> | ower Station CCB Management Facili | ty | | В | orehole #: | G124 |
| State- Plant Plane Coordinate: X 2,513,90 | 00.3 Y 876,304.9 (or) Latitud | e: | o ! !! | Longitud | e:° | |
| Surveyed By:Jeffrey D. Emr | rick | _ IL Reg | istration #:035-0 | 03507 | | |
| Drilling Contractor: <u>Layne-W</u> | Vestern Co | _ Driller: | T. List | | | |
| Consulting Firm: Hanson Pro | ofessional Services Inc. | _ Geolog | ist: Rhonald W. | Hasenyage | r, LPG #196-000 | 246 |
| Drilling Method: Hollow ster | _ Drilling | g Fluid (Type): <u>n/a</u> | ì | | | |
| Logged By: Suzanna L. Sim | pson | _ Date St | tarted: 2/3/201 | 10 Dat | e Finished: 2/ | 3/2010 |
| Report Form Completed By:S | uzanna L. Simpson | _ Date: _ | 2/5/2010 | | | |
| ANNULAR SPA | ACE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | <u> </u> | | 633.70 | , , , | Top of Protective | Casing |
| | | | 633.39 | -2.97 | Top of Riser Pipe | |
| Type of Surface Seal: <u>Concrete</u> | | | 630.42 | 0.00 | Ground Surface | |
| Type of Annular Sealant: High | -solids bentonite | | 625.45 | 4.97 | Top of Annular S | ealant |
| Installation Method:Trem | ie | | | | | |
| Setting Time: _ >24 hr. | | $\overline{\Delta}$ | 619.43 | 10.99 | Static Water Leve (After Completion) | |
| Type of Bentonite Seal Gra | nular Pellet Slurry (choose one) | | | | | |
| Installation Method: Gravi | ity | V V | 618.34 | 12.08 | Top of Seal | |
| Setting Time: 10 min | | | 616.50 | _13.92_ | Top of Sand Pack | |
| Type of Sand Pack: Quartz san | nd | | | | | |
| Grain Size:10/20 (s | sieve size) | == | 614.44 | 15.98 | Top of Screen | |
| Installation Method: Gravi | ity | | | | | |
| Type of Backfill Material: Qua | artz sand | | 609.91 609.36 | <u>20.51</u> <u>21.06</u> | Bottom of Screen Bottom of Well | |
| Table Mala C | (if applicable) | | (00.45 | 21.07 | D. # CD 1 | 1 |
| Installation Method: <u>Gravi</u> | ty | | * Referenced to a | 21.97 National Geodet | | oie |
| | | | CAS | ING MEA | SUREMENTS | |
| | | | Diameter of Boreho | | (inches) | 8.0 |
| | STRUCTION MATERIALS one type of material for each area) | | ID of Riser Pipe | | (inches) | 2.0 |
| | | | Protective Casing L | ength | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | R: (Steel) | Riser Pipe Length | End C | (feet) | 18.95 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | | Bottom of Screen to Screen Length (1s | | (feet) | 0.55 4.53 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | | Total Length of Cas | | (feet) | 24.03 |
| Screen | SS304 SS316 PTFE PVC OTHER | ₹: | Screen Slot Size ** | | (inches) | 0.010 |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviror | nmental Protection Agency | | | Well | Completio | n Report |
|---|------------------------------------|----------------|--|-------------------|-------------------|-------------|
| Site #: | County: M | ontgomery | | W | ell #: | G125 |
| Site Name:CCB Managemen | t Facility | | | Во | orehole #: | G125 |
| State Plane Coordinate: X 2,513,899 | 9.1 Y 876,409.5 (or) Latitud | e: <u>39</u> _ | 4! <u>15.600</u> Ä | Longitude | e: <u>-89</u> : | 24! 4.400Ä |
| Surveyed By: <u>Jeffrey D. Emric</u> | ck | _ IL Registr | ration #:035-0 | 03507 | | |
| Drilling Contractor: <u>Layne-We</u> | estern Co | _ Driller: _ | T. List | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | _ Geologist | : Rhonald W. | Hasenyager, | , LPG #196-00 | 00246 |
| Drilling Method: Hollow stem | auger | _ Drilling F | luid (Type):n/a | ì | | |
| Logged By: Suzanna Simpsor | 1 | _ Date Star | ted: 2/2/201 | 10 Date | Finished: | 2/3/2010 |
| Report Form Completed By: Su | zanna Simpson | Date: | 2/5/2010 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft | <u></u>) |
| | | | _633.82_ | | Top of Protecti | ve Casing |
| | T | | 633.51 | | Top of Riser Pi | |
| | | | _033.31_ | 2.03 | Top of Riser Fi | pe |
| Type of Surface Seal: Concrete | | | 630.68 | 0.00 | Ground Surface | e |
| Type of Annular Sealant: High- | solids bentonite | | 625.77 | 4.91 | Top of Annular | Sealant |
| Installation Method: Tremi | A | | | | | |
| | | ∇ | _622.10_ | 8.58 | Static Water Le | evel |
| | | | | | (After Completion | a) 3/1/2010 |
| Type of Bentonite Seal Gran | ular Pellet Slurry (choose one) | | | | | |
| Installation Method: Gravit | y | \bowtie | 617.15 | 13.53 | Top of Seal | |
| Setting Time: 10 min | | | 615.95 | 14.73 | Top of Sand Pa | ick |
| T CC ID I o | | | | | • | |
| Type of Sand Pack: Quartz sand Grain Size: 10/20 (six | | | 613.65 | _17.03_ | Top of Screen | |
| Installation Method: Gravit | eve size) | | | | | |
| installation Method. Gravit | <u>y</u> | | 609.12 | 21.56 | Bottom of Scre | en |
| Type of Backfill Material:n/a_ | (if applicable) | | 608.64 | _22.04_ | Bottom of Well | |
| Installation Method:n/a | | | 608.64 | 22.04 | Bottom of Bore | hole |
| | | | * Referenced to a | National Geodetic | c Datum | |
| | | | CAS | SING MEAS | SUREMENTS | |
| WELL CONS | STRUCTION MATERIALS | | Diameter of Boreho | ole | (inche | |
| | te type of material for each area) | | D of Riser Pipe | | (inche | |
| | | | Protective Casing L | ength | (fee | |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | | Riser Pipe Length Bottom of Screen to | End Con | (fee | 0.50 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | | Screen Length (1s | | (fee | 4.50 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | | Total Length of Cas | | (fee | 2405 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

| Illinois Environ | nmental Protection Agend | ey . | | Well | Completion | Report |
|--|--|-------------------------------------|---------------------------------------|-----------------|---|--------|
| Site #: | County: N | Iontgomery | ý | v | Vell #: G1 | 26 |
| Site Name: AEG Coffeen Pov | wer Station CCB Management Facili | ity | | В | Sorehole #: | G126 |
| State- Plant Plane Coordinate: X 2,513,895 | 5.4 Y 875,062.4 (or) Latitud | le: | · · · · · · · · · · · · · · · · · · · | Longitud | e:° | |
| Surveyed By: <u>Jeffrey D. Emri</u> | ck | IL Reg | istration #:035-0 | 03507 | | |
| Drilling Contractor: <u>Layne-We</u> | estern Co | Driller: | T. List | | | |
| Consulting Firm: Hanson Prof | Pessional Services Inc. | Geolog | ist: Rhonald W. | Hasenyage | er, LPG #196-000 | 246 |
| Drilling Method: Hollow stem auger Drill | | | g Fluid (Type): <u>n/a</u> | i . | | |
| Logged By: Diane M. Lamb | | _ Date St | tarted: 2/10/20 | 10 Dat | e Finished: 2/1 | 0/2010 |
| Report Form Completed By: | ane M. Lamb | Date: _ | 2/19/2010 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | <u></u> | | 625.69 | 2.73 | Top of Protective | Casing |
| | | | 625.39 | 2.43 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 622.96 | 0.00 | Ground Surface | |
| Type of Annular Sealant: High-s | solids bentonite | | 619.96 | 3.00 | Top of Annular S | ealant |
| Installation Method:Tremie | <u>;</u> | | | | | |
| Setting Time: >24 hr. | | $\mid \underline{\nabla} \mid \mid$ | 614.14 | 8.82 | Static Water Leve (After Completion) | |
| Type of Bentonite Seal Gran | ular Pellet Slurry (choose one) | | | | | |
| Installation Method: Granul | lar | | 613.96 | 9.00 | Top of Seal | |
| Setting Time: 10 min | | 1 1 | 612.86 | _10.10 | Top of Sand Pack | |
| Type of Sand Pack: Quartz sand | 1 | | | | | |
| Grain Size: 10/20 (sie | eve size) | | 610.07 | 12.89 | Top of Screen | |
| Installation Method: Gravity | y | | 605.52 | 17.43 | Bottom of Screen | |
| Type of Backfill Material: <u>n/a</u> | (C F H) | | 605.53 604.96 | 18.00 | Bottom of Well | |
| Installation Method: <u>n/a</u> | (if applicable) | | 604.96 * Referenced to a | | Bottom of Boreho | ble |
| | | | Referenced to a | National Geodet | ic Datum | |
| | | | | | SUREMENTS | 0.0 |
| | STRUCTION MATERIALS ne type of material for each area) | | Diameter of Boreho ID of Riser Pipe | ole | (inches) | 2.0 |
| (Choose of | as the or material for each area) | | Protective Casing I | ength | (feet) | 5.0 |
| D. e. d. G. d. | | | Riser Pipe Length | | (feet) | 15.32 |
| Protective Casing Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHE SS304 SS316 PTFE PVC OTHE | R: Steel | Bottom of Screen to | | (feet) | 0.57 |
| Riser Pipe Above W.T. Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHE | | Screen Length (1s Total Length of Cas | | | 20.43 |
| Screen | SS304 SS316 PTFE PVC OTHE | | Screen Slot Size ** | | (feet) | 0.010 |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | mental Protection Age | ency | | | Well | Completion | on Report |
|---|-----------------------------------|-------------------|-----------|----------------------------------|--------------------|-------------------------------------|------------|
| Site #: | County | y: <u>Montgom</u> | ery | | W | /ell #: | G151 |
| Site Name: CCB Managemen | t Facility | | | | В | orehole #: | G151 |
| State Plane Coordinate: X 2,513,805 | 5.9 Y <u>875,023.7</u> (or) 1 | Latitude: | | | Longitud | e: | |
| Surveyed By: | ek | IL R | Registrat | ion #: <u>035-0</u> 0 | 03507 | | |
| Drilling Contractor: Testing Se | ervice Corp. | Dril | ler: B | . Williamson | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | Geo | logist: _ | Rhonald W. | Hasenyager | , LPG #196-0 | 00246 |
| Drilling Method: Hollow stem auger Drill | | | ling Flui | d (Type): <u>n/a</u> | ı | | |
| Logged By: Ryne M. Fiorito | | Date | e Started | 12/19/20 |)11 Date | e Finished:1 | 2/19/2011 |
| Report Form Completed By: R | onald W. Hasenyager | Date | e: | 12/27/2011 | | | |
| ANNULAR SPA | CE DETAILS | | | Elevations (MSL)* | Depths (BGS) | (0.01 f | t.) |
| | | | 7 | 626.24 | 3.42 | Top of Protect | ive Casing |
| | | | _ | 625.93 | 3.11 | Top of Riser P | ipe |
| Type of Surface Seal: Concrete | | | //> | 622.82 | 0.00 | Ground Surfac | e |
| | | | | 620.49 | 2.33 | Top of Annula | r Sealant |
| Type of Annular Sealant: High- | | | 1 | | | | |
| Installation Method: Tremi | | | | 615.02 | 7.70 | Static Water I | aval |
| Setting Time: | | | | 615.03 | | Static Water L (After Completion | |
| Type of Bentonite Seal Gran | Pellet Slurry (choose one) | | | | | | |
| Installation Method: Gravit | , | | | 611.82 | _11.00_ | Top of Seal | |
| Setting Time: 24 min | | | | 609.07 | 13.75 | Top of Sand P | ack |
| Time of Sand Books O | | | | | | • | |
| Type of Sand Pack: Quartz sand Grain Size: 10/20 (six | l ve size) | | | 607.48 | 15.34 | Top of Screen | |
| Installation Method: Gravit | , | | | | | | |
| | , | | | 602.98 | 19.84 | Bottom of Scre | |
| Type of Backfill Material: <u>n/a</u> | (if applicable) | | | 602.36 | 20.46 | Bottom of Wel | l |
| Installation Method:n/a | | | | 602.36 * Referenced to a | 20.46 | Bottom of Bor | ehole |
| | | | | resortance to a | Traditional Geodec | o Butturi | |
| | | | | | | SUREMENTS | |
| | STRUCTION MATERIALS | | | meter of Boreho of Riser Pipe | ole | (inche | 2.0 |
| (Choose on | e type of material for each area) | | | tective Casing L | ength | (inche | |
| | | | | er Pipe Length | | (fe | 10.15 |
| Protective Casing | SS304 SS316 PTFE PVC | OTHER: | \Box | tom of Screen to | End Cap | (fe | 0.60 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC | OTHER: | Scr | een Length (1s | t slot to last slo | t) (fe | et) 4.50 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC | OTHER: | Tot | al Length of Cas | sing | (fe | et) 23.57 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | nmental Protection Agency | 7 | | Well | Completion | Report |
|---|-----------------------------------|---|--|-------------------|---|---------|
| Site #: | County: N | Iontgomery | | We | ell #: G1 | 52 |
| Site Name: CCB Managemen | t Facility | | | Bor | rehole #: | G152 |
| State Plane Coordinate: X 2,513,894 | 4.5 Y 874,687.5 (or) Latitud | le: | | Longitude: | | |
| Surveyed By: | ek | IL Registr | ration #: 035-00 | 03507 | | |
| Drilling Contractor: Testing Se | ervice Corp. | _ Driller: _ | B. Williamson | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | _ Geologist | : Rhonald W. | Hasenyager, | LPG #196-0002 | 246 |
| Drilling Method: Hollow stem auger Drill | | | luid (Type):n/a | l | | |
| Logged By: Ryne M. Fiorito | | _ Date Star | ted: 12/20/20 | 011 Date | Finished: 12/ | 20/2011 |
| Report Form Completed By: R | nonald W. Hasenyager | Date: | 12/27/2011 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | 626.67 | | Top of Protective | Casing |
| | | | 626.52 | -3.46 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 623.06 | 0.00 | Ground Surface | |
| | | | 621.06 | 2.00 | Top of Annular S | ealant |
| Type of Annular Sealant: Seal e. | 7 | | | | | |
| | | | 606.06 | 17.00 | | |
| Setting Time: | | $\left \begin{array}{c} \overline{\Delta} \end{array}\right $ | 606.06 | 17.00 | Static Water Leve (After Completion) | |
| Type of Bentonite Seal Gran | ular Pellet Slurry (choose one) | | | | | |
| Installation Method: Gravit | v | | 621.06 | 2.00 | Top of Seal | |
| Setting Time:>24 hr. | | | 611.56 | 11.50 | Top of Sand Pack | |
| T. (C. ID.) | | | | | · r | |
| Type of Sand Pack: Quartz sand | | | _609.47_ | _13.59_ | Top of Screen | |
| Grain Size: 10/20 (sie Installation Method: Gravit | eve size) | | | | | |
| | <u>y</u> | | _604.97_ | | Bottom of Screen | |
| Type of Backfill Material:n/a_ | (if applicable) | | _604.49_ | 18.57 | Bottom of Well | |
| Installation Method:n/a | | | 604.49 | | Bottom of Boreho | ole |
| | | | * Referenced to a | National Geodetic | Datum | |
| | | | CAS | ING MEASI | UREMENTS | |
| WELL CONS | STRUCTION MATERIALS | | Diameter of Boreho | le | (inches) | 8.0 |
| | e type of material for each area) | | D of Riser Pipe Protective Casing L | enath | (inches) | 5.0 |
| | | | Riser Pipe Length | ongui | (feet) | 17.05 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | | Bottom of Screen to | End Cap | (feet) | 0.48 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | | creen Length (1s | | | 4.50 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | | Total Length of Cas | | (feet) | 22.03 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | mental Protection Agency | | | Well | Completio | n Report |
|---|--|-----------------|--|-------------------|--------------------|------------|
| Site #: | County: <u>N</u> | ontgomery | | W | ell #: | 153 |
| Site Name:CCB Management | t Facility | | | Во | orehole #: | G153 |
| State Plane Coordinate: X 2,513,532 | 2.7 Y 874,532.7 (or) Latitud | e: | | Longitude | e: | |
| Surveyed By: <u>Jeffrey D. Emric</u> | k | _ IL Registr | ration #:035-00 | 03507 | | |
| Drilling Contractor: Testing Se | ervice Corp. | _ Driller: _ | B. Williamson | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | _ Geologist: | Rhonald W. | Hasenyager. | , LPG #196-000 | 0246 |
| Drilling Method: Hollow stem | _ Drilling F | luid (Type):n/a | ì | | | |
| Logged By: Ryne M. Fiorito | | _ Date Start | ted: 12/15/20 | 011 Date | Finished: 12 | 2/15/2011 |
| Report Form Completed By: Rh | onald W. Hasenyager | Date: | 12/27/2011 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft. |) |
| | | | 626.59 | | Top of Protectiv | e Casing |
| | T | | 626.35 | | Top of Riser Pip | |
| | | | | | | |
| Type of Surface Seal: Concrete | | | 623.30 | 0.00 | Ground Surface | |
| Type of Annular Sealant: High-s | solids bentonite | | 622.63 | 0.67 | Top of Annular | Sealant |
| Installation Method:Tremic | | | | | | |
| | | ∇ | 605.75 | 17.55 | Static Water Lev | |
| | | | | | (After Completion) | 12/21/2011 |
| Type of Bentonite Seal Gran | Pellet Slurry (choose one) | | | | | |
| Installation Method: Gravit | y | | 610.30 | _13.00_ | Top of Seal | |
| Setting Time: >24 hr. | | | 608.30 | 15.00 | Top of Sand Pag | ck |
| Towns of Court Davids | | | | | | |
| Type of Sand Pack: Quartz sand Grain Size: 10/20 (sie | 1 ve size) | | _607.40_ | _15.90_ | Top of Screen | |
| | | | | | | |
| Installation Method: <u>Gravit</u> | <u>y</u> | | 602.96 | 20.34 | Bottom of Scree | n |
| Type of Backfill Material: <u>n/a</u> | (if applicable) | | 602.54 | _20.76_ | Bottom of Well | |
| Installation Method:n/a | (a apparation) | | 602.54 | 20.76 | Bottom of Borel | nole |
| | | | * Referenced to a | National Geodetic | c Datum | |
| | | | CAS | SING MEAS | SUREMENTS | |
| WELL COM | TDI ICTION MATERIAI C | Б | iameter of Boreho | ole | (inches) | 8.0 |
| | TRUCTION MATERIALS e type of material for each area) | | O of Riser Pipe | | (inches) | |
| | | | rotective Casing L | ength | (feet) | |
| Protective Casing | SS304 SS316 PTFE PVC OTHE | | iser Pipe Length | | (feet) | |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | | Sottom of Screen to | | (feet) | |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | - 5 | creen Length (1s otal Length of Cas | | (feet) | 22.01 |
| - | | | om Longin or Cas | J1115 | (IEEE | 22.01 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

| Illinois Environ | mental Protection Agency | | | Well | Completio | on Report |
|---------------------------------------|-----------------------------------|--------------|--|-------------------|-------------------|---------------|
| Site #: | County: M | ontgomery | | W | ell #: | G154 |
| Site Name:CCB Management | t Facility | | | Во | orehole #: | G154 |
| State Plane Coordinate: X 2,513,243 | 3.1 Y 874,978.4 (or) Latitud | e: | | Longitude | :: | |
| Surveyed By: <u>Jeffrey D. Emric</u> | ck | _ IL Registr | ration #:035-00 | 03507 | | |
| Drilling Contractor: Testing Se | ervice Corp. | _ Driller: _ | B. Williamson | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | _ Geologist | : _ Rhonald W.] | Hasenyager. | , LPG #196-00 | 00246 |
| Drilling Method: Hollow stem | auger | _ Drilling F | luid (Type): <u>n/a</u> | 1 | | |
| Logged By: Ryne M. Fiorito | | _ Date Star | ted:12/16/20 | 011 Date | Finished: 1 | 2/16/2011 |
| Report Form Completed By: Rh | nonald W. Hasenyager | Date: | 12/27/2011 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 f | t.) |
| | | | _626.55_ | | Top of Protecti | ive Casing |
| | Ţ | | 626.35 | | Top of Riser P | |
| | | | | | Top of tuber 1 | |
| Type of Surface Seal: <u>Concrete</u> | | | 623.52 | 0.00 | Ground Surfac | e |
| Type of Annular Sealant: High-s | solids bentonite | | 622.44 | 1.08 | Top of Annula | r Sealant |
| Installation Method:Tremic | 7 | | | | | |
| | | ∇ | 612.42 | 11.10 | Static Water L | evel |
| | | | | | (After Completion | n) 12/21/2011 |
| Type of Bentonite Seal Gran | Pellet Slurry (choose one) | | | | | |
| Installation Method: Gravit | y | | 613.02 | _10.50_ | Top of Seal | |
| Setting Time: 24 min | | | 610.02 | _13.50_ | Top of Sand Pa | ack |
| Type of Sand Pack: Quartz sand | 1 | | | | | |
| | | | 609.26 | 14.26 | Top of Screen | |
| Installation Method: Gravit | | | | | | |
| | | | 604.76 | 18.76 | Bottom of Scre | |
| Type of Backfill Material:n/a_ | (if applicable) | | 604.42 | _19.10_ | Bottom of Wel | 1 |
| Installation Method:n/a | | | 603.52 | _20.00_ | Bottom of Boro | ehole |
| | | | * Referenced to a | National Geodetic | e Datum | |
| | | | CAS | ING MEAS | SUREMENTS | |
| WELL CONS | STRUCTION MATERIALS | | Diameter of Boreho | le | (inche | |
| | e type of material for each area) | | D of Riser Pipe | 41 | (inche | |
| | | | Protective Casing L | engtn | (fee | |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | | Riser Pipe Length Bottom of Screen to | End Can | (fee | 0.24 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | . 11 | Screen Length (1s | | • | 4.50 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | | Total Length of Cas | | (fee | 21.02 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

| Illinois Environ | mental Protection Agency | | | Well | Completion | Report |
|--|---|--------------|--------------------------|-----------------|--------------------|---------------|
| Site #: | County: <u>N</u> | ontgomery | | We | ell #: <u>G</u> | 155 |
| Site Name:CCB Management | t Facility | | | Во: | rehole #: | G155 |
| State Plane Coordinate: X 2,513,501 | 1.8 Y 875,127.7 (or) Latitud | e: | | Longitude | : | |
| Surveyed By: <u>Jeffrey D. Emric</u> | ck | IL Regist | ration #:035-00 | 03507 | | |
| Drilling Contractor: Testing Se | ervice Corp. | _ Driller: _ | B. Williamson | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | _ Geologist | : Rhonald W. I | Hasenyager, | LPG #196-000 | 246 |
| Drilling Method: Hollow stem auger Drill | | | Fluid (Type): <u>n/a</u> | l. | | |
| Logged By: Ryne M. Fiorito | | _ Date Star | ted: 12/19/20 | 011 Date | Finished: 12 | /19/2011 |
| Report Form Completed By: Rh | nonald W. Hasenyager | _ Date: | 12/27/2011 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) |) |
| | | | 626.07 | | Top of Protective | Casing |
| | T | | 625.86 | | Top of Riser Pipe | _ |
| | | | 023.00 | 2.) | Top of Riser 1 ip | - |
| Type of Surface Seal: Concrete | | | 622.89 | 0.00 | Ground Surface | |
| Type of Annular Sealant: High-s | solids bentonite | | 621.39 | 1.50 | Top of Annular S | Sealant |
| Installation Method:Tremic | λ | | | | | |
| | | ∇ | 614.99 | 7.90 | Static Water Lev | el |
| | | | | | (After Completion) | 12/21/2011 |
| Type of Bentonite Seal Gran | ular Pellet Slurry (choose one) | | | | | |
| Installation Method: <u>Gravit</u> | y | \bowtie | 611.89 | _11.00_ | Top of Seal | |
| Setting Time: 27 min | | | 609.14 | 13.75 | Top of Sand Pac | k |
| T. (G. 1D.) | | | | | 1 | |
| Type of Sand Pack: Quartz sand | | | 607.80 | 15.09 | Top of Screen | |
| (4.1 | eve size) | | | | • | |
| Installation Method: <u>Gravit</u> | <u>y</u> | | 603.31 | 19.58 | Bottom of Screen | 1 |
| Type of Backfill Material: <u>n/a</u> | (if applicable) | | 602.66 | 20.23 | Bottom of Well | |
| Installation Method: n/a | (ii applicable) | | 602.66 | 20.23 | Bottom of Boreh | ole |
| | | | * Referenced to a l | | | |
| | | | CAS | ING MEAS | UREMENTS | |
| WELL COM | | I | Diameter of Boreho | le | (inches) | 8.0 |
| | STRUCTION MATERIALS e type of material for each area) | 1 | D of Riser Pipe | | (inches) | 2.0 |
| | | | Protective Casing L | ength | (feet) | 5.0 |
| Protection C. : | CC204 CC216 PTEC PVC | | Riser Pipe Length | | (feet) | 18.28 |
| Protective Casing Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER SS304 SS316 PTFE PVC OTHER | | Bottom of Screen to | | (feet) | 0.43 |
| Riser Pipe Above W.T. Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | | Screen Length (1st | | | 4.49 |
| Tabel Tipe Below 11.1. | Jacob Sala The Tree office | | Total Length of Cas | ing | (feet) | 23.20 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

| Illinois Enviro | onmental Protection Agenc | y | Well Completion Report |
|---|--|--|--|
| Site #: | County: Mc | ntgomery | Well #: G200 |
| Site Name: AEG Coffeen Po | ower Station CCB Management Facili | tv | |
| State- Plant | 80.6 Y 2,515,650.0 (or) Latitude | | |
| Surveyed By: <u>Jeffrey D. Em</u> | rick | IL Registration #: 035- | 003507 |
| Drilling Contractor: Testing S | Service Corporation | Driller: B. Williamson | n |
| Consulting Firm: Hanson Pro | fessional Services Inc. | Geologist: Rhonald W | Hasenyager, LPG #196-000246 |
| Drilling Method: Hollow ster | n auger | Drilling Fluid (Type): | |
| Logged By: <u>Suzanna L Simp</u> | oson | Date Started: <u>2/25/2</u> | 008 Date Finished: 2/25/2008 |
| Report Form Completed By: St | uzanna L Simpson | Date: 2/29/2008 | |
| ANNULAR SPA | ACE DETAILS | Elevations (MSL)* | Depths (0.01 ft.) (BGS) |
| | _ | 626.54 | 2.34 Top of Protective Casing |
| | | _625.94 | Top of Riser Pipe |
| Type of Surface Seal: Concrete | | 624.20 | 0.00 Ground Surface |
| Type of Annular Sealant: Bento | onite chips | 620.70 | 3.50 Top of Annular Sealant |
| Installation Method: Gravit | ·v | | |
| Setting Time: >24 hr. | | <u>621.45</u> | Static Water Level (After Completion) 3/12/2008 |
| Type of Bentonite Seal Gran | ular Pellet Slurry | VIII . | |
| Installation Method: Gravit | v | 620.70 | 3.50 Top of Seal |
| Setting Time: >24 hr. | | 614.20 | 10.00 Top of Sand Pack |
| Type of Sand Pack: Quartz sand | d | | |
| Grain Size: 10/20 (sie | eve size) | 612.01 | 12.19 Top of Screen |
| Installation Method: Gravit | y E | | |
| Type of Backfill Material: Form | nation Sand (if applicable) | 607.22 606.84 | 16.98 Bottom of Screen 17.36 Bottom of Well |
| Installation Method: Slough | 1 | 606.20 * Referenced to | 18.00 Bottom of Borehole a National Geodetic Datum |
| | | . | |
| | | | SING MEASUREMENTS |
| | STRUCTION MATERIALS ne type of material for each area) | Diameter of Borel ID of Riser Pipe | hole (inches) 8.0 (inches) 2.0 |
| \- | | Protective Casing | |
| D | F | Riser Pipe Length | (feet) 13.93 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER: | Steel Bottom of Screen | to End Cap (feet) 0.38 |
| Riser Pipe Above W.T. Riser Pipe Below W.T. | SS304 SS316 PTFE (PVC) OTHER: SS304 SS316 PTFE (PVC) OTHER: | Screen Length (1 | |
| Screen | SS304 SS316 PTFE (PVC) OTHER: | Total Length of Co | |
| Well Completion Form (revised 02/06/02 | | Screen Slot Size * **Hand-Slotted Well So | * (inches) 0.010 creens Are Unacceptable |

| Illinois Enviro | | Well Completion Repor | | | | | | |
|--|------------------------------------|---|--|------------------|--------------------|----------|--|--|
| Site #: | 7 | We | ell #:G2 | 201 | | | | |
| Site Name: <u>AEG Coffeen Po</u> | wer Station CCB Management Faci | ility | | Во | rehole #: | G201 | | |
| State- Plant Plane Coordinate: X 877,92 | 4.9 Y 2,514,849.5 (or) Latitud | de:° | | Longitude | : | , " | | |
| Surveyed By:Jeffrey D. Emr | | | Registration #: 035-003507 | | | | | |
| Drilling Contractor: <u>Testing S</u> | ervice Corporation | _ Driller: | B. Williamson | | | | | |
| Consulting Firm: Hanson Pro | fessional Services Inc. | Geolog | ist: Rhonald W I | Hasenyager, | , LPG #196-00 | 0246 | | |
| Drilling Method: Hollow stem auger Drillin | | | g Fluid (Type): | | | | | |
| Logged By: Suzanna L Simp | son | _ Date St | arted: 2/25/20 | 08 Date | Finished: 2/2 | 25/2008 | | |
| Report Form Completed By: Su | ızanna L Simpson | Date: _ | 2/29/2008 | | | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | | | |
| | | | 627.66 | 3.76 | Top of Protective | e Casing | | |
| | | | 627.12 | 3.22_ | Top of Riser Pipe | e | | |
| Type of Surface Seal: Concrete | | | 623.90 | 0.00 | Ground Surface | | | |
| Type of Annular Sealant: Bento | nite chine | | 620.60 | 3.30 | Top of Annular S | Sealant | | |
| Installation Method: Gravit | | | | | | | | |
| Setting Time: _ >24 hr. | | $\left \begin{array}{c} \overline{\Delta} \end{array}\right $ | 621.73 | 2.17 | Static Water Lev | el | | |
| | | | | | (After Completion) | | | |
| Type of Bentonite Seal Gran | nular Pellet Slurry (choose one) | | | | | | | |
| Installation Method: Gravit | <u>y</u> | | 620.60 | 3.30 | Top of Seal | | | |
| Setting Time: >24 hr. | | | 611.80 | 12.10 | Top of Sand Pacl | k | | |
| Tyme of Cond Dooly | | | | | | | | |
| Type of Sand Pack: Quartz san Grain Size: 10/20 (si | d eve size) | | 610.89 | _13.01_ | Top of Screen | | | |
| Installation Method: Gravit | | | | | | | | |
| | | | 606.10 | | Bottom of Screen | 1 | | |
| Type of Backfill Material: n/a | (if applicable) | | 605.75 | 18.15 | Bottom of Well | | | |
| Installation Method: <u>n/a</u> | | | 605.75 * Referenced to a | | Bottom of Boreh | ole | | |
| | | | * Referenced to a | National Geodeti | ic Datum | | | |
| | | [| CAS | ING MEAS | SUREMENTS | | | |
| WELL CON | STRUCTION MATERIALS | ŀ | Diameter of Boreh | ole | (inches) | 8.0 | | |
| | ne type of material for each area) | | ID of Riser Pipe Protective Casing I | anath | (inches) | 5.0 | | |
| | | | Protective Casing I Riser Pipe Length | Lengui | (feet) | 16.23 | | |
| Protective Casing | SS304 SS316 PTFE PVC OTHE | R: Steel | Bottom of Screen t | o End Cap | (feet) | 0.35 | | |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHE | R: | Screen Length (1s | | ì | 4.79 | | |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHE | R: | Total Length of Ca | | (feet) | 21.37 | | |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

ILLINOIS DEPARTMENT OF PUBLIC HEALTH DIVISION OF ENVIRONMENTAL HEALTH 525 W. JEFFERSON ST. SPRINGFIELD, IL 62761

WATER WELL SEALING FORM

TYPE OR PRESS FIRMLY

RETURN ALL COPIES TO IDPH OR LOCAL HEALTH DEPARTMENT

This form shall be submitted to this Department or the local health department not more than 30 days after a water well, boring or monitoring well is sealed. Such wells are to be sealed not more than 30 days after they are abandoned in accordance with the sealing requirements in the Water Well Construction Code. THE LOCAL HEALTH DEPARTMENT OR REGIONAL PUBLIC HEALTH DEPARTMENT MUST BE NOTIFIED AT LEAST 48 HOURS PRIOR TO SEALING.

| Ownership (Name of Controlling Party) AEG C | offeen Power Stat | ion | | (G104) |) |
|---|-------------------|-----------|---------------|------------|------|
| Well Location 134 CIPS Trail | | Coffe | een | Montgon | nery |
| Address - Lot Number | | | City | County | 7 |
| General Description Township 7 (N) | ⊗ Range | 3 (| K)(W) | Section | 10 |
| SEQuarter of theNE | _Quarter of the _ | NE | Qua | arter | |
| Year Drilled 2010 | | | | | |
| Drilling Permit Number (and date, if known)n/a | | | | | _ |
| Type of Well Bored Drilled_ ✓ | | | | | |
| Total Depth 20.0 ft. Diame | eter (inches) | 2 | | | |
| Formation clear of obstructionYes | | | | | |
| DETAILS OF PLUGGING | | | | | |
| Filled with Bentonite grout (cement or other materials) | from | 0.5 | _to20.0 |)ft. | |
| | | | 0.5 | | |
| Kind of plug Random soil | from | 0 | _to0.5 | ft. | |
| Filled with | from | | _to | ft. | |
| Kind of plug | from | | _to | ft. | |
| Filled with | from | | _to | ft. | |
| Kind of plug | from | | _to | ft. | |
| CASING RECORD Upper 2 feet of casing remove | ed <u>√</u> Ye | s | No | | |
| Date well was sealed Month October Da | ay8 | Year | 2010 | | |
| Licensed water well driller or other person approve | ed by the Departi | nent perf | orming wel | l sealing. | |
| Rhonald W. Hasenyager, L.P.G. | 196-0002 | 246 | | | |
| Name | Complete | License I | Number | | _ |
| Hanson Professional Services Inc., 1525 S. 6th St. | Springfie | eld | | IL 62703 | _ |
| Address | City | | | State/ZIP | |

This state agency is requesting disclosure of information that is necessary to accomplish the statutory purpose as outlined under Public Act 85-0863. Disclosure of this information is mandatory. This form has been approved by the Forms Management Center.

IL 482-0631

| Illinois Enviro | nmental Protection | n Agency | 7 | | 7 | Well (| Complet | ion Report |
|--|---|------------------|----------|-----------------------|-----------------|--------------------|-------------------------------|--------------------------|
| Site #: | Co | unty: <u>Mon</u> | tgomer | y. | | W | ell #: | G205 |
| Site Name: AEG Coffeen Por | wer Station CCB Manager | nent Facility | V | | | Во | rehole #: | G205 |
| State- Plant Plane Coordinate: X 875,550 | • | • | | | | | | |
| Surveyed By: <u>Jeffrey D. Emri</u> | ck | | IL Reg | istration #:0 | 35-00350 | 7 | | |
| Drilling Contractor: Testing Se | ervice Corporation | | Driller: | B. Willian | nson | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | | Geolog | ist: Rhonal | d W Hase | nyager | , LPG #196 | -000246 |
| Drilling Method: Hollow stem | auger | | Drilling | g Fluid (Type): | : | | | |
| Logged By: Suzanna L Simps | son | | Date St | arted: 2/2 | 21/2008 | Date | Finished: | 2/21/2008 |
| Report Form Completed By: Su | zanna L Simpson | | Date: _ | 2/29/20 | 008 | | | |
| ANNULAR SPA | CE DETAILS | | | Elevatio | | pths GS) | (0.01 | ft.) |
| | | | | 624.8 | <u>7 -2</u> | 2.72 | Top of Protec | ctive Casing |
| | | T | | 624.4 | <u>5 -2</u> | 2.30 | Top of Riser | Pipe |
| Type of Surface Seal: Concrete | _ | | | 622.1: | 50 | .00_ | Ground Surfa | ace |
| | | | | // 619.9: | 5 2 | .20 | Top of Annu | lar Sealant |
| Type of Annular Sealant: Benton | | | | | | | • | |
| Installation Method: Gravit | | | | 615 0. | a - | 0.6 | | |
| Setting Time: >24 hr. | | . _ | <u>Z</u> | 617.09 | 9 5 | .06 | Static Water (After Comple | Level tion) 3/12/2008 |
| Type of Bentonite Seal Gran | | | | | | | | |
| Installation Method: <u>Gravit</u> | (choose one) | | | 619.9 | 52 | .20 | Top of Seal | |
| Setting Time: >24 hr. | | | | | | | • | D 1 |
| <u> </u> | | | | 613.33 | <u> 8</u> | .80 | Top of Sand | Pack |
| Type of Sand Pack: Quartz sand | I | | | (12.1 | 1 1/ | 0.4 | T. 60 | |
| Grain Size: 10/20 (sie | ve size) | | | 612.1 | <u> </u> | 0.04_ | Top of Scree | n |
| Installation Method: Gravit | У | | | 607.6 | 2 1/ | 1.52 | D 60 | |
| Type of Backfill Material: Form | | | | 607.62 607.03 | | | Bottom of Sc Bottom of W | |
| I all a Mai I ol I | (if applicable) | | | (0)(1) | 5 1/ | . 00 | D # CD | 1.1 |
| Installation Method: Slough | l | | | 606.1: * Reference | ced to a Nation | | Bottom of Bo | orenoie |
| | | | | | CASING | MEAS | SUREMENT | ΓS |
| | | | | Diameter of I | | 1412716 | (incl | |
| | STRUCTION MATERIAL ne type of material for each area) | LS | | ID of Riser P | | | (incl | 2.0 |
| | | | | Protective Ca | sing Lengt | h | (f | eet) 5.0 |
| n | | | | Riser Pipe Le | | | (f | (eet) 12.34 |
| Protective Casing | SS304 SS316 PTFE PV | <u>`</u> | Steel | Bottom of Sc | | | | eet) 0.54 |
| Riser Pipe Above W.T. | | OTHER: | | Screen Lengt | | o last slot | (f | eet) 4.49 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE (PV | C OTHER: | | Total Length | of Casing | | (f | eet) 17.37 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

ILLINOIS DEPARTMENT OF PUBLIC HEALTH DIVISION OF ENVIRONMENTAL HEALTH 525 W. JEFFERSON ST. SPRINGFIELD, IL 62761

WATER WELL SEALING FORM

TYPE OR PRESS FIRMLY

RETURN ALL COPIES TO IDPH OR LOCAL HEALTH DEPARTMENT

This form shall be submitted to this Department or the local health department not more than 30 days after a water well, boring or monitoring well is sealed. Such wells are to be sealed not more than 30 days after they are abandoned in accordance with the sealing requirements in the Water Well Construction Code. THE LOCAL HEALTH DEPARTMENT OR REGIONAL PUBLIC HEALTH DEPARTMENT MUST BE NOTIFIED AT LEAST 48 HOURS PRIOR TO SEALING.

| Well Location 134 CIPS Lane | | Coffeen | Montgome | ry |
|---|---------------------|----------------------------|-------------------|----|
| Address - Lot Number | | City | County | |
| General Description Township 7 (N)(%) | Range | 3 (X)(W) | Section _ | |
| SWQuarter of the NEQ | uarter of the | NW_Q | uarter | |
| Year Drilled 2008 | | | | |
| Drilling Permit Number (and date, if known) n/a | | | | |
| Type of Well Bored Drilled✓ | Other | | | |
| Total Depth16 Diameter | er (inches) | 8 | | |
| Formation clear of obstructionYes | No | | | |
| DETAILS OF PLUGGING (riser pipe and screen p | | lus was arouted) | | |
| DETAILS OF LEGGING (113e) pipe and screen p | Julieu allu allilui | us was grouteu, | | |
| | | 0 1 | 6.0 | |
| | | 0 to 1 | 6.0 ft. | |
| Filled with Bentonite grout (cement or other materials) | from | | | |
| | from | | | |
| Filled with Bentonite grout (cement or other materials) | from from | to | ft. | |
| Filled with Bentonite grout (cement or other materials) Kind of plug | from from | to | ft. ft. | |
| Filled with Bentonite grout (cement or other materials) Kind of plug Filled with | fromfromfromfrom | toto | ft. ft. ft. | |
| Filled with Bentonite grout (cement or other materials) Kind of plug Filled with Kind of plug | fromfromfrom | tototo | ftftftft. | |
| Filled with Bentonite grout (cement or other materials) Kind of plug Filled with Kind of plug Filled with | fromfromfromfrom | totototo | ftftftft. | |
| Filled with Bentonite grout (cement or other materials) Kind of plug Filled with Kind of plug Filled with Kind of plug | from | toto | ftftftft. | |
| Filled with Bentonite grout (cement or other materials) Kind of plug Filled with Kind of plug Filled with Kind of plug CASING RECORD Upper 2 feet of casing removed | fromfrom | to | ftftftftftft. | |
| Filled withBentonite grout (cement or other materials) Kind of plug Filled with Kind of plug Filled with Kind of plug CASING RECORD Upper 2 feet of casing removed Date well was sealed Month March Day | from | totototo | ftftftftftft. | |

This state agency is requesting disclosure of information that is necessary to accomplish the statutory purpose as outlined under Public Act 85-0863. Disclosure of this information is mandatory. This form has been approved by the Forms Management Center.

IL 482-0631

| Illinois Environ | | Well Completion Repo | | | | |
|---|---|----------------------|---------------------------------------|---------------------|--|--|
| Site #: | County: M | ontgomery | | We | ell #:G | 206 |
| Site Name: CCB Management | t Facility | | | Bor | rehole #: | G206 |
| State Plane Coordinate: X 2,514,669 | 9.2 Y 875,103.9 (or) Latitud | e: <u>39</u> | 4! <u>2.600Ä</u> | Longitude: | -892 | <u>3! 54.800</u> Ä |
| Surveyed By: <u>Jeffrey D. Emric</u> | :k | _ IL Regist | tration #: <u>035-0</u> | 03507 | | |
| Drilling Contractor: <u>Layne-We</u> | stern Co | Driller: _ | D. Mahurin | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | _ Geologis | t: Rhonald W. | Hasenyager, | LPG #196-000 | 0246 |
| Drilling Method: Hollow stem | auger | Drilling I | Fluid (Type):n/a | a | | |
| Logged By: Suzanna Simpson | - | _ | rted: 10/14/20 | | | |
| | zanna Simpson | _ | 10/15/2010 | | | <u>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</u> |
| | - | _ Datc | | | (0.01.0 | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft. |) |
| | F | | 633.07 | 2.53 | Top of Protectiv | e Casing |
| | | | 632.82 | -2.28 | Top of Riser Pip | e |
| Type of Surface Seal: Concrete | | | 630.54 | 0.00 | Ground Surface | |
| | | | 627.84 | 2.70 | Top of Annular | Sealant |
| Type of Annular Sealant: <u>High-s</u> | 7 | | | | • | |
| Installation Method:Tremie | | | | 10.50 | | |
| Setting Time: >24 hr. | | $\overline{\Delta}$ | 611.96 | _18.58_ | Static Water Lev (After Completion) | |
| Type of Bentonite Seal Gran | ular Pellet Slurry | | | | | |
| Installation Method: Gravit | (choose one) | | 616.24 | 14.30 | Top of Seal | |
| Setting Time: 15 min | , | | | | - | |
| | × | | 615.04 | _15.50_ | Top of Sand Pac | :k |
| Type of Sand Pack: Quartz sand | 1 | | (12.02 | 17.51 | | |
| Grain Size:10/20 (sie | ve size) | | 613.03 | _17.51_ | Top of Screen | |
| Installation Method: Gravit | <u>y</u> | | 608.62 | 21.92 | Bottom of Scree | |
| Type of Backfill Material:n/a | | == | 608.12 | | Bottom of Well | П |
| Installation Method:n/a | (if applicable) | | 606.54 | 24.00 | Bottom of Borel | nole |
| instantation (viction). | | | | National Geodetic | | |
| | | | CAS | SING MEAS | UREMENTS | |
| ****** | | 1 | Diameter of Boreho | ole | (inches) | 8.0 |
| | STRUCTION MATERIALS e type of material for each area) | _1 | ID of Riser Pipe | | (inches) | 2.0 |
| | | 1 | Protective Casing I | ength | (feet) | |
| Protective Cosine | SS304 SS316 PTFE PVC OTHER | | Riser Pipe Length | | (feet) | |
| Protective Casing Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER SS304 SS316 PTFE (PVC) OTHER | | Bottom of Screen to | • | (feet) | |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | . + | Screen Length (1s) Total Length of Ca | | (feet) | 24.70 |
| | | | Total Longill Of Ca | J1115 | (ieet) | <u>∠</u> ⊤./∪ |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environmental Protection Agency | | | | Well Completion Report | | | | | |
|--|--|---|---|--|-----------------|---------------------------------------|-------------|--|--|
| Site #: | Cc | ounty: <u>Mon</u> | tgomery | | W | /ell #:G | 207 | | |
| Site Name: <u>AEG Coffeen Pov</u> | ver Station CCB Managen | nent Facility | | | Во | orehole #: | G207 | | |
| State Plane Coordinate: X 2,514,837 | 7.9 Y 875,166.4 (or |) Latitude: | 39° | 4'_3.2" | Longitude | e:e | 23 ' 52.6 " | | |
| Surveyed By: | ek | | IL Regis | stration #:035-0 | 03507 | | | | |
| Drilling Contractor: <u>Layne-We</u> | stern Co | | Driller: | D. Mahurin | | | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | | Geologist: Rhonald W. Hasenyager, LPG #196-000246 | | | | | | |
| Drilling Method: Hollow stem | auger | | Drilling | Fluid (Type):n/a | 1 | | | | |
| Logged By: Suzanna L. Simps | son | | Date Sta | rted: 10/8/20 | 10 Date | e Finished:1 | 0/8/2010 | | |
| Report Form Completed By: Su | zanna L. Simpson | | Date: _ | 10/8/2010 | | | | | |
| ANNULAR SPA | CE DETAILS | | | Elevations (MSL)* | Depths (BGS) | (0.01 ft. |) | | |
| | | | | 633.37 | 2.76 | Top of Protectiv | e Casing | | |
| | | | | 633.21 | -2.60 | Top of Riser Pip | e | | |
| Type of Surface Seal: Concrete | | - 31 | | 630.61 | 0.00 | Ground Surface | | | |
| | | | | 628.61 | 2.00 | Top of Annular | Sealant | | |
| Type of Annular Sealant: High-s | olids bentonite | - | | 020.01 | | Top of Timuda | Source | | |
| Installation Method: <u>Tremie</u> | | - | | | | | | | |
| Setting Time: >24 hr. | | _ \[\breve{\brev}}}}}}}}}}}}}}} | <u>Z</u> | 612.86 | <u>17.75</u> | Static Water Lev (After Completion | | | |
| Type of Bentonite Seal Grant | | + | | | | | | | |
| Installation Method: Gravity | (choose one) | | | 614.76 | 15.85 | Top of Seal | | | |
| Setting Time: 15 min | | _ | | | | • | | | |
| <u> </u> | | | | 613.63 | 16.98 | Top of Sand Pac | ek | | |
| Type of Sand Pack: Quartz sand | | - | | (12.27 | 10.24 | T. CC | | | |
| Grain Size:10/20 (sie | ve size) | | | _612.37_ | _18.24_ | Top of Screen | | | |
| Installation Method: Gravity | <i>I</i> | - | | 607.84 | 22.77 | Bottom of Scree | n | | |
| Type of Backfill Material: <u>n/a</u> | (6 17 11) | | | 607.31 | 23.30 | Bottom of Well | 11 | | |
| Installation Method: n/a | (if applicable) | | | 606.61 | 24.00 | Bottom of Borel | nole | | |
| institution rection. <u>In a</u> | | | | * Referenced to a | | | | | |
| | | | | CAS | SING MEAS | SUREMENTS | | | |
| WELL CONG | TRUCTION IN TERMINA | a | | Diameter of Boreho | ole | (inches) | 8.0 | | |
| | TRUCTION MATERIALS e type of material for each area) | 5 | | ID of Riser Pipe | | (inches) | | | |
| | | | | Protective Casing L | ength | (feet) | | | |
| Protective Casing | SS304 SS316 PTFE P | VC OTHER: (| | Riser Pipe Length | | (feet) | | | |
| Riser Pipe Above W.T. | | VC OTHER: (| | Bottom of Screen to | • | (feet) | | | |
| Riser Pipe Below W.T. | | VC OTHER: | + | Screen Length (1s Total Length of Cas | | t) (feet) (feet) | 2.5.00 | | |
| | | | | . Juni Longui Oi Ca | 5 | (1001) | 20.70 | | |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | y | Well Completion Report | | | | | | |
|--------------------------------------|--|------------------------|---|------------------------------|------------------------------------|---------------|--|--|
| Site #: | County: <u>M</u> | ontgomery | | W | /ell #: <u>G2</u> | 208 | | |
| Site Name: AEG Coffeen Pov | ver Station CCB Management Facilit | ty | | В | orehole #: | G208 | | |
| State Plane Coordinate: X 2,514,993 | 3.6 Y 875,231.5 (or) Latitude | e: <u>39°</u> | 4' 3.9" | Longitud | e:2 | 3 ' 50.6 " | | |
| Surveyed By: <u>Jeffrey D. Emri</u> | ck | _ IL Regis | stration #:035-0 | 03507 | | | | |
| Drilling Contractor: <u>Layne-We</u> | stern Co | _ Driller: | D. Mahurin | | | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | _ Geologis | Geologist: Rhonald W. Hasenyager, LPG #196-000246 | | | | | |
| Drilling Method: Hollow stem | auger | _ Drilling | Fluid (Type): <u>n/a</u> | ı | | | | |
| Logged By: Suzanna L. Simps | son | _ Date Sta | arted: 10/7/20 | 10 Date | e Finished:10 | /7/2010 | | |
| Report Form Completed By: Su | zanna L. Simpson | _ Date: _ | 10/8/2010 | | | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | | | |
| | | | 633.43 | -2.86 | Top of Protective | Casing | | |
| | | | 633.16 | -2.59 | Top of Riser Pipe | | | |
| Type of Surface Seal: Concrete | | | 630.57 | 0.00 | Ground Surface | | | |
| Type of Annular Sealant: High-s | valids bentanite | | 627.77 | 2.80 | Top of Annular S | ealant | | |
| Installation Method: Tremie | 7 | | | | | | | |
| Setting Time: >24 hr. | | ∇ | 614.76 | 15.81 | Static Water Leve | el | | |
| <u> </u> | | | | | (After Completion) | 11/15/2010 | | |
| Type of Bentonite Seal Grant | ular Pellet Slurry (choose one) | | | | | | | |
| Installation Method: Gravity | / <u> </u> | | 616.07 | 14.50 | Top of Seal | | | |
| Setting Time: 9 min | | | 613.90 | _16.67_ | Top of Sand Pack | | | |
| Type of Sand Pack: Quartz sand | | | | | | | | |
| Grain Size:10/20 (sie | | | 613.04 | 17.53 | Top of Screen | | | |
| Installation Method: Gravity | / | | | | | | | |
| Type of Backfill Material:n/a | | | 608.51 607.97 | <u>22.06</u> <u>22.60</u> | Bottom of Screen Bottom of Well | | | |
| Installation Mathada n/a | (if applicable) | | 606.57 | 24.00 | Dattam of Daroh | Jo. | | |
| Installation Method:n/a | | | * Referenced to a | | Bottom of Boreho | ne | | |
| | | | CAS | ING MEAS | SUREMENTS | | | |
| WELL GOVE | TRANSPORTATION AND THE PARTY OF | | Diameter of Boreho | ole | (inches) | 8.0 | | |
| | TRUCTION MATERIALS the type of material for each area) | | ID of Riser Pipe | | (inches) | 2.0 | | |
| | | - | Protective Casing L | ength | (feet) | 5.0 | | |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | : (Steel) | Riser Pipe Length | - LC | (feet) | 20.12 | | |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | | Bottom of Screen to | | (feet) | 0.54 | | |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | | Screen Length (1s | | t) (feet) | 4.53 25.19 | | |

PTFE PVC OTHER:

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

(inches)

SS304

Well Completion Form (revised 02/06/02)

SS316

| Illinois Environ | mental Protection Agend | ey | | Well C | ompletion | Report | | |
|---|---|----------------|---|----------------------|--------------------------------------|-----------------|--|--|
| Site #: | County: | Montgomery | | Well | #:G2 | .09 | | |
| Site Name: CCB Management | t Facility | | | Borel | hole #: | G209 | | |
| State Plane Coordinate: X 2,515,149 | 9.6 Y 875,298.2 (or) Latit | ude: <u>39</u> | 4! <u>4.500Ä</u> | Longitude: _ | -89 23 | <u>48.700</u> Ä | | |
| Surveyed By: <u>Jeffrey D. Emric</u> | ck | IL Regis | stration #:035-00 | 03507 | | | | |
| Drilling Contractor: <u>Layne-We</u> | stern Co | Driller: | D. Mahurin | | | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | Geologi | Geologist: Rhonald W. Hasenyager, LPG #196-000246 | | | | | |
| Drilling Method: Hollow stem | auger | Drilling | Fluid (Type):n/a | ı | | | | |
| Logged By: Suzanna Simpson | 1 | Date Sta | arted:10/7/20 | 10 Date Fi | nished: 10 | /7/2010 | | |
| Report Form Completed By:Su | zanna Simpson | Date: _ | 10/8/2010 | | | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | | | |
| | | | _633.16_ | | op of Protective | Casing | | |
| | | | 632.91 | | op of Riser Pipe | | | |
| Type of Surface Seal: Concrete | | | 630.57 | 0.00 Gr | round Surface | | | |
| | | | 627.57 | | op of Annular S | ealant | | |
| Type of Annular Sealant: <u>High-s</u> | | | | | · F | | | |
| Installation Method:Tremio | | | | | | | | |
| Setting Time: >24 hr. | | | 615.52 | | atic Water Leve After Completion) | | | |
| Type of Bentonite Seal Gran | ular Pellet Slurry | | | | | | | |
| Installation Method: Gravit | (choose one) | | 616.07 | 14.50 To | op of Seal | | | |
| Setting Time: 15 min | 9 | | (14.67 | | | | | |
| | | | 614.67 | 15.90 To | op of Sand Pack | : | | |
| Type of Sand Pack: Quartz sand | 1 | | 612.02 | 17.74 T. | | | | |
| Grain Size: 10/20 (sie | ve size) | | 612.83 | <u>17.74</u> To | op of Screen | | | |
| Installation Method: <u>Gravit</u> | У | | 608.29 | 22.28 Bo | ottom of Screen | | | |
| Type of Backfill Material:n/a | (Construit) | | 607.76 | | ottom of Well | | | |
| Installation Method: n/a | (if applicable) | | 606.57 | 24.00 Bo | ottom of Boreho | ole | | |
| | | | | National Geodetic Da | | | | |
| | | | CAS | ING MEASUI | REMENTS | | | |
| WELL COM | TENLOTION MATERIAL C | | Diameter of Boreho | le | (inches) | 8.0 | | |
| | STRUCTION MATERIALS e type of material for each area) | | ID of Riser Pipe | | (inches) | 2.0 | | |
| | | | Protective Casing L | ength | (feet) | 5.0 | | |
| Protesting C. : | CC204 CC214 PTEE PVC | | Riser Pipe Length | | (feet) | 20.08 | | |
| Protective Casing Riser Pipe Above W.T. | | HER: | Bottom of Screen to | | (feet) | 0.53 | | |
| Riser Pipe Below W.T. | | HER: | Screen Length (1s | | (feet) | 4.54 | | |
| Table I ipe Below W.1. | 112 (170) 011 | | Total Length of Cas | sing | (feet) | 25.15 | | |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

| Illinois Environ | e y | Well Completion Repo | | | | | | |
|---------------------------------------|--|-----------------------------------|---|-------------------------|-----------------|--------------|--|--|
| Site #: | County: <u>M</u> | Iontgomery | | Well #: | G2 | 10 | | |
| | ver Station CCB Management Facili | | | | ole #: | G210 | | |
| State | 0.0 Y 875,359.7 (or) Latitud | • | | | | | | |
| Surveyed By: | ck | IL Regist | tration #:035-00 | 3507 | | | | |
| Drilling Contractor: <u>Layne-We</u> | stern Co | Driller: _ | D. Mahurin | | | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | Geologis | Geologist: Rhonald W. Hasenyager, LPG #196-000246 | | | | | |
| Drilling Method: Hollow stem | auger | Drilling Fluid (Type): <u>n/a</u> | | | | | | |
| Logged By: Suzanna L. Simps | son | Date Star | rted: 10/6/201 | 10 Date Fini | shed:10/ | 6/2010 | | |
| Report Form Completed By: Su: | zanna L. Simpson | Date: | 10/8/2010 | | | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | | | |
| | | | 633.17 | | of Protective | Casing | | |
| | | | 632.99 | -2.51 Top | | Cuomg | | |
| | | | | rop | or ruser rape | | | |
| Type of Surface Seal: Concrete | | | 630.48 | Gro | und Surface | | | |
| Type of Annular Sealant: High-s | olids bentonite | | 627.48 | | of Annular Se | ealant | | |
| Installation Method:Tremie | | | | | | | | |
| Setting Time: >24 hr. | | $ \underline{\nabla} $ | 615.38 | 15.10 Stat | ic Water Leve | I | | |
| | | | | (Af | ter Completion) | 11/15/2010 | | |
| Type of Bentonite Seal Grant | Pellet Slurry (choose one) | | | | | | | |
| Installation Method: Gravity | , | | 614.03 | 16.45 Top | of Seal | | | |
| Setting Time: 15 hrs | | 1 [7] | 612.98 | 17.50 Top | of Sand Pack | | | |
| T. 60 ID I | | | | | | | | |
| Type of Sand Pack: Quartz sand | | | 611.09 | 19.39 Top | of Screen | | | |
| Grain Size: 10/20 (sie | | | | | | | | |
| Installation Method: <u>Gravity</u> | <u>'</u> | | _606.55_ | | tom of Screen | | | |
| Type of Backfill Material: <u>n/a</u> | (if applicable) | | 606.02 | 24.46 Bott | tom of Well | | | |
| Installation Method:n/a | (Tr) | | 605.48 | | tom of Boreho | le | | |
| | | | * Referenced to a N | Vational Geodetic Datur | m | | | |
| | | | CASI | NG MEASUR | EMENTS | | | |
| WELL CONS | TDUCTION MATERIALS |] | Diameter of Borehol | le | (inches) | 8.0 | | |
| | TRUCTION MATERIALS e type of material for each area) | | ID of Riser Pipe | | (inches) | 2.0 | | |
| | | | Protective Casing Le | ength | (feet) | 5.0 | | |
| Protective Casing | SS304 SS316 PTFE PVC OTHE | | Riser Pipe Length | End Com | (feet) | 21.90 | | |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHE | l' | Bottom of Screen to Screen Length (1st | | (feet) | 0.53 4.54 | | |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHE | 11 | Total Length of Casi | | (feet) | 26.97 | | |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

 $\hbox{**Hand-Slotted Well Screens Are Unacceptable}\\$

0.010

| Illinois Environ | e y | Well Completion Repo | | | | | | |
|--|---|--------------------------|---|-------------------------|-----------------|---------|--|--|
| Site #: | County: <u>M</u> | Iontgomery | | Well #: | : <u>G2</u> | 11 | | |
| | wer Station CCB Management Facili | | | | ole#: C | G211 | | |
| State | 9.1 Y 875,424.5 (or) Latitud | • | | | | | | |
| Surveyed By: | ck | IL Regist | ration #: <u>035-00</u> | 03507 | | | | |
| Drilling Contractor: <u>Layne-We</u> | stern Co | _ Driller: _ | D. Mahurin | | | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | _ Geologist | Geologist: Rhonald W. Hasenyager, LPG #196-000246 | | | | | |
| Drilling Method: Hollow stem | auger | _ Drilling I | Fluid (Type): <u>n/a</u> | | | | | |
| Logged By: Suzanna L. Simps | son | _ Date Star | ted: 10/11/20 | 10 Date Fini | shed:10/ | 11/2010 | | |
| Report Form Completed By: Su | zanna L. Simpson | _ Date: | 10/15/2010 | | | | | |
| ANNULAR SPA | CE DETAILS | | Elevations | Depths | (0.01 ft.) | | | |
| | | | (MSL)* 632.83 | (BGS) 2.52 Top | of Protective | Casing | | |
| | T | | | | | _ | | |
| | | | _632.64_ | 2.33 Top | of Riser Pipe | | | |
| Type of Surface Seal: Concrete | | | 630.31 | | und Surface | | | |
| Type of Annular Sealant: High-s | colids bentonite | | 627.31 | | of Annular So | ealant | | |
| Installation Method: Tremie | | | | | | | | |
| Setting Time: _ >24 hr. | | $ \underline{\nabla} $ | 616.17 | 14.14 Stat | ic Water Leve | 1 | | |
| Setting Time. 27 III. | | <u>*</u> | | | ter Completion) | | | |
| Type of Bentonite Seal Grant | ular Pellet Slurry (choose one) | | | | | | | |
| Installation Method: Gravity | | | 616.01 | 14.30 Top | of Seal | | | |
| Setting Time: 15 min | | | 614.91 | 15.40 Top | of Sand Pack | | | |
| | | | | | or Sund Tuck | | | |
| Type of Sand Pack: Quartz sand | <u> </u> | | _612.97_ | 17.34 Top | of Screen | | | |
| Grain Size:10/20 (sie | | | 012.57 | | of Scient | | | |
| Installation Method: <u>Gravity</u> | <i>I</i> | | 608.43 | 21.88 Bot | tom of Screen | | | |
| Type of Backfill Material: <u>n/a</u> | (C V I I) | | 607.90 | | tom of Well | | | |
| Installation Method: n/a | (if applicable) | | 606.31 | 24.00 Bott | tom of Boreho | le | | |
| instanction viction. <u>in a</u> | | | | National Geodetic Datus | | | | |
| | | | CASI | ING MEASUR | EMENTS | | | |
| | |] | Diameter of Borehol | | (inches) | 8.0 | | |
| | TRUCTION MATERIALS ne type of material for each area) |] | D of Riser Pipe | | (inches) | 2.0 | | |
| | | <u> 1</u> | Protective Casing Le | ength | (feet) | 5.0 | | |
| Production C. | 00204 00217 PEPP 2272 | | Riser Pipe Length | | (feet) | 19.67 | | |
| Protective Casing | SS304 SS316 PTFE PVC OTHER SS304 SS316 PTFE PVC OTHER | | Bottom of Screen to | | (feet) | 0.53 | | |
| Riser Pipe Above W.T. Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | | Screen Length (1st | | (feet) | 4.54 | | |
| Table Tipe Below 11.1. | 1112 (170) OHE | | Total Length of Cas | шg | (feet) | 24.74 | | |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

 $\hbox{**Hand-Slotted Well Screens Are Unacceptable}\\$

0.010

| Illinois Environ | nmental Protection Agenc | y | | Well C | Completion | Report |
|--------------------------------------|--|---|---------------------------|-----------------------------|----------------------------------|------------------|
| Site #: | County:! | Montgomery | | Well | #: G2 | 212 |
| Site Name: CCB Managemen | t Facility | | | Bore | hole #: | G212 |
| State Plane Coordinate: X 2,515,583 | 3.0 Y 875,486.5 (or) Latitu | ide:39 | 4! <u>6.300Ä</u> | Longitude: _ | -89 23 | <u> 43.100</u> Ä |
| Surveyed By: <u>Jeffrey D. Emric</u> | ck | IL Registr | ation #:035-0 | 03507 | | |
| Drilling Contractor: <u>Layne-We</u> | estern Co | Driller: _ | D. Mahurin | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | Geologist: | Rhonald W. | Hasenyager, L | PG #196-000 | 246 |
| Drilling Method: Hollow stem | auger | Drilling F | uid (Type):n/a | ı | | |
| Logged By: Suzanna Simpson | 1 | Date Start | ed:10/11/20 | 010 Date F | inished:10/ | 11/2010 |
| Report Form Completed By:Su | ızanna Simpson | Date: | 10/19/2010 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | 633.12 | | op of Protective | Casing |
| | | | 632.89 | 2.30 T | op of Riser Pipe | ; |
| Type of Surface Seal: Concrete | | | _630.59_ | 0.00 G | round Surface | |
| Type of Annular Sealant: High- | solids bentonite | | 627.59 | 3.00 T | op of Annular S | ealant |
| Installation Method: Tremio | 7 | | | | | |
| Setting Time: >24 hr. | | $\left \begin{array}{c} \overline{\nabla} \end{array}\right $ | 616.10_ | 14.49 St | tatic Water Leve | el |
| | | | | (| After Completion) | 11/15/2010 |
| Type of Bentonite Seal Gran | Pellet Slurry (choose one) | | | | | |
| Installation Method: Gravit | <u>y</u> | | 616.89 | 13.70 T | op of Seal | |
| Setting Time: 17 min | | | 615.79 | 14.80 Te | op of Sand Pack | ζ |
| Type of Sand Pack: Quartz sand | d | | | | | |
| Grain Size:10/20 (sign | eve size) | | 613.85 | 16.74 T | op of Screen | |
| Installation Method:Gravit | y | | | | | |
| Type of Backfill Material: n/a | | | 609.30 608.78 | | ottom of Screen ottom of Well | |
| 1) pe of 2 autim 13 autim | (if applicable) | | | | | |
| Installation Method: <u>n/a</u> | | | 606.59 * Referenced to a | 24.00 B National Geodetic D | ottom of Boreho atum | ole |
| | | | CAS | INIC MEASI | DEMENITO | |
| | | Г | riameter of Boreho | SING MEASU | (inches) | 8.0 |
| | STRUCTION MATERIALS ne type of material for each area) | | O of Riser Pipe | | (inches) | 2.0 |
| (- 1000 0 | · / | P | rotective Casing L | ength | (feet) | 5.0 |
| | T | | iser Pipe Length | | (feet) | 19.04 |
| Protective Casing | SS304 SS316 PTFE PVC OTH | | ottom of Screen to | | (feet) | 0.52 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTH | | creen Length (1s | | (feet) | 4.55 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTH | EK: T | otal Length of Ca | sing | (feet) | 24.11 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | y | Well Completion Repo | | | | |
|--|---|---------------------------|-------------------------|-------------------------|--------------------|------|
| Site #: | County: M | ontgomery | | Well #: | G213 | |
| | ver Station CCB Management Facilit | | | | #: <u>G213</u> | |
| State | 3.5 Y 875,544.4 (or) Latitude | • | | | | |
| Surveyed By:Jeffrey D. Emri | ck | _ IL Regist | ration #: <u>035-00</u> | 3507 | | |
| Drilling Contractor: <u>Layne-We</u> | stern Co | _ Driller: _ | D. Mahurin | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | _ Geologist | :: _ Rhonald W. I | Hasenyager, LPG | #196-000246 | |
| Drilling Method: Hollow stem | auger | Drilling Fluid (Type):n/a | | | | |
| Logged By: Suzanna L. Simp | son | _ Date Star | ted: 10/12/20 | 10 Date Finishe | ed: 10/12/20 | 010 |
| Report Form Completed By:Su | zanna L. Simpson | _ Date: | 10/19/2010 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | | (0.01 ft.) | |
| | | | 633.08 | (BGS)2.74 Top of | Protective Casi | no |
| | T | | | | | 15 |
| | \[\begin{align*} \text{ \lefty} \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ | | _632.81_ | 2.47 Top of | Riser Pipe | |
| Type of Surface Seal: Concrete | | | 630.34 | 0.00 Ground | d Surface | |
| Type of Annular Sealant: High-s | colids bentonite | | 627.64 | | Annular Sealan | t |
| Installation Method: Tremie | 7 | | | | | |
| Setting Time: _ >24 hr. | | Δ | 615.01 | 15.33 Static | Water Level | |
| Setting Time. 27 III. | | <u>*</u> | | | Completion) 11/15/ | 2010 |
| Type of Bentonite Seal Gran | ular Pellet Slurry (choose one) | | | | | |
| Installation Method: Gravity | | | 616.54 | | Seal | |
| Setting Time: 10 min | | | 615.34 | 15.00 Top of | Sand Pack | |
| | | | | | build I dek | |
| Type of Sand Pack: Quartz sand | <u> </u> | | 613.59 | 16.75 Top of | Screen | |
| Grain Size:10/20 (sie | | | 013.37 | | Sciech | |
| Installation Method: <u>Gravity</u> | / | | 609.05 | 21.29 Bottom | n of Screen | |
| Type of Backfill Material: <u>n/a</u> | (if applicable) | | 608.52 | | n of Well | |
| Installation Method: n/a | (if applicable) | | 606.34 | 24.00 Bottom | n of Borehole | |
| instanction rection. <u>194</u> | | | | Internal Geodetic Datum | TOT BOTCHOIC | |
| | | | CASI | NG MEASUREN | MENTS | |
| | |] | Diameter of Borehol | | | 3.0 |
| | TRUCTION MATERIALS the type of material for each area) | | D of Riser Pipe | | (inches) 2 | 2.0 |
| | | 1 | Protective Casing Le | ength | (feet) 5 | 5.0 |
| Durkasking C | GC204 GC216 PEEP 2776 5 | | Riser Pipe Length | | | 0.22 |
| Protective Casing | | | Bottom of Screen to | | | 0.53 |
| Riser Pipe Above W.T. Riser Pipe Below W.T. | SS304 SS316 PTFE (PVC) OTHER SS304 SS316 PTFE (PVC) OTHER | | Screen Length (1st | | | 1.54 |
| Tabel Tipe Delow W.1. | SSSOT SSSTO THE TVC OTHER | | Γotal Length of Casi | ng | (feet) 24 | 1.29 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

 $\hbox{**Hand-Slotted Well Screens Are Unacceptable}\\$

0.010

| Illinois Environmental Protection Agency | | | | Well Completion Repor | | | | | |
|--|----------------------------|------------|-----------|---|---------------------|--------------------|--------------|--|--|
| Site #: | C | ounty: Mor | ntgomery | | Wei | 11 #: G2 | 214 | | |
| Site Name: AEG Coffeen Power Sta | | | | | | rehole #: | G214 | | |
| State Plane Coordinate: X 2,515,960.8 | | • | | | | | | | |
| Surveyed By:Jeffrey D. Emrick | | | IL Regis | stration #: <u>035-0</u> | 03507 | | | | |
| Drilling Contractor: Layne-Western C | Co | | Driller: | D. Mahurin | | | | | |
| Consulting Firm: Hanson Profession: | al Services Inc. | | Geologis | Geologist: Rhonald W. Hasenyager, LPG #196-000246 | | | | | |
| Drilling Method: Hollow stem auger | | | Drilling | Drilling Fluid (Type):n/a | | | | | |
| Logged By: Suzanna L. Simpson | | | Date Sta | arted:10/14/20 | 010 Date l | Finished:10/ | 14/2010 | | |
| Report Form Completed By: Suzanna | L. Simpson | | Date: | 10/19/2010 | | | | | |
| ANNULAR SPACE D | ETAILS | | | Elevations | Depths | (0.01 ft.) |) | | |
| | | | | (MSL)* 633.08 | (BGS) -2.69 | Top of Protective | Casina | | |
| | | | | | | • | | | |
| | | | | 632.85 | 2.46 | Top of Riser Pipe | 2 | | |
| Type of Surface Seal: Concrete | | - | | 630.39 | 0.00 | Ground Surface | | | |
| Type of Annular Sealant: High-solids be | entonite | | | 626.99 | 3.40 | Top of Annular S | Sealant | | |
| Installation Method: Tremie | Cittorite | - | | | | | | | |
| Setting Time: _ >24 hr. | | _ | <u>_</u> | 609.48 | 20.91 | Static Water Leve | el | | |
| seeing Time. ———————————————————————————————————— | | _ - | <u>-</u> | | | (After Completion) | | | |
| Type of Bentonite Seal Granular | Pellet Slurry (choose one) | | | | | | | | |
| Installation Method: <u>Gravity</u> | | _ | \bowtie | 615.39 | _15.00_ | Гор of Seal | | | |
| Setting Time: 14 min | | _ 🐰 | | 614.34 | 16.05 | Top of Sand Pacl | ζ. | | |
| Town of Court Dealer of the | | | | | | • | | | |
| Type of Sand Pack: Quartz sand Grain Size: 10/20 (sieve size) | | _ _ | | 612.64 | 17.75 | Top of Screen | | | |
| Grain Size: 10/20 (sieve size) Installation Method: Gravity | | | | | | | | | |
| instanation inclined. Otavity | | | | 608.25 | | Bottom of Screen | ı | | |
| Type of Backfill Material:n/a | (if applicable) | _ _ | | 607.74 | 22.651 | Bottom of Well | | | |
| Installation Method:n/a | | | | 606.39 | | Bottom of Boreh | ole | | |
| | | | | * Referenced to a | National Geodetic I | Datum | | | |
| | | | _ | CAS | SING MEASU | UREMENTS | | | |
| WELL CONSTRUC | TION MATERIAI | S | | Diameter of Boreho | ole | (inches) | 8.0 | | |
| | material for each area) | | | ID of Riser Pipe | | (inches) | 2.0 | | |
| | | | | Protective Casing I | Length | (feet) | 5.0 | | |
| Protective Casing SS304 | SS316 PTFE I | PVC OTHER: | | Riser Pipe Length | o End C- | (feet) | 20.21 | | |
| Riser Pipe Above W.T. SS304 | | OTHER: | | Bottom of Screen to Screen Length (1) | | (feet) | 0.51 4.39 | | |
| Riser Pipe Below W.T. SS304 | | OTHER: | | Total Length of Ca | | (feet) | 25.11 | | |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

 $\hbox{**Hand-Slotted Well Screens Are Unacceptable}\\$

0.010

| Illinois Environ | mental Protection Agend | ey | | Well C | Completion | Report | | |
|---------------------------------------|---|-------------------------|---|---------------------|---------------------------------------|-----------------|--|--|
| Site #: | County: | Montgomery | | Well | #: <u>G2</u> | 215 | | |
| Site Name: CCB Management | t Facility | | | Bore | hole #: | G215 | | |
| State Plane Coordinate: X 2,515,971 | 1.6 Y 875,810.2 (or) Latit | tude: <u>39</u> | 4!9.500Ä | Longitude: _ | <u>-89</u> <u>23</u> | <u>38.200</u> Ä | | |
| Surveyed By: <u>Jeffrey D. Emric</u> | ck | IL Regi | stration #:035-00 | 03507 | | | | |
| Drilling Contractor: <u>Layne-We</u> | stern Co | Driller: | D. Mahurin | | | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | Geologi | Geologist: Rhonald W. Hasenyager, LPG #196-000246 | | | | | |
| Drilling Method: Hollow stem | auger | Drilling | Fluid (Type):n/a | ı | | | | |
| Logged By: Suzanna Simpson | 1 | Date Sta | arted: 10/13/20 | 010 Date Fi | inished:10/ | 13/2010 | | |
| Report Form Completed By:Su | zanna Simpson | Date: _ | 10/19/2010 | | | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | | | |
| | | | 633.30 | | op of Protective | Casing | | |
| | | | 633.06 | | op of Riser Pipe | _ | | |
| Type of Surface Seal: Concrete | | | 630.48 | 0.00 G | round Surface | | | |
| | | | 627.58 | | op of Annular S | ealant | | |
| Type of Annular Sealant: High-s | solids bentonite | | _027.30 | 2.90 | op of Familiaia 5 | cuiuiit | | |
| Installation Method:Tremie | 2 | | | | | | | |
| Setting Time: >24 hr. | | $ \overline{\Delta} $ | _607.64_ | | tatic Water Leve After Completion) | | | |
| Type of Bentonite Seal Gran | ular Pellet Slurry — | | | | | | | |
| Installation Method: Gravit | (choose one) | | 614.08 | 16.40 T | op of Seal | | | |
| Setting Time: 20 min | | | | | | | | |
| | | | 612.98 | 17.50 To | op of Sand Pack | <u>C</u> | | |
| Type of Sand Pack: Quartz sand | <u> </u> | | (11.07 | 10.41 m | c a | | | |
| Grain Size:10/20 (sie | eve size) | | 611.07 | 19.41 T | op of Screen | | | |
| Installation Method: Gravit | <u>y</u> | | 606.69 | 23.80 В | -# | | | |
| Type of Backfill Material: <u>n/a</u> | | | 606.68 606.17 | | ottom of Screen ottom of Well | | | |
| Installation Mathada n/a | (if applicable) | | 606.17 | 24.31 B | attam of Darish | ala. | | |
| Installation Method:n/a | | | | National Geodetic D | ottom of Boreho atum | ne | | |
| | | | CAS | ING MEASU | REMENTS | | | |
| | | | Diameter of Boreho | | (inches) | 8.0 | | |
| | STRUCTION MATERIALS e type of material for each area) | | ID of Riser Pipe | | (inches) | 2.0 | | |
| , | | | Protective Casing L | ength | (feet) | 5.0 | | |
| | I | | Riser Pipe Length | | (feet) | 21.99 | | |
| Protective Casing | | HER: | Bottom of Screen to | End Cap | (feet) | 0.51 | | |
| Riser Pipe Above W.T. | | HER: | Screen Length (1s | | (feet) | 4.39 | | |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTI | HER: | Total Length of Cas | sing | (feet) | 26.89 | | |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

| Illinois Environ | y | Well Completion Repo | | | | | | |
|---------------------------------------|---|----------------------|---|-------------------------|---------------------------|--|--|--|
| Site #: | County: M | ontgomery | | Well #: | G216 | | | |
| | ver Station CCB Management Facili | | | | e#: <u>G216</u> | | | |
| State | 8.5 Y 875,976.1 (or) Latitud | - | | | | | | |
| Surveyed By:Jeffrey D. Emri | ck | IL Regist | ration #: <u>035-00</u> | 03507 | | | | |
| Drilling Contractor: <u>Layne-We</u> | stern Co | _ Driller: _ | D. Mahurin | | | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | _ Geologist | Geologist: Rhonald W. Hasenyager, LPG #196-000246 | | | | | |
| Drilling Method: Hollow stem | auger | _ Drilling F | Fluid (Type): <u>n/a</u> | | | | | |
| Logged By: Suzanna L. Simp | son | _ Date Star | ted: 10/13/20 | 110 Date Finisl | hed: 10/13/2010 | | | |
| Report Form Completed By:Su | zanna L. Simpson | _ Date: | 10/19/2010 | | | | | |
| ANNULAR SPA | CE DETAILS | | Elevations | Depths | (0.01 ft.) | | | |
| | | | (MSL)* 633.02 | (BGS) | of Protective Casing | | | |
| | T | | | | _ | | | |
| | | | 632.76 | 2.48 Top o | of Riser Pipe | | | |
| Type of Surface Seal: Concrete | | | 630.28 | | nd Surface | | | |
| Type of Annular Sealant: High-s | volids bentonite | | 627.78 | | of Annular Sealant | | | |
| Installation Method: Tremie | , h | | | | | | | |
| | | ∇ | 607.52 | 22.76 Static | e Water Level | | | |
| Setting Time: >24 hr. | | ∇ | 007.32 | | er Completion) 11/15/2010 | | | |
| Type of Bentonite Seal Gran | ular Pellet Slurry (choose one) | | | | | | | |
| Installation Method: Gravity | | | 613.28 | | of Seal | | | |
| Setting Time: 15 min | | | 612.08 | 18.20 Top o | of Sand Baak | | | |
| | | | 012.00 | | n Sand Fack | | | |
| Type of Sand Pack: Quartz sand | L | | 610.24 | 20.04 Top o | of Screen | | | |
| Grain Size:10/20 (sie | ve size) | | _010.24_ | Top (| n screen | | | |
| Installation Method: <u>Gravity</u> | <i>I</i> | | 605.86 | 24.42 Botto | om of Screen | | | |
| Type of Backfill Material: <u>n/a</u> | (C. F. H.) | | 605.35 | | om of Well | | | |
| Installation Method: n/a | (if applicable) | | 604.28 | 26.00 Botto | om of Borehole | | | |
| instanation victiod. <u>IV</u> a | | | | National Geodetic Datum | | | | |
| | | | CASI | ING MEASURE | EMENTS | | | |
| | | I | Diameter of Borehol | | (inches) 8.0 | | | |
| | TRUCTION MATERIALS the type of material for each area) | | D of Riser Pipe | | (inches) 2.0 | | | |
| | | <u> </u> | Protective Casing Le | ength | (feet) 5.0 | | | |
| D | T | | Riser Pipe Length | | (feet) 22.52 | | | |
| Protective Casing | | | Bottom of Screen to | | (feet) 0.51 | | | |
| Riser Pipe Above W.T. | SS304 SS316 PTFE (PVC) OTHER SS304 SS316 PTFE (PVC) OTHER | | Screen Length (1st | | (feet) 4.38 | | | |
| Riser Pipe Below W.T. | 55504 55510 FIFE (FVC) OTHER | <u> </u> | Total Length of Cas | ing | (feet) 27.41 | | | |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

 $\hbox{**Hand-Slotted Well Screens Are Unacceptable}\\$

0.010

| Illinois Environmental Protection Agency | | | | Well Completion Report | | | | | |
|--|--|-------------------|---|------------------------|-----------------|--|-------------|--|--|
| Site #: | Co | ounty: <u>Mon</u> | tgomery | | W | Tell #: G | 217 | | |
| Site Name: <u>AEG Coffeen Pov</u> | ver Station CCB Managen | nent Facility | | | Во | orehole #: | G217 | | |
| State Plane Coordinate: X 2,515,963 | 8.0 Y 876,185.6 (or | r) Latitude: | 39° | 4'13.2" | Longitude | e:89 °2 | 23 ' 38.3 " | | |
| Surveyed By: | ek | | IL Regis | stration #:035-0 | 03507 | | | | |
| Drilling Contractor: <u>Layne-We</u> | stern Co | | Driller: | D. Mahurin | | | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | | Geologist: Rhonald W. Hasenyager, LPG #196-000246 | | | | | | |
| Drilling Method: Hollow stem | auger | | Drilling | Fluid (Type):n/a | 1 | | | | |
| Logged By: Suzanna L. Simps | son | | Date Sta | arted: 10/12/20 | 010 Date | Finished: 10 | /12/2010 | | |
| Report Form Completed By: Su | zanna L. Simpson | | Date: _ | 10/19/2010 | | | | | |
| ANNULAR SPA | CE DETAILS | | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) |) | | |
| | | | | 633.34 | 2.67 | Top of Protective | e Casing | | |
| | | | | 633.10 | -2.43 | Top of Riser Pipe | e | | |
| Type of Surface Seal: Concrete | | | | 630.67 | 0.00 | Ground Surface | | | |
| | | | | 628.27 | 2.40 | Top of Annular S | Sealant | | |
| Type of Annular Sealant: High-s | | - | | | | • | | | |
| Installation Method:Tremie | | - _ | _ | (00.00 | 21.20 | | | | |
| Setting Time: >24 hr. | | - Ž | _ | 609.28 | _21.39_ | Static Water Lev (After Completion) | | | |
| Type of Bentonite Seal Grant | | | | | | | | | |
| Installation Method: Gravity | (choose one) | | | 612.82 | 17.85 | Top of Seal | | | |
| Setting Time: 11 min | | _ | | 611.92 | 10 05 | Top of Sand Dag | 1- | | |
| | | | M | 611.82 | _10.03_ | Top of Sand Pac | K. | | |
| Type of Sand Pack: Quartz sand | 1 | _ | | 610.18 | 20.49 | Top of Screen | | | |
| Grain Size:10/20 (sie | ve size) | | | 010.18 | | Top of Screen | | | |
| Installation Method: <u>Gravity</u> | I | - | | 605.79 | 24.88 | Bottom of Screen | 1 | | |
| Type of Backfill Material:n/a | (2 ti 1) | | | 605.29 | 25.38 | Bottom of Well | 1 | | |
| Installation Method: n/a | (if applicable) | | | 604.67 | 26.00 | Bottom of Boreh | olo | | |
| installation Method. <u>Wa</u> | | _ | | * Referenced to a | | | oie | | |
| | | | | CAS | SING MEAS | SUREMENTS | | | |
| | | | | Diameter of Boreho | | (inches) | 8.0 | | |
| | TRUCTION MATERIALS e type of material for each area) | S | | ID of Riser Pipe | | (inches) | 2.0 | | |
| | | | | Protective Casing L | ength | (feet) | | | |
| D | | 1 | | Riser Pipe Length | | (feet) | | | |
| Protective Casing | | VC OTHER: (| Steel | Bottom of Screen to | • | (feet) | | | |
| Riser Pipe Above W.T. | | VC OTHER: | | Screen Length (1s | | t) (feet) | 4.39 | | |
| Riser Pipe Below W.T. | SS304 SS316 PTFE P | VC) OTHER: | | Total Length of Cas | sing | (feet) | 27.81 | | |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environmental Protection Agency | | | | Well Completion Rep | | | | ion Report |
|---|--|--------------------|--|---------------------|------------------|-----------------------------|-----------------|---------------------------|
| Site #: | | County: <u>Mor</u> | ntgomery | 7 | | W | /ell #: | G218 |
| Site Name: CCB Management Fac | cility | | | | | В | orehole #: | G218 |
| State Plane Coordinate: X 2,515,962.2 | · | | | | | | | |
| | | | | | ±:035-0 | | c. <u>-09</u> _ | |
| | _ | | _ | | | | | |
| Drilling Contractor: <u>Layne-Westerr</u> | 1 Co | | Driller: | _ D. Ma | ahurin | | | |
| Consulting Firm: <u>Hanson Profession</u> | onal Services Inc. | | Geolog | ist: Rh | onald W. | Hasenyager | r, LPG #196- | 000246 |
| Drilling Method: Hollow stem auge | er | | Drilling | g Fluid (T | ype): <u>n/a</u> | a | | |
| Logged By: Suzanna Simpson | | | Date St | arted: | 10/12/20 | 010 Dat | e Finished: | 10/12/2010 |
| Report Form Completed By: Suzanr | na Simpson | | Date: _ | 10/ | 19/2010 | | | |
| ANNULAR SPACE | DETAILS | | | | vations MSL)* | Depths (BGS) | (0.01 | ft.) |
| | | | | ` | 33.34 | -2.70 | Top of Prote | ctive Casing |
| | | | | _6 | 33.11 | 2.47 | Top of Riser | Pipe |
| Type of Surface Seal: Concrete | | | | , 6 | 30.64 | 0.00 | Ground Surf | ace |
| | | | | /— — | 27.14 | 3.50 | | |
| Type of Annular Sealant: High-solids | s bentonite | | | _0 | 27.14 | | Top of Alliu | iai Scaiaiii |
| Installation Method: Tremie | | | | | | | | |
| Setting Time: >24 hr. | | | ot = ot | _6 | 09.89 | _20.75_ | Static Water | Level tion) 11/15/2010 |
| Type of Bentonite Seal Granular | Dollat Cl | | | | | | (Autor Complex | 11/15/2010 |
| Type of Bentonite Seaf Granular | Pellet Sh (choose one) | ırry | | | | | | |
| Installation Method: Gravity | | | | _6 | 13.14 | 17.50 | Top of Seal | |
| Setting Time: 17 min | | —— | | _6 | 12.14 | _18.50_ | Top of Sand | Pack |
| Type of Sand Pack: Quartz sand | | | | | | | | |
| | | | | _6 | 10.31 | _20.33_ | Top of Scree | n |
| Grain Size: 10/20 (sieve size | e) | | | | | | | |
| Installation Method: <u>Gravity</u> | | | | 6 | 05.87 | 24.77 | Bottom of So | ereen |
| Type of Backfill Material:n/a | (if applicable) | | | | 05.37 | 25.27 | Bottom of W | 'ell |
| Installation Method: n/a | (ii applicable) | | | 6 | 04.64 | 26.00 | Bottom of Bo | orehole |
| | | | | * R | Referenced to a | National Geodet | | |
| | | | | | CAS | SING MEAS | SUREMENT | S |
| | | | | Diamete | r of Boreho | | | thes) 8.0 |
| WELL CONSTRU (Choose one type | JCTION MATE of material for each area | | | ID of Ri | ser Pipe | | (inc | thes) 2.0 |
| | | | | | ve Casing I | ength | (| feet) 5.0 |
| Protective Casing SS3 | 304 SS316 PTF | E PVC OTHER:(| | | pe Length | | | feet) 22.80 |
| Riser Pipe Above W.T. SS3 | | | | | of Screen to | • | | feet) 0.50 |
| Riser Pipe Below W.T. SS3 | | | | | ength (1s | st slot to last slo sing | | feet) 4.44 feet) 27.74 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | | Well Completion Report | | | | |
|---|---------------------------------------|---------------------------------|--|------------------|-----------------------------------|------------------------|
| Site #: | County: M | ontgomery | | W | /ell #: | G270 |
| Site Name: CCB Management | t Facility | | | Во | orehole #: | G270 |
| State Plane Coordinate: X 2,514,996 | 6.8 Y 874,801.9 (or) Latitud | e: <u>39</u> | 3! <u>59.600</u> Ä | Longitude | e: <u>-89</u> _ | 23! <u>50.700</u> Ä |
| Surveyed By: <u>Jeffrey D. Emric</u> | :k | _ IL Regist | ration #:035-00 | 03507 | | |
| Drilling Contractor: Testing Se | ervice Corp. | _ Driller: _ | B. Williamson | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | _ Geologist | t: Rhonald W. | Hasenyager | , LPG #196-0 | 000246 |
| Drilling Method: Hollow stem | auger | _ Drilling F | Fluid (Type): | | | |
| Logged By: Suzanna Simpson | l | Date Star | ted:2/26/20 | 08 Date | e Finished: | 2/26/2008 |
| | zanna Simpson | _ | 2/29/2008 | | | |
| ANNULAR SPA | * | | Elevations (MSL)* | Depths (BGS) | (0.01 | ft.) |
| | | | 626.41 | 3.49 | Top of Protec | tive Casing |
| | | | 625.97 | -3.05 | Top of Riser | Pipe |
| Type of Surface Seal: Concrete | | | 622.92 | 0.00 | Ground Surfa | ce |
| | | | 619.92 | 3.00 | Top of Annul | ar Sealant |
| Type of Annular Sealant: Benton |) | | | | | |
| Installation Method: Gravit | | | 617.20 | 5.60 | Static Water | aval |
| Setting Time: _ >24 hr. | | $\stackrel{\checkmark}{\Delta}$ | 617.30 | 5.62 | Static Water 1 (After Completi | |
| Type of Bentonite Seal Gran | ular Pellet Slurry (choose one) | | | | | |
| Installation Method: Gravit | , , , | | 619.92 | 3.00 | Top of Seal | |
| Setting Time:>24 hr. | | | 610.92 | 12.00 | Top of Sand 1 | Pack |
| | | VV | 010.72 | | Top of Sand I | uck |
| Type of Sand Pack: Quartz sand | | | 609.79 | 13.13 | Top of Screen | |
| Grain Size: 10/20 (sie Installation Method: Gravit | , , , , , , , , , , , , , , , , , , , | | | | | |
| installation Method. Gravit | <u>y</u> | | 605.00 | _17.92_ | Bottom of Sci | reen |
| Type of Backfill Material: <u>n/a</u> | (if applicable) | | 604.65 | _18.27_ | Bottom of We | ell |
| Installation Method:n/a | | | 604.65 | 18.27 | Bottom of Bo | rehole |
| | | | * Referenced to a | National Geodeti | c Datum | |
| | | | CAS | ING MEAS | SUREMENT | S |
| WELL CONS | STRUCTION MATERIALS | | Diameter of Boreho | le | (incl | |
| (Choose on | e type of material for each area) | | D of Riser Pipe Protective Casing L | anath | (incl | |
| | | | Riser Pipe Length | viigui | • | eet) 5.0 eet) 16.18 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | | Bottom of Screen to | End Cap | • | eet) 0.35 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | | Screen Length (1s | | • | eet) 4.79 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | :] | Гotal Length of Cas | sing | (f | eet) 21.32 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

| Illinois Environ | | | Well Completion Report | | | |
|--------------------------------------|---|---------------------|--|----------------|--------------------------------------|---------------------|
| Site #: | County: M | ontgomery | | W | /ell #: | G271 |
| Site Name: CCB Management | t Facility | | | Во | orehole #: | G271 |
| State Plane Coordinate: X 2,515,517 | 7.1 Y 874,239.4 (or) Latitud | e: <u>39</u> | 3! <u>54.000</u> Ä | Longitude | e: <u>-89</u> | 23! <u>44.100</u> Ä |
| Surveyed By:Jeffrey D. Emric | ek | _ IL Registr | ration #:035-00 | 03507 | | |
| Drilling Contractor: <u>Layne-We</u> | stern Co | _ Driller: _ | G. Mills | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | _ Geologist: | Rhonald W. l | Hasenyager | , LPG #196-00 | 0246 |
| Drilling Method: Hollow stem | auger | _ Drilling F | luid (Type): | | | |
| Logged By: Rhonald W. Hase | nyager | Date Start | ted:9/9/200 | 9 Date | e Finished: | 0/10/2009 |
| | zanna Simpson | | 10/7/2009 | | | |
| ANNULAR SPA | | | Elevations | Depths | (0.01 ft | <u>.</u> .) |
| | | | (MSL)* _625.88_ | (BGS) -2.99 | Top of Protectiv | ve Casing |
| | T | | | | | _ |
| | | | 625.57 | 2.68 | Top of Riser Pi | pe |
| Type of Surface Seal: Concrete | | | 622.89 | 0.00 | Ground Surface | e |
| | | | 619.89 | 3.00 | Top of Annular | Sealant |
| Type of Annular Sealant: High-s | λ | | | | | |
| Installation Method: Tremie | | | 610.20 | 12.50 | Statia Watan I a | wal |
| Setting Time: >24 hr. | | $\overline{\Delta}$ | 610.39 | | Static Water Le (After Completion | |
| Type of Bentonite Seal Gran | | | | | | |
| Installation Method: Gravit | (choose one) | | 616.16 | 6.73 | Top of Seal | |
| Setting Time: 10 min | | | (12.07 | | - | |
| | | | 613.87 | 9.02 | Top of Sand Pa | ck |
| Type of Sand Pack: Quartz sand | 1 | | 612.02 | 0.06 | T | |
| Grain Size: 10/20 (sie | ve size) | | 612.93 | 9.96 | Top of Screen | |
| Installation Method: <u>Gravit</u> | <u>y</u> | | 608.58 | 14.31 | Bottom of Scre | en en |
| Type of Backfill Material: Quar | | | 608.10 | 14.79 | Bottom of Well | |
| Installation Method: Gravit | (if applicable) | | 606.89 | 16.00 | Bottom of Bore | hole |
| | | | * Referenced to a | | | |
| | | | CAS | ING MEAS | SUREMENTS | |
| WELL CONS | TDUCTION MATERIALS | Ε | Diameter of Boreho | le | (inches | 8.0 |
| | STRUCTION MATERIALS e type of material for each area) | | D of Riser Pipe | | (inches | |
| | | | rotective Casing L | ength | (fee | |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | | Riser Pipe Length Bottom of Screen to | End Con | (fee | 0.40 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | | creen Length (1st | • | ` | 4.2.5 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | | otal Length of Cas | | (fee | 15.45 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviro | nmental Protection Agency | | | Well | Completion | Report | |
|--|-------------------------------------|------------|--|------------------------|------------------------------------|--------|--|
| Site #: | County: Mor | ntgomery | | W | Vell #: <u>G2</u> | 72 | |
| Site Name: <u>AEG Coffeen Po</u> | wer Station CCB Management Facility | | | В | orehole #: | 3272 | |
| State- Plant Plane Coordinate: X 2,515,74 | 5.0 Y 874,234.8 (or) Latitude: | | <u>"</u> | Longitude | e:° | | |
| Surveyed By:Jeffrey D. Emr | ick | IL Regist | ration #: <u>035-00</u> | 3507 | | | |
| Drilling Contractor: <u>Layne-We</u> | estern Co | Driller: _ | G. Mills | | | | |
| Consulting Firm: Hanson Professional Services Inc. | | | : Rhonald W. H | Hasenyage | r, LPG #196-0002 | 246 | |
| Drilling Method: Hollow stem | n auger | Drilling I | Orilling Fluid (Type): | | | | |
| Logged By: Rhonald W. Has | enyager | Date Star | Date Started: 9/10/2009 Date Finished: 9/10/2009 | | | | |
| Report Form Completed By: Su | ızanna L. Simpson | Date: | 10/7/2009 | | | | |
| ANNULAR SPA | CE DETAILS | | Elevations | Depths | (0.01 ft.) | | |
| | | | (MSL)* | (BGS) | (*** **) | | |
| | | | 624.11 | -3.39 | Top of Protective | Casing | |
| | | | 623.81 | -3.09 | Top of Riser Pipe | | |
| Type of Surface Seal: Concrete | | | 620.72 | 0.00 | Ground Surface | | |
| T CA LOLL WIL | | | 617.72 | 3.00 | Top of Annular Se | ealant | |
| Type of Annular Sealant: High- | 7 | | | | | | |
| Installation Method: Tremi | | _ | 611.23 | 9.49 | Static Water Level | I | |
| Setting Time. 224 III. | | ☑ | 011.23 | | (After Completion) | | |
| Type of Bentonite Seal Gran | nular Pellet Slurry (choose one) | | | | | | |
| Installation Method: <u>Gravit</u> | ` ' | X X | 614.55 | 6.17 | Top of Seal | | |
| Setting Time: 10 min | | | 612.74 | 7.98 | Top of Sand Pack | | |
| Type of Sand Pack: Quartz sand | d | | | | | | |
| | eve size) | : | 611.61 | 9.11 | Top of Screen | | |
| Installation Method: <u>Gravit</u> | <u>y</u> | | | | | | |
| Type of Backfill Material:n/a_ | | | 606.74 606.40 | 13.98 14.32 | Bottom of Screen Bottom of Well | | |
| Type of Backfill Material. <u>11/a</u> | (if applicable) | | | 17.32 | Bottom of wen | | |
| Installation Method:n/a | | | 606.40 * Referenced to a N | 14.32 Tational Geodeti | Bottom of Boreho | le | |
| | | | CAST | | | | |
| | | Γ, | | | SUREMENTS | 9.0 | |
| | STRUCTION MATERIALS | | Diameter of Borehol D of Riser Pipe | <u> </u> | (inches) | 2.0 | |
| (Choose o | ne type of material for each area) | | Protective Casing Le | ength | (feet) | 5.0 | |
| | | | Riser Pipe Length | | (feet) | 12.20 | |
| Protective Casing | SS304 SS316 PTFE PVC OTHER: | Steel | Bottom of Screen to | End Cap | (feet) | 0.34 | |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER: | | Screen Length (1st | | t) (feet) | 4.87 | |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER: | - | Total Length of Casi | nα | (feet) | 17 41 | |

SS304

Screen

Well Completion Form (revised 02/06/02)

SS316

PTFE PVC OTHER:

**Hand-Slotted Well Screens Are Unacceptable

0.010

(inches)

Screen Slot Size **

| Illinois Environ | | Well | Completion | Report | | |
|--|-----------------------------------|--------------------|--------------------------------------|----------------------------|-------------------------|-----------------|
| Site #: | County | y: <u>Montgome</u> | ry | W | /ell #:G2 | 273 |
| Site Name: CCB Management | Facility | | | В | orehole #: | G273 |
| State Plane Coordinate: X 2,515,975 | 6.5 Y 874,235.2 (or) | Latitude: 39 | 3! 53.90 | <u>00</u> Ä Longitude | e: <u>-89</u> <u>23</u> | <u>38.300</u> Ä |
| Surveyed By: | k | IL Re | egistration #: 03: | 5-003507 | | |
| Drilling Contractor: <u>Layne-Wes</u> | stern Co | Drille | er: <u>G. Mills</u> | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | Geold | ogist: Rhonald | W. Hasenyager | , LPG #196-000 | 246 |
| Drilling Method: Hollow stem | auger | Drilli | ng Fluid (Type): _ | | | |
| Logged By: Rhonald W. Haser | nyager | Date | Started:9/10 | /2009 Date | e Finished:9/ | 10/2009 |
| Report Form Completed By: Suz | zanna Simpson | Date: | 10/7/200 | 9 | | |
| ANNULAR SPAC | CE DETAILS | | Elevation (MSL)* | ns Depths (BGS) | (0.01 ft.) | |
| | | | 623.33 | ` ' | Top of Protective | Casing |
| | | | 623.02 | -2.85 | Top of Riser Pipe | ; |
| Type of Surface Seal: Concrete | | | | 0.00 | Ground Surface | |
| T CA 1 C 1 4 W 1 | | | 617.17 | 3.00 | Top of Annular S | ealant |
| Type of Annular Sealant: High-s | | | , | | | |
| Installation Method: <u>Tremie</u> Setting Time: _ >24 hr. | | | 610.28 | 9.89 | Static Water Leve | ما |
| Setting Time | | | 010.20 | | (After Completion) | |
| Type of Bentonite Seal Grant | Pellet Slurry (choose one) | | _ | | | |
| Installation Method: Gravity | , | | 614.07 | 6.10 | Top of Seal | |
| Setting Time: 10 min | | | 612.45 | 7.72 | Top of Sand Pacl | ζ |
| True of Cond Dooley O | | | | | • | |
| Type of Sand Pack: Quartz sand Grain Size: 10/20 (sie) | | | 611.09 | 9.08 | Top of Screen | |
| Installation Method: Gravity | , | | | | | |
| | | | 605.61 | | Bottom of Screen | 1 |
| Type of Backfill Material: Quart | Z sand (if applicable) | | 605.07 | 15.10 | Bottom of Well | |
| Installation Method: Gravity | / | | 604.17 | 16.00to a National Geodeti | Bottom of Boreh | ole |
| | | | Referenced | to a rational Geodesi | o Butuiii | |
| | | | | CASING MEAS | SUREMENTS | |
| WELL CONS | TRUCTION MATERIALS | | Diameter of Bor | | (inches) | 8.0 |
| (Choose one | e type of material for each area) | | ID of Riser Pipe Protective Casir | | (inches) | 5.0 |
| | | | Riser Pipe Leng | | (feet) | 11.93 |
| Protective Casing | SS304 SS316 PTFE PVC | OTHER: | Bottom of Scree | | (feet) | 0.54 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC | OTHER: | | (1st slot to last slo | | 5.48 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC | OTHER: | Total Length of | | (feet) | 17.95 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

| Illinois Enviro | nmental Protection | n Agency | | | Well | Completion | Report | | |
|---|------------------------------------|-----------------|----------|--------------------------------------|-----------------|--|------------------|--|--|
| Site #: | (| County: Mon | tgomery | Ī | W | /ell #:G | 274 | | |
| Site Name: <u>AEG Coffeen Po</u> | wer Station CCB Manage | ment Facility | | | В | orehole #: | G274 | | |
| State- Plant Plane Coordinate: X 2,516,19 | 5.6 Y 874,239.2 (| or) Latitude: | | · | Longitud | e:° | | | |
| Surveyed By: <u>Jeffrey D. Emri</u> | ck | | IL Reg | istration #: <u>035-0</u> | 03507 | | | | |
| Drilling Contractor: <u>Layne-We</u> | estern Co | | Driller: | G. Mills | | | | | |
| Consulting Firm: Hanson Pro | fessional Services Inc. | | Geolog | ist: Rhonald W. | Hasenyage | r, LPG #196-000 |)246 | | |
| Drilling Method: Hollow stem | n auger | | Drilling | ing Fluid (Type): | | | | | |
| Logged By: Rhonald W. Has | enyager | | Date St | arted: 9/16/20 | 009 Dat | e Finished: 9/ | 16/2009 | | |
| Report Form Completed By: Su | ızanna L. Simpson | | Date: | 10/7/2009 | | | | | |
| ANNULAR SPA | CE DETAILS | | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) |) | | |
| | | | | 624.32 | -2.65 | Top of Protective | e Casing | | |
| | | T | | 624.04 | | Top of Riser Pipe | _ | | |
| Type of Surface Seal: <u>Concrete</u> | | | | 621.67 | 0.00 | Ground Surface | | | |
| Type of Annular Sealant: High- | solids bentonite | | | 618.67 | 3.00 | Top of Annular S | Sealant | | |
| Installation Method:Tremi | | | | | | | | | |
| Setting Time:>24 hr. | | _ \[\breez | <u>z</u> | 608.55 | 13.12 | Static Water Lev (After Completion) | | | |
| Type of Bentonite Seal Gran | ular Pellet Slurry | | | | | (riner completion) | <i>3</i> ,21,200 | | |
| Installation Method: <u>Gravit</u> | (choose one) | _ | ×× | 611.93 | 9.74 | Top of Seal | | | |
| Setting Time: 15 min | | _ | | 610.15 | _11.52_ | Top of Sand Pac | k | | |
| Type of Sand Pack: Quartz sand | 1 | | | | | | | | |
| | eve size) | _ | | 608.77 | _12.90_ | Top of Screen | | | |
| Installation Method: <u>Gravit</u> | У | _ | | 604.00 | 15.65 | - | | | |
| Type of Backfill Material:n/a | (if applicable) | _ | | 604.00 603.61 | 17.67 18.06 | Bottom of Screen Bottom of Well | 1 | | |
| Installation Method:n/a | (ii applicable) | | | 603.61 | 18.06 | Bottom of Boreh | ole | | |
| | | | | * Referenced to a | National Geodet | ic Datum | | | |
| | | | | CAS | SING MEA | SUREMENTS | | | |
| WELL CONS | STRUCTION MATERIAL | LS | | Diameter of Boreh | ole | (inches) | 8.0 | | |
| | ne type of material for each area) | • | | ID of Riser Pipe | . 41 | (inches) | 2.0 | | |
| | | | | Protective Casing I | Length | (feet) | 5.0 | | |
| Protective Casing | SS304 SS316 PTFE | PVC OTHER: (| Steel | Riser Pipe Length Bottom of Screen t | o End Can | (feet) | 0.39 | | |
| Riser Pipe Above W.T. | SS304 SS316 PTFE | PVC OTHER: | | Screen Length (1 | - | | 4.77 | | |
| Riser Pipe Below W.T. | SS304 SS316 PTFE | PVC OTHER: | | Total Length of Ca | | (feet) | 20.43 | | |

SS304

Well Completion Form (revised 02/06/02)

SS316

PTFE PVC OTHER:

**Hand-Slotted Well Screens Are Unacceptable

Screen Slot Size **

0.010

| Illinois Environ | mental Protection Agency | y | | Well | Completion | Report |
|---|---|--------------|-------------------------------------|------------------------|---|---------------|
| Site #: | County: M | ontgomery | | W | /ell #: <u>G2</u> | 275 |
| Site Name: AEG Coffeen Pow | ver Station CCB Management Facilit | V | | Ве | orehole #: | G275 |
| State- Plant | .9 Y 874,298.9 (or) Latitude | - | | | | |
| Surveyed By: <u>Jeffrey D. Emric</u> | k | _ IL Registr | ration #:035-0 | 03507 | | |
| Drilling Contractor: <u>Layne-Wes</u> | stern Co | _ Driller: _ | G. Mills | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | _ Geologist: | Rhonald W. | Hasenyager | r, LPG #196-000 |)246 |
| Drilling Method: Hollow stem | _ Drilling F | luid (Type): | | | | |
| Logged By: Rhonald W. Hase: | nyager | _ Date Start | ed: 9/16/20 | 09 Date | e Finished: 9/2 | 16/2009 |
| Report Form Completed By: Suz | zanna L. Simpson | Date: | 10/7/2009 | | | |
| ANNULAR SPAC | CE DETAILS | | Elevations | | (0.01 ft.) |) |
| | | | (MSL)* | (BGS) | | |
| | T | | 618.53 | 2.39 | Top of Protective | Casing |
| | l f. | | 618.26 | 2.12 | Top of Riser Pipe | e |
| Type of Surface Seal: Concrete | | | 616.14 | 0.00 | Ground Surface | |
| | | | _613.14_ | 3.00 | Top of Annular S | Sealant |
| Type of Annular Sealant: High-se | 71 | | | | | |
| Installation Method: Tremie | | | (05.90 | 10.25 | Cont. What I | 1 |
| Setting Time: >24 hr. | | Ž | _605.89_ | 10.25 | Static Water Leve (After Completion) | |
| Type of Bentonite Seal Granu | | | | | | |
| Installation Method: Gravity | (choose one) | | _610.42_ | 5.72 | Top of Seal | |
| Setting Time: 15 min | | | 600 16 | 6.98 | Ton of Cond Dool | - |
| | | | 609.16 | 0.98 | Top of Sand Pack | |
| Type of Sand Pack: Quartz sand | | | 607.92 | 8.22 | Top of Screen | |
| Grain Size:10/20 (siev | ve size) | | _007.92_ | 0.22 | Top of Screen | |
| Installation Method: <u>Gravity</u> | | | 603.52 | 12.62 | Bottom of Screen | |
| Type of Backfill Material:n/a | | == | 602.95 | 13.19 | Bottom of Well | L |
| T (U.C. M.A. I.) | (if applicable) | | (02.05 | 12.10 | D # CD 1 | |
| Installation Method:n/a | | | 602.95 * Referenced to a | 13.19 National Geodeti | | ole |
| | | | CAS | SING MEAS | SUREMENTS | |
| | | D | Diameter of Boreho | | (inches) | 8.0 |
| | FRUCTION MATERIALS etype of material for each area) | П | O of Riser Pipe | | (inches) | 2.0 |
| | | P | rotective Casing I | ength | (feet) | 5.0 |
| | 99994 | | iser Pipe Length | | (feet) | 10.34 |
| Protective Casing Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER SS304 SS316 PTFE PVC OTHER | | ottom of Screen to | - | | 0.52 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | | creen Length (1storal Length of Cas | | t) (feet) | 4.45 15.31 |

SS304

Screen

Well Completion Form (revised 02/06/02)

SS316

PTFE

PVC OTHER:

**Hand-Slotted Well Screens Are Unacceptable

Screen Slot Size **

0.010

| Site #: County: Montgomery Site Name: CCB Management Facility | ongitude:8923!33.400\text{\tiny{\text{\tiny{\text{\texi{\text{\text{\text{\text{\text{\text{\text{\text{\text{\text{\tiny{\tiny{\text{\text{\text{\text{\text{\text{\text{\text{\text{\tiny{\text{\tiny{\text{\tex{\tex |
|---|---|
| | ongitude:8923!33.400Å |
| | |
| State Plane Coordinate: X 2,516,358.8 Y 874,438.6 (or) Latitude: 39 3! 55.900Ä Lo | 7 |
| Surveyed By:Jeffrey D. Emrick | 1 |
| Drilling Contractor: Layne-Western Co Driller: G. Mills | |
| Consulting Firm: Hanson Professional Services Inc. Geologist: Rhonald W. Hase | nyager, LPG #196-000246 |
| Drilling Method: Hollow stem auger Drilling Fluid (Type): | |
| | Date Finished: 9/16/2009 |
| Report Form Completed By: Suzanna Simpson Date: 10/7/2009 | |
| | pths (0.01 ft.) |
| | GS) (0.01 it.) |
| | .26 Top of Protective Casing |
| | 2.86 Top of Riser Pipe |
| Type of Surface Seal: Concrete 629.14 0 | .00 Ground Surface |
| 626.14 3 | .00 Top of Annular Sealant |
| Type of Annular Sealant: High-solids bentonite | |
| Installation Method: Tremie | |
| Setting Time: $ > 24 \text{ hr.} $ $ $ | Static Water Level (After Completion) 9/21/2009 |
| Type of Bentonite Seal Granular Pellet Slurry | |
| Installation Method: Gravity | 9.08 Top of Seal |
| Setting Time: 15 min | |
| 608.11 <u>21</u> | 1.03 Top of Sand Pack |
| Type of Sand Pack: Quartz sand | 0.41 T. CC |
| Grain Size: 10/20 (sieve size) 606.73 22 | Z.41 Top of Screen |
| Installation Method: Gravity 601.92 27 | 7.22 Bottom of Screen |
| Type of Backfill Material: Quartz sand 601.49 27 | 7.65 Bottom of Well |
| (if applicable) Installation Method: Gravity 601.14 28 | 3.00 Bottom of Borehole |
| * Referenced to a Nation | |
| CASING | MEASUREMENTS |
| Diameter of Borehole | (inches) 8.0 |
| WELL CONSTRUCTION MATERIALS (Choose one type of material for each area) ID of Riser Pipe | (inches) 2.0 |
| Protective Casing Length | |
| Protective Casing SS304 SS316 PTFE PVC OTHER: Riser Pipe Length Riser Pipe Length Rottom of Screen to End | (feet) 25.27 |
| D. D. H. W.T. Good Golf Diff. N.C | |
| Riser Pipe Above W.1. SS304 SS316 PIFE PVC OTHER: Screen Length (1st slot to Total Length of Casing | o last slot) (feet) 4.81 (feet) 30.51 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | nmental Protection Agency | | | Well | Completion | Report | |
|--|---|--------------|-----------------------------|------------------------|------------------------------------|-----------|--|
| Site #: | County: Mo | ntgomery | | W | /ell #: <u>G2</u> | 77 | |
| Site Name: AEG Coffeen Pov | wer Station CCB Management Facility | | | Be | orehole #: | 277 | |
| State- Plant Plane Coordinate: X 2,516,370 | 0.5 Y 874,581.8 (or) Latitude: | | | Longitude | e:° | ' | |
| Surveyed By:Jeffrey D. Emri | ck | IL Registra | ation #:035-00 |)3507 | | | |
| Drilling Contractor: <u>Layne-We</u> | estern Co | Driller: | G. Mills | | | | |
| Consulting Firm: Hanson Prof | Sessional Services Inc. | Geologist: | Rhonald W. 1 | Hasenyager | r, LPG #196-0002 | 246 | |
| Drilling Method: Hollow stem | auger | Drilling Flo | rilling Fluid (Type): | | | | |
| Logged By: Rhonald W. Hase | enyager | Date Starte | ed:9/14/200 | 09 Date | e Finished: 9/1 | 4/2009 | |
| Report Form Completed By: Su | zanna L. Simpson | Date: | 10/7/2009 | | | | |
| ANNULAR SPA | - | | Elevations | Depths | (0.01 ft.) | | |
| | C2 2211120 | | (MSL)* | (BGS) | (0.01 10.) | | |
| | | | 623.35 | -2.56 | Top of Protective | Casing | |
| | | = | 623.08 | 2.29 | Top of Riser Pipe | | |
| Type of Surface Seal: Concrete | | | 620.79 | 0.00 | Ground Surface | | |
| Type of Annular Sealant: High-s | solids bentonite | | 617.79 | 3.00 | Top of Annular Se | ealant | |
| Installation Method: Tremie | 7 | | | | | | |
| Setting Time: >24 hr. | | abla | _602.56_ | 18.23 | Static Water Level | | |
| | | | | | (After Completion) | 9/21/2009 | |
| Type of Bentonite Seal Gran | ular Pellet Slurry (choose one) | | | | | | |
| Installation Method: Gravity | —————————————————————————————————————— | | _608.00_ | _12.79_ | Top of Seal | | |
| Setting Time: 18 min | | | 607.00 | 13.79 | Top of Sand Pack | | |
| Type of Sand Pack: Quartz sand | <u> </u> | | | | | | |
| Grain Size:10/20 (sign | eve size) | | _606.50_ | _14.29_ | Top of Screen | | |
| Installation Method: Gravity | y | | 602.02 | 10.77 | - | | |
| Type of Backfill Material: Quar | | | 602.02 601.55 | 18.77 19.24 | Bottom of Screen Bottom of Well | | |
| | (if applicable) | | | | | | |
| Installation Method: <u>Gravity</u> | <i>y</i> | | 600.79 * Referenced to a N | 20.00 National Geodeti | Bottom of Boreho | le | |
| | | | CAS | ING MEAS | SUREMENTS | | |
| | | Di | iameter of Boreho | | (inches) | 8.0 | |
| | TRUCTION MATERIALS ne type of material for each area) | | of Riser Pipe | | (inches) | 2.0 | |
| | | Pr | otective Casing Lo | ength | (feet) | 5.0 | |
| n | GG004 GG016 PTTT | | iser Pipe Length | | (feet) | 16.58 | |
| Protective Casing Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER: SS304 SS316 PTFE (PVC) OTHER: | | ottom of Screen to | - | (feet) | 0.47 | |
| Riser Pipe Below W.T. | SS304 SS316 PTFE (PVC) OTHER: | | ereen Length (1st | | t) (feet) | 21.53 | |

SS304

Screen

Well Completion Form (revised 02/06/02)

SS316

PTFE PVC OTHER:

**Hand-Slotted Well Screens Are Unacceptable

0.010

(inches)

Screen Slot Size **

| Illinois Environ | nmental Protection Agency | 7 | | Well | Completion | Report |
|--|---|---------------------|---------------------------|---------------------------|---|------------|
| Site #: | County: <u>Mo</u> | ntgomery | | W | /ell #: <u>G2</u> | 278 |
| Site Name: AEG Coffeen Pov | wer Station CCB Management Facility | <i>I</i> | | В | orehole #: | G278 |
| State- Plant Plane Coordinate: X 2,516,200 |).7 Y 874,875.4 (or) Latitude: | | | Longitude | e:° | |
| Surveyed By: <u>Jeffrey D. Emri</u> | ck | IL Registra | ation #:035-0 | 03507 | | |
| Drilling Contractor: <u>Layne-We</u> | estern Co | Driller: _ | G. Mills | | | |
| Consulting Firm: Hanson Prof | Geologist: | Rhonald W. | Hasenyager | r, LPG #196-000 |)246 | |
| Drilling Method: Hollow stem | Drilling Fl | uid (Type): | | | | |
| Logged By: Rhonald W. Hase | enyager | Date Starte | ed: 9/11/20 | 09 Date | e Finished: 9/ | 11/2009 |
| Report Form Completed By: Su | zanna L. Simpson | Date: | 10/7/2009 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations | | (0.01 ft.) |) |
| | | | (MSL)* | (BGS) | T (D () | <i>C</i> : |
| | | | _631.49_ | 2.04 | Top of Protective | Casing |
| | | | _631.17_ | 2.32 | Top of Riser Pipe |) |
| Type of Surface Seal: Concrete | | | _628.85_ | 0.00 | Ground Surface | |
| T CA L C L 4 HT L | | | 625.85 | 3.00 | Top of Annular S | Sealant |
| Type of Annular Sealant: High-s | 71 | | | | | |
| Installation Method: Tremie | | | 604.05 | 22.00 | | |
| Setting Time: >24 hr. | | $\overline{\Delta}$ | _604.87_ | 23.98 | Static Water Leve (After Completion) | |
| Type of Bentonite Seal Gran | | | | | | |
| Installation Method: Gravity | (choose one) | | 613.74 | 15 11 | Ton of Seal | |
| Setting Time: 22 min | | | | | Top of Scar | |
| Setting Time. 22 min | <u> </u> | X | 611.90 | 16.95 | Top of Sand Pack | ζ |
| Type of Sand Pack: Quartz sand | <u> </u> | | | | | |
| Grain Size:10/20 (sign | eve size) | ≣ │ | 609.92 | 18.93 | Top of Screen | |
| Installation Method: Gravity | | | | | | |
| Type of Backfill Material: n/a | | | 605.15 604.79 | 23.70 24.06 | Bottom of Screen Bottom of Well | ı |
| 1)pe of Buomm 11 | (if applicable) | | | | Bowell of Well | |
| Installation Method: <u>n/a</u> | | | 604.79 * Referenced to a | 24.06 National Geodeti | Bottom of Boreho | ole |
| | | | CAS | | | |
| | | n | riameter of Boreho | | SUREMENTS (inches) | 8.0 |
| | TRUCTION MATERIALS ue type of material for each area) | | O of Riser Pipe | - | (inches) | 2.0 |
| (2.13000 0.1 | • | | rotective Casing L | ength | (feet) | 5.0 |
| | I | | iser Pipe Length | | (feet) | 21.25 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER: | Steel | ottom of Screen to | o End Cap | (feet) | 0.36 |
| Riser Pipe Above W.T. Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER: SS304 SS316 PTFE PVC OTHER: | | creen Length (1s | | | 4.77 |
| Mod Tipe Delow W.1. | DOSOT DOSTO TITE (FVC) OTHER. | 1 T | otal Length of Cas | sing | (feet) | 26.38 |

SS304

Screen

Well Completion Form (revised 02/06/02)

SS316

PTFE

PVC OTHER:

**Hand-Slotted Well Screens Are Unacceptable

Screen Slot Size **

0.010

| Illinois Enviror | ey | | Well Completion Report | | | |
|--------------------------------------|------------------------------------|---|---------------------------|------------------------------|------------------------------------|-----------------|
| Site #: | County: | Montgomery | | W | ell #:G2 | 279 |
| Site Name:CCB Managemen | t Facility | | | Во | orehole#: | G279 |
| State Plane Coordinate: X 2,516,245 | 5.6 Y 875,028.1 (or) Latit | ude:39 | 4! <u>1.800Ä</u> | Longitude | : <u>-89</u> <u>23</u> | <u>34.800</u> Ä |
| Surveyed By:Jeffrey D. Emrio | ck | IL Regis | tration #: <u>035-00</u> | 03507 | | |
| Drilling Contractor: <u>Layne-We</u> | estern Co | Driller: | G. Mills | | | |
| Consulting Firm: <u>Hanson Prof</u> | essional Services Inc. | Geologis | st: <u>Rhonald W.</u> | Hasenyager, | LPG #196-000 | 246 |
| Drilling Method: Hollow stem | auger | Drilling | Fluid (Type): | | | |
| Logged By: Rhonald W. Hase | nyager | Date Sta | rted: 9/10/200 | 09 Date | Finished: 9/1 | 10/2009 |
| Report Form Completed By: Su | ızanna Simpson | Date: | 10/7/2009 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | _ | | 632.33 | | Top of Protective | Casing |
| | _ | | 632.04 | 2.85 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 629.19 | 0.00 | Ground Surface | |
| Towns of Assessing Contacts. It's | | | 626.19 | 3.00 | Top of Annular S | ealant |
| Type of Annular Sealant: High- | | | | | | |
| | e | $\left \begin{array}{c} \overline{\Delta} \end{array}\right $ | 601.66 | 27.53 | Static Water Leve | el |
| | | | | | (After Completion) | |
| Type of Bentonite Seal Gran | ular Pellet Slurry (choose one) | | | | | |
| Installation Method: Gravit | у | \forall | _610.45_ | 18.74 | Top of Seal | |
| Setting Time: 18 min | | | 608.77 | 20.42 | Top of Sand Pack | ζ. |
| Type of Sand Pack: Quartz sand | 4 | | | | | |
| Grain Size: 10/20 (signature) | | | 606.79 | _22.40_ | Top of Screen | |
| Installation Method: Gravit | y | | | | | |
| Type of Backfill Material: Quar | tz Sand | | 602.40 604.51 | <u>26.79</u> <u>24.68</u> | Bottom of Screen Bottom of Well | |
| Type of Backini Material. Qual | (if applicable) | | _004.51_ | 27.3 | Bottom of Wen | |
| Installation Method: <u>Gravit</u> | у | | 601.19 * Referenced to a | | Bottom of Boreho | ole |
| | | | CAS | | I IDENTENTO | |
| | | Г | Diameter of Boreho | | UREMENTS (inches) | 8.0 |
| | STRUCTION MATERIALS | | ID of Riser Pipe | ic | (inches) | 2.0 |
| (Choose on | te type of material for each area) | | Protective Casing L | ength | (feet) | 5.0 |
| | | | Riser Pipe Length | | (feet) | 25.25 |
| Protective Casing | SS304 SS316 PTFE PVC OTF | | Bottom of Screen to | End Cap | (feet) | 0.53 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTF | HER: | Screen Length (1s | t slot to last slot |) (feet) | 4.39 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTF | HER: | Total Length of Cas | sing | (feet) | 30.17 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

| Illinois Environ | Illinois Environmental Protection Agency | | | | Well Completion Report | | | |
|---|--|---------------------|---------------------|-----------|---|------------|--|--|
| Site #: | County: M | ontgomery | | W | /ell #:G2 | 280 | | |
| Site Name: CCB Managemen | | | | В | orehole #: | G280 | | |
| State Plane Coordinate: X 2,515,67 | 9.5 Y 875,045.1 (or) Latitud | e:39 | 4! 2.000Ä | Longitude | e: <u>-89</u> <u>23</u> | s! 42.000Ä | | |
| Surveyed By:Jeffrey D. Emri | ck | IL Registr | ration #:035-0 | 03507 | | | | |
| - | ervice Corp. | | B. Williamson | | | | | |
| _ | Pessional Services Inc. | | | | , LPG #196-000 | | | |
| Drilling Method: Hollow stem auger Drilling | | | g Fluid (Type): | | | | | |
| Logged By: Suzanna Simpson | - | _ | | | e Finished: 2/2 | | | |
| | ızanna Simpson | _ | 2/29/2008 | | | | | |
| ANNULAR SPA | | | Elevations | Depths | (0.01 ft.) | | | |
| HUULINGIA | CE DETAILS | | (MSL)* | (BGS) | (0.01 1) | | | |
| | <u></u> | | 625.79 | 2.84 | Top of Protective | Casing | | |
| | | | 625.30 | 2.35 | Top of Riser Pipe | ; | | |
| Type of Surface Seal: Concrete | | | 622.95 | 0.00 | Ground Surface | | | |
| | | | 620.85 | 2.10 | Top of Annular S | ealant | | |
| Type of Annular Sealant: Bento | 7 | | | | 1 | | | |
| Installation Method: <u>Gravi</u> | | | 610.61 | 4.2.4 | | | | |
| Setting Time: >24 hr. | | $\overline{\Delta}$ | 618.61 | 4.34 | Static Water Leve (After Completion) | | | |
| Type of Bentonite Seal Gran | | | | | | | | |
| Installation Method: Graving | (choose one) | | _620.85_ | 2.10 | Top of Seal | | | |
| Setting Time: >24 hr. | | | 611.75 | 11.20 | Top of Sand Pack | - | | |
| | | | _011./3_ | 11.20 | Top of Sand Faci | | | |
| Type of Sand Pack: Quartz san | | | 610.16 | 12.79 | Top of Screen | | | |
| Grain Size: 10/20 (si | , , , , , , , , , , , , , , , , , , , | | 010.10 | | rop or sereen | | | |
| Installation Method: <u>Gravi</u> | y | | 605.32 | 17.63 | Bottom of Screen | | | |
| Type of Backfill Material:n/a | (if applicable) | | 604.97 | 17.98 | Bottom of Well | | | |
| Installation Method: n/a | (ii applicatic) | | 604.97 | 17.98 | Bottom of Boreho | ole | | |
| 110th | | | * Referenced to a | | | | | |
| | | | CAS | SING MEAS | SUREMENTS | | | |
| | | Г | Diameter of Boreho | | (inches) | 8.0 | | |
| | STRUCTION MATERIALS ne type of material for each area) | П | D of Riser Pipe | | (inches) | 2.0 | | |
| | | P | rotective Casing L | ength | (feet) | 5.0 | | |
| B + 4: G : | GG204 GG214 PG777 | | iser Pipe Length | | (feet) | 15.14 | | |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | | Sottom of Screen to | | (feet) | 0.35 | | |
| Riser Pipe Above W.T. Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER SS304 SS316 PTFE PVC OTHER | | creen Length (1s | | | 4.84 | | |
| MISELT IPE DEIOW W.I. | SS304 SS316 PTFE (PVC) OTHER | | otal Length of Ca | sıng | (feet) | 20.33 | | |

PTFE PVC OTHER:

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

SS304

Well Completion Form (revised 02/06/02)

SS316

| Illinois Environ | nmental Protection Agency | | | Well | Completion | n Report |
|--|--|--------------|--|-----------------|--|---------------|
| Site #: | County: M | ontgomery | | W | Vell #:G | 281 |
| Site Name: Natural Resource | Technology, Inc. Coffeen Energy Cer | nter | | В | orehole #: | G281 |
| State Plane Coordinate: X 874,375 | 5.4 Y 2,514,455.5 (or) Latitud | e: | | Longitud | e: | |
| Surveyed By: Gary C. Rogers | | _ IL Regist | ration #: <u>035-0</u> | 02957 | | |
| Drilling Contractor: Ramsey G | eotechnical Engineering, LLC | _ Driller: _ | D. Crump | | | |
| Consulting Firm: Hanson Professional Services Inc. Geo | | | : Rhonald W. | Hasenyager | -, LPG #196-000 | 246 |
| Drilling Method: Hollow stem auger Drilli | | | Fluid (Type):no | ne | | |
| Logged By: Kristen L. Theesf | èld | _ Date Star | ted: 9/8/20 | 15 Date | e Finished: 9 | /8/2015 |
| Report Form Completed By:Su | ızanna L. Keim | _ Date: | 10/6/2015 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) |) |
| | | | 626.64 | 2.82 | Top of Protective | Casing |
| | | | 626.36 | -2.54 | Top of Riser Pipe | e |
| Type of Surface Seal: Concrete | | | 623.82 | 0.00 | Ground Surface | |
| | | | 622.82 | 1.00 | Top of Annular S | Sealant |
| Type of Annular Sealant: High- | 7 | | | | · · · · · · | |
| Installation Method:Tremi | e | | | | | |
| Setting Time: >24 hours | | ∇ | | | Static Water Lev (After Completion) | el |
| Type of Bentonite Seal Gran | | | | | | |
| Installation Method: Gravit | (choose one) | | 612.59 | _11.23_ | Top of Seal | |
| Setting Time: 25 minutes | | | 610.37 | 13.45 | Top of Sand Pac | k |
| T. 40 ID I | | | | | 1 | |
| Type of Sand Pack: Quartz San | | | 608.31 | 15.51 | Top of Screen | |
| Grain Size: 10-20 (sign | | | | | 1 | |
| Installation Method: <u>Gravit</u> | <u>y</u> | | 603.66 | 20.16 | Bottom of Screen | 1 |
| Type of Backfill Material:n/a_ | (if applicable) | | 603.53 | 20.29 | Bottom of Well | |
| Installation Method: | | | 603.53 | 20.29 | Bottom of Boreh | ole |
| | | | * Referenced to a | National Geodet | ic Datum | |
| | | | CAS | SING MEAS | SUREMENTS | |
| WELL COM | CTDLICTION MATERIAL C | Ι | Diameter of Boreho | ole | (inches) | 8.0 |
| | STRUCTION MATERIALS e type of material for each area) | | D of Riser Pipe | | (inches) | 2.0 |
| | | | Protective Casing I | ength | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | | Riser Pipe Length | o End C | (feet) | 17.80 0.38 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | . 1 | Bottom of Screen to Screen Length (1s | • | | 4.65 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | | Total Length of Ca | | (feet) | 22.83 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

| Illinois Enviror | nmental Protection Agency | | | Well | Completion | n Report |
|--|-------------------------------------|--------------|--|-----------------|--|----------|
| Site #: | County: _ Mo | ontgomery | | W | /ell #:G | 301 |
| Site Name: Natural Resource | Technology, Inc. Coffeen Energy Cen | ter | | В | orehole #: | G301 |
| State Plane Coordinate: X 872,23 | 4.8 Y 2,515,583.0 (or) Latitude | e: | | Longitud | e: | |
| Surveyed By: Gary C. Rogers | | IL Registr | ration #: <u>035-0</u> | 02957 | | |
| Drilling Contractor: Ramsey G | eotechnical Engineering, LLC | _ Driller: _ | D. Crump | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | Geologist | : Rhonald W. | Hasenyager | r, LPG #196-000 | 246 |
| Drilling Method: Hollow stem | auger | _ Drilling F | luid (Type): <u>no</u> | ne | | |
| Logged By: Kristen L. Theest | îeld | _ Date Star | ted: 9/4/201 | 15 Date | e Finished: 9 | /4/2015 |
| Report Form Completed By: Su | ızanna L. Keim | Date: | 10/6/2015 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) |) |
| | | | 622.98 | 2.71 | Top of Protective | e Casing |
| | l E | | 622.65 | 2.38 | Top of Riser Pipe | e |
| Type of Surface Seal: Concrete | | | 620.27 | 0.00 | Ground Surface | |
| Type of Annular Sealant: Bento | nite Chips | | 618.20 | 2.07 | Top of Annular S | Sealant |
| Installation Method: <u>Gravit</u> | <u>y</u> | | | | | |
| Setting Time: _ >24 hours | | ∇ | | | Static Water Lev (After Completion) | el |
| Type of Bentonite Seal Gran | Pellet Slurry (choose one) | | | | | |
| Installation Method: <u>Gravit</u> | y | | n/a | n/a | Top of Seal | |
| Setting Time: 25 minutes | | | 612.75 | 7.52 | Top of Sand Pac | k |
| Type of Sand Pack: Quartz San | d | | | | | |
| Grain Size:10-20 (signal of the content | eve size) | | _608.96_ | 11.31 | Top of Screen | |
| Installation Method: Gravit | y | | 604.31 | 15.96 | Bottom of Screen | 1 |
| Type of Backfill Material:n/a | (if applicable) | == | 604.06 | 16.21 | Bottom of Well | I |
| Installation Method: | (ii applicative) | | 604.06 | 16.21 | Bottom of Boreh | ole |
| | | | * Referenced to a | National Geodet | ic Datum | |
| | | | CAS | SING MEAS | SUREMENTS | |
| WELL CONS | STRUCTION MATERIALS | | Diameter of Boreho | ole | (inches) | 8.0 |
| | ne type of material for each area) | | D of Riser Pipe | | (inches) | 2.0 |
| | | | Protective Casing L | ength | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER: | a. 1 | Riser Pipe Length Bottom of Screen to | o End Can | (feet) | 0.38 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER: | | Screen Length (1s | - | | 4.65 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | | Total Length of Ca | | (feet) | 18.59 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

| Illinois Environ | mental Protection Agency | 7 | | Well | Completion | n Report |
|------------------------------------|---|-------------------------|--|------------------------------|--|----------|
| Site #: | | W | /ell #:G | 302 | | |
| Site Name: Natural Resource | Technology, Inc. Coffeen Energy Ce. | nter | | В | orehole #: | G302 |
| State Plane Coordinate: X 872,253 | 3.0 Y 2,516,214.2 (or) Latitud | le: | | Longitud | e: | |
| Surveyed By: Gary C. Rogers | | IL Regis | stration #: <u>035-0</u> | 02957 | | |
| Drilling Contractor: Ramsey G | eotechnical Engineering, LLC | _ Driller: | D. Crump | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | _ Geologis | st: Rhonald W. | Hasenyager | r, LPG #196-000 |)246 |
| Drilling Method: Hollow stem | auger | _ Drilling | Fluid (Type): <u>no</u> | one | | |
| Logged By: Kristen L. Theesf | eld | _ Date Sta | arted: 9/3/20 | 15 Date | e Finished:9 | /4/2015 |
| Report Form Completed By:Su | zanna L. Keim | _ Date: _ | 10/7/2015 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft. |) |
| | | | 620.34 | 2.39 | Top of Protectiv | e Casing |
| | | | 620.04 | -2.09 | Top of Riser Pip | e |
| Type of Surface Seal: Concrete | | | 617.95 | 0.00 | Ground Surface | |
| Type of Annular Sealant: High-s | solids bentonite | | 615.95 | 2.00 | Top of Annular | Sealant |
| Installation Method:Tremic | e | | | | | |
| Setting Time: >24 hours | | $ \overline{\Delta} $ | | | Static Water Lev (After Completion) | |
| Type of Bentonite Seal Gran | ular Pellet Slurry (choose one) | | | | | |
| Installation Method: <u>Gravit</u> | ` ′ | | 607.78 | 10.17 | Top of Seal | |
| Setting Time: 25 minutes | | | 605.88 | _12.07_ | Top of Sand Pac | :k |
| Type of Sand Pack: Quartz San | d | | | | | |
| Grain Size: 10-20 (sie | eve size) | | 604.74 | 13.21 | Top of Screen | |
| Installation Method: <u>Gravit</u> | y | | 600.00 | 17.06 | D 66 | |
| Type of Backfill Material:n/a | | | <u>600.09</u> <u>599.56</u> | <u>17.86</u> <u>18.39</u> | Bottom of Scree Bottom of Well | n |
| Installation Method: | (if applicable) | | 599.56 | 18.39 | Bottom of Borel | iole |
| | | | * Referenced to a | | | |
| | | | CAS | SING MEAS | SUREMENTS | |
| WELL COM | | | Diameter of Boreho | ole | (inches) | 8.0 |
| | STRUCTION MATERIALS e type of material for each area) | | ID of Riser Pipe | | (inches) | |
| | | | Protective Casing I | | (feet) | |
| Protective Casing | SS304 SS316 PTFE PVC OTHE | | Riser Pipe Length Pottom of Screen t | | (feet) | |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHE | | Bottom of Screen to Screen Length (1s | | | 4.65 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHE | | Total Length of Ca | | (feet) | 20.40 |

PTFE PVC OTHER:

Screen Slot Size **

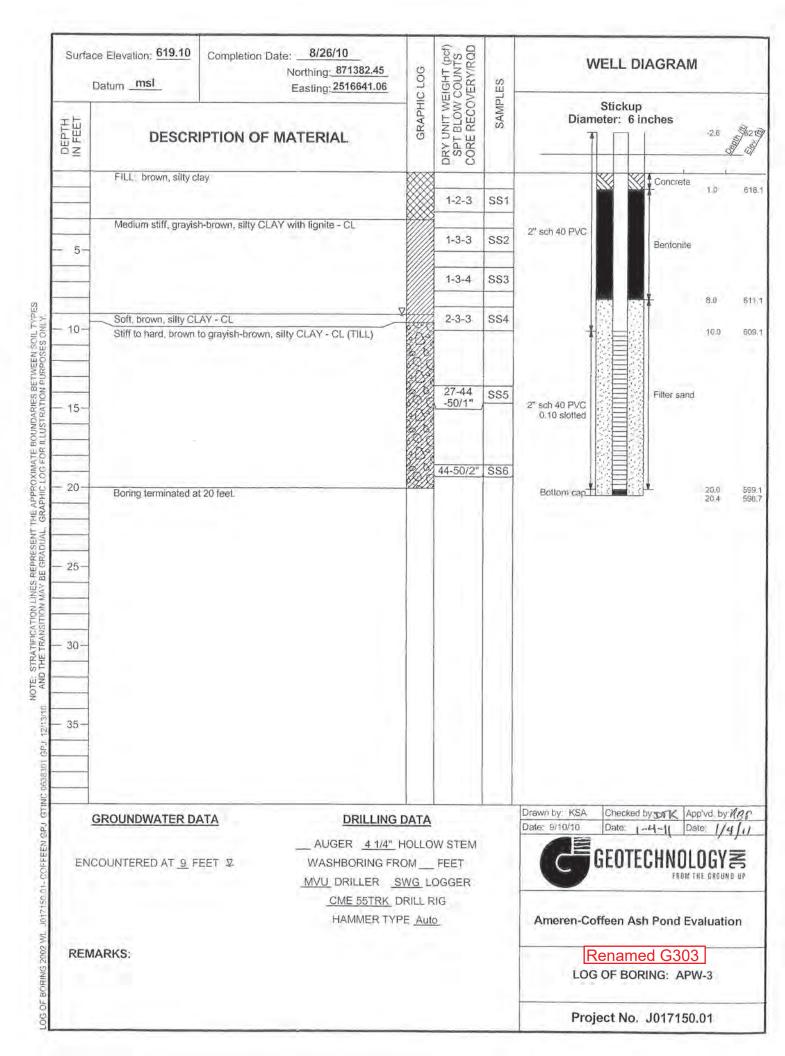
**Hand-Slotted Well Screens Are Unacceptable

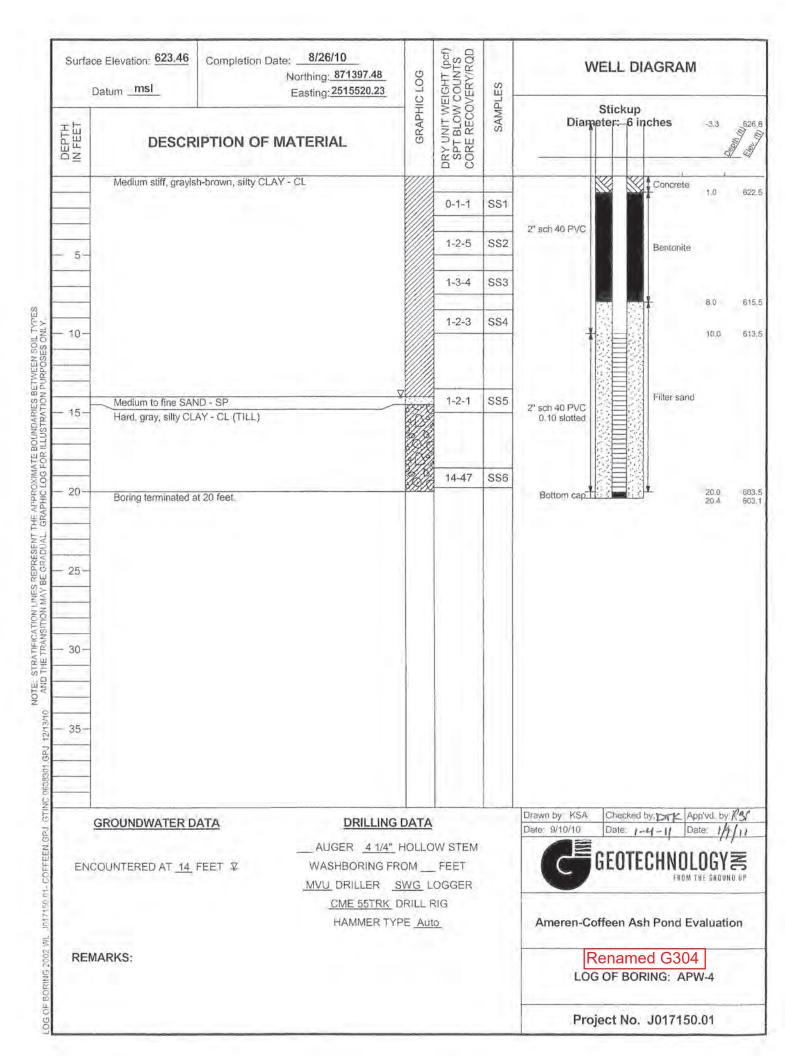
0.010

SS304

Well Completion Form (revised 02/06/02)

SS316





ILLINOIS DEPARTMENT OF PUBLIC HEALTH DIVISION OF ENVIRONMENTAL HEALTH 525 W. JEFFERSON ST. SPRINGFIELD, IL 62761

WATER WELL SEALING FORM

TYPE OR PRESS FIRMLY

RETURN ALL COPIES TO IDPH OR LOCAL HEALTH DEPARTMENT

This form shall be submitted to this Department or the local health department not more than 30 days after a water well, boring or monitoring well is sealed. Such wells are to be sealed not more than 30 days after they are abandoned in accordance with the sealing requirements in the Water Well Construction Code. THE LOCAL HEALTH DEPARTMENT OR REGIONAL PUBLIC HEALTH DEPARTMENT MUST BE NOTIFIED AT LEAST 48 HOURS PRIOR TO SEALING.

| Ownership (Name of Controlling Party) AEG (| Coffeen Power Stat | ion | | (G104) |
|---|--------------------|-----------------|---------------|------------|
| Well Location 134 CIPS Trail | | Coffeen | | Montgomery |
| Address - Lot Number | | Ci | ity | County |
| General Description Township 7 (N) | (%) Range_ | 3 (K) (V | W) | Section |
| SEQuarter of theNE | _Quarter of the | NE | Quarter | |
| Year Drilled 2010 | | | | |
| Drilling Permit Number (and date, if known) n/a | | | | |
| Type of Well Bored Drilled_ ✓ | _ Other | | | |
| Total Depth 20.0 ft. Dian | neter (inches) | 2 | | _ |
| Formation clear of obstructionYes | | | | |
| DETAILS OF PLUGGING | | | | |
| Filled with Bentonite grout (cement or other materials) | from | 0.5 to | 20.0 | _ft. |
| | | | | e. |
| Kind of plug Random soil | from | to_ | 0.5 | _ft. |
| Filled with | from | to | | _ft. |
| Kind of plug | from | to_ | | _ft. |
| Filled with | from | to | | _ft. |
| Kind of plug | from | to_ | | _ft. |
| CASING RECORD Upper 2 feet of casing remov | red <u>√</u> Ye | es | No | |
| Date well was sealed Month October D |)ay8 | Year 201 | 0• | |
| Licensed water well driller or other person approv | ed by the Depart | ment perform | ing well seal | ling. |
| Rhonald W. Hasenyager, L.P.G. | 196-000 | 246 | | |
| Name | Complete | License Num | ber | |
| Hanson Professional Services Inc., 1525 S. 6th St. | Springfi | eld | | IL 62703 |
| Address | — City | | S | State/ZIP |

This state agency is requesting disclosure of information that is necessary to accomplish the statutory purpose as outlined under Public Act 85-0863. Disclosure of this information is mandatory. This form has been approved by the Forms Management Center.

IL 482-0631

| Illinois Environ | mental Protection Agency | , | | Well | Completio | n Report |
|-----------------------------------|--|--|--|-----------------|--------------------------------------|----------|
| Site #: | County: <u>M</u> | lontgomery | | W | /ell #: | G305 |
| Site Name: Coffeen Power Sta | ation | | | В | orehole #: | G305 |
| State Plane Coordinate: X 871,156 | 5.3 Y <u>2,515,199.4</u> (or) Latitud | le: | | Longitud | e: | |
| Surveyed By: Gary C. Rogers | | _ IL Regist | tration #: <u>035-0</u> | 02957 | | |
| Drilling Contractor: Ramsey G | eotechnical Engineering LLC | _ Driller: _ | B. Williamson | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | _ Geologis | t: Rhonald W. | Hasenyager | <u>, LPG #196-00</u> | 0246 |
| Drilling Method: Hollow stem | auger | _ Drilling l | Fluid (Type): <u>no</u> | ne | | |
| Logged By: Suzanna L. Keim | | _ Date Star | rted:5/3/201 | 16 Date | e Finished: | 5/3/2016 |
| Report Form Completed By: Su | zanna L. Keim | _ Date: | 5/19/2016 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft | .) |
| | _ | | 625.88 | 3.34 | Top of Protectiv | e Casing |
| | | | 625.55 | 3.01 | Top of Riser Pi | pe |
| Type of Surface Seal: Concrete | | | 622.54 | 0.00 | Ground Surface | ; |
| Type of Annular Sealant: Benton | nite Chips | | 621.54 | 1.00 | Top of Annular | Sealant |
| Installation Method: Gravit | γ | | | | | |
| Setting Time: _ >12 hours | | $ \nabla $ | | | Static Water Le (After Completion | |
| Type of Bentonite Seal Grant | ular Pellet Slurry (choose one) | | | | | |
| Installation Method:n/a | | | n/a | n/a | Top of Seal | |
| Setting Time: <u>n/a</u> | | | 611.04 | _11.50_ | Top of Sand Pa | ck |
| Type of Sand Pack: Quartz Sand | d | | | | | |
| Grain Size: 10-40 (sie | ve size) | | 609.10 | _13.44_ | Top of Screen | |
| Installation Method: Gravity | у | | | | | |
| Type of Backfill Material:n/a | | | 604.27 604.09 | 18.27 18.45 | Bottom of Scree Bottom of Well | |
| Installation Method: | (if applicable) | | 604.09 | 18.45 | Bottom of Bore | hole |
| instantation (vicinot. | | | * Referenced to a | | | |
| | | | CAS | SING MEAS | SUREMENTS | |
| WELL CONO | |] | Diameter of Boreho | ole | (inches | 8.0 |
| | TRUCTION MATERIALS e type of material for each area) | | ID of Riser Pipe | | (inches | 1 |
| | | | Protective Casing L | | (feet | |
| Protective Casing | SS304 SS316 PTFE PVC OTHE | | Riser Pipe Length | | (feet | |
| Riser Pipe Above W.T. | SS304 SS316 PTFE (PVC) OTHE | | Bottom of Screen to Screen Length (1s | | | 4.02 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | —————————————————————————————————————— | Total Length of Cas | | t) (feet | |

PTFE PVC OTHER:

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

SS304

Well Completion Form (revised 02/06/02)

SS316

| Illinois Environ | mental Protection Agency | | | Well | Completio | n Report |
|---------------------------------------|-----------------------------------|---------------------------------|-------------------------------------|-----------------------|-------------------|-----------|
| Site #: | County:M | ontgomery | | W | Vell #: | G306 |
| Site Name: Coffeen Power Sta | ation | | | В | orehole #: | G306 |
| State Plane Coordinate: X871,141 | 1.0 Y 2,516,120.4 (or) Latitude | e: | | Longitud | e: | |
| Surveyed By: Gary C. Rogers | | IL Regist | ration #:035-0 | 02957 | | |
| Drilling Contractor: Ramsey G | eotechnical Engineering LLC | _ Driller: _ | B. Williamson | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | _ Geologist | : Rhonald W. | Hasenyager | r, LPG #196-00 | 0246 |
| Drilling Method: Hollow stem | auger | _ Drilling F | fluid (Type): <u>no</u> | ne | | |
| Logged By: Suzanna L. Keim | | _ Date Star | ted: <u>5/3/201</u> | 16 Dat | e Finished: | 5/3/2016 |
| Report Form Completed By:Su | zanna L. Keim | _ Date: | 5/19/2016 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft | .) |
| | | | 626.12 | 3.28 | Top of Protectiv | ve Casing |
| | | | 625.72 | 2.88 | Top of Riser Pip | pe |
| Type of Surface Seal: Concrete | | | 622.84 | 0.00 | Ground Surface | |
| | | | 621.84 | 1.00 | Top of Annular | Sealant |
| Type of Annular Sealant: Benton | 7 | | | | | |
| Installation Method: Gravit | <u>y</u> | | | | Static Water Le | vol |
| Setting Time: _ >12 hours | | $\stackrel{\checkmark}{\Delta}$ | | | (After Completion | |
| Type of Bentonite Seal Gran | ular Pellet Slurry (choose one) | | | | | |
| Installation Method:n/a | | X | n/a | n/a | Top of Seal | |
| Setting Time: <u>n/a</u> | | | 611.24 | 11.60 | Top of Sand Pa | ck |
| Type of Sand Pack: Quartz San | | | | | - | |
| Grain Size: 10-40 (sie | | | 609.77 | _13.07_ | Top of Screen | |
| Installation Method: Gravit | | | | | | |
| | | | 605.16 | 17.68 | | en |
| Type of Backfill Material: <u>n/a</u> | (if applicable) | | 604.98 | 17.86 | Bottom of Well | |
| Installation Method: | | | 604.84 * Referenced to a | 18.00 National Geodet | Bottom of Bore | hole |
| | | | | | | |
| | | Γ. | | | SUREMENTS | |
| | STRUCTION MATERIALS | | Diameter of Boreho D of Riser Pipe | | (inches | 2.0 |
| (Choose on | e type of material for each area) | | Protective Casing L | | (inches | |
| | | | Riser Pipe Length | | (feet | 1 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | a. 1 | Bottom of Screen to | End Cap | (feet | 0.18 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | <u>:</u> | Screen Length (1s | st slot to last slo | ot) (feet | 4.61 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | : 7 | Total Length of Cas | sing | (feet | 20.74 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

| Illinois Enviror | mental Protectio | n Agency | | | Well | Completion | n Report |
|-------------------------------------|-----------------------------------|----------------|----------------|--|------------------------------|-----------------------------------|-------------|
| Site #: | | County: Mon | tgomery | | W | /ell #: | 307 |
| Site Name: Coffeen Power Sta | ation Ash Pond 1 | | | | В | orehole #: | G307 |
| State Plane Coordinate: X 2,515,553 | .3 Y 871,398.6 | (or) Latitude: | | | Longitud | e: | |
| Surveyed By: | | | IL Regis | tration #: | | | |
| Drilling Contractor: Bulldog D | rilling, Inc. | | Driller: | J. Gates | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | | Geologis | t: Rhonald W. | Hasenyage | r, LPG #196-00 | 0246 |
| Drilling Method: Hollow Stem | Auger | | Drilling 1 | Fluid (Type): <u>no</u> | ne | | |
| Logged By: Rhonald W. Hase | nyager | | Date Sta | rted: 7/26/20 | 16 Dat | e Finished:7 | /27/2016 |
| Report Form Completed By: Rh | onald W. Hasenyager | | Date: _ | 7/28/2016 | | | |
| ANNULAR SPA | CE DETAILS | | | Elevations (MSL)* | Depths (BGS) | (0.01 ft |) |
| | | | | 624.72 | -2.64 | Top of Protectiv | e Casing |
| | | | | 624.47 | 2.39 | Top of Riser Pip | oe e |
| Type of Surface Seal: Concrete | | | | 622.08 | 0.00 | Ground Surface | |
| Type of Annular Sealant: Benton | ita China | | | _620.08_ | | Top of Annular | Sealant |
| Installation Method: Gravity | | | | | | | |
| Setting Time: 18 hrs. | | _ \sqrt{z} | z I I | 623.84 | -1.76 | Static Water Lev | /el |
| | | | | | | (After Completion |) 7/27/2016 |
| Type of Bentonite Seal Grant | llar Pellet Slurry (choose one) | | YT. | | | | |
| Installation Method: | | | \overline{X} | n/a | <u>n/a</u> | Top of Seal | |
| Setting Time: | | — X | | 610.10 | 11.98 | Top of Sand Pag | ek |
| Type of Sand Pack: Quartz sand | | _ | | | | | |
| Grain Size: 10/20 (sie | ve size) | | | _609.12_ | _12.96_ | Top of Screen | |
| Installation Method: <u>Gravity</u> | , | $ \parallel$ | | COA 20 | 17.00 | D | |
| Type of Backfill Material:none | | _ E | | 604.28 603.86 | <u>17.80</u> <u>18.22</u> | Bottom of Scree Bottom of Well | n |
| Installation Method: n/a | (if applicable) | | | 603.86 | 18.22 | Bottom of Borel | nole |
| | | | | * Referenced to a | | | |
| | | | | CAS | SING MEA | SUREMENTS | |
| WELL CONG | TRUCTION MATERIA | 10 | | Diameter of Boreho | ole | (inches | 8.0 |
| | e type of material for each area) | ഥാ | Г | ID of Riser Pipe | | (inches | |
| | | | | Protective Casing L | ength | (feet | |
| Protective Casing | SS304 SS316 PTFE | PVC OTHER: S | | Riser Pipe Length | o End C | (feet) | |
| Riser Pipe Above W.T. | | PVC OTHER: | | Bottom of Screen to Screen Length (1s | • | | 4.04 |
| Riser Pipe Below W.T. | | PVC OTHER: | | Total Length of Cas | | t) (feet) (feet) | 20.61 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

 $\hbox{**Hand-Slotted Well Screens Are Unacceptable}\\$

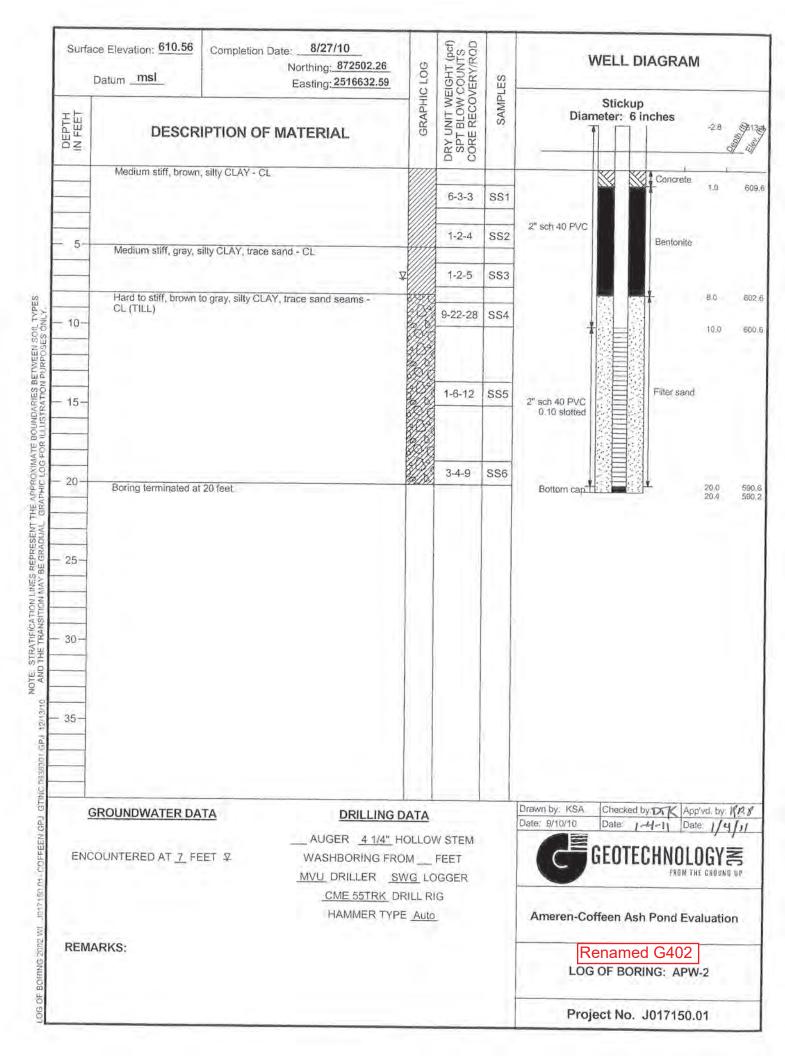
0.010

| Illinois Environ | nmental Protection Agency | y | | Well | Completion | Report |
|-----------------------------------|------------------------------------|---|-------------------------------------|------------------------|------------------------------------|---------|
| Site #: | County: | Montgomery | | W | Vell #:G4 | 101 |
| Site Name: Natural Resource | Technology, Inc. Coffeen Energy Ce | enter | | В | orehole #: | G401 |
| State Plane Coordinate: X 872,510 | 0.6 Y 2,515,614.8 (or) Latitu | de: | | Longitude | e: | |
| Surveyed By: Gary C. Rogers | | IL Regis | tration #: <u>035-0</u> | 02957 | | |
| Drilling Contractor: Ramsey G | eotechnical Engineering, LLC | Driller: | D. Crump | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | Geologis | st: Rhonald W. | Hasenyager | <u>, LPG #196-000</u> | 246 |
| Drilling Method: Hollow stem | auger | Drilling | Fluid (Type):nc | one | | |
| Logged By: Rhonald W. Hase | enyager | Date Sta | rted: 9/14/20 | 015 Date | e Finished:9/ | 14/2015 |
| Report Form Completed By:Su | ızanna L. Keim | Date: _ | 10/7/2015 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | _ | | 625.84 | 2.81 | Top of Protective | Casing |
| | | | 625.57 | 2.54 | Top of Riser Pipe | ; |
| Type of Surface Seal: Concrete | | | 623.03 | 0.00 | Ground Surface | |
| Type of Annular Sealant: Bento | nite Chins | | 621.33 | 1.70 | Top of Annular S | ealant |
| Installation Method: Gravit | 7 | | | | | |
| Setting Time: >24 hours | y | $\left \begin{array}{c} \overline{\Delta} \end{array}\right $ | | | Static Water Leve | el |
| | | | | | (After Completion) | |
| Type of Bentonite Seal Gran | ular Pellet Slurry (choose one) | | | | | |
| Installation Method: Gravit | у | * 🙀 | <u>n/a</u> | n/a | Top of Seal | |
| Setting Time: 25 minutes | | | 610.12 | 12.91 | Top of Sand Pack | ζ |
| Type of Sand Pack: Quartz San | d | | | | | |
| Grain Size:10-20 (sign | eve size) | | 608.67 | _14.36_ | Top of Screen | |
| Installation Method: Gravit | у | | | | | |
| Type of Backfill Material:n/a | | | 604.24 603.74 | <u>18.79</u> 19.29 | Bottom of Screen Bottom of Well | |
| Type of Backini Material | (if applicable) | | 003.74 | 17.27 | Bottom of Wen | |
| Installation Method: | | | 603.73 * Referenced to a | 19.30 National Geodeti | Bottom of Boreho | ole |
| | | | | | | |
| | | Γ | | | SUREMENTS | 0.0 |
| | STRUCTION MATERIALS | | Diameter of Boreho ID of Riser Pipe | | (inches) | 2.0 |
| (Choose on | e type of material for each area) | | Protective Casing I | | (inches) | 5.0 |
| | | | Riser Pipe Length | | (feet) | 16.70 |
| Protective Casing | SS304 SS316 PTFE PVC OTHI | - D C 1 | Bottom of Screen t | o End Cap | (feet) | 0.50 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHI | ER: | Screen Length (1 | st slot to last slo | t) (feet) | 4.63 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHI | ER: | Total Length of Ca | sing | (feet) | 21.83 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable



| Illinois Enviror | nmental Protection A | gency | | | Well | l Completion | Report |
|--|------------------------------------|--------------|----------|--------------------------------------|--------------------------------|--------------------|---------------|
| Site #: | Cou | inty: Mon | tgomery | | W | Vell #: G | 403 |
| Site Name: Natural Resource | Technology, Inc. Coffeen Er | nergy Center | r | | В | orehole #: | G403 |
| State Plane Coordinate: X 873,56 | 1.3 Y 2,514,616.6 (or) | Latitude: | | | Longitud | e: | |
| Surveyed By: Gary C. Rogers IL Re | | | IL Regis | stration #:035 | 5-002957 | | |
| Drilling Contractor: Ramsey G | eotechnical Engineering, LL | <u>.C</u> | Driller: | D. Crump | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | | Geologi | st: Rhonald V | W. Hasenyager | r, LPG #196-000 | 246 |
| Drilling Method: Hollow stem | auger | | Drilling | Fluid (Type): _ | none | | |
| Logged By: Kristen L. Theest | eld eld | | Date Sta | arted: 9/11/ | <u>2015</u> Dat | e Finished:9/ | 11/2015 |
| Report Form Completed By: Su | ızanna L. Keim | | Date: _ | 10/7/2015 | 5 | | |
| ANNULAR SPA | CE DETAILS | | | Elevation (MSL)* | s Depths (BGS) | (0.01 ft.) | |
| | | | | 626.72 | | Top of Protective | Casing |
| | | | | 626.47 | 2.66 | Top of Riser Pipe | e |
| Type of Surface Seal: Concrete | | | | 623.81 | 0.00 | Ground Surface | |
| | · | | | 621.81 | 2.00 | Top of Annular S | Sealant |
| Type of Annular Sealant: Bento | | | | | | | |
| Installation Method: <u>Gravit</u> Setting Time: <u>>24 hours</u> | У | | 7 | | | Static Water Lev | al |
| Setting Time. 24 hours | | | - | | | (After Completion) | O1 |
| Type of Bentonite Seal Gran | ular Pellet Slurry (choose one) | | | | | | |
| Installation Method:n/a | | \boxtimes | | n/a | n/a | Top of Seal | |
| Setting Time:n/a | | | | 612.64 | _11.17_ | Top of Sand Pac | ζ |
| Type of Sand Pack: Quartz San | 1 | | | | | | |
| Grain Size: 10-20 (si | | | | 610.70 | 13.11 | Top of Screen | |
| Installation Method: Gravit | | | | | | | |
| | | | ▋┃ | 606.03 | | | ı |
| Type of Backfill Material:n/a | (if applicable) | | | 605.66 | 18.15 | Bottom of Well | |
| Installation Method: | | | | 605.66 * Referenced | 18.15_ to a National Geodet | Bottom of Boreh | ole |
| | | | | Tielereneed | | ac Butum | |
| | | | [| | | SUREMENTS | |
| | STRUCTION MATERIALS | | | Diameter of Bor | | (inches) | 8.0 2.0 |
| (Choose or | ne type of material for each area) | | | ID of Riser Pipe Protective Casin | | (inches) | 5.0 |
| | | | | Riser Pipe Lengt | | (feet) | 15.77 |
| Protective Casing | SS304 SS316 PTFE PVC | C OTHER: St | teel | Bottom of Scree | | (feet) | 0.37 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC | OTHER: | | Screen Length | | | 4.67 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC | OTHER: | | Total Length of | Casing | (feet) | 20.81 |

PTFE PVC OTHER:

SS304

Well Completion Form (revised 02/06/02)

SS316

Total Length of Casing

**Hand-Slotted Well Screens Are Unacceptable

Screen Slot Size **

| Illinois Environmental Protection Agency | | 1 | Well Completion | n Report |
|--|--------------------|-----------------------------------|---------------------------------------|-------------------|
| Site #: County: _Mc | ontgomery | | Well #: | i404 |
| Site Name: Coffeen Energy Center | | | Forme | rly MW22S SB22 |
| State | | | | |
| Plane Coordinate: X 2,516,397.9 Y 873,999.8 (or) Latitude | | | ngitude: | |
| Surveyed By: Darren E. Forgy | IL Registration # | 035-003637 | 7 | |
| Drilling Contractor: Reynolds Drilling Corp. | Driller: A. Ra | chford | | |
| Consulting Firm: Hanson Professional Services Inc. | Geologist:, LI | PG# | | |
| Drilling Method: Hollow stem auger | Drilling Fluid (Ty | pe): <u>none</u> | | |
| Logged By: Rhonald W. Hasenyager | Date Started: | 5/1/2007 | _ Date Finished:5 | 5/1/2007 |
| Report Form Completed By: Rhonald W. Hasenyager | Date:5/2 | 2/2007 | | |
| ANNULAR SPACE DETAILS | | vations Dep | (|) |
| | ` | , | 92 Top of Protectiv | e Casing |
| | | 15.77 -2. | 67 Top of Riser Pip | e |
| Type of Surface Seal: Concrete | 6 | 13.10 0.0 | 00 Ground Surface | |
| Type of Annular Sealant: Bentonite chips | 6 | 13.10 0.0 | 00 Top of Annular | Sealant |
| Installation Method:gravity | | | | |
| Setting Time:>12 hours | ∑ 62 | 11.03 2.0 | O7 Static Water Lev | |
| Type of Bentonite Seal Granular Pellet Slurry | | | (After Completion) | 3/10/2007 |
| Installation Method: | _ | <u>n/a</u> <u>n/</u> | /a Top of Seal | |
| Setting Time: | | 08.05 5.0 | O5 Top of Sand Pag | ck |
| Type of Sand Pack: Quartz sand | | | | |
| Grain Size: 10/20 (sieve size) | == 60 | 06.68 6.4 | Top of Screen | |
| Installation Method: gravity | | | | |
| Type of Backfill Material: Formation sand | | | Bottom of Scree Bottom of Well | n |
| (if applicable) | | <u> </u> | Bottom of Wen | |
| Installation Method: slough | | 01.10 12. eferenced to a National | .00 Bottom of Borel Geodetic Datum | nole |
| | | CASING | MEASUREMENTS | |
| | Diameter | of Borehole | (inches) | 8.0 |
| WELL CONSTRUCTION MATERIALS (Choose one type of material for each area) | ID of Ris | ser Pipe | (inches) | 2.0 |
| | Protectiv | e Casing Length | (feet) | 5.0 |
| D. J. C | | 0 | (feet) | |
| Protective Casing SS304 SS316 PTFE PVC OTHER: Riser Pipe Above W.T. SS304 SS316 PTFE PVC OTHER: | Dottom | of Screen to End (| | |
| Riser Pipe Above W.1. SS304 SS316 PIFE PVC OTHER: Riser Pipe Below W.T. SS304 SS316 PTFE PVC OTHER: | SCICCII L | ength (1st slot to | last slot) (feet) | 4.4.0 |

SS304

Well Completion Form (revised 02/06/02)

SS316

PTFE PVC OTHER:

Total Length of Casing

**Hand-Slotted Well Screens Are Unacceptable

0.010

Screen Slot Size **

| Illinois Environ | mental Protection Agency | 7 | | Well | Completion | Report |
|--|--|-------------------------|---------------------------|---|---------------------|-----------|
| Site #: | County: N | Montgomery | | W | /ell #:G4 | |
| Site Name: Coffeen Energy Co | enter | | | В | Formerly orehole #: | |
| State Plane Coordinate: X 2,515,335 | 5.7 Y <u>873,996.8</u> (or) Latitud | de: | | Longitud | e: | |
| Surveyed By: Darren E. Forgy | | IL Regis | tration #:035-0 | 03637 | | |
| Drilling Contractor: Reynolds | Drilling Corp. | Driller: | A. Rachford | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | Geologis | st:, LPG# | | | |
| Drilling Method: Hollow stem | auger | Drilling | Fluid (Type): <u>no</u> | ne | | |
| Logged By: Rhonald W. Hase | nyager | Date Sta | rted:5/1/200 |)7 Date | e Finished:5/ | 1/2007 |
| Report Form Completed By: Rh | onald W. Hasenyager | Date: | 5/2/2007 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | 624.04 | -3.14 | Top of Protective | Casing |
| | T | | 623.78 | -2.88 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 620.90 | 0.00 | Ground Surface | |
| Type of Annular Sealant: Benton | nite chips | | 620.90 | 0.00 | Top of Annular S | ealant |
| Installation Method:gravity | , | | | | | |
| Setting Time: >12 hours | | $ \overline{\Delta} $ | 619.67 | 1.23 | Static Water Leve | |
| Type of Bentonite Seal Grant | ılar Pellet Slurry | | | | (After Completion) | 5/10/2007 |
| Installation Method: | (choose one) | | n/a | n/a | Top of Seal | |
| Setting Time: | | | 613.19 | 7.71 | Top of Sand Pack | - |
| | <u> </u> | | 013.17 | | Top of Sand Lack | • |
| Type of Sand Pack: Quartz sand | | | 611.89 | 9.01 | Top of Screen | |
| Grain Size: 10/20 (sie Installation Method: gravity | | | | | • | |
| | | | 607.14 | _13.76 | | |
| Type of Backfill Material: | (if applicable) | | 606.69 | 14.21 | Bottom of Well | |
| Installation Method: | | | 606.69 * Referenced to a | 14.21 National Geodet | Bottom of Boreho | ble |
| | | | CAS | | | |
| | | Γ | Diameter of Boreho | 1 | SUREMENTS (inches) | 8.0 |
| | TRUCTION MATERIALS e type of material for each area) | | ID of Riser Pipe | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | | 2.0 |
| (0.0000 | V1 | | Protective Casing L | | (feet) | 5.0 |
| | | | Riser Pipe Length | | (feet) | 11.89 |
| Protective Casing | | | Bottom of Screen to | End Cap | (feet) | 0.45 |
| Riser Pipe Above W.T. Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHE SS304 SS316 PTFE PVC OTHE | | Screen Length (1s | | | 4.75 |
| Misci Tipe Delow W.1. | OTHE CACO LILE (LACO HER | AX. | Total Length of Cas | sino | (feet) | 17 09 |

Total Length of Casing

**Hand-Slotted Well Screens Are Unacceptable

0.010

Screen Slot Size **

SS316

PTFE PVC OTHER:

SS304

Well Completion Form (revised 02/06/02)

| Illinois Environ | mental Protection | on Agency | | | Well | Completio | n Report |
|---|-----------------------------------|----------------|------------------------------|---------------------------------------|-----------------------|--------------------------------------|---------------------|
| Site #: | | County: Mor | ntgomery | | W | /ell #: | G406 |
| Site Name: Coffeen Power Sta | ation - Ash Pond 2 | | | | В | orehole #: | G406 |
| State Plane Coordinate: X 2,514,702 | 2.4 Y 872,521.3 | (or) Latitude: | 39 | 3! <u>37.114</u> | À Longitud | e: <u>-89</u> 2 | 23! <u>54.628</u> Ä |
| Surveyed By: Gary C. Rogers | | | IL Registra | ation #:035-0 | 02957 | | |
| Drilling Contractor: Bulldog D | rilling, Inc. | | Driller: _ | J. Dittmaier | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | | Geologist: | Rhonald W. | Hasenyager | r, LPG #196-00 | 0246 |
| Drilling Method: Hollow stem | auger | | Drilling Fl | uid (Type):nc | one | | |
| Logged By: Kristen L. Theesf | eld | | Date Start | ed: 8/19/20 | 016 Dat | e Finished:8 | 3/19/2016 |
| Report Form Completed By: Su | zanna L. Keim | | Date: | 8/24/2016 | | | |
| ANNULAR SPA | CE DETAILS | | | Elevations (MSL)* | Depths (BGS) | (0.01 ft | .) |
| | | | | 625.70 | 3.84 | Top of Protectiv | ve Casing |
| | | | | 625.36 | 3.50_ | Top of Riser Pi | pe |
| Type of Surface Seal: Concrete | | | | _621.86_ | 0.00 | Ground Surface | ; |
| | | | | 619.86 | 2.00 | Top of Annular | Sealant |
| Type of Annular Sealant: High- | solids bentonite | — Ŋ | | | | Top of Fundam | Source |
| Installation Method:Tremie | 2 | | | | | | |
| Setting Time: >24 hours | | | $\mathbb{Z} \mid \cdot \mid$ | | | Static Water Le (After Completion | |
| Type of Bentonite Seal Gran | ular Pellet Slurr | y \downarrow | | | | | |
| Installation Method: Gravit | (choose one) V | | | 610.74 | 11.12 | Top of Seal | |
| Setting Time: 30 minutes | , | | | | | • | |
| seeing time. <u>30 minutes</u> | | | | 609.65 | 12.21 | Top of Sand Pa | ck |
| Type of Sand Pack: Quartz San | d | | | | | | |
| Grain Size: 10-20 (sie | eve size) | | | 608.30 | 13.56 | Top of Screen | |
| Installation Method: Gravit | У | | | | | | |
| Type of Backfill Material: n/a | | | | 603.49 603.11 | 18.37 18.75 | Bottom of Scree Bottom of Well | |
| 1)po 01 Buolini illutoriui. <u>12 u</u> | (if applicable) | | | | | Bottom of Wen | |
| Installation Method: | | | | 603.11 * Referenced to a | 18.75 National Geodet | Bottom of Bore | hole |
| | | | | | | | |
| | | | | | | SUREMENTS | |
| | STRUCTION MATERI | ALS | | iameter of Boreh | | (inches | |
| (Choose on | e type of material for each area) | | | O of Riser Pipe rotective Casing I | enoth | (inches | |
| | | | | iser Pipe Length | | (feet | 4 - 0 - |
| Protective Casing | SS304 SS316 PTFE | PVC OTHER: | | ottom of Screen t | | • | 0.00 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE | PVC OTHER: | | creen Length (1 | | | 4.01 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE | PVC OTHER: | T | otal Length of Ca | sing | (feet | 22.25 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | mental Protection | Agency | | | | Well | Completic | n Report |
|-------------------------------------|--|---|------------------------------|-------------|---------------------------|--------------------------|--------------------------------------|-------------------|
| Site #: | Co | ounty: Mon | itgomery | 7 | | W | Vell #: | G407 |
| Site Name: Coffeen Power Sta | ation - Ash Pond 2 | | | | | В | orehole #: | G407 |
| State Plane Coordinate: X 2,513,705 | 5.9 Y <u>872,973.4</u> (o | r) Latitude: | 39 | 3! | <u>41.665</u> Ä | Longitud | e:89 | 24! <u>7.213Ä</u> |
| Surveyed By: Gary C. Rogers | | | IL Regi | stration | #:035-0 | 02957 | | |
| Drilling Contractor: Bulldog D | rilling, Inc. | | Driller: | <u>J. D</u> | ittmaier | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | | Geolog | ist: R | honald W. | Hasenyage | r, LPG #196-00 | 00246 |
| Drilling Method: Hollow stem | auger | | Drilling | g Fluid (| Type): <u>no</u> | ne | | |
| Logged By: Kristen L. Theesfe | eld | | Date St | arted: _ | 8/16/20 | 16 Dat | e Finished: | 3/16/2016 |
| Report Form Completed By: Su | | | | | /24/2016 | | | |
| ANNULAR SPA | | | | El | evations (MSL)* | Depths | (0.01 f | <u></u>) |
| | | | | | 621.70_ | (BGS) 3.35_ | Top of Protecti | ve Casing |
| | | T | | | 621.32 | -2.97 | Top of Riser Pi | |
| Type of Surface Seal: Concrete | | | | | 618.35 | 0.00 | Ground Surface | |
| | | | | / | | | | |
| Type of Annular Sealant: High-s | olids bentonite | - | | _ | 616.35 | 2.00 | Top of Annula | Sealant |
| Installation Method: Tremie | · | _ | | | | | | |
| Setting Time: >24 hours | | _ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ | $\mathbb{Z} \mid \cdot \mid$ | _ | | | Static Water Le (After Completion | |
| Type of Bentonite Seal Grant | Pellet Slurry (choose one) | | | | | | | |
| Installation Method: <u>Gravity</u> | , | | XX | _ | 607.50 | _10.85_ | Top of Seal | |
| Setting Time: 15 minutes | | - | | _ | 605.50 | _12.85_ | Top of Sand Pa | ick |
| Type of Sand Pack: Quartz Sand | 1 | | | | | | | |
| Grain Size: 10-20 (sie | ve size) | | | _ | 604.57 | 13.78 | Top of Screen | |
| Installation Method: Gravity | y | _ | ∄ | | | | | |
| Type of Backfill Material: Quart | z Sand | | ₹ | | 599.74 599.31 | <u>18.61</u> 19.04 | Bottom of Scre Bottom of Well | |
| | (if applicable) | _ _ | | | | | | |
| Installation Method: Gravity | У | | | _ | 598.35 Referenced to a | 20.00 National Geodet | Bottom of Bore | hole |
| | | | | | CAS | ING MEA | SUREMENTS | |
| | | | | Diame | ter of Boreho | | (inche | s) 8.0 |
| | TRUCTION MATERIALS e type of material for each area) | S | | | Riser Pipe | - | (inche | 2.0 |
| | • | | | Protec | tive Casing L | ength | (fee | |
| Protective Casing | SS304 SS316 PTFE P | VC OTHER: (S | taal | | Pipe Length | | (fee | |
| Riser Pipe Above W.T. | | VC OTHER: S | nicei) | | n of Screen to | | (fee | |
| Riser Pipe Below W.T. | | VC OTHER: | | | Length (1s | | ot) (fee | 22.01 |

SS304

Well Completion Form (revised 02/06/02)

SS316

Total Length of Casing

**Hand-Slotted Well Screens Are Unacceptable

Screen Slot Size **

0.010

| Illinois Environmental Protection Ager | ncy Well Completion Report |
|---|--|
| Site #: County: _Mon | ntgomery Well #: G410 |
| Site Name: Coffeen Power Station - Ash Pond 2 | Borehole #: G410 |
| State Plan€oordinate: X 2,513,206.3 Y 872,968.5 (or) Latitude: | |
| Surveyed By:Matthew H. Schrader | IL Registration #:035-003487 |
| Drilling Contractor: Bulldog Drilling, Inc. | Driller: C. Dutton |
| Consulting Firm: Hanson Professional Services Inc. | Geologist: Rhonald W. Hasenyager, LPG #196-000246 |
| Drilling Method: Hollow stem auger | Drilling Fluid (Type):none |
| Logged By: Rhonald W. Hasenyager | Date Started: <u>2/23/2018</u> Date Finished: <u>2/23/2018</u> |
| Report Form Completed By: Suzanna L. Keim | Date:2/26/2018 |
| ANNULAR SPACE DETAILS | Elevations Depths (0.01 ft.) (MSL)* (BGS) |
| | 620.18 -2.97 Top of Protective Casing |
| | |
| | |
| Type of Surface Seal: Concrete | 617.21 0.00 Ground Surface |
| Type of Annular Sealant: | n/a Top of Annular Sealant |
| Installation Method: | |
| Setting Time: | 7 612.39 4.82 Static Water Level |
| Secting Finite. | (After Completion) 3/1/2018 |
| Type of Bentonite Seal Granular Pellet Slurry (choose one) | |
| Installation Method: <u>Gravity</u> | 616.71 0.50 Top of Seal |
| Setting Time:>24 hours | 609.81 7.40 Top of Sand Pack |
| | |
| Type of Sand Pack: Filter Sand | |
| Grain Size: 20/40 (sieve size) | |
| Installation Method: Gravity | |
| Type of Backfill Material: (if applicable) | 603.12 14.09 Bottom of Well |
| Installation Method: <u>n/a</u> | 603.12 14.09 Bottom of Borehole |
| | * Referenced to a National Geodetic Datum |
| | CASING MEASUREMENTS |
| MIELL CONCEDUCTION MATERIALS | Diameter of Borehole (inches) 8.0 |
| WELL CONSTRUCTION MATERIALS (Choose one type of material for each area) | ID of Riser Pipe (inches) 2.0 |
| | Protective Casing Length (feet) 5.0 |
| Protective Casing SS304 SS316 PTFE PVC OTHER: S | Riser Pipe Length (feet) 11.47 Bottom of Screen to End Cap (feet) 0.41 |
| Riser Pipe Above W.T. SS304 SS316 PTFE PVC OTHER: | Bottom of Screen to End Cap (feet) 0.41 Screen Length (1st slot to last slot) (feet) 4.79 |
| Riser Pipe Below W.T. SS304 SS316 PTFE PVC OTHER: | Total Length of Casing (feet) 16.67 |

SS304

Well Completion Form (revised 02/06/02)

SS316

Total Length of Casing

**Hand-Slotted Well Screens Are Unacceptable

Screen Slot Size **

0.010

| Illinois Environmental Protection Ager | ісу | Well Complet | ion Report |
|--|-------------------------------------|--|-------------------------------|
| Site #: County: _Mon | ntgomery | Well #: | G411 |
| Site Name: Coffeen Power Station - Ash Pond 2 | | Borehole #: | G411 |
| State Plan€oordinate: X_2,513,122.4 Y 873,844.8 (or) Latitude: | 39Ä 3! 50.326 | Longitude: -89Ä | 24! 14.517 |
| Surveyed By: Matthew H. Schrader | IL Registration #:035 | 5-003487 | |
| Drilling Contractor: Bulldog Drilling, Inc. | Driller: <u>C. Dutton</u> | | |
| Consulting Firm: Hanson Professional Services Inc. | Geologist: Rhonald W | V. Hasenyager, LPG # | 196-000246 |
| Drilling Method: Hollow stem auger | Drilling Fluid (Type): | none | |
| Logged By: Rhonald W. Hasenyager | Date Started: 2/22/2 | 2018 Date Finished: | 2/22/2018 |
| Report Form Completed By: Suzanna L. Keim | Date: 2/26/2018 | <u>: </u> | |
| ANNULAR SPACE DETAILS | Elevations (MSL)* | Depths (0.0 |)1 ft.) |
| | 623.60 | 3.11_ Top of Pro | tective Casing |
| | 623.25 | 2.76_ Top of Ris | er Pipe |
| Type of Surface Seal: Concrete | 620.49 | 0.00 Ground Su | urfaca |
| | 020.19 | | |
| Type of Annular Sealant: | | n/a Top of Ani | nular Sealant |
| Installation Method: | | | |
| Setting Time: | 617.84 | 2.65 Static Wat | er Level pletion) 3/1/2018 |
| Type of Bentonite Seal Granular Pellet Slurry (choose one) | | | |
| Installation Method: Gravity | 619.99 | | 1 |
| Setting Time: _ >24 hours | 610.42 | 10.07 Top of San | ıd Pack |
| | | | id i dek |
| Type of Sand Pack: Filter Sand | 609.28 | 11.21 Top of Scr | een |
| Grain Size: 20/40 (sieve size) | | | |
| Installation Method: Gravity | _604.42_ | | Screen |
| Type of Backfill Material: <u>n/a</u> (if applicable) | 604.02 | | Well |
| Installation Method:n/a | 604.02 | | Borehole |
| | * Referenced to | a National Geodetic Datum | |
| | CA | SING MEASUREMEN | ΓS |
| WELL CONSTRUCTION MATERIALS | Diameter of Bore | | nches) 8.0 |
| (Choose one type of material for each area) | ID of Riser Pipe | | nches) 2.0 |
| | Protective Casing Riser Pipe Lengtl | _ | (feet) 5.0 (feet) 13.97 |
| Protective Casing SS304 SS316 PTFE PVC OTHER: § | | | (feet) 13.97 (feet) 0.40 |
| Riser Pipe Above W.T. SS304 SS316 PTFE PVC OTHER: | Screen Length (2 | | (feet) 4.86 |
| Riser Pipe Below W.T. SS304 SS316 PTFE PVC OTHER: | Total Length of C | | (feet) 19.23 |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

(inches)

SS304

Well Completion Form (revised 02/06/02)

SS316

| Illinois Enviro | nmental Protection A | Agency | | | Well (| Completion | Report |
|---------------------------------------|--|-------------|----------|---|-----------------|--|----------|
| Site #: | Count | y: Mont | gomer | У | We | ell #:MV | V1D |
| Site Name: <u>AEG Coffeen Po</u> | wer Station CCB Managemen | nt Facility | | | Bo: | rehole #:S | B-01 |
| State Plane Coordinate: X 874,972 | 2.6 Y 2,513,478.0 (or) | Latitude: _ | c | | Longitude | | ' |
| Surveyed By: <u>Darren E. Forg</u> | y | | IL Reg | istration #:035-00 |)3637 | | |
| Drilling Contractor: <u>Testing S</u> | ervice Corporation | | Driller: | B. Williamson | | | |
| Consulting Firm: Hanson Pro | fessional Services Inc. | | Geolog | ist: Rhonald W I | Hasenyager | , LPG #196-00 | 0246 |
| Drilling Method: Hollow stem | n auger | | Drilling | g Fluid (Type): Por | table water | | |
| Logged By: <u>Testing Services</u> | Corp. | | Date St | arted: 5/3/200 | 6 Date | Finished:5/ | 3/2006 |
| Report Form Completed By: R | nonald W Hasenyager | | Date: _ | 6/7/2006 | | | |
| ANNULAR SPA | CE DETAILS | | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | | 609.29 | -1.89 | Top of Protective | e Casing |
| | | | | 609.01 | -1.61 | Top of Riser Pipe | e |
| Type of Surface Seal: Concrete | | | | 607.40_ | 0.00 | Ground Surface | |
| | | | | 604.80 | 2.60 | Top of Annular S | Sealant |
| Type of Annular Sealant: Bento | | | | | | | |
| Installation Method: <u>Tremi</u> | | | | 571 10 | 26.20 | C W | 1 |
| Setting Time: +24 hr. | | | | 571.12 | 36.28 | Static Water Lev (After Completion) | |
| Type of Bentonite Seal Gran | | | | | | | |
| Installation Method: <u>Gravit</u> | (choose one) | | | 578.90 | 28.50 | Top of Seal | |
| Setting Time: 21 min. | | | | _575.82_ | 31.58 | Top of Sand Pacl | 7 |
| | | V | | 373.62 | | Top of Sand Laci | X. |
| Type of Sand Pack: Quartz sand | | | | _574.11_ | 33.29 | Top of Screen | |
| Grain Size: #5 (sie | | | | | | Top of Sciecti | |
| Installation Method: <u>Gravit</u> | У | | | _569.35_ | 38.05 | Bottom of Screen | 1 |
| Type of Backfill Material: <u>n/a</u> | (if applicable) | |] | 568.99 | | Bottom of Well | |
| Installation Method: n/a | (ii applicable) | | | 567.40 | 40.00 | Bottom of Boreh | ole |
| | | | | * Referenced to a l | | | 0.10 |
| | | | | CASI | NG MEAS | UREMENTS | |
| WELL COM | TRUCTION NA TERMA | | | Diameter of Boreho | ole | (inches) | 7.3 |
| | TRUCTION MATERIALS e type of material for each area) | | | ID of Riser Pipe | | (inches) | 2.0 |
| | | | | Protective Casing L | ength | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC | OTHER: | Steel | Riser Pipe Length | | (feet) | 35.17 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC | | | Bottom of Screen to | - | | 0.36 |
| Riser Pipe Below W.T. | | OTHER: | | Screen Length (1st Total Length of Cas | | (feet) | 4.76 |
| | | | | 1 Juli Longui oi Cas | ,1115 | (1001) | 10.27 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

ILLINOIS DEPARTMENT OF PUBLIC HEALTH DIVISION OF ENVIRONMENTAL HEALTH 525 W. JEFFERSON ST. SPRINGFIELD, IL 62761

WATER WELL SEALING FORM

TYPE OR PRESS FIRMLY

RETURN ALL COPIES TO IDPH OR LOCAL HEALTH DEPARTMENT

This form shall be submitted to this Department or the local health department not more than 30 days after a water well, boring or monitoring well is sealed. Such wells are to be sealed not more than 30 days after they are abandoned in accordance with the sealing requirements in the Water Well Construction Code. THE LOCAL HEALTH DEPARTMENT OR REGIONAL PUBLIC HEALTH DEPARTMENT MUST BE NOTIFIED AT LEAST 48 HOURS PRIOR TO SEALING.

| Ownership (Name of Controlling Party) AEG C | offeen Power Stat | ion | | (G104) |) |
|---|-------------------|-----------|---------------|------------|------|
| Well Location 134 CIPS Trail | | Coffe | een | Montgon | nery |
| Address - Lot Number | | | City | County | 7 |
| General Description Township 7 (N) | ⊗ Range | 3 (| K)(W) | Section | 10 |
| SEQuarter of theNE | _Quarter of the _ | NE | Qua | arter | |
| Year Drilled 2010 | | | | | |
| Drilling Permit Number (and date, if known)n/a | | | | | _ |
| Type of Well Bored Drilled_ ✓ | | | | | |
| Total Depth 20.0 ft. Diame | eter (inches) | 2 | | | |
| Formation clear of obstructionYes | | | | | |
| DETAILS OF PLUGGING | | | | | |
| Filled with Bentonite grout (cement or other materials) | from | 0.5 | _to20.0 | <u>ft.</u> | |
| | | | 0.5 | C4 | |
| 1 0 | | | | | |
| Filled with | from | | _to | ft. | |
| Kind of plug | from | | _to | ft. | |
| Filled with | from | | _to | ft. | |
| Kind of plug | from | | _to | ft. | |
| CASING RECORD Upper 2 feet of casing remove | ed <u>√</u> Ye | s | No | | |
| Date well was sealed Month October Da | ay8 | Year | 2010 | | |
| Licensed water well driller or other person approve | ed by the Departi | nent perf | orming wel | l sealing. | |
| Rhonald W. Hasenyager, L.P.G. | 196-0002 | 246 | | | |
| Name | Complete | License 1 | Number | | _ |
| Hanson Professional Services Inc., 1525 S. 6th St. | Springfie | eld | | IL 62703 | _ |
| Address | City | | | State/ZIP | |

This state agency is requesting disclosure of information that is necessary to accomplish the statutory purpose as outlined under Public Act 85-0863. Disclosure of this information is mandatory. This form has been approved by the Forms Management Center.

IL 482-0631

| Illinois Enviro | nmental Protection Ager | ncy | | Well Co | mpletion | Report |
|--|------------------------------------|---------------------------|--------------------------------------|----------------------------------|------------------------------------|--------|
| Site #: | County: N | Iontgomery | 7 | Well # | #:MW | /2D |
| Site Name: <u>AEG Coffeen Po</u> | wer Station CCB Management Fac | ility | | Boreh | ole #:SI | 3-02b |
| State Plane Coordinate: X 876,414 | 4.0 Y 2,513,209.7 (or) Latitud | de:° | | Longitude: | 0 | _' |
| Surveyed By: <u>Darren E. Forg</u> | y | IL Regi | stration #:035-0 | 03637 | | |
| Drilling Contractor: <u>Testing S</u> | ervice Corporation | _ Driller: | B. Williamson | | | |
| Consulting Firm: Hanson Pro | fessional Services Inc. | Geologi | ist: Rhonald W | Hasenyager, I | _PG #196-00 | 0246 |
| Drilling Method: Hollow sten | n auger | _ Drilling | Fluid (Type): Po | otable water | | |
| Logged By:Testing Services | Corp. | _ Date Sta | arted: 5/5/200 | Date Fir | nished: 5/ | 5/2006 |
| Report Form Completed By: R | honald W Hasenyager | _ Date: _ | 6/7/2006 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | _ | | 627.52 | ` / | p of Protective | Casing |
| | | | 627.07 | 2.97_ To | p of Riser Pipe | ÷ |
| Type of Surface Seal: Concrete | | | 624.10 | 0.00 Gro | ound Surface | |
| | | | 621.00 | | p of Annular S | ealant |
| Type of Annular Sealant: Bento | onite grout | | | | r | |
| Installation Method:Tremi | <u>e</u> | | | | | |
| Setting Time: +24 hr. | | $ \overline{\Delta} $ | 616.74 | | tic Water Leve fter Completion) | |
| Type of Bentonite Seal Gran | ular Pellet Slurry | | | | | |
| Installation Method: Graving | (choose one) | | 606.00 | 18.10 To | n of Seal | |
| Setting Time: 20 min. | | 1 1/1 | | | p or sour | |
| Setting Time. 20 min. | <u> </u> | | 603.92 | | p of Sand Pack | ζ |
| Type of Sand Pack: Quartz sand | d | | | | | |
| Grain Size: #5 (sie | eve size) | | 602.07 | | p of Screen | |
| Installation Method: Gravit | ty | | | | | |
| Type of Backfill Material: | | | <u>597.27</u> 596.88 | | ttom of Screen ttom of Well | ı |
| Type of Buckini Muterial. <u>III a</u> | (if applicable) | | | | ttom of wen | |
| Installation Method: Re-dri | ill borehole | | | 27.22 Bo National Geodetic Da | ttom of Boreho | ole |
| | | | | | | |
| | | Γ | | ING MEASUF | REMENTS | |
| | STRUCTION MATERIALS | | Diameter of Boreho | ole | (inches) | 8.0 |
| (Choose or | ne type of material for each area) | | ID of Riser Pipe Protective Casing I | Lenoth | (inches) | 5.0 |
| | | | Riser Pipe Length | Lengul | (feet) | 25.00 |
| Protective Casing | SS304 SS316 PTFE PVC OTHE | R: Steel | Bottom of Screen t | o End Cap | <u> </u> | 0.39 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHE | R: | Screen Length (1s | - | (feet) | 4.80 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHE | R: | Total Length of Ca | sing | (feet) | 30.19 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

ILLINOIS DEPARTMENT OF PUBLIC HEALTH DIVISION OF ENVIRONMENTAL HEALTH 525 W. JEFFERSON ST. SPRINGFIELD, IL 62761

WATER WELL SEALING FORM

TYPE OR PRESS FIRMLY

RETURN ALL COPIES TO IDPH OR LOCAL HEALTH DEPARTMENT

This form shall be submitted to this Department or the local health department not more than 30 days after a water well, boring or monitoring well is sealed. Such wells are to be sealed not more than 30 days after they are abandoned in accordance with the sealing requirements in the Water Well Construction Code. THE LOCAL HEALTH DEPARTMENT OR REGIONAL PUBLIC HEALTH DEPARTMENT MUST BE NOTIFIED AT LEAST 48 HOURS PRIOR TO SEALING.

| Ownership (Name of Controlling Party) AEG C | offeen Power Stat | ion | | (G104) |) |
|---|-------------------|-----------|---------------|------------|------|
| Well Location 134 CIPS Trail | | Coffe | een | Montgon | nery |
| Address - Lot Number | | | City | County | 7 |
| General Description Township 7 (N) | ⊗ Range | 3 (| K)(W) | Section | 10 |
| SEQuarter of theNE | _Quarter of the _ | NE | Qua | arter | |
| Year Drilled 2010 | | | | | |
| Drilling Permit Number (and date, if known)n/a | | | | | _ |
| Type of Well Bored Drilled_ ✓ | | | | | |
| Total Depth 20.0 ft. Diame | eter (inches) | 2 | | | |
| Formation clear of obstructionYes | | | | | |
| DETAILS OF PLUGGING | | | | | |
| Filled with Bentonite grout (cement or other materials) | from | 0.5 | _to20.0 | <u>ft.</u> | |
| | | | 0.5 | C4 | |
| 1 0 | | | | | |
| Filled with | from | | _to | ft. | |
| Kind of plug | from | | _to | ft. | |
| Filled with | from | | _to | ft. | |
| Kind of plug | from | | _to | ft. | |
| CASING RECORD Upper 2 feet of casing remove | ed <u>√</u> Ye | s | No | | |
| Date well was sealed Month October Da | ay8 | Year | 2010 | | |
| Licensed water well driller or other person approve | ed by the Departi | nent perf | orming wel | l sealing. | |
| Rhonald W. Hasenyager, L.P.G. | 196-0002 | 246 | | | |
| Name | Complete | License 1 | Number | | _ |
| Hanson Professional Services Inc., 1525 S. 6th St. | Springfie | eld | | IL 62703 | _ |
| Address | City | | | State/ZIP | |

This state agency is requesting disclosure of information that is necessary to accomplish the statutory purpose as outlined under Public Act 85-0863. Disclosure of this information is mandatory. This form has been approved by the Forms Management Center.

IL 482-0631

| Illinois Enviro | nmental Protection A | gency | | | Well (| Completio | n Report |
|--|-----------------------------------|--------------|------------------------------------|-----------------------------------|---------------------|------------------|--------------|
| Site #: | County: | Montgon | nery | | Wo | ell #:M | IW2S |
| Site Name: <u>AEG Coffeen Por</u> | wer Station CCB Management | Facility | | | Во | orehole #: | SB-02a |
| State Plane Coordinate: X 876,408 | 3.9 Y 2,513,210.0 (or) La | atitude: | <u> </u> | | Longitude | e:° | ' |
| Surveyed By: <u>Darren E. Forg</u> | y | IL I | Registra | tion #: <u>035-0</u> | 03637 | | |
| Drilling Contractor: Testing S | ervice Corporation | Dril | ller:] | B. Williamson | | | |
| Consulting Firm: Hanson Pro | fessional Services Inc. | Geo | ologist: | Rhonald W | Hasenyager | ., LPG #196-0 | 000246 |
| Drilling Method: Hollow stem | n auger | Dril | lling Fl | uid (Type): Po | table water | | |
| Logged By:Testing Services | Corp. | Dat | e Starte | d:5/5/200 | 06 Date | Finished: | 5/5/2006 |
| Report Form Completed By: R | nonald W Hasenyager | Dat | e: | 6/7/2006 | | | |
| ANNULAR SPA | CE DETAILS | | | Elevations (MSL)* | Depths (BGS) | (0.01 ft | <i>i.</i> .) |
| | | | 7 | 627.55 | 3.45 | Top of Protecti | ve Casing |
| | | | _ | 627.07 | 2.97 | Top of Riser Pi | pe |
| Type of Surface Seal: Concrete | | | <u> </u> | 624.10 | 0.00 | Ground Surface | e |
| T. CA. I. C. I. (D.) | | | | 619.72 | 4.38 | Top of Annular | Sealant |
| Type of Annular Sealant: Bento | | | | | | | |
| Installation Method: <u>Gravit</u> Setting Time: +24 hr. | | | | 616.68 | 7.42 | Static Water Le | evel |
| Setting Time | | | | | | (After Completio | |
| Type of Bentonite Seal Gran | Pellet Slurry - | | | | | | |
| Installation Method: <u>Gravit</u> | <u>y</u> | | a | 619.72 | 4.38 | Top of Seal | |
| Setting Time: +24 hr. | | | 1 | 614.60 | 9.50 | Top of Sand Pa | ck |
| Type of Sand Pack: Quartz sand | 1 | | | | | | |
| Grain Size: #5 (sie | | | | 613.76 | _10.34_ | Top of Screen | |
| Installation Method: Gravit | | | | | | | |
| Type of Dealrfill Matarial | | | | 608.98 | | Bottom of Scre | |
| Type of Backfill Material:n/a_ | (if applicable) | | | _008.39_ | _13.31_ | Bottom of Wel | I |
| Installation Method:n/a | | | | 608.59 * Referenced to a | | Bottom of Bore | ehole |
| | | | | G L G | | | |
| | | | D: | | | SUREMENTS | |
| | TRUCTION MATERIALS | | | ameter of Boreho of Riser Pipe | oie | (inches | 2.0 |
| (Choose on | e type of material for each area) | | | otective Casing I | Length | (feet | |
| | | | | ser Pipe Length | | (feet | 12.21 |
| Protective Casing | SS304 SS316 PTFE PVC (| OTHER: Steel | $\square \mid_{\operatorname{Bc}}$ | ttom of Screen t | o End Cap | (feet | 0.39 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC | OTHER: | Sc | reen Length (1s | t slot to last slot | t) (feet | 4.78 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC | OTHER: | To | tal Length of Ca | sing | (feet | 18.48 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

ILLINOIS DEPARTMENT OF PUBLIC HEALTH DIVISION OF ENVIRONMENTAL HEALTH 525 W. JEFFERSON ST. SPRINGFIELD, IL 62761

WATER WELL SEALING FORM

TYPE OR PRESS FIRMLY

RETURN ALL COPIES TO IDPH OR LOCAL HEALTH DEPARTMENT

This form shall be submitted to this Department or the local health department not more than 30 days after a water well, boring or monitoring well is sealed. Such wells are to be sealed not more than 30 days after they are abandoned in accordance with the sealing requirements in the Water Well Construction Code. THE LOCAL HEALTH DEPARTMENT OR REGIONAL PUBLIC HEALTH DEPARTMENT MUST BE NOTIFIED AT LEAST 48 HOURS PRIOR TO SEALING.

| Ownership (Name of Controlling Party) AEG C | offeen Power Stat | ion | | (G104) |) |
|---|-------------------|-----------|---------------|------------|------|
| Well Location 134 CIPS Trail | | Coffe | een | Montgon | nery |
| Address - Lot Number | | | City | County | 7 |
| General Description Township 7 (N) | ⊗ Range | 3 (| K)(W) | Section | 10 |
| SEQuarter of theNE | _Quarter of the _ | NE | Qua | arter | |
| Year Drilled 2010 | | | | | |
| Drilling Permit Number (and date, if known)n/a | | | | | _ |
| Type of Well Bored Drilled_ ✓ | | | | | |
| Total Depth 20.0 ft. Diame | eter (inches) | 2 | | | |
| Formation clear of obstructionYes | | | | | |
| DETAILS OF PLUGGING | | | | | |
| Filled with Bentonite grout (cement or other materials) | from | 0.5 | _to20.0 | <u>ft.</u> | |
| | | | 0.5 | C4 | |
| 1 0 | | | | | |
| Filled with | from | | _to | ft. | |
| Kind of plug | from | | _to | ft. | |
| Filled with | from | | _to | ft. | |
| Kind of plug | from | | _to | ft. | |
| CASING RECORD Upper 2 feet of casing remove | ed <u>√</u> Ye | s | No | | |
| Date well was sealed Month October Da | ay8 | Year | 2010 | | |
| Licensed water well driller or other person approve | ed by the Departi | nent perf | orming wel | l sealing. | |
| Rhonald W. Hasenyager, L.P.G. | 196-0002 | 246 | | | |
| Name | Complete | License 1 | Number | | _ |
| Hanson Professional Services Inc., 1525 S. 6th St. | Springfie | eld | | IL 62703 | _ |
| Address | City | | | State/ZIP | |

This state agency is requesting disclosure of information that is necessary to accomplish the statutory purpose as outlined under Public Act 85-0863. Disclosure of this information is mandatory. This form has been approved by the Forms Management Center.

IL 482-0631

| Illinois Environmental Protection | Agency | | | Well C | Completion | Report |
|--|--------------------|---|---------------------------------|-------------------|--------------------|--------------|
| Site #: Col | unty: <u>Montg</u> | omery | | We | 11 #:MV | V3D |
| Site Name: AEG Coffeen Power Station CCB Manager | | | | Bor | rehole #:S | B-03 |
| State Plane Coordinate: X 876,554.5 Y 2,514,535.3 (or) | · | | | | | |
| Surveyed By: Darren E. Forgy | | | ation #: <u>035-0</u> | | | |
| Drilling Contractor: Testing Service Corporation | | Oriller: | B. Williamson | | | |
| Consulting Firm: Hanson Professional Services Inc. | | Geologist: | Rhonald W | Hasenyager, | LPG #196-00 | 00246 |
| Drilling Method: Hollow stem auger | Г | Orilling Fl | uid (Type): <u>Po</u> | otable water | | |
| Logged By:Testing Services Corp. | Г | Date Starte | ed: <u>4/27/20</u> | 06 Date 1 | Finished: 4/2 | 27/2006 |
| Report Form Completed By: Rhonald W Hasenyager | Г | Date: | 6/7/2006 | | | |
| ANNULAR SPACE DETAILS | | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | 629.37 | ` / | Γop of Protective | e Casing |
| | | T | | | | _ |
| | |] | 628.94 | 3.24_ | Гор of Riser Pip | e |
| Type of Surface Seal: Concrete | | | 625.70 | 0.000 | Ground Surface | |
| Type of Annular Sealant: Bentonite grout | | | 623.00 | | Γop of Annular S | Sealant |
| Installation Method:Tremie | | | | | | |
| Setting Time: _ +24 hr. | | | 570.30 | 55.40 | Static Water Lev | el |
| | | | | | (After Completion) | |
| Type of Bentonite Seal Granular Pellet Slurry | | | | | | |
| Installation Method: Gravity | | | 576.70 | 49.00 | Γop of Seal | |
| Setting Time: 25 min. | | | 575.60 | 50.10 | Γop of Sand Pac | ζ. |
| | v v | | | | | |
| Type of Sand Pack: Quartz sand | | | 573.41 | 52.29 | Γop of Screen | |
| Grain Size: #5 (sieve size) | | | | | | |
| Installation Method: <u>Gravity</u> | | | 568.64 | 57.06 I | Bottom of Screen | 1 |
| Type of Backfill Material: Cuttings (if applicable) | | | 568.30 | _57.40_ I | Bottom of Well | |
| Installation Method: Over-drill borehole | | | 567.70 | | Bottom of Boreh | ole |
| | | | * Referenced to a | National Geodetic | : Datum | |
| | | | CAS | ING MEASI | UREMENTS | |
| WELL CONSTRUCTION MATERIAL | S | | ameter of Boreh | ole | (inches) | 8.0 |
| (Choose one type of material for each area) | | | of Riser Pipe | | (inches) | 2.0 |
| | | | otective Casing 1 | Length | (feet) | 5.0 |
| Protective Casing SS304 SS316 PTFE PV | C OTHER: S | | ser Pipe Length | F 10 | (feet) | 55.51 |
| Riser Pipe Above W.T. SS304 SS316 PTFE PV | | | ottom of Screen t | - | (feet) | 0.36 4.77 |
| | C OTHER: | | reen Length (1stal Length of Ca | | (feet) | 60.64 |
| | | —— T | Longin or Co | b | (ICCI) | 00.01 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviror | nmental Protection Agen | cy | | Well Cor | npletion Report |
|---------------------------------------|---------------------------------|----------------|--|--------------------------------------|--|
| Site #: | County:M | ontgomery | | Well #: | MW4S |
| Site Name: AEG Coffeen Pov | ver Station CCB Management Faci | lity | | Boreho | le #: SB-04a |
| State | .7 Y 2,514,450.6 (or) Latitud | | | | |
| Surveyed By: <u>Darren E. Forgy</u> | I | _ IL Regis | stration #:035-0 | 03637 | |
| Drilling Contractor: Testing Se | ervice Corporation | _ Driller: | B. Williamson | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | _ Geologis | st: Rhonald W | Hasenyager, Ll | PG #196-000246 |
| Drilling Method: Hollow stem | auger | _ Drilling | Fluid (Type): Po | otable water | |
| Logged By: <u>Testing Services</u> | Corp. | _ Date Sta | rted:5/11/20 | 06 Date Fini | shed:5/11/2006 |
| Report Form Completed By: Rh | onald W Hasenyager | _ Date: _ | 6/7/2006 | | |
| ANNULAR SPAC | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) |
| | _ | | 626.07 | · · | of Protective Casing |
| | | | 625.60 | 3.20_ Top | of Riser Pipe |
| Type of Surface Seal: Concrete | | | 622.40_ | | and Surface |
| | | | 619.57 | 2.83 Top | of Annular Sealant |
| Type of Annular Sealant: Benton | λ | | | | |
| Installation Method: <u>Gravity</u> | | | | | |
| Setting Time: +24 hr. | | $\bar{\Delta}$ | 616.73 | | c Water Level er Completion) 6/1/2006 |
| Type of Bentonite Seal Granu | | | | | |
| Installation Method: Gravity | (choose one) | | 619.57 | 2.83 Top | of Seal |
| Setting Time:+24 hr. | | | | | |
| | | | 614.15 | 8.25 Top | of Sand Pack |
| Type of Sand Pack: Quartz sand | <u> </u> | | | | |
| Grain Size: #5 (siev | ve size) | | 612.57 | <u>9.83</u> Top | of Screen |
| Installation Method: <u>Gravity</u> | у | | 600.14 | 14.06 | |
| Type of Backfill Material: <u>n/a</u> | | | 608.14 607.63 | | om of Screen om of Well |
| | (if applicable) | | | | |
| Installation Method: <u>n/a</u> | | | 607.63 * Referenced to a | 14.77 Bott National Geodetic Date | om of Borehole |
| | | | | | |
| | | Γ. | | ING MEASUR | |
| | TRUCTION MATERIALS | | Diameter of Boreho ID of Riser Pipe | oie | (inches) 7.3 (inches) 2.0 |
| (Choose one | type of material for each area) | | Protective Casing I | ength | (feet) 5.0 |
| | | | Riser Pipe Length | <u></u> | (feet) 14.25 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | C(1) | Bottom of Screen to | o End Cap | |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | | Screen Length (1s | - | (feet) 4.43 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | . 11 | Total Length of Ca | | (feet) 19.19 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environmental Protection Agency | y Well Completion Report |
|--|--|
| Site #: County: _Mon | ntgomery Well #: MW5D |
| Site Name: AEG Coffeen Power Station CCB Management Facilit | y Borehole #:SB-05 |
| State Plane Coordinate: X 878,174.8 Y 2,513,290.3 (or) Latitude: | °'" Longitude:°'" |
| Surveyed By: Darren E. Forgy | IL Registration #:035-003637 |
| Drilling Contractor: Testing Service Corporation | Driller: B. Williamson |
| Consulting Firm: Hanson Professional Services Inc. | Geologist: Rhonald W Hasenyager, LPG #196-000246 |
| Drilling Method: Hollow stem auger | Drilling Fluid (Type): Potable water |
| Logged By:Testing Services Corp. | Date Started:5/12/2006 Date Finished:5/17/2006 |
| Report Form Completed By: Rhonald W Hasenyager | Date:6/7/2006 |
| ANNULAR SPACE DETAILS | Elevations Depths (0.01 ft.) (MSL)* (BGS) |
| | |
| | |
| Type of Surface Seal: Concrete | |
| Type of Annular Sealant: Bentonite grout | |
| 7 | |
| Installation Method:Tremie Setting Time: _ +24 hr | |
| 500mig 7 mio | (After Completion) 6/1/2006 |
| Type of Bentonite Seal Granular Pellet Slurry | |
| Installation Method: Gravity | |
| Setting Time: 18 min. | 579.14 43.46 Top of Sand Pack |
| Type of Sand Pack: Quartz sand | |
| Grain Size: #5 (sieve size) | |
| Installation Method: Gravity | |
| | 572.27 50.33 Bottom of Screen |
| Type of Backfill Material: (if applicable) | |
| Installation Method:n/a | * Referenced to a National Geodetic Datum |
| | |
| | CASING MEASUREMENTS |
| WELL CONSTRUCTION MATERIALS | Diameter of Borehole (inches) 8.0 ID of Riser Pipe (inches) 2.0 |
| (Choose one type of material for each area) | ID of Riser Pipe (inches) 2.0 Protective Casing Length (feet) 5.0 |
| | Riser Pipe Length (feet) 48.74 |
| Protective Casing SS304 SS316 PTFE PVC OTHER: | |
| Riser Pipe Above W.T. SS304 SS316 PTFE PVC OTHER: | Screen Length (1st slot to last slot) (feet) 4.76 |
| Riser Pipe Below W.T. SS304 SS316 PTFE PVC OTHER: | Total Length of Casing (feet) 53.89 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviro | nmental Protection Ago | ency | | Well | Completion | Report |
|------------------------------------|-----------------------------------|------------|--|-------------------|---|---------------|
| Site #: | County: _ | Montgomer | y | W | ell #:MW | 75S |
| Site Name: <u>AEG Coffeen Po</u> | wer Station CCB Management F | acility | | Во | orehole #:SI | 3-05a |
| State Plane Coordinate: X 878,175 | 5.6 Y 2,513,285.5 (or) Lati | tude: | | Longitude | e:° | _'" |
| Surveyed By: <u>Darren E. Forg</u> | y | IL Reg | istration #: <u>035-0</u> | 003637 | | |
| Drilling Contractor: Testing S | ervice Corporation | Driller: | B. Williamson | | | |
| Consulting Firm: Hanson Pro- | fessional Services Inc. | Geolog | ist: Rhonald W | Hasenyage | r, LPG #196-00 | 0246 |
| Drilling Method: Hollow sten | n auger | Drilling | g Fluid (Type): Po | otable water | r | |
| Logged By:Testing Services | Corp. | Date St | arted:5/17/20 | 006 Date | Finished: 5/1 | 7/2006 |
| Report Form Completed By: R | nonald W Hasenyager | Date: _ | 6/7/2006 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | 626.14 | ` / | Top of Protective | Casing |
| | C | | | | - | |
| | | | 625.73 | 3.13 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 622.60 | 0.00 | Ground Surface | |
| Town of American Contract. Donto | with allies | | | 2.11 | Top of Annular S | ealant |
| Type of Annular Sealant: Bento | | | | | | |
| Installation Method: <u>Gravit</u> | <u>y</u> | | 61 7 0 6 | c = 1 | | |
| Setting Time: +24 hr. | | | 615.86 | 6.74 | Static Water Leve (After Completion) | |
| Type of Bentonite Seal Gran | ular Pellet Slurry — | | | | | |
| Installation Method: Gravit | (choose one) | | 620.49 | 2.11 | Top of Seal | |
| Setting Time: +24 hr. |) | | | | Top of Sour | |
| Setting Time | | | 611.06 | 11.54 | Top of Sand Pack | |
| Type of Sand Pack: Quartz sand | <u>d</u> | | | | | |
| Grain Size: #5 (sie | eve size) | | 609.94 | 12.66 | Top of Screen | |
| Installation Method: Gravit | <u>y</u> | | | | | |
| T CD ICHMA : 1 C W | | | 605.19 | 17.41 | Bottom of Screen | |
| Type of Backfill Material:Cutt | (if applicable) | | 604.89 | _17.71_ | Bottom of Well | |
| Installation Method: Over- | drill borehole | | 604.89 * Referenced to a | | Bottom of Boreho | ole |
| | | | * Referenced to a | i National Geodel | ne Datum | |
| | | | CAS | ING MEAS | SUREMENTS | |
| WELL CONS | TRUCTION MATERIALS | | Diameter of Boreh | ole | (inches) | 8.0 |
| | e type of material for each area) | | ID of Riser Pipe | r 3 | (inches) | 2.0 |
| | | | Protective Casing | Length | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC OT | HER: Steel | Riser Pipe Length | to End C | (feet) | 15.69 0.40 |
| Riser Pipe Above W.T. | | HER: | Bottom of Screen to Screen Length (1s | - | t) (feet) | 4.75 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OT | HER: | Total Length of Ca | | (feet) | 20.84 |
| | | | | | - ` 7 | |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | nmental Protectio | n Agency | 7 | | Well (| Completion | Report |
|---------------------------------------|---|-------------------------|----------|--|-------------------|--------------------|---------------|
| Site #: | C | ounty: Mor | itgomer | у | We | II #:MV | W6S |
| Site Name: <u>AEG Coffeen Pov</u> | wer Station CCB Manage | ement Facility | У | | Bor | ehole #:S | B-06a |
| State Plane Coordinate: X 879,021 | <u>.2</u> Y <u>2,513,189.4</u> (o | or) Latitude: | | o ' " | Longitude: | o | |
| Surveyed By: <u>Darren E. Forgy</u> | у | | IL Reg | gistration #:035-0 | 03637 | | |
| Drilling Contractor: Testing Se | ervice Corporation | | Driller | B. Williamson | | | |
| Consulting Firm: Hanson Prof | Pessional Services Inc. | | Geolog | gist: Rhonald W | Hasenyager, | LPG #196-00 | 00246 |
| Drilling Method: Hollow stem | auger | | Drillin | g Fluid (Type): Po | table water | | |
| Logged By: <u>Testing Services</u> | Corp. | | Date S | tarted: 5/4/200 | 06 Date 1 | Finished: 5/ | /4/2006 |
| Report Form Completed By: Rh | nonald W Hasenyager | | Date: | 6/7/2006 | | | |
| ANNULAR SPA | CE DETAILS | | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) |) |
| | | | | 626.67 | 3.57 | Γop of Protective | e Casing |
| | | | | 626.21 | 3.11 | Гор of Riser Pip | e |
| Type of Surface Seal: Concrete | | | | 623.10 | 0.000 | Ground Surface | |
| T CA L C L A D A | 20 11 | | | 620.10 | 3.00 | Γop of Annular : | Sealant |
| Type of Annular Sealant: Benton | | - | | | | | |
| Installation Method: Gravity | | _ | 7 | 616.89 | 6.21 | Static Water Lev | al. |
| Setting Time: +24 hr. | | _ \[\sqrt{\bar{Z}} | <u> </u> | _010.89_ | | (After Completion) | |
| Type of Bentonite Seal Granu | Pellet Slurry | | | <u>-</u> - | | | |
| Installation Method: <u>Gravit</u> | (* ************************************ | | | 620.10 | 3.00 | Γop of Seal | |
| Setting Time: +24 hr. | | | | 613.34 | 9.76 | Гор of Sand Pac | k |
| | | <u> </u> | | 013.31 | | rop or same rac | |
| Type of Sand Pack: Quartz sand | | _ | | 612.06 | 11.04 | Γop of Screen | |
| Grain Size: #5 (sie | | | | | | r | |
| Installation Method: <u>Gravit</u> | y | - | | _607.48_ | 15.62 1 | Bottom of Scree | n |
| Type of Backfill Material: <u>n/a</u> | (if applicable) | _ 🗀 | | 607.02 | 16.08 | Bottom of Well | |
| Installation Method:n/a | (IF we y | _ | | _607.02 | 16.08 1 | Bottom of Boreh | ole |
| | | | | * Referenced to a | National Geodetic | Datum | |
| | | | | CASI | ING MEAS | UREMENTS | |
| WELL CONG | TRUCTION MATERIA | I C | | Diameter of Boreho | ole | (inches) | 7.3 |
| | TRUCTION MATERIAL e type of material for each area) | LS | | ID of Riser Pipe | | (inches) | 2.0 |
| | | | | Protective Casing I | Length | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE P | VC OTHER: (| Steel | Riser Pipe Length | F 10 | (feet) | 14.15 |
| Riser Pipe Above W.T. | | VC OTHER: (| | Bottom of Screen to Screen Length (1s | - | | 0.46 4.58 |
| Riser Pipe Below W.T. | | OTHER: | | Total Length of Ca | | (feet) | 19.19 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviro | nmental Protection A | gency | | | Well (| Completion | Report |
|---------------------------------------|-------------------------------------|------------|------------|---|-----------------|------------------------------------|--------------|
| Site #: | County | : Montg | gomery | | We | ell #:MV | V7S |
| Site Name: AEG Coffeen Po | wer Station CCB Management | t Facility | | | Во | rehole #:S | B-07a |
| State | 1.1 Y 2,514,397.5 (or) L | • | | | | | |
| Surveyed By: Darren E. Forg | y | I | L Regis | tration #:035-0 | 03637 | | |
| Drilling Contractor: Reynolds | Drilling Corp. | I | Oriller: _ | P. McIntire | | | |
| Consulting Firm: Hanson Pro | fessional Services Inc. | (| Geologis | et: Rhonald W | Hasenyager | , LPG #196-00 | 0246 |
| Drilling Method: Hollow sten | n auger | I | Orilling l | Fluid (Type): Po | otable water | | |
| Logged By: Rhonald W Hase | enyager | I | Date Sta | rted:5/9/200 | 06 Date | Finished: 5/ | 9/2006 |
| Report Form Completed By: R | honald W Hasenyager | I | Date: | 6/7/2006 | | | |
| ANNULAR SPA | CE DETAILS | | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | | 627.71 | , , | Top of Protective | e Casing |
| | | | | 627.56 | 3.06_ | Top of Riser Pipe | e |
| Type of Surface Seal: Concrete | | | | 624.50_ | 0.00 | Ground Surface | |
| Type of Annular Sealant: Bento | unite chins | | | 621.70 | 2.80 | Top of Annular S | Sealant |
| Installation Method: Gravi | | | | | | | |
| Setting Time:+24 hr. | | | | 619.60 | 4.90 | Static Water Lev | |
| | | | | | | (After Completion) | 6/1/2006 |
| Type of Bentonite Seal Gran | ular Pellet Slurry (choose one) | | | | | | |
| Installation Method: <u>Gravi</u> | ty | | | 621.70 | 2.80 | Top of Seal | |
| Setting Time: +24 hr. | | | | 616.23 | 8.27 | Top of Sand Pacl | ζ |
| Type of Sand Pack: Quartz san | d | | | | | | |
| Grain Size: #JC50FS (sie | eve size) | | | 614.59 | 9.91 | Top of Screen | |
| Installation Method: <u>Gravi</u> | ty | | | 610.71 | 13.79 | D-# £C | |
| Type of Backfill Material: <u>n/a</u> | (if applicable) | | | 610.71 610.11 | | Bottom of Screen Bottom of Well | 1 |
| Installation Method:n/a | (if applicable) | | | 610.11 | 14.39 | Bottom of Boreh | ole |
| | | | | * Referenced to a | | | |
| | | | | CAS | ING MEAS | UREMENTS | |
| WELL CONS | TRUCTION MATERIALS | | 1 | Diameter of Boreh | ole | (inches) | 8.0 |
| | the type of material for each area) | | | ID of Riser Pipe | | (inches) | 2.0 |
| | | | | Protective Casing 1 | Length | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC | OTHER: (S | | Riser Pipe Length | to End C-: | (feet) | 12.37 |
| Riser Pipe Above W.T. | | OTHER: | | Bottom of Screen t Screen Length (1s | _ | (feet)) (feet) | 0.60 4.48 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC | OTHER: | | Total Length of Ca | | (feet) | 17.45 |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

(inches)

SS304

Well Completion Form (revised 02/06/02)

SS316

| Illinois Environmental Prot | tection Agency | | | Well C | ompletion | Report |
|--|---------------------|------------|---------------------------------------|-------------------|---------------------------------------|---------------|
| Site #: | County: Montgo | omery | | Wel | 1#:MV | V8S |
| Site Name: _AEG Coffeen Power Station CCB N | Management Facility | | | Bore | ehole #:S | B-08a |
| State Plane Coordinate: X 879,776.6 Y 2,514,475 | 8.8 (or) Latitude: | 0 | | Longitude: | · | |
| Surveyed By: Darren E. Forgy | II | L Regist | ration #:035-0 | 03637 | | |
| Drilling Contractor: Reynolds Drilling Corp. | D | Oriller: _ | K. Doetzel | | | |
| Consulting Firm: Hanson Professional Services | Inc. | Geologist | : Rhonald W | Hasenyager, | LPG #196-00 | 00246 |
| Drilling Method: Hollow stem auger | D | Orilling F | luid (Type): Po | otable water | | |
| Logged By: Reynolds Drilling Corp. | С | Date Star | ted:5/10/20 | 06 Date F | inished: 5/ | 10/2006 |
| Report Form Completed By: Rhonald W Hasenya | iger D | Date: | 6/7/2006 | | | |
| ANNULAR SPACE DETAILS | | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) |) |
| | | | 628.26 | . , | op of Protective | e Casing |
| | | T | 627.92 | 3.22_ T | op of Riser Pip | e |
| Type of Surface Seal: Concrete | | | 624.70 | 0.00 | Fround Surface | |
| | | | | | | |
| Type of Annular Sealant: Bentonite chips | | | 622.20 | | op of Annular S | Sealant |
| Installation Method: Gravity | | | | | | |
| Setting Time: +24 hr. | <u>\</u> | | 619.37 | | tatic Water Lev (After Completion) | |
| Type of Bentonite Seal Granular Pellet S | Slurry | | | | (| 0, 1, 200 |
| (choose one) | Sturry | | | | | |
| Installation Method: <u>Gravity</u> | | | 622.20 | 2.50 T | op of Seal | |
| Setting Time: +24 hr. | | | 614.72 | 9.98 T | op of Sand Pac | k |
| Type of Sand Pack: Quartz sand | | | | | | |
| Grain Size: #JC50FS (sieve size) | | | 613.19 | 11.51 T | op of Screen | |
| Installation Method: Gravity | | | | | | |
| · · · · · | | | 608.70 | | Bottom of Screen | 1 |
| Type of Backfill Material: Quartz sand (if applicable) | |] | 608.10 | 16.60 B | Bottom of Well | |
| Installation Method: <u>Gravity</u> | | | 607.62 | | Bottom of Boreh | ole |
| | | | * Referenced to a | National Geodetic | Datum | |
| | | | CAS | ING MEASU | JREMENTS | |
| WELL CONSTRUCTION MAT | TEDIALS | Е | iameter of Boreh | ole | (inches) | 8.0 |
| (Choose one type of material for each | | | O of Riser Pipe | | (inches) | 2.0 |
| | | | rotective Casing I | Length | (feet) | 5.0 |
| Protective Casing SS304 SS316 PT | TFE PVC OTHER: St | | iser Pipe Length ottom of Screen t | o End Com | (feet) | 0.60 |
| | FE PVC OTHER: | | creen Length (1s | - | (feet) | 4.49 |
| Riser Pipe Below W.T. SS304 SS316 PT | FE PVC OTHER: | | otal Length of Ca | | (feet) | 19.82 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviro | onmental Protection Agen | cy | • | Well Comp | oletion | Report |
|--|-------------------------------------|-------------------|---|---------------------|--------------|---------------|
| Site #: | County: M | ontgomery | | Well #: | MW | 9D |
| Site Name: AEG Coffeen Po | ower Station CCB Management Facil | ity | | Borehole # | :S] | B-09 |
| State Plane Coordinate: X 879,67 | 79.7 Y 2,515,666.3 (or) Latitude | e:°_ | '" I | ongitude: | ° | |
| Surveyed By: Darren E. Forg | gy | IL Regis | tration #:035-0036 | 537 | | |
| Drilling Contractor: Reynolds | s Drilling Corp. | Driller: | K. Doetzel | | | |
| Consulting Firm: Hanson Pro | ofessional Services Inc. | Geologis | st: _ Rhonald W Has | senyager, LPG | #196-000 | 0246 |
| Drilling Method: Hollow ster | m auger | Drilling | Fluid (Type): <u>Potab</u> | le water | | |
| Logged By: Reynolds Drilling | ng Corp. | Date Sta | rted: 5/3/2006 | Date Finishe | d:5/3 | 3/2006 |
| Report Form Completed By: Report Form Comple | Chonald W Hasenyager | Date: _ | 6/7/2006 | _ | | |
| ANNULAR SPA | ACE DETAILS | | Elevations Do | epths (BGS) | 0.01 ft.) | |
| | | | 627.84 | 3.24 Top of | Protective | Casing |
| | l E | | 627.52 | 2.92 Top of | Riser Pipe | |
| Type of Surface Seal: Concrete | | | 624.60 | 0.00 Ground | Surface | |
| Type of Annular Sealant: Bent | onite grout | | 621.70 | 2.90 Top of | Annular S | ealant |
| | 7 | | | | | |
| Installation Method: <u>Trem</u> Setting Time: +24 hr. | | ∇ | 572.14 5 | 52.46 Static V | Vater Leve | :l |
| | | <u>*</u> | | | ompletion) (| |
| Type of Bentonite Seal Gran | nular Pellet Slurry (choose one) | | | | | |
| Installation Method: <u>Grav</u> | ` ' ' | \longrightarrow | _582.604 | 2.00 Top of | Seal | |
| Setting Time: 15 min. | | | _580.804 | 3.80 Top of | Sand Pack | |
| Town of Court Dools | | | | | | |
| Type of Sand Pack: Quartz san Grain Size: #JC50FS (si | | | 578.79 4 | 5.81 Top of | Screen | |
| Installation Method: Grav | | | | | | |
| mstanation Method. <u>Grav</u> | ity | | 574.03 5 | 50.57 Bottom | of Screen | |
| Type of Backfill Material: Qua | artz sand (if applicable) | | 573.60 5 | 51.00 Bottom | of Well | |
| Installation Method: Grav | ity | | | | of Boreho | ole |
| | | | * Referenced to a Natio | onal Geodetic Datum | | |
| | | _ | CASINO | G MEASUREM | IENTS | |
| WELL CON | STRUCTION MATERIALS | | Diameter of Borehole | | (inches) | 8.0 |
| | one type of material for each area) | | ID of Riser Pipe | | (inches) | 2.0 |
| | | | Protective Casing Leng | gth | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | | Riser Pipe Length Bottom of Screen to Er | nd Con | (feet) | 52.25 0.43 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | | Screen Length (1st slot | - | (feet) | 4.76 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | | Total Length of Casing | | (feet) | 57.44 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviro | nmental Protection Agen | cy | | Well Cor | npletion | Report |
|--|------------------------------------|------------|--|------------------------|------------------------------------|--------|
| Site #: | County: <u>M</u> | ontgomery | | Well #: | MWS | 9S |
| Site Name: <u>AEG Coffeen Po</u> | wer Station CCB Management Faci | lity | | Boreho | le #:SB | -09a |
| State Plane Coordinate: X 879,68 | 4.9 Y 2,515,666.2 (or) Latitud | e:°_ | | Longitude: | 0 | ' " |
| Surveyed By: Darren E. Forg | sy | _ IL Regis | tration #:035-0 | 03637 | | |
| Drilling Contractor: Reynolds | Drilling Corp. | _ Driller: | K. Doetzel | | | |
| Consulting Firm: Hanson Pro | fessional Services Inc. | _ Geologis | st: Rhonald W | Hasenyager, Ll | PG #196-000 | 246 |
| Drilling Method: Hollow ster | n auger | _ Drilling | Fluid (Type): Po | table water | | |
| Logged By: Reynolds Drillin | ng Corp. | _ Date Sta | rted: 5/3/200 | 06 Date Fini | shed:5/3/ | 2006 |
| Report Form Completed By: Report Form Comple | honald W Hasenyager | _ Date: _ | 6/7/2006 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | 627.84 | ` / | of Protective (| Casing |
| | | = | 627.51 | 2.91_ Top | of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 624.60 | 0.00 Gro | and Surface | |
| | | | 621.35 | | of Annular Se | alant |
| Type of Annular Sealant: Bento | onite chips | | 021.33 | | of Affilular Se | aiaiii |
| Installation Method: <u>Gravi</u> | ty | | | | | |
| Setting Time: +24 hr. | | ∇ | 619.37 | | c Water Level er Completion) 6/ | |
| Type of Bentonite Seal Gran | ular Pellet Slurry | | | | | |
| | (choose one) | | 621.35 | 2 25 Ton | of Sool | |
| Installation Method: <u>Gravi</u> | ty | | 021.33 | | of Seal | |
| Setting Time:+24 hr. | | | 615.49 | 9.11 Top | of Sand Pack | |
| Type of Sand Pack: Quartz san | d | | | | | |
| Grain Size: #JC50FS (sie | eve size) | == | 613.39 | 11.21 Top | of Screen | |
| Installation Method: <u>Gravi</u> | ty | | | | | |
| True of Doolrfill Motorial | | | 608.98 | | om of Screen | |
| Type of Backfill Material: <u>n/a</u> | (if applicable) | | 608.40 | 16.20 Bott | om of Well | |
| Installation Method:n/a | | | 608.40 | 16.20 Bott | om of Borehol | e |
| | | | Referenced to a | National Geodetic Dati | ,iii | |
| | | Г | CASI | ING MEASUR | EMENTS | |
| WELL CONS | STRUCTION MATERIALS | | Diameter of Boreho | ole | (inches) | 8.0 |
| | ne type of material for each area) | | ID of Riser Pipe | amath | (inches) | 2.0 |
| | | | Protective Casing I Riser Pipe Length | Length | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | | Bottom of Screen to | o End Can | (feet) | 0.58 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | | Screen Length (1s | | (feet) | 4.41 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | | Total Length of Ca | | (feet) | 19.11 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviro | nmental Protection Agen | cy | | Well (| Completion | Report |
|------------------------------------|--|------------|---|-------------------|--------------------|--------------|
| Site #: | County: M | ontgomer | у | We | ll #:MW | 10D |
| Site Name: <u>AEG Coffeen Po</u> | wer Station CCB Management Faci | ity | | Bor | ehole #:S | B-10 |
| State Plane Coordinate: X 878,245 | 5.1 Y 2,515,914.0 (or) Latitud | e: | | Longitude: | | |
| Surveyed By: <u>Darren E. Forg</u> | y | IL Reg | istration #:035-00 | 03637 | | |
| Drilling Contractor: Reynolds | Drilling Corp. | _ Driller: | K. Doetzel | | | |
| Consulting Firm: Hanson Pro | fessional Services Inc. | Geolog | ist: Rhonald W l | Hasenyager, | LPG #196-00 | 0246 |
| Drilling Method: Hollow stem | n auger | _ Drilling | g Fluid (Type): <u>Po</u> | table water | | |
| Logged By: Reynolds Drillin | g Corp. | _ Date St | earted: 5/1/200 | 06 Date 1 | Finished: 5/ | 1/2006 |
| Report Form Completed By: R | nonald W Hasenyager | Date: | 6/7/2006 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | 624.72 | 3.52 | Гор of Protective | e Casing |
| | | | 624.42 | 3.22 | Гор of Riser Pipe | e |
| Type of Surface Seal: Concrete | | | 621.20_ | 0.00 | Ground Surface | |
| | | | | 1.43 | Гор of Annular S | Sealant |
| Type of Annular Sealant: Bento | 7 | | | | | |
| Installation Method:Tremi | | | 573.72 | 47.48 | Static Water Lev | al |
| Setting Time: +24 hr. | | Ž | _313.12_ | _47.46_ | (After Completion) | |
| Type of Bentonite Seal Gran | ular Pellet Slurry (choose one) | | | | | |
| Installation Method:Tremi | e | | 619.77 | 1.43 | Γop of Seal | |
| Setting Time: 22 min. | | | 581.65 | 39.55 | Гор of Sand Pacl | ζ. |
| | Y Y | | | | rop or sumar we | - |
| Type of Sand Pack: Quartz sand | | | 579.46 | 41.74 | Γop of Screen | |
| Grain Size: #JC50FS (sie | | | | | r | |
| Installation Method: <u>Gravit</u> | <u>y</u> | | _574.63_ | 46.57 | Bottom of Screen | 1 |
| Type of Backfill Material: Quan | tz sand (if applicable) | | 574.18 | 47.02 | Bottom of Well | |
| Installation Method: Gravit | . 22 | | 572.45 | 48.75 | Bottom of Boreh | ole |
| | | | * Referenced to a | National Geodetic | Datum | |
| | | | CASI | NG MEAS | UREMENTS | |
| WELL CONG | TRUCTION MATERIAL C | | Diameter of Boreho | ole | (inches) | 8.0 |
| | TRUCTION MATERIALS e type of material for each area) | | ID of Riser Pipe | | (inches) | 2.0 |
| | | | Protective Casing I | ength | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | : (Steel) | Riser Pipe Length | F. 1.C | (feet) | 45.06 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE (PVC) OTHER | | Bottom of Screen to Screen Length (1st | | | 0.45 4.73 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | | Total Length of Car | | (feet) | 50.24 |
| | | | | U | (1001) | |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviro | nmental Protection Agen | cy | Well Completion Report |
|--|--|------------------------------------|---|
| Site #: | County: M | ontgomery | Well #:MW10S |
| Site Name: <u>AEG Coffeen Po</u> | wer Station CCB Management Faci | lity | Borehole #:SB-10a |
| State Plane Coordinate: X 878,25 | 0.5 Y 2,515,914.4 (or) Latitud | e:'' | ' Longitude:°'" |
| Surveyed By: Darren E. Forg | y | IL Registration #:035- | 003637 |
| Drilling Contractor: Reynolds | Drilling Corp. | Driller: K. Doetzel | |
| Consulting Firm: Hanson Pro | fessional Services Inc. | Geologist: Rhonald W | Hasenyager, LPG #196-000246 |
| Drilling Method: Hollow ster | n auger | _ Drilling Fluid (Type): _ P | Potable water |
| Logged By: Reynolds Drillin | ng Corp. | Date Started: 5/2/20 | 006 Date Finished: 5/2/2006 |
| Report Form Completed By: Report Form Comple | honald W Hasenyager | Date: 6/7/2006 | |
| ANNULAR SPA | CE DETAILS | Elevations (MSL)* | Depths (0.01 ft.) (BGS) |
| | | 624.55 | 3.35 Top of Protective Casing |
| | | 624.24 | 3.04 Top of Riser Pipe |
| Type of Surface Seal: Concrete | | 621.20 | 0.00 Ground Surface |
| | | 618.83 | |
| Type of Annular Sealant: Bento | 7 | | |
| Installation Method: <u>Gravi</u> | | - (16.20 | 401 |
| Setting Time: +24 hr. | | ☑ 616.29 | 4.91 Static Water Level (After Completion) 6/1/2006 |
| Type of Bentonite Seal Gran | - | | |
| Installation Method: Gravi | (choose one) | 618.83 | 2.37 Top of Seal |
| Setting Time: +24 hr. | | | 0.20 To 00 10 1 |
| <u> </u> | | 611.90 | 9.30 Top of Sand Pack |
| Type of Sand Pack: Quartz san | <u>d</u> | (00.02 | 11.20 T. CC |
| Grain Size: #JC50FS (sie | eve size) | | 11.28 Top of Screen |
| Installation Method: <u>Gravi</u> | ty | 605.44 | 15.76 Bottom of Screen |
| Type of Backfill Material: <u>n/a</u> | (Controll) | 604.90 | 16.30 Bottom of Well |
| Installation Method:n/a | (if applicable) | 604.90 | 16.30 Bottom of Borehole |
| <u> </u> | | | a National Geodetic Datum |
| | | CAS | SING MEASUREMENTS |
| WELL COM | TTDLICTION MATERIAL C | Diameter of Bore | hole (inches) 8.0 |
| | STRUCTION MATERIALS ne type of material for each area) | ID of Riser Pipe | (inches) 2.0 |
| | | Protective Casing | |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | Riser Pipe Length Bottom of Screen | |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | Bottom of Screen | - |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | | |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviro | nmental Protection Agen | cy | | Well Cor | npletion | Report |
|------------------------------------|------------------------------------|------------|--|------------------------|--------------------------------|---------|
| Site #: | County: M | ontgomery | | Well #: | MW | 11D |
| Site Name: <u>AEG Coffeen Po</u> | wer Station CCB Management Faci | lity | | Boreho | le #:S] | B-11 |
| State Plane Coordinate: X 876,749 | 9.6 Y 2,515,976.7 (or) Latitud | e:° | | Longitude: | | ' " |
| Surveyed By: <u>Darren E. Forg</u> | y | _ IL Regis | stration #:035-0 | 03637 | | |
| Drilling Contractor: Reynolds | Drilling Corp. | _ Driller: | K. Doetzel | | | |
| Consulting Firm: Hanson Pro | fessional Services Inc. | _ Geologis | st: Rhonald W | Hasenyager, LI | PG #196-00 | 0246 |
| Drilling Method: Hollow sten | n auger | _ Drilling | Fluid (Type): Po | table water | | |
| Logged By: Reynolds Drillin | ig Corp. | _ Date Sta | rted: 4/27/20 | 06 Date Finis | shed: <u>4/2</u> | 8/2006 |
| Report Form Completed By:R | honald W Hasenyager | _ Date: | 6/7/2006 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | 625.70 | 3.70 Top | of Protective | Casing |
| | | | 625.36 | 3.36_ Top | of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 622.00 | 0.00 Grou | and Surface | |
| | | | 618.89 | | of Annular S | ealant |
| Type of Annular Sealant: Bento | onite grout | | | | of Affilular S | caiaiii |
| Installation Method:Tremi | <u>e</u> | | | | | |
| Setting Time: +24 hr. | | ∇ | 615.97 | | c Water Leve er Completion) | |
| Type of Bentonite Seal Gran | ular Pellet Slurry | | | | | |
| Installation Method: Gravin | (choose one) | | 597.20 | 24.80 Top | of Seal | |
| | ty | | 397.20 | | oi seai | |
| Setting Time: 18 min. | | | 595.59 | | of Sand Pack | |
| Type of Sand Pack: Quartz sand | d | | | | | |
| Grain Size: #JC50FS (sie | eve size) | ≡≡ | 593.69 | | of Screen | |
| Installation Method: Gravit | ty | | | | | |
| Type of Backfill Material: n/a | | | <u>588.96</u> <u>588.50</u> | | om of Screen om of Well | |
| Type of Backfill Material | (if applicable) | | _300.30_ | | om or wen | |
| Installation Method: <u>n/a</u> | | | | Bott | om of Boreho | ole |
| | | | referenced to a | National Geodetic Date | **** | |
| | | Г | CASI | ING MEASUR | EMENTS | |
| WELL CONS | TRUCTION MATERIALS | | Diameter of Boreho | ole | (inches) | 8.0 |
| | ne type of material for each area) | | ID of Riser Pipe | anath | (inches) | 5.0 |
| | | | Protective Casing I Riser Pipe Length | Length | (feet) | 31.67 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | | Bottom of Screen to | o End Cap | | 0.46 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | | Screen Length (1s | | (feet) | 4.73 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | . 11 | Total Length of Ca | | (feet) | 36.86 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | nmental Protectio | n Agency | 7 | | Well (| Completion | n Report |
|---------------------------------------|--|----------------------|---------|---|-----------------|--|--------------|
| Site #: | C | ounty: Mor | itgomer | у | We | ell #:MW | V11S |
| Site Name: AEG Coffeen Pov | wer Station CCB Manage | ement Facilit | у | | Во | rehole #: S | B-11a |
| State Plane Coordinate: X 876,749 | 0.4 Y 2,515,971.2 (c | or) Latitude: | | 0 ! !! | Longitude | ·° | |
| Surveyed By: Darren E. Forgy | У | | IL Reg | sistration #:035-00 | 03637 | | |
| Drilling Contractor: Reynolds | Drilling Corp. | | Driller | : K. Doetzel | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | | Geolog | gist: Rhonald W l | Hasenyager | , LPG #196-00 | 00246 |
| Drilling Method: Hollow stem | auger | | Drillin | g Fluid (Type): <u>Po</u> | table water | | |
| Logged By: Reynolds Drilling | g Corp. | | Date S | tarted: 4/28/200 | 06 Date | Finished: 4/2 | 28/2006 |
| Report Form Completed By: R | nonald W Hasenyager | | Date: | 6/7/2006 | | | |
| ANNULAR SPA | CE DETAILS | | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) |) |
| | | | | 625.47 | 3.47 | Top of Protective | e Casing |
| | | | | 625.16 | 3.16 | Top of Riser Pip | e |
| Type of Surface Seal: Concrete | | | | 622.00 | 0.00 | Ground Surface | |
| | | | | 620.00 | 2.00 | Top of Annular S | Sealant |
| Type of Annular Sealant: Benton | | - 🎵 | R | | | • | |
| Installation Method: <u>Gravit</u> | | - _ | | 616.70 | | | |
| Setting Time: +24 hr. | | _ \[\sum_{\sum} | _ | 616.58 | 5.42 | Static Water Lev (After Completion) | |
| Type of Bentonite Seal Grand | | | | • | | | |
| Installation Method: Gravit | (choose one) V | | | 620.00 | 2.00 | Top of Seal | |
| Setting Time: 26 min. | | | | (15.05 | | T | |
| | | | | 615.25 | 6.75 | Top of Sand Pac | K |
| Type of Sand Pack: Quartz sand | 1 | _ | | (12.11 | 0.00 | T. CO | |
| Grain Size: #JC50FS (sie | ve size) | | | _613.11_ | 8.89 | Top of Screen | |
| Installation Method: <u>Gravit</u> | У | - | | 608.37 | 13.63 | Bottom of Screen | n |
| Type of Backfill Material: <u>n/a</u> | (Continue) | _ 🗏 | | 607.92 | | Bottom of Well | 11 |
| Installation Method:n/a | (if applicable) | | | 607.92 | 14.08 | Bottom of Boreh | iole |
| instantion (viction) | | | | * Referenced to a | | | |
| | | | | CASI | ING MEAS | UREMENTS | |
| WELL CONG | TRUCTION MATERIA | T C | | Diameter of Boreho | ole | (inches) | 8.0 |
| | TRUCTION MATERIA e type of material for each area) | LS | | ID of Riser Pipe | | (inches) | 2.0 |
| | | | | Protective Casing I | Length | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE F | PVC OTHER: (| Steel | Riser Pipe Length | F 16 | (feet) | 12.04 |
| Riser Pipe Above W.T. | | OTHER: | | Bottom of Screen to Screen Length (1st | - | (feet) | 0.46 4.74 |
| Riser Pipe Below W.T. | | OTHER: | | Total Length of Car | | (feet) | 17.24 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | nmental Protection Agend | c y | Well Completion Report |
|---|----------------------------------|---------------------------------------|--------------------------------|
| Site #: | County: Mc | ontgomery | Well #:MW12D |
| Site Name: <u>AEG Coffeen Pow</u> | ver Station CCB Management Facil | ity | Borehole #: SB-12 |
| State Plane Coordinate: X 875,515. | .1 Y 2,515,900.6 (or) Latitude | : | Longitude:°'" |
| Surveyed By: <u>Darren E. Forgy</u> | ī | IL Registration #: 035-0 | 03637 |
| Drilling Contractor: Testing Se | ervice Corporation | Driller: B. Williamson | |
| Consulting Firm: Hanson Profe | essional Services Inc. | Geologist: Rhonald W | Hasenyager, LPG #196-000246 |
| Drilling Method: Hollow stem | auger | Drilling Fluid (Type): Po | otable water |
| Logged By: Reynolds Drilling | g Corp. | Date Started:5/10/20 | 06 Date Finished:5/10/2006 |
| Report Form Completed By: Rho | onald W Hasenyager | Date:6/7/2006 | |
| ANNULAR SPAC | CE DETAILS | Elevations (MSL)* | Depths (0.01 ft.) |
| | | | Top of Protective Casing |
| | | | 2.83_ Top of Riser Pipe |
| Type of Surface Seal: Concrete | | 622.20 | Ground Surface |
| T CA LC LA DA | | 619.43 | Top of Annular Sealant |
| Type of Annular Sealant: Benton | 7 | | |
| Installation Method:Tremie Setting Time: +24 hr. | | ∑ 575.30 | 46.90 Static Water Level |
| Setting Time | | <u> </u> | (After Completion) 6/1/2006 |
| Type of Bentonite Seal Granu | Pellet Slurry (choose one) | | |
| Installation Method: <u>Gravity</u> | | _585.50_ | <u>36.70</u> Top of Seal |
| Setting Time: +24 hr. | | 581.69 | 40.51 Top of Sand Pack |
| Type of Cond Dealty | | | |
| Type of Sand Pack: Quartz sand Grain Size: #5 (siev | | | 42.46 Top of Screen |
| Installation Method: Gravity | | | |
| | | _575.21_ | 46.99 Bottom of Screen |
| Type of Backfill Material: <u>n/a</u> | (if applicable) | | 47.47 Bottom of Well |
| Installation Method: Over-de | rill borehole | 572.20 | 50.00 Bottom of Borehole |
| | | * Referenced to a | National Geodetic Datum |
| | | CAS | ING MEASUREMENTS |
| WELL CONST | FRUCTION MATERIALS | Diameter of Boreho | |
| | type of material for each area) | ID of Riser Pipe | (inches) 2.0 |
| | | Protective Casing I Riser Pipe Length | Length (feet) 5.0 (feet) 45.29 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER: | | o End Cap (feet) 0.48 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER: | | • |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER: | | |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviro | nmental Protection Age | ncy | | Well C | completion | Report |
|--|------------------------------------|--|---------------------------------------|-------------------|--------------------|----------|
| Site #: | County:] | Montgomer | y | Wel | 1#:MW | 12S |
| Site Name: AEG Coffeen Po | ower Station CCB Management Fac | cility | | Bore | ehole #:S | B-12a |
| State Plane Coordinate: X 875,52 | 0.1 Y 2,515,900.5 (or) Latitu | ıde: | | Longitude: | o | |
| Surveyed By: Darren E. Forg | зу | IL Reg | istration #: <u>035-0</u> | 03637 | | |
| Drilling Contractor: Testing S | Service Corporation | Driller | B. Williamson | | | |
| Consulting Firm: Hanson Pro | fessional Services Inc. | Geolog | sist: Rhonald W | Hasenyager, | LPG #196-00 | 0246 |
| Drilling Method: Hollow ster | n auger | Drilling | g Fluid (Type): Po | table water | | |
| Logged By: Reynolds Drillin | ng Corp. | Date S | tarted:5/10/20 | 06 Date F | Finished: 5/1 | 0/2006 |
| Report Form Completed By: Report Form Comple | honald W Hasenyager | Date: _ | 6/7/2006 | | | |
| ANNULAR SPA | ACE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | 625.58 | 3.38_ T | op of Protective | Casing |
| | | | 625.10 | 2.90 T | op of Riser Pipe | : |
| Type of Surface Seal: Concrete | | | 622.20 | 0.00 0 | Ground Surface | |
| | | | 619.20 | 3.00 T | Top of Annular S | Sealant |
| Type of Annular Sealant: Bento | 7 | | | | | |
| Installation Method: <u>Gravi</u> Setting Time: +24 hr. | | $\left \begin{array}{c} \downarrow \\ \searrow \end{array}\right $ | 615.44 | 6.76 S | Static Water Leve | al a |
| Setting Time | | \ | | | (After Completion) | |
| Type of Bentonite Seal Gran | nular Pellet Slurry (choose one) | | | | | |
| Installation Method: <u>Gravi</u> | ty | X X | 619.20 | 3.00 T | op of Seal | |
| Setting Time: 18 min. | | | 613.95 | 8.25 T | op of Sand Pack | ζ. |
| Type of Sand Books | , | | | | | |
| Type of Sand Pack: Quartz san Grain Size: #5 (si | | | 611.59 | 10.61 T | op of Screen | |
| Installation Method: Gravi | | | | | | |
| | · | | 607.02 | | Bottom of Screen | 1 |
| Type of Backfill Material:n/a_ | (if applicable) | | 606.59 | 15.61 B | Bottom of Well | |
| Installation Method:n/a | | | 606.59 | 15.61 B | Bottom of Boreh | ole |
| | | | · Referenced to a | National Geodetic | Datum | |
| | | | CAS | ING MEASU | JREMENTS | |
| WELL CONS | STRUCTION MATERIALS | | Diameter of Boreho | ole | (inches) | 7.3 |
| | ne type of material for each area) | | ID of Riser Pipe | anath | (inches) | 5.0 |
| | | | Protective Casing I Riser Pipe Length | zugu | (feet) | 13.51 |
| Protective Casing | SS304 SS316 PTFE PVC OTH | ER: Steel | Bottom of Screen to | o End Can | <u> </u> | 0.43 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTH | ER: | Screen Length (1s | _ | (feet) | 4.57 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTH | ER: | Total Length of Ca | | (feet) | 18.51 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviro | nmental Protection Age | ency | | Well C | ompletion | Report |
|--|--|------------|--|---------------------|--------------------|---------------|
| Site #: | County: _ | Montgomer | ту | Well | I#:MW | 13D |
| Site Name: <u>AEG Coffeen Po</u> | wer Station CCB Management F | acility | | Bore | ehole #:S | B-13 |
| State Plane Coordinate: X 874,694 | 4.3 Y 2,513,929.9 (or) Lati | tude: | <u> </u> | Longitude: | <u> </u> | |
| Surveyed By: Darren E. Forg | у | IL Reg | gistration #:035-00 | 03637 | | |
| Drilling Contractor: Testing S | ervice Corporation | Driller | B. Williamson | | | |
| Consulting Firm: Hanson Pro | fessional Services Inc. | Geolo | gist: Rhonald W l | Hasenyager, | LPG #196-00 | 0246 |
| Drilling Method: Hollow sten | n auger | Drillin | g Fluid (Type): <u>Po</u> | table water | | |
| Logged By: Reynolds Drillin | g Corp. | Date S | tarted:5/9/200 | 06 Date F | inished:5/ | 9/2006 |
| Report Form Completed By: R | honald W Hasenyager | Date: | 6/7/2006 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | 626.33 | 3.63_ T | op of Protective | Casing |
| | | | 625.87 | 3.17 T | op of Riser Pipe | 2 |
| Type of Surface Seal: Concrete | | | 622.70 | 0.00 G | Fround Surface | |
| Time of American Contents. Donto | mita amout | | 619.64 | 3.06 T | op of Annular S | Sealant |
| Type of Annular Sealant: Bento | \ | | | | | |
| Installation Method:Tremi Setting Time:+24 hr. | | | 566.67 | 56.03 S | tatic Water Lev | al |
| Setting Time. 124 m. | | \ __\ | | | (After Completion) | |
| Type of Bentonite Seal Gran | ular Pellet Slurry — (choose one) | | - - | | | |
| Installation Method: Gravit | (* * * * * * * * * * * * * * * * * * * | | 577.48 | 45.22 T | op of Seal | |
| Setting Time: +24 hr. | | | 574.76 | 47.94 T | op of Sand Pack | ζ |
| Tyme of Sand Dealy | | | | | • | |
| Type of Sand Pack: Quartz sand Grain Size: #5 (sic | | | 572.89 | _49.81 T | op of Screen | |
| Installation Method: Gravit | | | | | | |
| instantation inclined. Otavi | ., | | _568.10 | | Sottom of Screen | 1 |
| Type of Backfill Material:n/a_ | (if applicable) | | _567.70_ | 55.00 B | Sottom of Well | |
| Installation Method: <u>n/a</u> | | | 567.70 | | Sottom of Boreh | ole |
| | | | * Referenced to a | National Geodetic | Datum | |
| | | | CASI | ING MEASU | JREMENTS | |
| WELL CONS | TRUCTION MATERIALS | | Diameter of Boreho | ole | (inches) | 8.0 |
| | type of material for each area) | | ID of Riser Pipe | | (inches) | 2.0 |
| | | | Protective Casing I | Length | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC OT | HER: Steel | Riser Pipe Length Bottom of Screen to | o End Con | (feet) | 52.98 0.40 |
| Riser Pipe Above W.T. | | HER: | Screen Length (1st | - | (feet) | 4.79 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OT | HER: | Total Length of Car | | (feet) | 58.17 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviro | nmental Protection Agen | cy | Well Completion Report |
|--|--|--------------------------------------|---|
| Site #: | County: M | ontgomery | Well #: MW13S |
| Site Name: <u>AEG Coffeen Po</u> | wer Station CCB Management Faci | lity | Borehole #: SB-13a |
| State Plane Coordinate: X 874,69 | 5.7 Y 2,513,925.3 (or) Latitud | e:' | Longitude:°'" |
| Surveyed By: Darren E. Forg | S.Y. | IL Registration #:035- | -003637 |
| Drilling Contractor: <u>Testing S</u> | service Corporation | Driller:B. Williamso | n |
| Consulting Firm: Hanson Pro | fessional Services Inc. | Geologist: Rhonald W | / Hasenyager, LPG #196-000246 |
| Drilling Method: Hollow ster | n auger | Drilling Fluid (Type):I | Potable water |
| Logged By: Reynolds Drillin | ng Corp. | _ Date Started:5/9/20 | 006 Date Finished: 5/9/2006 |
| Report Form Completed By: Report Form Comple | honald W Hasenyager | Date:6/7/2006 | |
| ANNULAR SPA | ACE DETAILS | Elevations (MSL)* | Depths (0.01 ft.) |
| | _ | 626.42 | 3.72 Top of Protective Casing |
| | | | 3.22 Top of Riser Pipe |
| Type of Surface Seal: Concrete | | 622.70 | 0.00 Ground Surface |
| | | 619.35 | 3.35 Top of Annular Sealant |
| Type of Annular Sealant: Bento | 7 | | |
| Installation Method: <u>Gravi</u> | | | 0.24 |
| Setting Time: +24 hr. | | ☑ 614.46 | 8.24 Static Water Level (After Completion) 6/1/2006 |
| Type of Bentonite Seal Gran | - | | |
| Installation Method: Gravi | (choose one) | 619.35 | |
| Setting Time: 21 min. | | 612.65 | 10.05 T CC ID I |
| | | 612.65 | 10.05 Top of Sand Pack |
| Type of Sand Pack: Quartz san | d | 611.27 | 11.43 Top of Screen |
| Grain Size: #5 (si | | | |
| Installation Method: <u>Gravi</u> | ty | 606.47 | 16.23 Bottom of Screen |
| Type of Backfill Material:n/a_ | (if applicable) | 606.08 | 16.62 Bottom of Well |
| Installation Method:n/a | (II applicable) | 606.08 | 16.62 Bottom of Borehole |
| | | * Referenced to | o a National Geodetic Datum |
| | | CA | SING MEASUREMENTS |
| WELL COM | | Diameter of Bore | chole (inches) 7.3 |
| | STRUCTION MATERIALS ne type of material for each area) | ID of Riser Pipe | (inches) 2.0 |
| | | Protective Casing | _ |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | Riser Pipe Length Riser Pipe Length | h (feet) 14.65 h to End Cap (feet) 0.39 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | Bottom of Screen | • |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | | |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environmen | tal Protection Agenc | y | | Well Co | ompletion | Report |
|---|---------------------------|------------|---------------------------------------|---------------------|-------------------|---------|
| Site #: | County: Mo | ntgomery | | Well | #:MW | 14S |
| Site Name: AEG Coffeen Power Stat | ion CCB Management Facili | ty | | Borel | nole #:Sl | o-14a |
| State Plane Coordinate: X 875,737.8 Y | 2,514,125.9 (or) Latitude | · | | Longitude: _ | 0 | _'" |
| Surveyed By: Darren E. Forgy | | IL Regis | tration #:035-0 | 03637 | | |
| Drilling Contractor: <u>Testing Service C</u> | Corporation | Driller: | B. Williamson | | | |
| Consulting Firm: Hanson Professiona | l Services Inc. | Geologis | t: Rhonald W | Hasenyager, | LPG #196-00 | 0246 |
| Drilling Method: Hollow stem auger | | Drilling l | Fluid (Type): Po | otable water | | |
| Logged By: Reynolds Drilling Corp. | | Date Star | rted: 5/2/200 | Date Fi | nished: 5/2 | 2/2006 |
| Report Form Completed By: Rhonald V | W Hasenyager | Date: | 6/7/2006 | | | |
| ANNULAR SPACE DE | ETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | 627.23 | , , | op of Protective | Casing |
| | T _E | | 626.82 | 2.22_ To | op of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 624.60 | 0.00 Gr | ound Surface | |
| | | | 622.20 | | op of Annular S | ealant |
| Type of Annular Sealant: Bentonite chip | s | | 022.20 | TC | op of Allifular S | Calalit |
| Installation Method: Gravity | | | | | | |
| Setting Time: +24 hr. | | ∇ | 620.11 | | atic Water Leve | |
| Type of Bentonite Seal Granular | Pellet Slurry | | | | | |
| (6 | Phoose one) | | (22.20 | 2.40 | 66. 1 | |
| Installation Method: <u>Gravity</u> | | | 622.20 | | pp of Seal | |
| Setting Time: 23 min. | | | 613.67 | 10.93 To | p of Sand Pack | |
| Type of Sand Pack: Quartz sand | | | | | | |
| Grain Size: #5 (sieve size) | | | 612.34 | 12.26 To | op of Screen | |
| Installation Method: Gravity | | | | | | |
| T CD LCHA(: 1 / | | | 607.58 | | ottom of Screen | |
| Type of Backfill Material: <u>n/a</u> | (if applicable) | | 607.22 | 17.38 Bo | ottom of Well | |
| Installation Method:n/a | | | 607.22 | | ottom of Boreho | ole |
| | | | * Referenced to a | National Geodetic D | vatum | |
| | | _ | CAS | ING MEASU | REMENTS | |
| WELL CONSTRUCT | ION MATERIALS | | Diameter of Boreh | ole | (inches) | 8.0 |
| (Choose one type of ma | | | D of Riser Pipe | 1 | (inches) | 2.0 |
| | | | Protective Casing I | Length | (feet) | 5.0 |
| Protective Casing SS304 | SS316 PTFE PVC OTHER: | (C) 1) | Riser Pipe Length Bottom of Screen t | o End Can | (feet) | 0.36 |
| Riser Pipe Above W.T. SS304 | SS316 PTFE PVC OTHER: | | Screen Length (1s | | (feet) | 4.76 |
| Riser Pipe Below W.T. SS304 | SS316 PTFE PVC OTHER: | | Гotal Length of Ca | | (feet) | 19.60 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

ILLINOIS DEPARTMENT OF PUBLIC HEALTH DIVISION OF ENVIRONMENTAL HEALTH 525 W. JEFFERSON ST. SPRINGFIELD, IL 62761

WATER WELL SEALING FORM

TYPE OR PRESS FIRMLY

RETURN ALL COPIES TO IDPH OR LOCAL HEALTH DEPARTMENT

This form shall be submitted to this Department or the local health department not more than 30 days after a water well, boring or monitoring well is sealed. Such wells are to be sealed not more than 30 days after they are abandoned in accordance with the sealing requirements in the Water Well Construction Code. THE LOCAL HEALTH DEPARTMENT OR REGIONAL PUBLIC HEALTH DEPARTMENT MUST BE NOTIFIED AT LEAST 48 HOURS PRIOR TO SEALING.

| Ownership (Name of Controlling Party) AEG C | Coffeen Power Stat | tion | | (| (G104) | |
|---|--------------------|----------|------------------|-------------|-----------|---|
| Well Location 134 CIPS Trail | | Co | ffeen | Mo | ontgomery | |
| Address - Lot Number | | | City | C | County | |
| General Description Township 7 (N) | XX) Range | 3 | _ (K) (W) | \$ | Section | 1 |
| SEQuarter of theNE | _Quarter of the _ | NE | QuQu | arter | | |
| Year Drilled2010 | | | | | | |
| Drilling Permit Number (and date, if known) n/a | | | | | | |
| Type of Well Bored Drilled_ ✓ | _ Other | | | | | |
| Total Depth 20.0 ft. Diam | neter (inches) | 2 | | | | |
| Formation clear of obstruction Yes | | | | | | |
| DETAILS OF PLUGGING | | | | | | |
| Filled with Bentonite grout (cement or other materials) | from | 0.5 | to20. | 0ft. | | |
| | | | | | | |
| Kind of plug Random soil | from | 0 | to0.5 | ft. | | |
| Filled with | from | | to | ft. | | |
| Kind of plug | from | | to | ft. | | |
| Filled with | from | | to | ft. | | |
| Kind of plug | from | | to | ft. | | |
| CASING RECORD Upper 2 feet of casing remov | ed <u>√</u> Ye | es | No | | | |
| Date well was sealed Month October D | ay8 | Year_ | 2010 | | | |
| Licensed water well driller or other person approv | ed by the Departi | ment pe | rforming we | ll sealing. | | |
| Rhonald W. Hasenyager, L.P.G. | 196-000 | 246 | | | | |
| Name | Complete | e Licens | e Number | | | |
| Hanson Professional Services Inc., 1525 S. 6th St. | Springfi | eld | | IL 62703 | | |
| Address | City | | | State/ZIP | | |

This state agency is requesting disclosure of information that is necessary to accomplish the statutory purpose as outlined under Public Act 85-0863. Disclosure of this information is mandatory. This form has been approved by the Forms Management Center.

IL 482-0631

| Illinois Environmental Protection Agen | ncy Well Completion Report |
|---|---|
| Site #: County: N | Montgomery Well #:MW15D |
| Site Name: _ AEG Coffeen Power Station CCB Management Fac | Borehole #: SB-15b |
| State Plane Coordinate: X 875,970.5 Y 2,515,080.7 (or) Latitu | de:°'" Longitude:°'" |
| Surveyed By: Darren E. Forgy | IL Registration #:035-003637 |
| Drilling Contractor: Testing Service Corporation | Driller: B. Williamson |
| Consulting Firm: Hanson Professional Services Inc. | Geologist: Rhonald W Hasenyager, LPG #196-000246 |
| Drilling Method: Hollow stem auger | Drilling Fluid (Type): Potable water |
| Logged By: Reynolds Drilling Corp. | Date Started:4/24/2006 Date Finished:4/25/2006 |
| Report Form Completed By: Rhonald W Hasenyager | Date:6/7/2006 |
| ANNULAR SPACE DETAILS | Elevations Depths (0.01 ft.) (MSL)* (BGS) |
| | 626.93 -3.13 Top of Protective Casing |
| | |
| Type of Surface Seal: Concrete | 623.80 0.00 Ground Surface |
| | 620.55 3.25 Top of Annular Sealant |
| Type of Annular Sealant: Bentonite grout | |
| Installation Method:Tremie | |
| Setting Time:+24 hr. | |
| Type of Bentonite Seal Granular Pellet Slurry | |
| (choose one) Installation Method: Gravity | 594.80 29.00 Top of Seal |
| | |
| Setting Time: +24 hr. | |
| Type of Sand Pack: Quartz sand | |
| Grain Size: #5 (sieve size) | |
| Installation Method: Gravity | |
| Type of Backfill Material: n/a | 585.35 38.45 Bottom of Screen 585.00 38.80 Bottom of Well |
| (if applicable) | |
| Installation Method: Re-drill borehole | |
| | |
| | CASING MEASUREMENTS |
| WELL CONSTRUCTION MATERIALS | Diameter of Borehole (inches) 8.0 ID of Riser Pipe (inches) 2.0 |
| (Choose one type of material for each area) | ID of Riser Pipe (inches) 2.0 Protective Casing Length (feet) 5.0 |
| | Riser Pipe Length (feet) 36.32 |
| Protective Casing SS304 SS316 PTFE PVC OTHER | Bottom of Screen to End Cap (feet) 0.36 |
| Riser Pipe Above W.T. SS304 SS316 PTFE PVC OTHE | |
| Riser Pipe Below W.T. SS304 SS316 PTFE PVC OTHE | |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

ILLINOIS DEPARTMENT OF PUBLIC HEALTH DIVISION OF ENVIRONMENTAL HEALTH

525 W. JEFFERSON ST. SPRINGFIELD, IL 62761

Sealing Form for MW15D - Original Mislabelled as MW15S

WATER WELL SEALING FORM

TYPE OR PRESS FIRMLY

RETURN ALL COPIES TO IDPH OR LOCAL HEALTH DEPARTMENT

This form shall be submitted to this Department or the local health department not more than 30 days after a water well, boring or monitoring well is sealed. Such wells are to be sealed not more than 30 days after they are abandoned in accordance with the sealing requirements in the Water Well Construction Code. THE LOCAL HEALTH DEPARTMENT OR REGIONAL PUBLIC HEALTH DEPARTMENT MUST BE NOTIFIED AT LEAST 48 HOURS PRIOR TO SEALING.

| Well Location 134 CIPS Trail | | Со | offeen | | Ν | Iontgome: | rv |
|---|---------------|---------|--------------------|----------|------|-----------|----|
| Address - Lot Number | | | City | | | County | |
| General Description Township 7 (N) | Range | 3 | _() K()(W) | | | Section _ | |
| SEQuarter of theNEQu | uarter of the | NE | E (| Quarter | ŗ | | |
| Year Drilled 2010 | | | | | | | |
| Drilling Permit Number (and date, if known)n/a | | | | | | | |
| Type of Well Bored Drilled_ ✓ | Other | | | | | | |
| Total Depth 20.0 ft. Diamete | r (inches) | 2 | | | _ | | |
| Formation clear of obstruction Yes | | | | | | | |
| DETAILS OF PLUGGING | | | | | | | |
| Filled with Bentonite grout (cement or other materials) | from | 0.5 | to | 20.0 | _ft. | | |
| | | 0 | | 0.5 | | | |
| Kind of plug Random soil | from | | to | 0.3 | _ft. | | |
| Filled with | from | | to | | _ft. | | |
| Kind of plug | from | | to | | _ft. | | |
| Filled with | from | | to | | _ft. | | |
| Kind of plug | from | | to | | _ft. | | |
| CASING RECORD Upper 2 feet of casing removed | ✓ Ye | es | No | | | | |
| 0.4.1 | 8 | Year_ | 2010 | · | | | |
| Date well was sealed Month October Day | | | | wall saa | ling | | |
| Date well was sealed Month October Day_ Licensed water well driller or other person approved by | y the Departi | ment pe | rforming | wen sea | mng. | | |
| | 196-0002 | • | rforming | wen sea | g. | | |

This state agency is requesting disclosure of information that is necessary to accomplish the statutory purpose as outlined under Public Act 85-0863. Disclosure of this information is mandatory. This form has been approved by the Forms Management Center.

IL 482-0631

| Illinois Environ | nmental Protectio | on Agency | y | | Well (| Completion | Report |
|---------------------------------------|--|-------------------------------------|----------|--|------------------|--|---------------|
| Site #: | | County: <u>Mor</u> | ntgomer | у | We | ell #:MW | /15S |
| Site Name: <u>AEG Coffeen Pov</u> | wer Station CCB Manag | ement Facilit | у | | Bo: | rehole #: S | B-15a |
| State Plane Coordinate: X 875,971 | .1 Y 2,515,076.3 (| or) Latitude: | | o ' " | Longitude | ·° | |
| Surveyed By: Darren E. Forgy | У | | IL Reg | gistration #:035-0 | 003637 | | |
| Drilling Contractor: Testing Se | ervice Corporation | | Driller | B. Williamson | l . | | |
| Consulting Firm: Hanson Prof | Pessional Services Inc. | | Geolog | gist: Rhonald W | Hasenyager | , LPG #196-00 | 00246 |
| Drilling Method: Hollow stem | auger | | Drillin | g Fluid (Type): Po | otable water | | |
| Logged By: Reynolds Drilling | g Corp. | | Date S | tarted: 4/25/20 | 006 Date | Finished: 4/2 | 25/2006 |
| Report Form Completed By: Rh | nonald W Hasenyager | | Date: | 6/7/2006 | | | |
| ANNULAR SPA | CE DETAILS | | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | , |
| | | | | 627.06 | -3.26 | Top of Protective | e Casing |
| | | | | 626.60 | 2.80 | Top of Riser Pip | e |
| Type of Surface Seal: Concrete | | | | 623.80 | 0.00 | Ground Surface | |
| | | | | 623.30 | 0.50 | Top of Annular S | Sealant |
| Type of Annular Sealant: Benton | nite chips | - 1 | | | | 1 | |
| Installation Method: <u>Gravit</u> | | _ | | | | | |
| Setting Time: +24 hr. | | \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ | <u>Z</u> | 618.81 | 4.99 | Static Water Lev (After Completion) | |
| Type of Bentonite Seal Granu | | | | - - | | | |
| Installation Method: Gravit | (choose one) | | | 614.30 | 9.50 | Top of Seal | |
| Setting Time: 20 min. | | | | | | • | |
| <u> </u> | | | | 611.60 | 12.20 | Top of Sand Pac | K |
| Type of Sand Pack: Quartz sand | 1 | _ | | (00.20 | 1.4.41 | T. 60 | |
| Grain Size: #5 (sie | ve size) | | | 609.39 | _14.41_ | Top of Screen | |
| Installation Method: <u>Gravity</u> | У | - | | 604.64 | 19.16 | Bottom of Screen | 1 |
| Type of Backfill Material: <u>n/a</u> | (if applicable) | | 3 | 604.18 | | Bottom of Well | 1 |
| Installation Method:n/a | (if applicable) | | | 604.18 | 19.62 | Bottom of Boreh | ole |
| instantion (viction). | | | | | National Geodeti | | |
| | | | | CAS | ING MEAS | UREMENTS | |
| WELL CONG | TDIICTIONI MA TEDIA | I C | | Diameter of Boreh | ole | (inches) | 8.0 |
| | TRUCTION MATERIA e type of material for each area) | LS | | ID of Riser Pipe | | (inches) | 2.0 |
| | | | | Protective Casing | _ | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE | PVC OTHER: (| Steel | Riser Pipe Length | | (feet) | 17.28 |
| Riser Pipe Above W.T. | | PVC OTHER: | | Bottom of Screen to Screen Length (1st | - | | 19.62 4.77 |
| Riser Pipe Below W.T. | | PVC OTHER: | | Total Length of Ca | | (feet) | 41.67 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

ILLINOIS DEPARTMENT OF PUBLIC HEALTH DIVISION OF ENVIRONMENTAL HEALTH 525 W. JEFFERSON ST. SPRINGFIELD, IL 62761

WATER WELL SEALING FORM

TYPE OR PRESS FIRMLY

RETURN ALL COPIES TO IDPH OR LOCAL HEALTH DEPARTMENT

This form shall be submitted to this Department or the local health department not more than 30 days after a water well, boring or monitoring well is sealed. Such wells are to be sealed not more than 30 days after they are abandoned in accordance with the sealing requirements in the Water Well Construction Code. THE LOCAL HEALTH DEPARTMENT OR REGIONAL PUBLIC HEALTH DEPARTMENT MUST BE NOTIFIED AT LEAST 48 HOURS PRIOR TO SEALING.

| Ownership (Name of Controlling Party) AEG C | offeen Power Stat | ion | | (G104) |) |
|---|-------------------|-----------|---------------|------------|------|
| Well Location 134 CIPS Trail | | Coffe | een | Montgon | nery |
| Address - Lot Number | | | City | County | 7 |
| General Description Township 7 (N) | ⊗ Range | 3 (| K)(W) | Section | 10 |
| SEQuarter of theNE | _Quarter of the _ | NE | Qua | arter | |
| Year Drilled 2010 | | | | | |
| Drilling Permit Number (and date, if known)n/a | | | | | _ |
| Type of Well Bored Drilled_ ✓ | | | | | |
| Total Depth 20.0 ft. Diame | eter (inches) | 2 | | | |
| Formation clear of obstructionYes | | | | | |
| DETAILS OF PLUGGING | | | | | |
| Filled with Bentonite grout (cement or other materials) | from | 0.5 | _to20.0 | <u>ft.</u> | |
| | | | 0.5 | C4 | |
| 1 0 | | | | | |
| Filled with | from | | _to | ft. | |
| Kind of plug | from | | _to | ft. | |
| Filled with | from | | _to | ft. | |
| Kind of plug | from | | _to | ft. | |
| CASING RECORD Upper 2 feet of casing remove | ed <u>√</u> Ye | s | No | | |
| Date well was sealed Month October Da | ay8 | Year | 2010 | | |
| Licensed water well driller or other person approve | ed by the Departi | nent perf | orming wel | l sealing. | |
| Rhonald W. Hasenyager, L.P.G. | 196-0002 | 246 | | | |
| Name | Complete | License 1 | Number | | _ |
| Hanson Professional Services Inc., 1525 S. 6th St. | Springfie | eld | | IL 62703 | _ |
| Address | City | | | State/ZIP | |

This state agency is requesting disclosure of information that is necessary to accomplish the statutory purpose as outlined under Public Act 85-0863. Disclosure of this information is mandatory. This form has been approved by the Forms Management Center.

IL 482-0631

| Illinois Enviro | nmental Protection Agend | e y | | Well (| Completion | Report |
|---|-----------------------------------|---------------------|-------------------------------------|-----------------|--|----------|
| Site #: | County:Mo | ontgomery | r | We | ell #:MW | 16D |
| Site Name: AEG Coffeen Po | wer Station CCB Management Facil | ity | | Во | rehole #:S | 3-16b |
| State Plane Coordinate: X 877,354 | 4.9 Y 2,515,079.4 (or) Latitude | :° | | Longitude | ::° | |
| Surveyed By: Darren E. Forg | у | IL Regi | stration #: <u>035-0</u> | 03637 | | |
| Drilling Contractor: Reynolds | Drilling Corp. | Driller: | K. Doetzel | | | |
| Consulting Firm: Hanson Pro- | fessional Services Inc. | Geologi | st: Rhonald W | Hasenyager | ; LPG #196-00 | 0246 |
| Drilling Method: Hollow sten | n auger | Drilling | Fluid (Type): Po | otable water | | |
| Logged By: Rhonald W Hase | enyager | Date Sta | arted: 4/21/20 | <u>06</u> Date | Finished: 4/2 | 25/2006 |
| Report Form Completed By: R | honald W Hasenyager | Date: _ | 6/7/2006 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | 629.68 | ` / | Top of Protective | Casing |
| | | | 629.33 | | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 626.10 | 0.00 | Ground Surface | |
| | | | 623.77 | | Top of Annular S | ealant |
| Type of Annular Sealant: Bento | 7 | | | | 1 | |
| Installation Method: Tremi | | | 574.72 | 51 27 | C. C. W. L | 1 |
| Setting Time: +24 hr. | | $\overline{\Delta}$ | 574.73 | _51.37_ | Static Water Lev (After Completion) | |
| Type of Bentonite Seal Gran | ular Pellet Slurry (choose one) | | | | | |
| Installation Method:Gravit | ty | | 584.65 | 41.45 | Top of Seal | |
| Setting Time: +24 hr. | | | 582.65 | 43.45 | Top of Sand Pack | C |
| Town of Could Dealer | | | | | r | |
| Type of Sand Pack: Quartz sand Grain Size: #JC50FS (sie | | | 580.20 | 45.90 | Top of Screen | |
| Installation Method: Gravit | | | | | | |
| | | | 575.76 | | Bottom of Screen | l |
| Type of Backfill Material:n/a_ | (if applicable) | | _575.32_ | _50.78_ | Bottom of Well | |
| Installation Method: Re-dri | ill borehole | | | | Bottom of Boreh | ole |
| | | | | | | |
| | | Г | | | SUREMENTS | |
| | TRUCTION MATERIALS | Г | Diameter of Boreho ID of Riser Pipe | ole | (inches) | 2.0 |
| (Choose on | e type of material for each area) | | Protective Casing I | ength | (inches) | 5.0 |
| | | | Riser Pipe Length | | (feet) | 48.83 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER: | (0: 1) | Bottom of Screen t | o End Cap | (feet) | 0.44 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER: | | Screen Length (1s | _ | | 4.74 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER: | | Total Length of Ca | sing | (feet) | 54.01 |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

(inches)

SS304

Well Completion Form (revised 02/06/02)

SS316

| Illinois Environmental | Protection Agency | 7 | | Well (| Completion | Report |
|--|--------------------------|------------|--|-----------------|--|----------|
| Site #: | County: <u>Mon</u> | tgomery | | We | ell #:MW | 716S |
| Site Name: <u>AEG Coffeen Power Station</u> | CCB Management Facility | / | | Во | rehole #: S | B-16a |
| State Plane Coordinate: X 877,355.1 Y 2,5 | 515,088.0 (or) Latitude: | <u> </u> | | Longitude | ·° | |
| Surveyed By: Darren E. Forgy | _ | IL Regist | tration #:035-0 | 03637 | | |
| Drilling Contractor: Reynolds Drilling Co | orp. | Driller: _ | K. Doetzel | | | |
| Consulting Firm: <u>Hanson Professional Se</u> | ervices Inc. | Geologis | t: Rhonald W | Hasenyager | , LPG #196-00 | 00246 |
| Drilling Method: Hollow stem auger | | Drilling I | Fluid (Type): Po | table water | | |
| Logged By: Rhonald W Hasenyager | | Date Star | rted: 4/25/20 | 06 Date | Finished: 4/2 | 25/2006 |
| Report Form Completed By: Rhonald W H | asenyager | Date: | 6/7/2006 | | | |
| ANNULAR SPACE DETA | AILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) |) |
| | | | 629.62 | . , | Top of Protective | e Casing |
| | | | 629.28 | 3.18 | Top of Riser Pip | e |
| Type of Surface Seal: Concrete | | | 626.10_ | 0.00 | Ground Surface | |
| | | | 624.66 | 1.44 | Top of Annular S | Sealant |
| Type of Annular Sealant: Bentonite chips | | R | | | • | |
| Installation Method: Gravity | | _ | (20.26 | 5.74 | | |
| Setting Time: +24 hr. | __ | _ | _620.36_ | 5.74 | Static Water Lev (After Completion) | |
| Type of Bentonite Seal Granular Pello | , | | | | | |
| (choos Installation Method: Gravity | | | 624.66 | 1.44 | Top of Seal | |
| Setting Time: 17 min. | | | (12.40 | 12.70 | T CC ID | |
| | | | 612.40 | 13.70 | Top of Sand Pac | X |
| Type of Sand Pack: Quartz sand | | | 611.51 | 14.50 | Top of Screen | |
| Grain Size: #JC50FS (sieve size) | | | 611.51 | 14.59 | Top of Screen | |
| Installation Method: <u>Gravity</u> | | | 606.69 | _19.41_ | Bottom of Screen | 1 |
| Type of Backfill Material: Quartz sand | plicable) | | 606.34 | | Bottom of Well | 1 |
| Installation Method: Gravity | pricatile) | | 606.20 | 19.90 | Bottom of Boreh | ole |
| | | | * Referenced to a | | | |
| | | | CASI | NG MEAS | UREMENTS | |
| WELL CONSTRUCTION | N MATEDIAI S | Ι | Diameter of Boreho | ole | (inches) | 8.0 |
| (Choose one type of materia | | | D of Riser Pipe | | (inches) | 2.0 |
| | | | Protective Casing I | Length | (feet) | 5.0 |
| Protective Casing SS304 SS3 | 316 PTFE PVC OTHER: (| | Riser Pipe Length Bottom of Screen to | n End Can | (feet) | 0.38 |
| Riser Pipe Above W.T. SS304 SS3 | 316 PTFE PVC OTHER: | | Screen Length (1s | - | | 4.82 |
| Riser Pipe Below W.T. SS304 SS3 | B16 PTFE PVC OTHER: | | Total Length of Ca | | (feet) | 22.94 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environmenta | l Protection Agenc | y | | Well | Completio | n Report |
|---|----------------------------|------------------------------|-------------------------|---------------------|------------------------------------|-----------|
| Site #: | County: Mo | ntgomery | | W | ell #:M | W17D |
| Site Name: <u>AEG Coffeen Power Statio</u> | n CCB Management Facilit | .y | | Во | orehole #: | SB-17 |
| State Plane Coordinate: X 878,659.0 Y 2 | 2,515,090.4 (or) Latitude: | | | Longitude | e:° | |
| Surveyed By: Darren E. Forgy | | IL Regis | tration #: <u>035-0</u> | 03637 | | |
| Drilling Contractor: Reynolds Drilling C | Corp. | Driller: | K. Doetzel | | | |
| Consulting Firm: Hanson Professional S | Services Inc. | Geologis | t: Rhonald W | Hasenyage | r, LPG #196- | 000246 |
| Drilling Method: Hollow stem auger | | Drilling l | Fluid (Type): <u>Po</u> | otable water | r | |
| Logged By: Reynolds Drilling Corp. | | Date Star | rted:5/4/200 | 06 Date | Finished: | 5/4/2006 |
| Report Form Completed By: Rhonald W | Hasenyager | Date: | 6/7/2006 | | | |
| ANNULAR SPACE DET | AILS | | Elevations (MSL)* | Depths (BGS) | (0.01 f | t.) |
| | | | 630.62 | -3.52 | Top of Protect | ve Casing |
| | | | 630.29 | 3.19 | Top of Riser P | ipe |
| Type of Surface Seal: Concrete | | | 627.10 | 0.00 | Ground Surfac | e |
| | | | 624.92 | 2.18 | Top of Annula | r Sealant |
| Type of Annular Sealant: Bentonite grout | | | | | | |
| Installation Method: Tremie | | _ | 570.65 | 54.45 | | |
| Setting Time: +24 hr. | | $\mathbb{Z} \mid \cdot \mid$ | 572.65 | _54.45_ | Static Water L (After Completic | |
| 71 | llet Slurry | | | | | |
| Installation Method: Gravity | ose one) | | 581.55 | 45.55 | Top of Seal | |
| Setting Time: +24 hr. | | | 580.25 | 16.95 | Top of Sand Pa | vals |
| | | | _580.25_ | _40.63_ | Top of Sand Pa | ick |
| Type of Sand Pack: Quartz sand | | | 570 20 | 48.82 | Top of Screen | |
| Grain Size: #JC50FS (sieve size) | | | 578.28 | 40.62 | Top of Screen | |
| Installation Method: <u>Gravity</u> | | | 573.78_ | 53.32 | Bottom of Scre | oon. |
| Type of Backfill Material:n/a | | | 573.23 | 53.87 | Bottom of Wel | |
| Installation Method: <u>n/a</u> | applicable) | | 573.23 | 53.87 | Bottom of Bor | ahola |
| instantation Method. <u>II/a</u> | | | * Referenced to a | | | enore |
| | | | CAS | ING MEAS | SUREMENTS | |
| | | I | Diameter of Boreh | | (inche | |
| WELL CONSTRUCTIO (Choose one type of mater | | | D of Riser Pipe | | (inche | |
| | • | <u> </u> | Protective Casing I | Length | (fee | 5.0 |
| | | | Riser Pipe Length | | (fee | 52.01 |
| 8 | S316 PTFE PVC OTHER: | | Bottom of Screen t | | | 0.55 |
| P | S316 PTFE PVC OTHER: | | Screen Length (1s | | t) (fee | |
| Riser Pipe Below W.T. SS304 S | S316 PTFE PVC OTHER: | | Γotal Length of Ca | sing | (fee | t) 57.06 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environmental Protection Agency | | | | | Well | Completion | Report |
|--|-----------------------------------|-------------|------------|--------------------------------------|-----------------|--|---------------|
| Site #: | County | : Montgo | mery | | Wo | ell #:MV | V17S |
| Site Name: AEG Coffeen Po | wer Station CCB Management | t Facility | | | Во | rehole #: S | B-17a |
| State Plane Coordinate: X 878,658 | - | • | | | | | |
| Surveyed By: Darren E. Forg | y | IL | Registra | ation #: <u>035-0</u> | 03637 | | |
| Drilling Contractor: Reynolds | Drilling Corp. | Dr | iller:] | K. Doetzel | | | |
| Consulting Firm: Hanson Pro | Sessional Services Inc. | Ge | eologist: | Rhonald W | Hasenyager | , LPG #196-00 | 00246 |
| Drilling Method: Hollow stem | ı auger | Dr | illing Flu | uid (Type): <u>Po</u> | otable water | | |
| Logged By: Reynolds Drillin | g Corp. | Da | ite Starte | ed: 5/4/200 | 06 Date | Finished: 5/ | /4/2006 |
| Report Form Completed By: Rl | nonald W Hasenyager | Da | ıte: | 6/7/2006 | | | |
| ANNULAR SPA | CE DETAILS | | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) |) |
| | | | | 630.68 | ` ′ | Top of Protective | e Casing |
| | | T | Ī | 630.34 | | Top of Riser Pip | |
| Type of Surface Seal: Concrete | | | | (27.10 | 0.00 | | |
| - , p | | | | 627.10 | | Ground Surface | 3.1. |
| Type of Annular Sealant: Bento | nite chips | | | 626.40 | 0.70 | Top of Annular | Sealant |
| Installation Method: <u>Gravit</u> | у | | | | | | |
| Setting Time: +24 hr. | | | | 620.21 | 6.89 | Static Water Lev (After Completion) | |
| Type of Bentonite Seal Gran | ular Pellet Slurry | | | | | | |
| Installation Method: Gravit | (choose one) V | | | 617.33 | 9.77 | Top of Seal | |
| Setting Time: 22 min. | | | | 614.80 | | | 1 |
| | | | | _014.80_ | 12.30 | Top of Sand Pac | K |
| Type of Sand Pack: Quartz sand | | | | 613.08 | 14.02 | Top of Screen | |
| Grain Size: #JC50FS (sie | | | | | | - op - o o o- | |
| Installation Method: <u>Gravit</u> | <u>y</u> | | | 603.54 | 23.56 | Bottom of Scree | n |
| Type of Backfill Material:n/a | (if applicable) | | | 602.99 | 24.11 | Bottom of Well | |
| Installation Method: <u>n/a</u> | | | | 602.99 | | Bottom of Borel | ole |
| | | | | * Referenced to a | National Geodet | ic Datum | |
| | | | | CAS | ING MEAS | SUREMENTS | |
| WELL CONS | TRUCTION MATERIALS | | | ameter of Boreh | ole | (inches) | 8.0 |
| | e type of material for each area) | | | of Riser Pipe | | (inches) | 2.0 |
| | | | | otective Casing I | Length | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC | OTHER: Stee | | ser Pipe Length ottom of Screen t | o End Con | (feet) | 17.26 0.55 |
| Riser Pipe Above W.T. | | OTHER: | _ 100 | reen Length (1s | _ | | 9.54 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC | OTHER: | | tal Length of Ca | | (feet) | 27.35 |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

(inches)

SS304

Well Completion Form (revised 02/06/02)

| Illinois Environmental Protection Agenc | y Well Completion Repor |
|---|---|
| Site #: County: Mo | ontgomery Well #:MW18S |
| Site Name: AEG Coffeen Power Station CCB Management Facili | |
| State Plane Coordinate: X 878,604.7 Y 2,513,745.2 (or) Latitude: | |
| Surveyed By: Darren E. Forgy | IL Registration #:035-003637 |
| Drilling Contractor: Reynolds Drilling Corp. | Driller: B. Williamson |
| Consulting Firm: Hanson Professional Services Inc. | Geologist: Rhonald W Hasenyager, LPG #196-000246 |
| Drilling Method: Hollow stem auger | Drilling Fluid (Type): Potable water |
| Logged By: Reynolds Drilling Corp. | Date Started:5/11/2006 Date Finished:5/11/2006 |
| Report Form Completed By: Rhonald W Hasenyager | Date:6/7/2006 |
| ANNULAR SPACE DETAILS | Elevations Depths (0.01 ft.) (MSL)* (BGS) |
| | 629.02 Top of Protective Casing |
| T | |
| Type of Surface Seal: Concrete | 625.60 0.00 Ground Surface |
| | 622.13 3.47 Top of Annular Sealant |
| Type of Annular Sealant: Bentonite chips | 022.13 3.47 Top of Allitural Scatain |
| Installation Method: Gravity | |
| Setting Time:+24 hr. | $ \underline{\nabla} $ 618.73 6.87 Static Water Level (After Completion) 6/1/2006 |
| Type of Bentonite Seal Granular Pellet Slurry | |
| (choose one) Installation Method: Gravity | 622.13 3.47 Top of Seal |
| | |
| Setting Time: 25 min. | 615.79 9.81 Top of Sand Pack |
| Type of Sand Pack: Quartz sand | |
| Grain Size: #JC50FS (sieve size) | 614.29 11.31 Top of Screen |
| Installation Method: Gravity | |
| Type of Backfill Material: n/a | 609.81 15.79 Bottom of Screen 609.20 16.40 Bottom of Well |
| (if applicable) | |
| Installation Method:n/a | 609.20 16.40 Bottom of Borehole * Referenced to a National Geodetic Datum |
| | CASING MEASUREMENTS |
| | Diameter of Borehole (inches) 8.0 |
| WELL CONSTRUCTION MATERIALS (Choose one type of material for each area) | ID of Riser Pipe (inches) 2.0 |
| (Choose one type of material for each area) | Protective Casing Length (feet) 5.0 |
| | Riser Pipe Length (feet) 14.42 |
| Protective Casing SS304 SS316 PTFE PVC OTHER: | |
| Riser Pipe Above W.T. SS304 SS316 PTFE PVC OTHER: | Screen Length (1st slot to last slot) (feet) 4.48 |
| Riser Pipe Below W.T. SS304 SS316 PTFE PVC OTHER: | Total Length of Casing (feet) 19.51 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environmental Protection Agency | Well Completion Report |
|---|---|
| Site#: County: _Mc | ontgomery Well #: MW20S |
| Site Name: Ash Pond Investigation | Borehole #: SB20 |
| State Plane Coordinate: X 2,515,867.9 Y 874,226.4 (or) Latitude | : Longitude: |
| Surveyed By: Darren E. Forgy | IL Registration #:035-003637 |
| Drilling Contractor: Reynolds Drilling Corp. | Driller: A. Rachford |
| Consulting Firm: Hanson Professional Services Inc. | Geologist: Rhonald W. Hasenyager, LPG #196-000246 |
| Drilling Method: Hollow stem auger | Drilling Fluid (Type): <u>none</u> |
| Logged By: Rhonald W. Hasenyager | Date Started:5/1/2007 Date Finished:5/1/2007 |
| Report Form Completed By: Rhonald W. Hasenyager | Date:5/2/2007 |
| ANNULAR SPACE DETAILS | Elevations Depths (0.01 ft.) (MSL)* (BGS) |
| | |
| | |
| Type of Surface Seal: Concrete | 620.30 0.00 Ground Surface |
| Type of Annular Sealant: Bentonite chips | |
| Installation Method: gravity | 7 |
| | |
| | (After Completion) 5/10/2007 |
| Type of Bentonite Seal Granular Pellet Slurry (choose one) | |
| Installation Method: | n/aTop of Seal |
| Setting Time: | |
| Type of Sand Pack: Quartz sand | |
| Grain Size: 10/20 (sieve size) | |
| Installation Method: <u>gravity</u> | |
| Type of Backfill Material:(if applicable) | 607.08 13.22 Bottom of Screen 606.63 13.67 Bottom of Well |
| (if applicable) Installation Method: | 604.30 16.00 Bottom of Borehole |
| maananon wana. | * Referenced to a National Geodetic Datum |
| | CASING MEASUREMENTS |
| WELL CONSTRUCTION WATERIALS | Diameter of Borehole (inches) 8.0 |
| WELL CONSTRUCTION MATERIALS (Choose one type of material for each area) | ID of Riser Pipe (inches) 2.0 |
| | Protective Casing Length (feet) 5.0 |
| Protective Casing SS304 SS316 PTFE PVC OTHER: | Riser Pipe Length (feet) 11.11 |
| Riser Pipe Above W.T. SS304 SS316 PTFE PVC OTHER: | Bottom of Screen to End Cap (feet) 0.45 |
| Riser Pipe Below W.T. SS304 SS316 PTFE PVC OTHER: | Screen Length (1st slot to last slot) (feet) 4.81 |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

(inches)

Screen

Well Completion Form (revised 02/06/02)

| Illinois Enviror | mental Protection Agency | 7 | | Well | l Completion | Report |
|---|--|------------------------|------------------------|------------------------------|------------------------------------|-------------------|
| Site #: | County: N | Iontgomery | | W | Vell #:R1 | 04 |
| Site Name: CCB Managemen | t Facility | | | В | orehole #:] | R104 |
| State Plane Coordinate: X 2,514,500 | 3.4 Y 875,857.8 (or) Latitud | de:39 | 4! <u>10.000</u> Ä | À Longitud | le: <u>-89</u> <u>23</u> | ! <u>56.800</u> Ä |
| Surveyed By: <u>Jeffrey D. Emrid</u> | ck | IL Registr | ration #: <u>035-0</u> | 03507 | | |
| Drilling Contractor: <u>Layne-We</u> | estern Co | Driller: _ | D. Mahurin | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | Geologist | : Rhonald W. | Hasenyage | r, LPG #196-000 | 246 |
| Drilling Method: Hollow stem | auger | Drilling F | fluid (Type):n/s | a | | |
| Logged By: Rhonald W. Hase | enyager | Date Star | ted: 10/8/20 |)10 Dat | e Finished:10 | /8/2010 |
| Report Form Completed By:Su | ızanna Simpson | Date: | 10/19/2010 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | _ | | 632.02 | 2.99 | Top of Protective | Casing |
| | | | 631.84 | 2.81 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 629.03 | 0.00 | Ground Surface | |
| Type of Annular Sealant: High- | solids bentonite | | 627.03 | 2.00 | Top of Annular S | ealant |
| Installation Method: Tremic | | | | | | |
| | | $ \underline{\nabla} $ | 612.85 | 16.18 | Static Water Leve | |
| Type of Bentonite Seal Gran | ular Pellet Slurry | | | | (After Completion) | 11/15/2010 |
| | (choose one) | | (17.02 | 12.00 | T. 60 1 | |
| Installation Method: Gravit | y | | 617.03 | 12.00 | Top of Seal | |
| Setting Time: 15 min | | | 616.01 | _13.02_ | Top of Sand Pack | [|
| Type of Sand Pack: Quartz sand | <u>d</u> | | | | | |
| Grain Size: 10/20 (sie | eve size) | | 614.44 | 14.59 | Top of Screen | |
| Installation Method: <u>Gravit</u> | <u>y</u> | | (00.71 | 10.22 | D # 60 | |
| Type of Backfill Material: | | | 609.71 609.18 | <u>19.32</u> <u>19.85</u> | Bottom of Screen Bottom of Well | |
| Installation Method: n/a | (if applicable) | | 609.18 | 19.85 | Bottom of Boreho | ale |
| instanction (viction). | | | * Referenced to a | | | ne - |
| | | | CAS | SING MEA | SUREMENTS | |
| WEY 1 GOV | | I | Diameter of Boreho | ole | (inches) | 8.0 |
| | STRUCTION MATERIALS ue type of material for each area) | I | D of Riser Pipe | | (inches) | 2.0 |
| | | F | Protective Casing I | ength | (feet) | 5.0 |
| Duotactiva Cosis - | SS304 SS316 PTFE PVC OTHE | | Riser Pipe Length | | (feet) | 17.60 |
| Protective Casing Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHE SS304 SS316 PTFE PVC OTHE | | Bottom of Screen t | | (feet) | 0.53 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHE | _ | Screen Length (1: | | ot) (feet) | 4.53 |

SS304

Well Completion Form (revised 02/06/02)

SS316

PTFE PVC OTHER:

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | mental Protection Agenc | y | | Well (| Completion | 1 Report |
|---|---|------------------|------------------------|-------------------|--|--------------------|
| Site #: | County: | Montgomery | | We | 11 #: <u> </u> | 201 |
| Site Name: CCB Management | t Facility | | | Bor | ehole #: | R201 |
| State Plane Coordinate: X 2,514,842 | 2.0 Y 877,925.3 (or) Latitu | ide: <u>39</u> _ | 4! <u>30.500</u> Ä | Longitude: | 892: | 3! <u>52.300</u> Ä |
| Surveyed By: <u>Jeffrey D. Emric</u> | k | IL Regist | ration #: <u>035-0</u> | 03507 | | |
| Drilling Contractor: <u>Layne-We</u> | stern Co | Driller: _ | D. Mahurin | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | Geologist | : Rhonald W. | Hasenyager, | LPG #196-000 | 246 |
| Drilling Method: Hollow stem | auger | Drilling F | Fluid (Type):n/a | ı | | |
| Logged By: Rhonald W. Hase | nyager | Date Star | ted:10/15/20 | 010 Date 1 | Finished:10 | /15/2010 |
| Report Form Completed By: Su | zanna Simpson | Date: | 10/19/2010 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) |) |
| | _ | | _626.51_ | | Top of Protective | e Casing |
| | | | 626.34 | -2.32 | Гор of Riser Pipe | 3 |
| Type of Surface Seal: Concrete | | | 624.02 | 0.00 | Ground Surface | |
| | | | 621.52 | | Top of Annular S | Sealant |
| Type of Annular Sealant: <u>High-s</u> | solids bentonite | | 021.32 | | rop or rumatar s | , carain |
| Installation Method:Tremie | | | | | | |
| Setting Time: >24 hr. | | | 618.70 | 5.32 | Static Water Lev (After Completion) | |
| Type of Bentonite Seal Gran | ular Pellet Slurry | | | | | |
| Installation Method: Gravit | (choose one) | | 614.47 | 9.55 | Top of Seal | |
| Setting Time: 48 min | · · · · · · · · · · · · · · · · · · · | | | | | |
| | | | 612.90 | 11.12 | Top of Sand Pac | K. |
| Type of Sand Pack: Quartz sand | 1 | | (11.75 | 12.27 | T. 60 | |
| Grain Size:10/20 (sie | ve size) | | 611.75 | 12.27 | Top of Screen | |
| Installation Method: Gravit | <u>y</u> | | 607.36 | 16.66 I | Bottom of Screer | |
| Type of Backfill Material:n/a | | | 606.80 | | Bottom of Well | ı |
| Installation Method: n/a | (if applicable) | | 606.80 | 17.22 | Bottom of Boreh | ole |
| instantation received. <u>In a</u> | | | | National Geodetic | | |
| | | | CAS | SING MEASU | UREMENTS | |
| W | | I | Diameter of Boreho | ole | (inches) | 8.0 |
| | STRUCTION MATERIALS e type of material for each area) | I | D of Riser Pipe | | (inches) | 2.0 |
| | | | Protective Casing L | ength | (feet) | |
| Protesting C. : | CC204 CC217 PTEC BYG | | Riser Pipe Length | | (feet) | |
| Protective Casing Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTH SS304 SS316 PTFE (PVC) OTH | | Bottom of Screen to | | (feet) | 0.56 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTH | | Screen Length (1s | | | 4.39 |
| Table I ipe Below W.1. | | | Total Length of Cas | sing | (feet) | 19.54 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environmental Protection Agency | | | | | Well Completion Report | | |
|--|--|----------------|---------------------------|---------------------------|-------------------------|-------------------|--|
| Site #: | County: M | ontgomery | | W | Vell #: R2 | 205 | |
| Site Name: Coffeen Power St | ation - Gypsum Mgmt Facility | | | В | orehole #:] | R205 | |
| State Plane Coordinate: X 2,515,91 | 0.1 Y 875,548.8 (or) Latitude | e: <u>39</u> _ | 4! <u>6.935Ä</u> | Longitude | e: <u>-89</u> <u>23</u> | ! 38.991 <u>Ä</u> | |
| Surveyed By: Gary C. Rogers | | _ IL Registra | ation #: <u>035-02</u> | 2957 | | | |
| Drilling Contractor: Bulldog I | Drilling | _ Driller: _ | J. Gates | | | | |
| Consulting Firm: Hanson Prof | fessional Services Inc. | _ Geologist: | Rhonald W. | Hasenyager | , LPG #196-000 | 246 | |
| Drilling Method: Hollow Sten | n Auger | _ Drilling Fl | uid (Type): | | | | |
| Logged By: Rhonald W. Hase | enyager | _ Date Start | ed: <u>3/20/20</u> | 17 Date | e Finished:3/2 | 20/2017 | |
| Report Form Completed By: Su | uzanna L. Keim | Date: | 3/27/2017 | | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | | |
| | | | 624.94 | 3.03 | Top of Protective | Casing | |
| | | | 624.52 | -2.61 | Top of Riser Pipe | | |
| Type of Surface Seal: Concrete | | | 621.91 | 0.00 | Ground Surface | | |
| | | | 619.91 | 2.00 | Top of Annular S | ealant | |
| Type of Annular Sealant: High- | 7 | | | | | | |
| Installation Method:Tremi | e | ∇ | 619.41 | 2.50 | Static Water Leve | <u>.</u> | |
| Setting Time | | <u>~</u> | | | (After Completion) | | |
| Type of Bentonite Seal Gran | Pellet Slurry (choose one) | | | | | | |
| Installation Method: Gravi | ty | \bowtie | 614.26 | 7.65 | Top of Seal | | |
| Setting Time: 95 minutes | | | 611.99 | 9.92 | Top of Sand Pack | | |
| Type of Sand Pack: Quartz san | d | | | | | | |
| Grain Size: #0 (si | | | 610.59 | _11.32_ | Top of Screen | | |
| Installation Method: Graving | | | | | | | |
| True of Dockfill Motorial | | | 605.90 605.49 | <u>16.01</u> 16.42 | Bottom of Screen | | |
| Type of Backfill Material:n/a_ | (if applicable) | | 003.49 | | Bottom of Well | | |
| Installation Method:n/a | | | 605.49 * Referenced to a | 16.42 National Geodeti | | ole | |
| | | | 0.10 | | | | |
| | | р | iameter of Boreho | | SUREMENTS (inches) | 8.0 | |
| | STRUCTION MATERIALS ne type of material for each area) | | of Riser Pipe | лс | (inches) | 2.0 | |
| (Choose of | type of material fol each alea) | | rotective Casing L | ength_ | (feet) | 5.0 | |
| | | | iser Pipe Length | | (feet) | 13.93 | |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | Steel | ottom of Screen to | End Cap | (feet) | 0.41 | |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | : Se | creen Length (1s | st slot to last slo | t) (feet) | 4.69 | |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | : T | otal Length of Cas | sing | (feet) | 19.03 | |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

SS304

Well Completion Form (revised 02/06/02)

| Illinois Environ | 7 | Well Completion Repor | | | | |
|--|--|-----------------------|--|------------------|--|--|
| Site #: | County: N | <u>Iontgomery</u> | | Well #: | | |
| Site Name: CCB Management | Facility | | | В | orehole #:T127 | |
| State Plane Coordinate: X 2,513,911 | <u>.0</u> Y <u>875,359.2</u> (or) Latitud | de: <u>39</u> | 4! <u>5.200Ä</u> | Longitude | e: <u>-89</u> <u>24!</u> <u>4.400Ä</u> | |
| Surveyed By: | | IL Regist | tration #: | | | |
| Drilling Contractor: <u>Layne-We</u> | stern Co | Driller: _ | T. List | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | Geologis | t: Rhonald W. | Hasenyager | ; LPG #196-000246 | |
| Drilling Method: Hollow stem | auger | Drilling l | Fluid (Type):n/a | a | | |
| Logged By: | | Date Star | rted: 2/10/20 | 10 Date | e Finished:2/10/2010 | |
| | | | 2/19/2010 | | | |
| ANNULAR SPA | | | Elevations | | (0.01 ft.) | |
| | | | (MSL)* | (BGS) | | |
| | T | | 631.29 | 3.22_ | Top of Protective Casing | |
| | | | 630.96 | 2.89 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 628.07 | 0.00 | Ground Surface | |
| True of Annular Coolant: High o | olida kontonito | | 622.43 | 5.64 | Top of Annular Sealant | |
| Type of Annular Sealant: High-s | A | | | | | |
| Installation Method: <u>Tremie</u> Setting Time: _ >24 hr. | | | 616.81_ | 11.26 | Static Water Level | |
| Setting Time | | $\overline{\Delta}$ | 010.81 | | (After Completion) 3/1/2010 | |
| Type of Bentonite Seal Grant | Pellet Slurry (choose one) | | | | | |
| Installation Method: Granul | , , , | | 613.43 | _14.64_ | Top of Seal | |
| Setting Time:10 min | | | 612.32 15.75 Top of Sand Pack | | | |
| | <u> </u> | | 012.32 | | rop of Sand Fack | |
| Type of Sand Pack: Quartz sand | <u> </u> | | 610.54 | 17.53 | Top of Screen | |
| Grain Size:10/20 (sie | , | | _010.34_ | 17.33 | Top of Screen | |
| Installation Method: Gravity | <u>/</u> | | 606.00 | 22.07 | Bottom of Screen | |
| Type of Backfill Material:n/a | (if applicable) | | 605.43 | 22.64 | Bottom of Well | |
| Installation Method: n/a | (ii applicable) | | 605.43 | 22.64 | Bottom of Borehole | |
| | | | * Referenced to a | National Geodeti | | |
| | | | CAS | SING MEAS | SUREMENTS | |
| WELL GOVE | TRANSPORTATION AND THE PARTY OF | | Diameter of Boreho | ole | (inches) 8.0 | |
| | TRUCTION MATERIALS e type of material for each area) | | ID of Riser Pipe | | (inches) 2.0 | |
| | | | Protective Casing L | ength | (feet) 5.0 | |
| Protective Casing | SS304 SS316 PTFE PVC OTHE | | Riser Pipe Length | | (feet) 20.42 | |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHE | | Bottom of Screen to | | (feet) 0.57 | |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHE | | Screen Length (1s) Total Length of Cas | | (feet) 4.54 (feet) 25.53 | |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviro | onmental Protection Agend | e y | | Well | Completion | Report |
|---|-------------------------------------|---------------------------|--|------------------------------|---|--------|
| Site #: | County: N | Iontgomery | V | W | Vell #:T1 | 28 |
| Site Name: <u>AEG Coffeen Po</u> | ower Station CCB Management Facili | ity | | В | Forehole #: | 128 |
| State- Plant Plane Coordinate: X 2,513,90 | 09.5 Y 875,509.7 (or) Latitud | le: | · | Longitud | e:° | '" |
| Surveyed By: | | _ IL Reg | istration #: | | | |
| Drilling Contractor: <u>Layne-W</u> | estern Co | _ Driller: | T. List | | | |
| Consulting Firm: Hanson Pro | ofessional Services Inc. | _ Geolog | ist: Rhonald W. | Hasenyage | er, LPG #196-000 | 246 |
| Drilling Method: Hollow ster | n auger | _ Drilling | g Fluid (Type): <u>n/a</u> | ı | | |
| Logged By: Suzanna L. Sim | pson | _ Date St | tarted: 2/9/201 | 0 Dat | e Finished: 2/ | 9/2010 |
| Report Form Completed By: S | uzanna L. Simpson | _ Date: _ | 2/18/2010 | | | |
| ANNULAR SPA | ACE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | <u></u> | | 631.23 | 2.79_ | Top of Protective | Casing |
| | | | 630.93 | 2.49 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 628.44 | 0.00 | Ground Surface | |
| Type of Annular Sealant: High | -solids bentonite | | 623.38 | 5.06 | Top of Annular S | ealant |
| Installation Method:Trem | ie J | | | | | |
| Setting Time: >24 hr. | | $ \overline{\Delta} $ | 616.09 | 12.35 | Static Water Leve (After Completion) | |
| Type of Bentonite Seal Gra | nular Pellet Slurry | | | | | |
| Installation Method: Granu | (choose one) | | 615.53 | 12.91 | Top of Seal | |
| Setting Time: 10 min | | | 614.13 | _14.31_ | Top of Sand Pack | : |
| Type of Sand Pack: Quartz san | nd | | | | | |
| | sieve size) | | 611.91 | 16.53 | Top of Screen | |
| Installation Method: Gravi | ity | | | | | |
| Type of Backfill Material: Qua | | | 607.40 606.80 | <u>21.04</u> <u>21.64</u> | Bottom of Screen Bottom of Well | |
| Installation Method: Gravi | (if applicable) | | 604.38 | 24.06 | Bottom of Boreho | ale. |
| ilistaliation friction. Oravi | | | * Referenced to a | | | iiC |
| | | | CAS | ING MEA | SUREMENTS | |
| WELL CON | STRUCTION MATERIALS | | Diameter of Boreho | ole | (inches) | 8.0 |
| | one type of material for each area) | | ID of Riser Pipe | | (inches) | 2.0 |
| | | | Protective Casing L | ength | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC OTHE | R: Steel | Riser Pipe Length Bottom of Screen to | End Can | (feet) | 0.60 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHE | R: | Screen Length (1s | | ` | 4.51 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHE | R: | Total Length of Cas | | (feet) | 25.13 |
| Screen | SS304 SS316 PTFE PVC OTHE | R: | Screen Slot Size ** | | (inches) | 0.010 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environmental Protection Agency | | | | Well Cor | npletion | Report |
|--|------------------------------------|--------------|---------------------------------------|-------------------------|------------------|-----------|
| Site #: | County: M | ontgomery | | Well #: | T20 |)2 |
| | wer Station CCB Management Facili | | | | le #:T | 202 |
| State | 5.0 Y 876,699.4 (or) Latitud | • | | | | |
| Surveyed By:Jeffrey D. Emri | ck | _ IL Registr | ration #:035-00 | 03507 | | |
| Drilling Contractor: <u>Layne-We</u> | estern Co | _ Driller: _ | D. Mahurin | | | |
| Consulting Firm: Hanson Prof | Sessional Services Inc. | _ Geologist: | Rhonald W. 1 | Hasenyager, LP | G #196-0002 | 246 |
| Drilling Method: Hollow stem | auger | _ Drilling F | luid (Type): <u>n/a</u> | Į. | | |
| Logged By: Suzanna L. Simp | son | _ Date Start | ed:10/15/20 | Date Finis | shed:10/1 | 5/2010 |
| Report Form Completed By: Su | zanna L. Simpson | Date: | 10/19/2010 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | 628.79 | | of Protective (| Casing |
| | T. | | 628.63 | | of Riser Pipe | |
| | | | | | or ruser rape | |
| Type of Surface Seal: Concrete | | | 626.22 | Grou | and Surface | |
| Type of Annular Sealant: High- | solids bentonite | | 623.42 | | of Annular Se | alant |
| Installation Method:Tremic | | | | | | |
| Setting Time:>24 hr. | | ∇ | 613.72 | | c Water Level | |
| | | | | (Aft | er Completion) 1 | 1/15/2010 |
| Type of Bentonite Seal Gran | Pellet Slurry (choose one) | | | | | |
| Installation Method: Gravit | y | | 616.50 | <u>9.72</u> Top | of Seal | |
| Setting Time: 15 min | | | 615.27 | | of Sand Pack | |
| Type of Sand Pack: Quartz sand | 1 | | | | | |
| | eve size) | | 613.95 | 12.27 Top | of Screen | |
| Installation Method: Gravit | · | | | | | |
| | , | | 609.57 | | om of Screen | |
| Type of Backfill Material: <u>n/a</u> | (if applicable) | | 609.01 | 17.21 Bott | om of Well | |
| Installation Method: <u>n/a</u> | | | 608.22 | Bott | om of Borehol | e |
| | | | * Referenced to a r | National Geodetic Datun | n | |
| | | | CAS | ING MEASURI | EMENTS | |
| WELL CONS | STRUCTION MATERIALS | | Diameter of Boreho | le | (inches) | 8.0 |
| | ne type of material for each area) | | O of Riser Pipe | 4 | (inches) | 2.0 |
| | | | rotective Casing L | ength | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER | | siser Pipe Length Sottom of Screen to | Fnd Can | (feet) | 0.56 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER | | creen Length (1s | | (feet) | 4.38 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | | otal Length of Cas | | (feet) | 19.62 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

 $\hbox{**Hand-Slotted Well Screens Are Unacceptable}\\$

0.010

| Illinois Environ | mental Protection Ag | gency | | | Well | Completi | on Report |
|-------------------------------------|--|--------------|--------------|---------------------------------------|------------------------------|------------------------------------|-------------|
| Site #: | Count | ty: Montgo | omery | | W | /ell #: | T408 |
| Site Name: Coffeen Power Sta | ation - Ash Pond 2 | | | | В | orehole #: | T408 |
| State Plane Coordinate: X 2,515,314 | +.9 Y <u>873,999.4</u> (or) | Latitude: | 39 | 3! <u>51.671</u> Ä | Longitud | e: <u>-89</u> _ | 23! 46.704Ä |
| Surveyed By: Gary C. Rogers | | II | L Registra | tion #:035-0 | 02957 | | |
| Drilling Contractor: Bulldog D | rilling, Inc. | D | Oriller:J | . Dittmaier | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | G | Geologist: | Rhonald W. | Hasenyager | , LPG #196-0 | 00246 |
| Drilling Method: Hollow stem | auger | D | Orilling Flu | id (Type): <u>no</u> | ne | | |
| Logged By: Kristen L. Theesfe | eld | D | Date Starte | d: <u>8/17/20</u> | 16 Date | e Finished: | 8/17/2016 |
| Report Form Completed By: Su | zanna L. Keim | D | Date: | 8/24/2016 | | | |
| ANNULAR SPA | CE DETAILS | | | Elevations (MSL)* | Depths (BGS) | (0.01 1 | t.) |
| | | | | 624.44 | 3.35 | Top of Protect | ive Casing |
| | | | | 624.08 | 2.99 | Top of Riser F | ipe |
| Type of Surface Seal: Concrete | | | | _621.09_ | 0.00 | Ground Surfac | æ |
| Type of Annular Sealant: High-s | olids bentonite | | | 619.09 | 2.00 | Top of Annula | r Sealant |
| Installation Method: Tremie | : | | | | | | |
| Setting Time: >24 hours | | | | | | Static Water L (After Completic | |
| Type of Bentonite Seal Grant | Pellet Slurry (choose one) | | | | | | |
| Installation Method: <u>Gravit</u> | | | | 602.99 | 18.10 | Top of Seal | |
| Setting Time: 30 minutes | | | | 602.04 | _19.05_ | Top of Sand P | ack |
| Type of Sand Pack: Quartz Sand | 1 | | | | | | |
| Grain Size: 10-20 (sie | ve size) | | | 600.43 | _20.66_ | Top of Screen | |
| Installation Method: Gravit | / | | | 505.60 | 25.40 | - | |
| Type of Backfill Material: | | | | <u>595.60</u> <u>595.17</u> | <u>25.49</u> <u>25.92</u> | Bottom of Scr Bottom of We | |
| Installation Method: | (if applicable) | | | 595.17 | 25.92 | Bottom of Bor | ehole |
| instanction rection. | | | | * Referenced to a | | | CHOIC |
| | | | | CAS | SING MEAS | SUREMENTS | |
| WELL GOVE | TRANSPORT OF THE PART OF | | Dia | ameter of Boreho | ole | (inch | es) 8.0 |
| | TRUCTION MATERIALS e type of material for each area) | | ID | of Riser Pipe | | (inch | es) 2.0 |
| | | | | otective Casing L | ength | | |
| Protective Casing | SS304 SS316 PTFE PVC | OTHER: Steel | | ser Pipe Length | F 10 | , | |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC | | | ttom of Screen to | | | 4.02 |
| Riser Pipe Below W.T. | | OTHER: | | reen Length (1st tal Length of Cas | | t) (fe | • • • • • |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

SS304

Well Completion Form (revised 02/06/02)

| Illinois Environ | nmental Protection Agency | | | Well | Completion | Report |
|---|--|----------------|--------------------------------|---------------------------|---|-------------------|
| Site #: | County: M | ontgomery | | W | /ell #:T4 | 09 |
| Site Name: Coffeen Power St | ation - Ash Pond 2 | | | В | orehole #: | Γ409 |
| State Plane Coordinate: X 2,514,69 | 3.9 Y 872,517.8 (or) Latitud | e: <u>39</u> _ | <u>3! 37.079</u> Ä | Longitude | e: <u>-89</u> <u>23</u> | ! <u>54.736</u> Ä |
| Surveyed By: Gary C. Rogers | | _ IL Registra | ation #:035-00 | 2957 | | |
| Drilling Contractor: Bulldog I | Orilling, Inc. | _ Driller: _ | J. Dittmaier | | | |
| Consulting Firm: Hanson Prof | fessional Services Inc. | _ Geologist: | Rhonald W. H | Hasenyager | , LPG #196-0002 | 246 |
| Drilling Method: Hollow stem | ı auger | _ Drilling Fl | uid (Type): <u>non</u> | ne | | |
| Logged By: Kristen L. Theest | feld | _ Date Starte | ed: 8/19/201 | .6 Date | e Finished: 8/1 | 9/2016 |
| Report Form Completed By: Su | uzanna L. Keim | _ Date: | 8/24/2016 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | 625.35 | -3.50 | Top of Protective | Casing |
| | | | 625.01 | -3.16 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 621.85 | 0.00 | Ground Surface | |
| Towns of Assessing Contacts. High | | | 619.85 | 2.00 | Top of Annular S | ealant |
| Type of Annular Sealant: High- Installation Method: Tremi | 7 | | | | | |
| Setting Time: >24 hours | | $\bar{\Delta}$ | | | Static Water Leve (After Completion) | :1 |
| Type of Bentonite Seal Gran | | | | | (| |
| Installation Method: <u>Gravit</u> | (choose one) | | 602.65 | 19.20 | Top of Seal | |
| Setting Time: 30 minutes | | | 601.30 | 20.55 | Top of Sand Pack | [|
| Type of Sand Pack: Quartz San | nd | | | | | |
| Grain Size: 10-20 (si | eve size) | == | 600.06 | 21.79 | Top of Screen | |
| Installation Method: Gravit | ty | | | | | |
| Type of Backfill Material: | | | <u>595.26</u> <u>594.86</u> | 26.59 26.99 | Bottom of Screen Bottom of Well | |
| | (if applicable) | | 504.96 | 26.00 | D-# | .1. |
| installation Method: | | | * Referenced to a N | 26.99 National Geodeti | Bottom of Boreho | ie |
| | | | CASI | NG MEAS | SUREMENTS | |
| | | D | iameter of Borehol | | (inches) | 8.0 |
| | STRUCTION MATERIALS ne type of material for each area) | II | O of Riser Pipe | | (inches) | 2.0 |
| | | Pı | rotective Casing Le | ength | (feet) | 5.0 |
| Dustrative Ci | SC204 SC217 PIEE PLG COVERN | | iser Pipe Length | | | 24.95 |
| Protective Casing Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTHER SS304 SS316 PTFE (PVC) OTHER | | ottom of Screen to | | (feet) | 0.40 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OTHER | | creen Length (1st | | | 4.80 30.15 |
| r | 1 (2.2) 3111151 | | otal Length of Casi | mg | (feet) | 30.13 |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

SS304

Well Completion Form (revised 02/06/02)

| Illinois Environ | mental Protection Agency | | | Well C | Completion | Report |
|--|---|----------------|-----------------------------|--|---------------------------------------|---------|
| Site #: | County: | | | Well | #:TA | .31 |
| Site Name: Coffeen Power Sta | ation | | | Borel | hole #: | ГА31 |
| State | 5.8 Y 876,542.2 (or) Latitud | e: <u>39</u> | 4! <u>16.930</u> Ä | | | |
| Surveyed By: Gary C. Rogers | | _ IL Registr | ation #: <u>035-0</u> | 02957 | | |
| Drilling Contractor: Ramsey | | _ Driller: _ | B. Williamson | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | _ Geologist: | Rhonald W. | Hasenyager, L | .PG #196-0002 | 246 |
| Drilling Method: Hollow Stem | Auger | _ Drilling Fl | luid (Type): <u>no</u> | ne | | |
| Logged By: Rhonald W. Hase | enyager | _ Date Start | ed: 10/28/20 | 014 Date Fi | inished: 10/ | 28/2014 |
| Report Form Completed By: Rh | nonald W. Hasenyager | _ Date: | 11/5/2014 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | | | 626.90 | | op of Protective | Casing |
| | | | 626.55 | | op of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 623.89 | 0.00 G | round Surface | |
| | | | 620.89 | | op of Annular S | ealant |
| Type of Annular Sealant: Benton | nite | | 020.87 | | op of Afficial S | calant |
| Installation Method: <u>tremie</u> | | | | | | |
| Setting Time: 45 min. | | $\bar{\Delta}$ | 615.78 | | tatic Water Leve After Completion) | |
| Type of Bentonite Seal Gran | ular Pellet Slurry | | | | | |
| Installation Method: Gravit | (choose one) | | 613.56 | 10.33 To | on of Seal | |
| Setting Time: 30 min. | | | | | • | |
| 5600mg 1 mile | | | 610.81 | 13.08 To | op of Sand Pack | : |
| Type of Sand Pack: Quartz Sand | d | | 600.00 | 15.00 | | |
| Grain Size:10/20 (sie | eve size) | | 608.80 | 15.09 To | op of Screen | |
| Installation Method: Gravit | y & Surge | | (04.22 | 10.57 D | | |
| Type of Backfill Material: <u>n/a</u> | | | 604.32 603.70 | | ottom of Screen ottom of Well | |
| Installation Method: | (if applicable) | | 602.70 | 20.10 D | -# | -1- |
| installation Method. | | | 603.70 * Referenced to a | 20.19 Boundary Bounda | ottom of Boreho atum | ne |
| | | | CAS | SING MEASU | REMENTS | |
| | | D | viameter of Boreho | | (inches) | 8.0 |
| | STRUCTION MATERIALS e type of material for each area) | | O of Riser Pipe | | (inches) | 2.0 |
| • | | P | rotective Casing L | ength | (feet) | 5.0 |
| D | | | iser Pipe Length | | ` ' | 17.82 |
| Protective Casing | SS304 SS316 PTFE PVC OTHER SS304 SS316 PTFE PVC OTHER | | ottom of Screen to | | (feet) | 0.55 |
| Riser Pipe Above W.T. Riser Pipe Below W.T. | SS304 SS316 PTFE (PVC) OTHER SS304 SS316 PTFE (PVC) OTHER | | creen Length (1s | | (feet) | 4.48 |
| raser i ipe below w.1. | SSSOT SSSTO THE TVC OTHER | <u> </u> | otal Length of Ca | sıng | (feet) | 22.85 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | mental Protection Ag | ency | | | Well | Completi | on Report |
|-------------------------------------|-----------------------------------|--------------|----------|--------------------------------------|------------------|-----------------------------------|-------------------------|
| Site #: | County | y: | | | W | /ell #: | TA32 |
| Site Name: Coffeen Power Sta | ation | | | | Во | orehole #: | TA32 |
| State Plane Coordinate: X 2,513,605 | 5.2 Y <u>877,532.6</u> (or) | Latitude: 3 | 9 | 4! <u>26.730</u> Ä | Longitude | e: <u>89</u> _ | 24! <u>8.000Ä</u> |
| Surveyed By: Gary C. Rogers | | IL F | Registra | tion #:035-00 | 02957 | | |
| Drilling Contractor: Ramsey | | Dril | ler:I | B. Williamson | | | |
| Consulting Firm: Hanson Profe | essional Services Inc. | Geo | ologist: | Rhonald W. | Hasenyager | , LPG #196-0 | 00246 |
| Drilling Method: Hollow Stem | Auger | Dril | ling Flu | uid (Type): <u>no</u> | ne | | |
| Logged By: Rhonald W. Hase | nyager | Date | e Starte | d: <u>10/27/20</u> |)14 Date | e Finished: | 10/27/2014 |
| Report Form Completed By: Rh | onald W. Hasenyager | Date | e: | 11/5/2014 | | | |
| ANNULAR SPA | CE DETAILS | | | Elevations (MSL)* | Depths (BGS) | (0.01 | ft.) |
| | | | | 621.76 | -2.83 | Top of Protec | tive Casing |
| | | | | 621.42 | -2.49 | Top of Riser I | · · |
| Type of Surface Seal: Concrete | | | | 618.93 | 0.00 | Ground Surfa | |
| | | | | | | | |
| Type of Annular Sealant: Benton | nite | | | 616.03 | 2.90 | Top of Annula | ar Sealant |
| Installation Method: <u>tremie</u> | | | | | | | |
| Setting Time: 30 min. | | | | 604.88 | _14.05_ | Static Water I (After Completi | |
| Type of Bentonite Seal Gran | ular Pellet Slurry | | | | | | |
| Installation Method: Gravit | (choose one) | | | 611.09 | 7.84 | Top of Seal | |
| Setting Time: 35 min. | | | | | | • | |
| | _ | | | _609.18_ | 9.75 | Top of Sand I | ack |
| Type of Sand Pack: Quartz Sand | <u>d</u> | | | 607.62 | 11.31 | Top of Screen | |
| Grain Size:10/20 (sie | | | | _007.02_ | | Top of Screen | |
| Installation Method: <u>Gravit</u> | y | | | 603.25 | 15.68 | Bottom of Scr | een |
| Type of Backfill Material:n/a_ | (if applicable) | | | 602.46 | 16.47 | Bottom of We | |
| Installation Method: | * ** | | | 602.46 | _16.47_ | Bottom of Bo | rehole |
| | | | | * Referenced to a | National Geodeti | c Datum | |
| | | | | CAS | ING MEAS | SUREMENTS | 3 |
| WELL CONS | STRUCTION MATERIALS | | Dia | ameter of Boreho | ole | (incl | |
| | e type of material for each area) | | | of Riser Pipe | .11 | (incl | |
| | | | | otective Casing L ser Pipe Length | | | eet) 5.0 eet) 13.94 |
| Protective Casing | SS304 SS316 PTFE PVC | OTHER: Steel | | ttom of Screen to | End Cap | • | eet) 13.94 eet) 0.65 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC | OTHER: | | reen Length (1s | | | eet) 4.37 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC | OTHER: | | tal Length of Cas | | | eet) 18.96 |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

SS304

Well Completion Form (revised 02/06/02)

| Illinois Environmental Protection Ag | ency | | Well Comp | letion Report |
|--|---------------|---|----------------------|-----------------------------------|
| Site #: County | y: Montgomery | | Well #: | TA33 |
| Site Name: Coffeen Well Sealing & Assmt Well Install | | | Borehole #: | TA33b |
| State Plane Coordinate: X 2,513,248.7 Y 876,605.4 (or) | Latitude: 39 | 4! <u>17.500</u> Ä | Longitude: 89 | 24!12.700Ä |
| Surveyed By: Gary C. Rogers | IL Regis | tration #:035-0029 | 957 | |
| Drilling Contractor: Ramsey | Driller: | B. Williamson | | |
| Consulting Firm: Hanson Professional Services Inc. | Geologis | t: <u>Rhonald W. Ha</u> | senyager, LPG#1 | 96-000246 |
| Drilling Method: Hollow Stem Auger | Drilling | Fluid (Type): None |) | |
| Logged By: Suzanna L. Keim | Date Sta | rted: 6/2/2015 | Date Finished | 6/2/2015 |
| Report Form Completed By: Suzanna L. Keim | Date: | 6/4/2015 | _ | |
| ANNULAR SPACE DETAILS | | | Depths (0 (BGS) | .01 ft.) |
| | | , , | | rotective Casing |
| | | 625.27 | -2.76 Top of R | iser Pipe |
| Type of Surface Seal: Concrete | | | 0.00 Ground | Surface |
| | | 620.51 | 2.00 Top of A | nnular Sealant |
| Type of Annular Sealant: High-solids bentonite | | | | |
| Installation Method: Tremie | | (15.51 | 7.00 Statis W | -4 Il |
| Setting Time: _ >48 hrs. | | _615.51 | | ater Level mpletion) 6/16/2015 |
| Type of Bentonite Seal Granular Pellet Slurry | | | | |
| Installation Method: Gravity | | 614.51 | 8.00 Top of S | eal |
| Setting Time: 30 minutes | | 612.11 | 10.40 Top of S | and Pack |
| | | 012.11 | 10,40 10p 01 5 | and I ack |
| Type of Sand Pack: Quartz sand | | 610.28 | 12.23 Top of S | creen |
| Grain Size: 10-20 (sieve size) | | | 12.23 10p 01 5 | or con |
| Installation Method: <u>Gravity</u> | | 605.62 | 16.89 Bottom o | of Screen |
| Type of Backfill Material:(if applicable) | | | 17.44 Bottom o | of Well |
| Installation Method: | | 605.07 | 17.44 Bottom o | of Borehole |
| | | * Referenced to a Nat | ional Geodetic Datum | |
| | _ | CASIN | G MEASUREME | ENTS |
| WELL CONSTRUCTION MATERIALS | | Diameter of Borehole | | (inches) 7.5 |
| (Choose one type of material for each area) | | ID of Riser Pipe | .d | (inches) 2.0 |
| | | Protective Casing Leng | | |
| Protective Casing SS304 SS316 PTFE PVC | | Riser Pipe Length Bottom of Screen to En | nd Con | , , , |
| Riser Pipe Above W.T. SS304 SS316 PTFE PVC | | Screen Length (1st slo | | (feet) 0.55 (feet) 4.66 |
| | OTTUEN | Total Length of Casing | | (feet) 4.00 (feet) 20.20 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | nmental Protection Agen | cy | | Well | Completion | Report |
|---|--|-----------------|-----------------------------|-----------------------|------------------------------------|------------------|
| Site #: | County: _ | Montgomery | | W | ell #:TA | .34 |
| Site Name: Coffeen Well Sea | ling & Assmt Well Install | | | Во | orehole #:T | A34 |
| State Plane Coordinate: X 2,513,46 | 6.7 Y 875,906.1 (or) Latin | tude: <u>39</u> | 4! <u>10.500</u> Ä | Longitude | : <u>89</u> <u>24</u> | <u> 10.000</u> Ä |
| Surveyed By: Gary C. Rogers | | IL Regis | tration #:035-0 | 02957 | | |
| Drilling Contractor: Ramsey | | Driller: | B. Williamson | | | |
| Consulting Firm: Hanson Prof | Pessional Services Inc. | Geologis | et: Rhonald W. | Hasenyager, | , LPG #196-0002 | 246 |
| Drilling Method: Hollow Sten | n Auger | Drilling | Fluid (Type): No | one | | |
| Logged By: Suzanna L. Keim | 1 | Date Sta | rted:6/3/201 | 15 Date | Finished: 6/2 | 3/2015 |
| Report Form Completed By: St | ızanna L. Keim | Date: | 6/4/2015 | | | |
| ANNULAR SPA | CE DETAILS | | Elevations (MSL)* | Depths (BGS) | (0.01 ft.) | |
| | _ | | 626.77 | · · | Top of Protective | Casing |
| | | | _626.52 | 2.42 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | | 624.10 | 0.00 | Ground Surface | |
| | | | 623.10 | 1.00 | Top of Annular So | ealant |
| Type of Annular Sealant: Bento Installation Method: Gravit | | | | | | |
| 0 | <u></u> | | 616.00 | 8.10 | Static Water Leve | 1 |
| | | | | | (After Completion) | 5/16/2015 |
| Type of Bentonite Seal Gran | nular Pellet Slurry (choose one) | | | | | |
| Installation Method:n/a | | | n/a | n/a | Top of Seal | |
| Setting Time: <u>n/a</u> | | | 615.10 | 9.00 | Top of Sand Pack | |
| Type of Sand Pack: Quartz san | d | | | | | |
| Grain Size: 10-20 (si | | | 613.18 | _10.92_ | Top of Screen | |
| Installation Method: Graving | ty | | | | | |
| Type of Backfill Material: n/a | | | 608.69 608.00 | <u>15.41</u> 16.10 | Bottom of Screen Bottom of Well | |
| Type of Backini Materialii/a_ | (if applicable) | | _008.00_ | | Bottom of Well | |
| Installation Method: | | | 608.00 * Referenced to a | | Bottom of Boreho | le |
| | | | CAS | | LIDEN GENERG | |
| | | Γ | Diameter of Boreho | | UREMENTS | 7.5 |
| | STRUCTION MATERIALS ne type of material for each area) | | ID of Riser Pipe | <i>7</i> 10 | (inches) | 2.0 |
| (Choose of | ic type of material for each area) | Г | Protective Casing L | ength | (feet) | 5.0 |
| | | | Riser Pipe Length | | ì | 13.34 |
| Protective Casing | SS304 SS316 PTFE PVC OT | HER: Steel | Bottom of Screen to | o End Cap | (feet) | 0.69 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OTI | HER: | Screen Length (1s | st slot to last slot |) (feet) | 4.49 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC OT | HER: | Total Length of Cas | sing | (feet) | 18.52 |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

SS304

Well Completion Form (revised 02/06/02)

| Illinois Enviro | nmental Protect | ion Agen | ıcy | | Wel | l Comple | etion | Report |
|--|--|-------------------|---------|-------------------|--------------------|-------------------|--------------|------------------|
| Site #: | Co | ounty: | | | | Well #: | TF | 132 |
| Site Name: <u>Coffeen Power S</u> | tation | | | | | Borehole # | : <i>'</i> | ГR32 |
| State Plan€oordinate: X_2,513,605 | .0 Y <u>877,523.7</u> (o: | r) Latitude: | 39° | <u>4'</u> 266 | 63.000"Long | gitude: 89° | 24 | <u>l' 8.070"</u> |
| Surveyed By: Kyle J. Nolan | | | IL Reg | istration #: | 035-00391 | .9 | | |
| Drilling Contractor: Ramsey | Geotechnical Engineerii | ng, LLC | Driller | : B. Willian | mson | | | |
| Consulting Firm: Hanson Pro | ofessional Services Inc. | | Geolog | ist: <u>Rhona</u> | ld W. Haseı | nyager, LPG | #196-0 | 000246 |
| Drilling Method: Hollow Ster | m Auger | | Drillin | g Fluid (Type) | : <u>none</u> | | | |
| Logged By: Rhonald W. Has | enyager | | Date S | tarted:7/ | 2/2019 | Date Finished | d: <u>7/</u> | 2/2019 |
| Report Form Completed By:F | Rhonald W. Hasenyager | | Date: | 7/3/20 |)19 | | | |
| ANNULAR SPAC | CE DETAILS | | | Elevation (MSL) | ons Dept * (BGS | | 0.01 ft.) |) |
| | | | | 621.9 | | 9 Top of P | rotectiv | e Casing |
| | | T | | | | | | |
| | | | | 621.6 | 82.4 | <u>0</u> Top of R | liser Pip | e |
| Type of Surface Seal: <u>Concrete</u> | | | | 619.28 | 8 0.00 | Cround | Surface | |
| Type of Annular Sealant: Bent | onite | | | 616.2 | 8 3.00 | Top of A | nnular S | Sealant |
| Installation Method: Grav | | - | 14 | | | | | |
| Setting Time: 30 min. | | - _ <u>\</u> | 7 | | | Static W | ater Lev | rel |
| Setting Time | | - - | - | | _ | | mpletion) | |
| Type of Bentonite Seal Grand | ular Pellet Slurry | | | | | | | |
| Installation Method: | | _ | × × | n/a | n/a | Top of S | eal | |
| Setting Time: | | - | | 609.7 | 7 95 | 1 Top of S | and Pac | k |
| | | | | | <u></u> | | uu. | |
| Type of Sand Pack: Quartz San | | - | | 608.2 | 8 11.0 | 0 Top of S | creen | |
| Grain Size: 10/20 (sie | • | | | | | <u> </u> | crecii | |
| Installation Method: <u>Grav</u> | ity | - | | 603.6 | 0 15.6 | 8 Bottom | of Scree | n |
| Type of Backfill Material: <u>n/a</u> | (if applicable) | | | 603.1 | | | | |
| Installation Method: | | | | 603.1 | 1 16.1 | 7 Bottom | of Borok | volo |
| installation Method. | | | | | ced to a National | | or borer | ioic |
| | | | | | CASING M | EASUREME | NTS | |
| | | | | Diameter of | | | (inches) | 8.0 |
| | TRUCTION MATERIALS type of material for each area) | | | ID of Riser P | ipe | | (inches) | 2.0 |
| | | | | Protective Ca | asing Length | | (feet) | 5.0 |
| D. d. di . C. d | 00004 00047 7777 | UC 2007 (F | | Riser Pipe Le | | | | 13.40 |
| Protective Casing Riser Pipe Above W.T. | | VC OTHER: St | teei | | | Сар | | 0.49 |
| Riser Pipe Above W.T. Riser Pipe Below W.T. | | VC OTHER: | | | | last slot) | | 4.68 |
| Taser I ipe Delow W.I. | | . J O | | Total Length | or casing | | (feet) | 18.57 |

SS304

Well Completion Form (revised 02/06/02)

SS316

Total Length of Casing

**Hand-Slotted Well Screens Are Unacceptable

Screen Slot Size **

0.010

| Illinois Environ | nmental Protection Age | ency | | | Well | Complet | tion Report |
|--|------------------------------------|-------------|------------|------------------------------------|-----------------------|------------------------------|-----------------------|
| Site #: | County: _ | Montgor | nery | | | Well #: | G307D |
| Site Name: Coffeen Part 845 | Groundwater | | | | Ι | Borehole #: | G307D |
| State | 0.3 Y 871,397.2 (or) Lat | | | | | | |
| | | | | tion #:035-0 | | | |
| Drilling Contractor: Roberts E | nv. Drilling Inc. | Dr | iller:] | Matt | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | Ge | ologist: | Rhonald W. | Hasenyage | er, LPG #196 | 5-000246 |
| Drilling Method: Hollow stem | auger | Dr | illing Flu | uid (Type): No | one | | |
| Logged By: Colin Winter | | Da | te Starte | d:2/9/202 | 21 Da | te Finished: _ | 2/9/2021 |
| Report Form Completed By:Co | lin Winter | Da | te: | 5/3/2021 | | | |
| ANNULAR SPA | CE DETAILS | | | Elevations (MSL)* | Depths (BGS) | (0.0) | 1 ft.) |
| | | | _ | 625.29 | -2.78 | Top of Prote | ective Casing |
| | | | | 624.88 | -2.37 | Top of Rise | r Pipe |
| Type of Surface Seal: Concrete | = | 4 | <u></u> | 622.51 | 0.00 | Ground Sur | face |
| | | | | 621.51 | 1.00 | • | |
| Type of Annular Sealant: High-s | solids bentonite | | | 021.31 | | _ 10p 01711111 | and Soundin |
| Installation Method: Tremie | | | | | | | |
| Setting Time: >24 hours | | | | | | Static Water (After Compl | |
| Type of Bentonite Seal Gran | ular Pellet Slurry — | | | | | | |
| Installation Method: Gravity | (choose one) | | | 575.51 | 47.00 | Top of Seal | |
| Setting Time: 30 minutes | | | \ I | | | . 1 | |
| setting Time. <u>30 minutes</u> | | | | 574.51 | 48.00 | Top of Sand | l Pack |
| Type of Sand Pack: Quartz sand | <u> </u> | | | | | | |
| Grain Size:10-20 (sie | ve size) | | | 573.53 | 48.98 | Top of Scree | en |
| Installation Method: Gravity | 1 | | | | | | |
| Type of Backfill Material: N/A | | | | <u>563.76</u> 562.91 | <u>58.75</u> 59.60 | Bottom of S Bottom of V | |
| Type of Backini Material. ———————————————————————————————————— | (if applicable) | | | 302.71 | | _ Boutoni or v | , cii |
| Installation Method: | | | | 562.51 * Referenced to a | 60.00 National Geode | Bottom of E | Borehole |
| | | | | | | | |
| | | | | | | SUREMEN' | |
| | TRUCTION MATERIALS | | | ameter of Boreho | | , | aches) 8.0 |
| (Choose or | te type of material for each area) | | | of Riser Pipe otective Casing L | | | (feet) 2.0 (feet) 5.0 |
| | | | | ser Pipe Length | ongui | | (feet) 51.85 |
| Protective Casing | SS304 SS316 PTFE PVC OT | THER: Steel | \neg | ottom of Screen to | End Cap | | (feet) 0.35 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC OF | THER: | | reen Length (1s | | | (feet) 9.77 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC O | THER: | Тс | tal Length of Cas | sing | | (feet) 61.97 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | nmental Protection | 1 Agency | | | | Well | Complet | ion Report |
|---|---------------------------------|---|-------------|------------|------------------------------------|-----------------|-------------------------------|-----------------------------|
| Site #: | C | ounty: Mon | tgomery | у | | | Well #: | G308 |
| Site Name: Coffeen Part 845 | Groundwater | | | | | F | Borehole #: | G308 |
| State Plane Coordinate: X 2,515,101 | 1.4 Y <u>871,454.7</u> (c | or) Latitude: | | | | Longitud | le: | |
| Surveyed By: Kyle J. Nolan | | | IL Reg | istrati | on #: <u>035-0</u> 0 | 03919 | | |
| Drilling Contractor: Roberts En | nv. Drilling Inc. | | Driller: | : <u>N</u> | S att | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | | Geolog | gist: _ | Rhonald W. | Hasenyage | er, LPG #196 | -000246 |
| Drilling Method: Hollow stem | auger | | Drilling | g Flui | d (Type): No | one | | |
| Logged By: Colin Winter | | | Date St | tarted | :1/13/20 | 21 Da | te Finished: | 1/13/2021 |
| Report Form Completed By:Co | lin Winter | | Date: | | 5/3/2021 | | | |
| ANNULAR SPA | CE DETAILS | | | | Elevations (MSL)* | Depths (BGS) | (0.01 | ft.) |
| | | | | | 624.96 | -3.37 | Top of Prote | ctive Casing |
| | | | | | 624.59 | -3.00 | Top of Riser | Pipe |
| Type of Surface Seal: Concrete | | - = | | - | 621.59 | 0.00 | Ground Surf | ace |
| | | | | | 621.39 | 0.20 | • | |
| Type of Annular Sealant: Benton | | - 1 | | | | | . 1 | |
| Installation Method: Gravity | 7 | _ | | | | | | |
| Setting Time: >24 hours | | _ \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\ | <u>Z</u> | | | | Static Water (After Comple | |
| Type of Bentonite Seal Gran | ular Pellet Slurry | | | - | | | | |
| Installation Method: | , | _ 😾 | \boxtimes | | n/a | n/a | Top of Seal | |
| Setting Time: | | _ | | | 612.59 | 9.00 | Top of Sand | Pack |
| Type of Sand Books of G | | | | | | | • | |
| Type of Sand Pack: Quartz Sand Grain Size: 10-20 (sie | | _ _ | | | 611.49 | 10.10 | Top of Scree | en |
| Installation Method: Gravity | | | | | | | | |
| nistanation Method. Oravity | | _ | | | 606.70 | 14.89 | Bottom of Se | creen |
| Type of Backfill Material: N/A | (if applicable) | _ _ | | | 606.35 | 15.24 | Bottom of W | /ell |
| Installation Method: | | | | | 605.79 | 15.80 | Bottom of B | orehole |
| | | | | | * Referenced to a | National Geode | tic Datum | |
| | | | | | CAS | ING MEA | SUREMENT | ΓS |
| WELL CONS | TRUCTION MATERIAL | S | | Dia | meter of Boreho | ole | (in | ches) 8.0 |
| | type of material for each area) | | | | of Riser Pipe | | | ches) 2.0 |
| | | | | | tective Casing L | - | | (feet) 5.0 |
| Protective Casing | SS304 SS316 PTFE F | PVC OTHER: S | teel | | er Pipe Length tom of Screen to | | | (feet) 13.10 (feet) 0.35 |
| Riser Pipe Above W.T. | | VC OTHER: | | | een Length (1s | • | | (feet) 0.35 (feet) 4.79 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE F | OTHER: | | | al Length of Cas | | | (feet) 4.79 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviror | imental Prot | ection Agency | | | | Well | Comple | tion Report |
|---|-------------------------------|----------------|------------------------------|---------------|--------------|------------------------------|------------------------------|-----------------------------|
| Site #: | | County: Mor | itgomery | 7 | | | Well #: | G309 |
| Site Name: Coffeen Part 845 | Groundwater | | | | | F | Borehole #: | G309 |
| State Plane Coordinate: X 2,515,067 | | | | | | | | |
| Surveyed By: Kyle J. Nolan | | | IL Reg | stration #: _ | 035-0 | 03919 | | |
| Drilling Contractor: Roberts En | nv. Drilling Inc. | | Driller: | Matt | | | | |
| Consulting Firm: Hanson Profe | essional Services l | Inc. | Geolog | ist: Rhon | ald W. | Hasenyage | er, LPG #196 | 6-000246 |
| Drilling Method: Hollow stem | auger | | Drilling | g Fluid (Type |): <u>No</u> | one | | |
| Logged By: Colin Winter | | | Date St | arted: | /12/20 |)21 Da | te Finished: _ | 1/12/2021 |
| Report Form Completed By:Co | lin Winter | | Date: _ | 5/3/2 | 2021 | | | |
| ANNULAR SPA | CE DETAILS | | | Eleva (MS | | Depths (BGS) | (0.0) | 1 ft.) |
| | | | | 626 | | 3.43 | Top of Prote | ective Casing |
| | | | | 625 | .88_ | -3.11 | Top of Rise | r Pipe |
| Type of Surface Seal: Concrete | | | | × 622 | .77 | 0.00 | Ground Sur | face |
| | | | | 622 | .27 | 0.50 | Top of Ann | ular Sealant |
| Type of Annular Sealant: Benton | | | | | | | | |
| Installation Method: <u>Gravity</u> | , | | | | | | | |
| Setting Time: >24 hours | | | $\mathbb{Z} \mid \cdot \mid$ | | | | Static Water (After Compl | |
| Type of Bentonite Seal Grant | ılar Pellet (choose one) | Slurry | | | | | | |
| Installation Method: | ` / | | | n/ | a | n/a | Top of Seal | |
| Setting Time: | | | | 610 | .77 | 12.00 | Top of Sano | ł Pack |
| Type of Sand Books | | | | | | | • | |
| Type of Sand Pack: Quartz sand Grain Size: 10-20 (sie | | | | 609 | .80_ | 12.97 | Top of Scre | en |
| Installation Method: Gravity | | | | | | | | |
| installation Method. Gravity | | | | 605 | .02_ | 17.75 | Bottom of S | Screen |
| Type of Backfill Material: N/A | (if applicable) | L | _ | 604 | .67_ | 18.10 | Bottom of V | Vell |
| Installation Method: | | | | 604 | .67_ | 18.10 | Bottom of E | Borehole |
| | | | | * Refer | enced to a | National Geode | tic Datum | |
| | | | | | CAS | SING MEA | SUREMEN | TS |
| WELL CONS | TRUCTION MAT | rediai c | | Diameter o | f Boreh | ole | (ir | nches) 8.0 |
| | e type of material for each a | | | ID of Riser | | | ` | nches) 2.0 |
| | | | | | _ | Length | | (feet) 5.0 |
| Protective Casing | SS304 SS316 P | TFE PVC OTHER: | Steel | Riser Pipe | | | | (feet) 16.08 |
| Riser Pipe Above W.T. | | TFE PVC OTHER: | | | | o End Cap st slot to last sl | | (feet) 0.35 (feet) 4.78 |
| Riser Pipe Below W.T. | | TFE PVC OTHER: | | Total Lengt | | | | (feet) 4.78 (feet) 21.21 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | nmental Protectio | n Agency | | | | Well | Complet | ion Report |
|---|------------------------------------|-------------------------------------|-------------|------------|----------------------------------|-----------------|-------------------------------|--------------------------|
| Site #: | | County: <u>Mon</u> | tgomery | у | | | Well #: | G310 |
| Site Name: Coffeen Part 845 | Groundwater | | | | | F | Borehole #: | G310 |
| State Plane Coordinate: X 2,515,159 | 9.4 Y <u>872,239.4</u> (| (or) Latitude: | | | | Longitud | le: | |
| Surveyed By: Kyle J. Nolan | | | IL Reg | istratio | on #:035-0 | 03919 | | |
| Drilling Contractor: Roberts Ex | nv. Drilling Inc. | | Driller: | : <u>M</u> | att | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | | Geolog | gist: _ | Rhonald W. | Hasenyage | er, LPG #196 | -000246 |
| Drilling Method: Hollow stem | auger | | Drilling | g Fluid | 1 (Type): <u>No</u> | one | | |
| Logged By: Colin Winter | | | Date St | tarted: | 1/15/20 | 21 Da | te Finished: | 1/15/2021 |
| Report Form Completed By:Co | olin Winter | | Date: _ | | 5/3/2021 | | | |
| ANNULAR SPA | CE DETAILS | | | I | Elevations (MSL)* | Depths (BGS) | (0.01 | ft.) |
| | | | | | 623.32 | -3.43 | Top of Prote | ctive Casing |
| | | | | | 622.87 | -2.98 | Top of Riser | Pipe |
| Type of Surface Seal: Concrete | | | | - | 619.89 | 0.00 | Ground Surf | ace |
| | | | | | 619.39 | 0.50 | • | |
| Type of Annular Sealant: Benton | | | | | | | . 1 | |
| Installation Method: Gravity | ÿ. | _ | | | | | | |
| Setting Time: >24 hours | | \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ | <u> </u> | | | | Static Water (After Comple | |
| Type of Bentonite Seal Gran | ular Pellet Slurry | | | - | | | | |
| Installation Method: | ` ' | _ | \boxtimes | | n/a | n/a | Top of Seal | |
| Setting Time: | | _ 🐰 | | | 610.69 | 9.20 | Top of Sand | Pack |
| Type of Sand Books | | | | | | | • | |
| Type of Sand Pack: Quartz sand Grain Size: 10-20 (sie | | _ _ | | | 609.65 | 10.24 | Top of Scree | en |
| Installation Method: Gravity | | | | | | | | |
| | | | | | 604.86 | 15.03 | | |
| Type of Backfill Material: N/A | (if applicable) | _ _ | | | 604.51 | 15.38 | Bottom of W | Vell . |
| Installation Method: | | | | | 603.99 * Referenced to a | 15.90 | Bottom of Bo | orehole |
| | | | | | * Referenced to a | National Geode | uc Datum | |
| | | | | | CAS | ING MEA | SUREMENT | TS |
| WELL CONS | TRUCTION MATERIA | LS | | | meter of Boreho | | | ches) 8.0 |
| | ne type of material for each area) | | | | f Riser Pipe | anath | ` | thes) 2.0 feet) 5.0 |
| | | | | | ective Casing L r Pipe Length | - | | feet) 5.0 feet) 13.22 |
| Protective Casing | SS304 SS316 PTFE | PVC OTHER: S | teel | | om of Screen to | | | feet) 0.35 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE | PVC OTHER: | | | en Length (1s | • | | feet) 4.79 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE | PVC OTHER: | | | l Length of Cas | | | feet) 18.36 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | nmental Protection | n Agency | | | | Well | Complet | ion Report |
|-------------------------------------|-----------------------------------|---------------|----------|-------------|----------------------------------|-----------------|---------------|--------------------------|
| Site #: | (| County: Mon | tgomer | у | | | Well #: | G311 |
| Site Name: Coffeen Part 845 | Groundwater | | | | | E | Borehole #: | G311 |
| State Plane Coordinate: X 2,515,881 | 1.8 Y <u>872,238.7</u> (6 | or) Latitude: | | | | Longitud | le: | |
| Surveyed By: Kyle J. Nolan | | | IL Reg | istratio | on #:035-0 | 03919 | | |
| Drilling Contractor: Roberts Ex | nv. Drilling Inc. | | Driller: | : <u>M</u> | att | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | | Geolog | gist: _ | Rhonald W. | Hasenyage | er, LPG #196 | -000246 |
| Drilling Method: Hollow stem | auger | | Drilling | g Fluid | 1 (Type): <u>No</u> | one | | |
| Logged By: Colin Winter | | | Date S | tarted: | 2/5/202 | 21 Da | te Finished: | 2/5/2021 |
| Report Form Completed By:Co | lin Winter | | Date: | | 5/3/2021 | | | |
| ANNULAR SPA | CE DETAILS | | | I | Elevations (MSL)* | Depths (BGS) | (0.01 | ft.) |
| | | | | | 621.55 | 3.23 | Top of Prote | ctive Casing |
| | | | | | 621.04 | -2.72 | Top of Riser | Pipe |
| Type of Surface Seal: Concrete | | | | - - > | 618.32 | 0.00 | Ground Surf | ace |
| | | | | | 617.52 | 0.80 | Top of Annu | ılar Sealant |
| Type of Annular Sealant: Benton | - | - | | | | | | |
| Installation Method: Gravity | / | _ 7 | 7 | | | | Static Water | I aval |
| Setting Time:>24 hours | | _ _ | _ | | | | (After Comple | |
| Type of Bentonite Seal Grant | ular Pellet Slurry | | | - | | | | |
| Installation Method: | , | _ | | | n/a | n/a | Top of Seal | |
| Setting Time: | | _ 🐰 | | | 610.12 | 8.20 | Top of Sand | Pack |
| Type of Sand Pack: Quartz sand | | | | | | | • | |
| Grain Size: 10-20 (sie | | _ _ | | | 609.05 | 9.27 | Top of Scree | en |
| Installation Method: Gravity | | | | | | | | |
| | | | ≣ | | 604.28 | 14.04 | | |
| Type of Backfill Material: N/A | (if applicable) | _ _ | _ | | 603.92 | 14.40 | Bottom of W | /ell |
| Installation Method: | | _ | | | 603.92 * Referenced to a | 14.40 | Bottom of B | orehole |
| | | | | | referenced to a | runonai Geode | de Buttairi | |
| | | | | | | | SUREMENT | |
| | TRUCTION MATERIAI | LS | | | neter of Boreho | | | ches) 8.0 |
| (Choose on | e type of material for each area) | | | | f Riser Pipe | enoth | ` | thes) 2.0 feet) 5.0 |
| | | | | | ective Casing L r Pipe Length | - | | feet) 5.0 feet) 11.99 |
| Protective Casing | SS304 SS316 PTFE I | PVC OTHER: S | teel | | om of Screen to | | | feet) 0.36 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE | PVC OTHER: | | | en Length (1s | • | | feet) 4.77 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE | PVC OTHER: | | | l Length of Cas | | | feet) 17.12 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | nmental Protection A | gency | | | | Well | Comple | tion 1 | Report |
|--|--|-------------|----------|------------|--------------------------------|-----------------------|---------------|-----------|--------|
| Site #: | Coun | ty: Mon | tgomer | у | | | Well #: | G311 | D |
| Site Name: Coffeen Part 845 | Groundwater | | | | |] | Borehole #: | G3 | 11D |
| State Plane Coordinate: X 2,515,881 | | | | | | | de: | | |
| Surveyed By: Kyle J. Nolan | | | IL Reg | istrat | ion #:035-00 | 03919 | | | |
| Drilling Contractor: Roberts En | nv. Drilling Inc. | | Driller: | : <u>N</u> | <u>latt</u> | | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | | Geolog | gist: _ | Rhonald W. | Hasenyag | er, LPG #19 | 6-0002 | 46 |
| Drilling Method: Hollow stem | auger | | Drilling | g Flui | id (Type): No | one | | | |
| Logged By: Colin Winter | | | Date S | tarted | l: <u>2/5/202</u> | 21 Da | te Finished: | 2/5/ | 2021 |
| Report Form Completed By:Co | lin Winter | | Date: | | 5/3/2021 | | | | |
| ANNULAR SPA | CE DETAILS | | | | Elevations (MSL)* | Depths (BGS) | (0.0) | 01 ft.) | |
| | | | | | 621.75 | 3.36 | Top of Pro | tective C | asing |
| | | | | | 621.24 | -2.85 | _ Top of Rise | er Pipe | |
| Type of Surface Seal: Concrete | | | | - | 618.39 | 0.00 | Ground Su | rface | |
| Type of Annular Sealant: High-s | alids bentanite | | | | 617.09 | 1.30 | Top of An | nular Sea | lant |
| Installation Method: Tremie | | | | | | | | | |
| Setting Time: 1 hour | | | <u>z</u> | | | | Static Water | | |
| | | | | - | | | (After Comp | oletion) | |
| Type of Bentonite Seal Gran | Pellet Slurry (choose one) | | Ý T | - | | | | | |
| Installation Method: <u>Gravity</u> | <i>I</i> | | | | 572.39 | 46.00 | Top of Sea | 1 | |
| Setting Time: 30 minutes | | | | | 569.39 | 49.00 | Top of San | d Pack | |
| Type of Sand Pack: Quartz sand | <u> </u> | | | | | | | | |
| Grain Size: 10-20 (sie | ve size) | | | | 568.23 | 50.16 | Top of Scr | een | |
| Installation Method: Tremie | | | | | | | | | |
| Type of Backfill Material: N/A | | | | | <u>558.29</u> <u>557.81</u> | 60.10 | - | | |
| Table Mala | (if applicable) | | | | 557.01 | (0.50 | D // 63 | D 1.1 | |
| Installation Method: | | | | | * Referenced to a l | 60.58 National Geode | _ Bottom of a | Borehole | |
| | | | | | CAS | ING MEA | ASUREMEN | ITS | |
| | | | | Dia | meter of Boreho | | | inches) | 6.0 |
| | TRUCTION MATERIALS e type of material for each area) | | | ID | of Riser Pipe | | (i | inches) | 2.0 |
| | | | | Pro | tective Casing L | ength | | (feet) | 5.0 |
| D + +: C : | 00204 00216 77777 | OFFITTO (** | | | er Pipe Length | | | (feet) | 53.01 |
| Protective Casing | SS304 SS316 PTFE PVC | OTHER: S | teel | | tom of Screen to | | | (feet) | 0.48 |
| Riser Pipe Above W.T. Riser Pipe Below W.T. | SS304 SS316 PTFE (PVC SS304 SS316 PTFE (PVC | OTHER: | | | een Length (1s | | lot) | (feet) | 9.94 |
| Risel I ipe Delow W. I. | 55507 55510 THE CIVE | OTTEK. | | Tot | al Length of Cas | sing | | (feet) | 63.43 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | nmental Protectio | n Agency | | | | Well | Complet | tion Report |
|---|-----------------------------------|--------------------|----------|------------|----------------------------------|-----------------|----------------------------|-----------------------------|
| Site #: | | County: <u>Mon</u> | tgomer | у | | | Well #: | G312 |
| Site Name: Coffeen Part 845 | Groundwater | | | | | I | Borehole #: | G312 |
| State Plane Coordinate: X 2,516,557 | 7.4 Y 872,260.9 | (or) Latitude: | | | | Longitue | de: | |
| Surveyed By: Kyle J. Nolan | | | IL Reg | istratio | on #: <u>035-0</u> | 03919 | | |
| Drilling Contractor: Roberts En | nv. Drilling Inc. | | Driller: | : <u>M</u> | att | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | | Geolog | gist: _ | Rhonald W. | Hasenyag | er, LPG #196 | 5-000246 |
| Drilling Method: Hollow stem | auger | | Drilling | g Fluid | l (Type): <u>No</u> | one | | |
| Logged By: Colin Winter | | | Date S | tarted: | 2/4/202 | 21 Da | te Finished: _ | 2/4/2021 |
| Report Form Completed By:Co | lin Winter | | Date: | | 5/3/2021 | | | |
| ANNULAR SPA | CE DETAILS | | | I | Elevations (MSL)* | Depths (BGS) | (0.01 | l ft.) |
| | | | | | 620.11 | 3.19 | Top of Prote | ective Casing |
| | | | | | 619.78 | -2.86 | Top of Riser | Pipe |
| Type of Surface Seal: Concrete | | | | - | 616.92 | 0.00 | Ground Surf | face |
| | | | | | 615.92 | 1.00 | Top of Annu | ılar Sealant |
| Type of Annular Sealant: Benton | | — Ŋ | | | | | - | |
| Installation Method: Gravity | 7 | _ | 7 | | | | Ct-ti- W-t- | T1 |
| Setting Time: <u>>24 hours</u> | | \[\sqrt{\zeta} | _ | | | | Static Water (After Comple | |
| Type of Bentonite Seal Grand | ılar Pellet Slurry | | | - | | | | |
| Installation Method: | , | | X X | | n/a | n/a | Top of Seal | |
| Setting Time: | | | | | 608.92 | 8.00 | Top of Sand | Pack |
| Town of Court Pools | | | | | | | - 1 | |
| Type of Sand Pack: Quartz sand Grain Size: 10-20 (sie | | _ _ | | | 607.13 | 9.79 | Top of Scree | en |
| Installation Method: Gravity | | | | | | | | |
| | | | | | 602.34 | _14.58 | - | |
| Type of Backfill Material: N/A | (if applicable) | _ _ | | | 601.99 | 14.93 | Bottom of V | Vell |
| Installation Method: | | | | | 601.67 | <u>15.25</u> | Bottom of B | orehole |
| | | | | | * Referenced to a | National Geode | etic Datum | |
| | | | | | CAS | SING MEA | SUREMEN | ΓS |
| WELL CONS | TRUCTION MATERIA | LS | | | neter of Boreho | | | ches) 8.0 |
| | e type of material for each area) | | | | f Riser Pipe | | | ches) 2.0 |
| | | | | | ective Casing L r Pipe Length | <u>-</u> | | (feet) 5.0 (feet) 12.65 |
| Protective Casing | SS304 SS316 PTFE | PVC OTHER: S | teel | | om of Screen to | | | (feet) 12.03 (feet) 0.35 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE | PVC OTHER: | - | | en Length (1s | | | (feet) 4.79 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE | PVC OTHER: | | | l Length of Cas | | | (feet) 17.79 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviro | nmental Protection A | gency | | | | Well | Complet | tion 1 | Report |
|---|---|----------------|---------------|----------|-----------------|-----------------|------------------------------|----------|---------------|
| Site #: | Count | y: <u>Mont</u> | gomery | 7 | | v | Vell #: | G31 | 3 |
| Site Name: Coffeen Part 845 | Groundwater | | | | | E | Sorehole #: | G3 | 313 |
| State Plane Coordinate: X 2,516,80 | 3.7 Y 871,976.8 (or) | Latitude: _ | | | | Longitud | le: | | |
| | | | | | | | | | |
| Drilling Contractor: Roberts I | Env. Drilling Inc. | | Driller: | Mat | t | | | | |
| | fessional Services Inc. | | | | | | er, LPG #196 | | |
| | n auger | | | | | | | | |
| _ | | | | | | | e Finished: | | |
| Report Form Completed By:C | | | | | 5/3/2021 | | _ | | |
| ANNULAR SPA | | | Date: _ | El | evations | Depths | (0.0) | 1 ft.) | |
| | | | | | (MSL)* | (BGS) | | | |
| | | \Box | $\overline{}$ | _ | 614.62 | 3.11_ | Top of Prote | ective C | asing |
| | | | \exists | _ | 614.30 | 2.79 | Top of Rise | r Pipe | |
| Type of Surface Seal: Concrete | | | | > | 611.51 | 0.00 | Ground Sur | face | |
| | , | | | / _ | 611.11 | 0.40 | Top of Ann | ular Sea | ılant |
| Type of Annular Sealant: Bento | | | 19 | | | | | | |
| Installation Method: <u>Gravi</u> | | | | | | | | | |
| Setting Time: >24 hours | | | - | _ | | | Static Water (After Compl | | |
| Type of Bentonite Seal Gran | nular Pellet Slurry | | | | | | | | |
| Installation Method: | (choose one) | | | | n/a | n/a | Top of Seal | | |
| | | | | _ | II u | | rop or sear | | |
| Setting Time: | | | | _ | 606.51 | 5.00 | Top of Sand | d Pack | |
| Type of Sand Pack: Quartz san | d | | | | | | | | |
| Grain Size: <u>10-20</u> (s | ieve size) | | | - | 605.21 | 6.30 | Top of Scre | en | |
| Installation Method: Gravi | ty | | | | | | | | |
| T CD 1CHM : 1 N/A | | | | _ | 600.40 | 11.11 | | | |
| Type of Backfill Material: N/A | (if applicable) | | | _ | 600.05 | 11.46 | Bottom of V | Vell | |
| Installation Method: | | | | _ | 599.51 | 12.00 | | Borehole | ; |
| | | | | * | Referenced to a | National Geodet | ic Datum | | |
| | | | | | CAS | SING MEA | SUREMEN | TS | |
| ***** | OFFICE ON A CONTRACT OF | | | Diame | ter of Boreho | ole | (ir | nches) | 8.0 |
| | STRUCTION MATERIALS one type of material for each area) | | | ID of I | Riser Pipe | | (ir | nches) | 2.0 |
| | | | | | tive Casing I | ength | | (feet) | 5.0 |
| Protective Cosine | SS304 SS316 PTFE PVC | OTHER: (Sto | aal | | Pipe Length | | | (feet) | 9.09 |
| Protective Casing Riser Pipe Above W.T. | SS304 SS316 PTFE PVC SS304 SS316 PTFE PVC | | | | of Screen to | | | (feet) | 0.35 |
| Riser Pipe Below W.T. | | OTHER: | -+ | | Length (1: | | • | (feet) | 4.81 14.25 |
| | 1 | | | 1 Otal I | ength of Ca | sing | | (feet) | 14.43 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | nmental Protectio | n Agency | | | | Well | Comple | tion Repor |
|-------------------------------------|------------------------------------|-------------------------------------|------------------------------|------------|----------------------------------|----------------------|----------------------------|--------------------------|
| Site #: | (| County: Mon | itgomery | у | | | Well #: | G314 |
| Site Name: Coffeen Part 845 | Groundwater | | | | | I | Borehole #: | G314 |
| State Plane Coordinate: X 2,516,852 | 2.1 Y 871,630.2 (| (or) Latitude: | | | | Longitue | de: | |
| Surveyed By: Kyle J. Nolan | | | IL Reg | istrati | on #: <u>035-0</u> | 03919 | | |
| Drilling Contractor: Holcomb | Foundation Engineering (| Co. | Driller: | : <u>S</u> | teve | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | | Geolog | gist: _ | Rhonald W. | Hasenyage | er, LPG #19 | 6-000246 |
| Drilling Method: Hollow stem | auger | | Drilling | g Flui | d (Type): No | one | | |
| Logged By: Colin Winter | | | Date St | tarted | :2/26/20 | 21 Da | te Finished: _ | 2/26/2021 |
| Report Form Completed By:Co | olin Winter | | Date: _ | | 5/3/2021 | | | |
| ANNULAR SPA | CE DETAILS | | | | Elevations (MSL)* | Depths (BGS) | (0.0) | 1 ft.) |
| | | | | | 614.28 | -3.17 | Top of Prot | ective Casing |
| | | | | | 613.88 | -2.77 | Top of Rise | er Pipe |
| Type of Surface Seal: Concrete | | | | - | 611.11 | 0.00 | Ground Sur | face |
| | | | | 7 | 609.11 | 2.00 | - | ular Sealant |
| Type of Annular Sealant: Benton | nite chips | | | | | | _ 10p 0171111 | adar Socialit |
| Installation Method: <u>Gravity</u> | V | _ | | | | | | |
| Setting Time: 1 hour | | \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ | $\mathbb{Z} \mid \cdot \mid$ | | | | Static Wate (After Comp | |
| Type of Bentonite Seal Gran | • | | | - | | | | |
| Installation Method: | (choose one) | | | | n/a | n/a | Top of Seal | 1 |
| Setting Time: | | | | | 507.61 | 12.50 | Ton of Con | d Dools |
| | | | M | | 597.61 | 13.30_ | Top of San | и Раск |
| Type of Sand Pack: Quartz sand | 1 | _ | | | 506 55 | 14 56 | Top of Son | 200 |
| Grain Size: 10-20 (sie | eve size) | | | | _596.55_ | 14.56 | Top of Scre | en |
| Installation Method: Gravity | ý | $- \mid \sqsubseteq$ | | | 501.52 | 10.59 | Bottom of S | 200000 |
| Type of Backfill Material: N/A | | | | | <u>591.53</u> <u>591.09</u> | 19.58 20.02 | Bottom of V | |
| | (if applicable) | | | | 5 01.06 | 20.05 | | |
| Installation Method: | | | | | | 20.05 National Geode | Bottom of I | Borehole |
| | | | | | | DIG ME | | TTC . |
| | | | | D:- | | | ASUREMEN | |
| | TRUCTION MATERIA | LS | | | meter of Boreho of Riser Pipe | ole | , | nches) 8.0 nches) 2.0 |
| (Choose or | ne type of material for each area) | | | | tective Casing L | | | (feet) 5.0 |
| | | | | | er Pipe Length | _ | | (feet) 17.30 |
| Protective Casing | SS304 SS316 PTFE | PVC OTHER: S | teel | Bot | tom of Screen to | End Cap | | (feet) 0.47 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE | PVC OTHER: | | Scre | een Length (1s | st slot to last sl | ot) | (feet) 5.02 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE | PVC OTHER: | | Tota | al Length of Cas | sing | | (feet) 22.79 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | nmental Protection | Agency | | | | Well | Comple | tion l | Report |
|-------------------------------------|---------------------------------|------------------|----------|------------|------------------------------------|-----------------|----------------------------|----------|--------|
| Site #: | Cou | ınty: <u>Mon</u> | tgomery | у | | | Well #: | G314 | D |
| Site Name: Coffeen Part 845 | Groundwater | | | | | I | Borehole #: | G3 | 14D |
| State Plane Coordinate: X 2,516,853 | 3.9 Y 871,642.0 (or) | Latitude: | | | | Longitue | de: | | |
| Surveyed By: Kyle J. Nolan | | | IL Reg | gistrat | ion #:035-00 | 03919 | | | |
| Drilling Contractor: Roberts Ex | nv. Drilling Inc. | | Driller: | : <u>N</u> | <u> latt</u> | | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | | Geolog | gist: _ | Rhonald W. | Hasenyage | er, LPG #19 | 6-0002 | 46 |
| Drilling Method: Hollow stem | auger | | Drilling | g Flu | id (Type): No | one | | | |
| Logged By: Colin Winter | | | Date St | tartec | 1:2/10/20 | 21 Da | te Finished: _ | 2/12 | /2021 |
| Report Form Completed By:Co | lin Winter | | Date: _ | | 5/3/2021 | | | | |
| ANNULAR SPA | CE DETAILS | | | | Elevations (MSL)* | Depths (BGS) | (0.0) | 1 ft.) | |
| | | | | | 614.10 | -3.23 | Top of Prot | ective C | asing |
| | | | | | 613.70 | -2.83 | Top of Rise | er Pipe | |
| Type of Surface Seal: Concrete | | | | - | 610.87 | 0.00 | Ground Sur | face | |
| | _ | | | | 608.87 | 2.00 | • | | ılant |
| Type of Annular Sealant: High-s | | | | | | | . 1 | | |
| Installation Method: Tremie | : | | | | | | | | |
| Setting Time: >24 hours | | | <u> </u> | | | | Static Wate (After Comp | | |
| Type of Bentonite Seal Gran | | | | - | | | | | |
| Installation Method: Gravity | (choose one) | | | | 574.07 | 36.80 | Top of Seal | | |
| Setting Time: 30 minutes | | | | | 572.97 | 37 90 | Top of San | d Dack | |
| | | | | | | | _ Top or San | u i ack | |
| Type of Sand Pack: Quartz sand | | | | | 571.53 | 39.34 | Top of Scre | een | |
| Grain Size: 10-20 (sie | | | | | | | . 1 | | |
| Installation Method: <u>Gravity</u> | | | | | 561.76 | 49.11 | Bottom of S | Screen | |
| Type of Backfill Material: N/A | (if applicable) | | | | 561.40 | 49.47 | Bottom of V | Well | |
| Installation Method: | | | | | 510.57 | 100.30 | Bottom of I | Borehole | ; |
| | | | | | * Referenced to a l | National Geode | tic Datum | | |
| | | | | | CAS | ING MEA | SUREMEN | TS | |
| WELL CONS | TRUCTION MATERIALS | | | Dia | meter of Boreho | ole | (i | nches) | 8.0 |
| | type of material for each area) | | | | of Riser Pipe | | | nches) | 2.0 |
| | | | | | tective Casing L | ength | | (feet) | 5.0 |
| Protective Casing | SS304 SS316 PTFE PVG | C OTHER: (S | teel | | er Pipe Length tom of Screen to | End Com | | (feet) | 0.36 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVG | | | | een Length (1s | • | | (feet) | 9.77 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC | OTHER: | | | al Length of Cas | | / | (feet) | 52.30 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | nmental Protectio | n Agency | | | | Well | Complet | tion Report |
|---|-----------------------------------|--------------------|----------|------------|------------------------------------|-----------------|------------------------------|-----------------------------|
| Site #: | | County: <u>Mon</u> | itgomery | у | | | Vell #: | G315 |
| Site Name: Coffeen Part 845 | Groundwater | | | | | E | Borehole #: | G315 |
| State Plane Coordinate: X 2,516,086 | 5.6 Y <u>871,385.0</u> | (or) Latitude: | | | | Longitud | le: | |
| Surveyed By: Kyle J. Nolan | | | IL Reg | istrati | on #: <u>035-0</u> | 03919 | | |
| Drilling Contractor: Roberts En | nv. Drilling Inc. | | Driller: | : <u>N</u> | <u>latt</u> | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | | Geolog | gist: _ | Rhonald W. | Hasenyage | er, LPG #196 | 5-000246 |
| Drilling Method: Hollow stem | auger | | Drilling | g Flui | d (Type): No | one | | |
| Logged By: Colin Winter | | | Date St | tarted | :1/13/20 | 21 Da | te Finished: _ | 1/13/2021 |
| Report Form Completed By:Co | lin Winter | | Date: _ | | 5/3/2021 | | | |
| ANNULAR SPA | CE DETAILS | | | | Elevations (MSL)* | Depths (BGS) | (0.0) | 1 ft.) |
| | | | | | 623.89 | 2.95 | Top of Prote | ective Casing |
| | | | | | 623.52 | -2.58 | Top of Rise | r Pipe |
| Type of Surface Seal: Concrete | | | | - | 620.94 | 0.00 | Ground Sur | face |
| | | | | | 620.54 | 0.40 | Top of Ann | ular Sealant |
| Type of Annular Sealant: Benton | | — ¶ | | | | | • | |
| Installation Method: Gravity | 7 | _ _ | _ | | | | | |
| Setting Time: <u>>24 hours</u> | | \frac{1}{2} | <u> </u> | | | | Static Water (After Compl | |
| Type of Bentonite Seal Grant | ular Pellet Slurry | | | - | | | | |
| Installation Method: | , | | × × | | n/a | n/a | Top of Seal | |
| Setting Time: | | | | | 612.64 | 8.30 | Top of Sand | l Pack |
| Town of Court Position | | | | | | | . 1 | |
| Type of Sand Pack: Quartz sand Grain Size: 10-20 (sie | | _ _ | | | 611.25 | 9.69 | Top of Scre | en |
| Installation Method: Gravity | | | | | | | | |
| | | | | | 606.46 | _14.48 | | |
| Type of Backfill Material: N/A | (if applicable) | _ _ | | | 606.09 | 14.85 | Bottom of V | Vell |
| Installation Method: | | | | | 605.04 | <u>15.90</u> | Bottom of E | Borehole |
| | | | | | * Referenced to a | National Geode | tic Datum | |
| | | | | | CAS | ING MEA | SUREMEN | TS |
| WELL CONS | TRUCTION MATERIA | LS | | | meter of Boreho | ole | | aches) 8.0 |
| | e type of material for each area) | - | | | of Riser Pipe | 41 | | nches) 2.0 |
| | | | | | tective Casing L | _ | | (feet) 5.0 (feet) 12.27 |
| Protective Casing | SS304 SS316 PTFE | PVC OTHER: S | teel | | er Pipe Length tom of Screen to | | | (feet) 12.27 (feet) 0.37 |
| Riser Pipe Above W.T. | _ | PVC OTHER: | | | een Length (1s | • | | (feet) 0.37 (feet) 4.79 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE | PVC OTHER: | | | al Length of Cas | | | (feet) 4.73 (feet) 17.43 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | nmental Pro | otection Agency | , | | | Well | Complet | ion Report |
|--|--|----------------------|---------------------|----------------|-------------|-------------------------------|-------------------------------|-----------------------------|
| Site #: | | County: Mo | ntgomery | 7 | | v | Vell #: | G316 |
| Site Name: Coffeen Part 845 | Groundwater | | | | | E | Sorehole #: | G316 |
| State Plane Coordinate: X 2,517,211 | .6 Y_ 871,6 | 543.1 (or) Latitude: | | | | Longitud | e: | |
| Surveyed By: Kyle J. Nolan | | | IL Reg | istration #: _ | 035-0 | 03919 | | |
| Drilling Contractor: Roberts En | nv. Drilling Inc. | | Driller: | Matt | | | | |
| Consulting Firm: Hanson Profe | essional Services | s Inc. | Geolog | ist: Rhona | ld W. | Hasenyage | er, LPG #196 | -000246 |
| Drilling Method: Hollow stem | auger | | Drilling | g Fluid (Type) | : <u>No</u> | one | | |
| Logged By: Colin Winter | | | Date St | arted: 1 | /14/20 | 021 Dat | e Finished: _ | 1/14/2021 |
| Report Form Completed By:Co | lin Winter | | Date: _ | 5/3/2 | 021 | | | |
| ANNULAR SPA | CE DETAILS | S | | Elevat (MS) | | Depths (BGS) | (0.01 | ft.) |
| | | | | 603. | _ | 3.42 | Top of Prote | ective Casing |
| | | T | | 602. | 59_ | 2.95 | Top of Riser | Pipe |
| Type of Surface Seal: Concrete | | | | 599. | 64 | 0.00 | Ground Surf | ace |
| | | | | / _598. | 84_ | 0.80 | Top of Annu | ılar Sealant |
| Type of Annular Sealant: Benton | | | | | | | | |
| Installation Method: Gravity | <u>, </u> | | | | | | | |
| Setting Time: <u>>24 hours</u> | | | $\overline{\Delta}$ | | | | Static Water (After Comple | |
| Type of Bentonite Seal Grant | ılar Pellet (choose one) | Slurry | | | | | | |
| Installation Method: | ` / | | | n/a | <u> </u> | n/a | Top of Seal | |
| Setting Time: | | | | 590. | 64 | 9.00 | Top of Sand | Pack |
| T. 60 1D 1 | | V | | | | | | |
| Type of Sand Pack: Quartz sand | | | | _589. | 62 | 10.02 | Top of Scree | en |
| Grain Size: 10-20 (sie Installation Method: Gravity | | | | | | | | |
| instanation Method. Oravity | <u>'</u> | | | _584. | 82_ | _14.82 | Bottom of S | creen |
| Type of Backfill Material: N/A | (if applicable | e) | | _584. | 48_ | 15.16 | Bottom of V | Vell |
| Installation Method: | | | | _583. | 89_ | 15.75 | Bottom of B | orehole |
| | | | | * Refere | nced to a | National Geode | ic Datum | |
| | | | | | CAS | SING MEA | SUREMEN | ΓS |
| WELL CONG | TRUCTION MA | ATEDIAI C | | Diameter of | Boreho | ole | (in | ches) 8.0 |
| | e type of material for each | | | ID of Riser | | | | ches) 2.0 |
| | | | | | | ength | | (feet) 5.0 |
| Protective Casing | SS304 SS316 | PTFE PVC OTHER: | Steel | Riser Pipe I | | | | (feet) 12.97 |
| Riser Pipe Above W.T. | SS304 SS316 | PTFE (PVC) OTHER: | | | | o End Cap st slot to last slo | | (feet) 0.34 (feet) 4.80 |
| Riser Pipe Below W.T. | SS304 SS316 | PTFE PVC OTHER: | | Total Lengt | | | • | (feet) 4.80 (feet) 18.11 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environ | nmental Protection A | gency | | | | Well | Complet | tion Report |
|-------------------------------------|---------------------------------|-----------------|----------|-------------|------------------------------------|-----------------|------------------------------|-----------------------------|
| Site #: | County | y: <u>Mon</u> t | tgomery | у | | | Well #: | G317 |
| Site Name: Coffeen Part 845 | Groundwater | | | | | I | Borehole #: | G317 |
| State Plane Coordinate: X 2,517,087 | 7.4 Y 871,234.2 (or) | Latitude: | | | | Longitud | le: | |
| Surveyed By: Kyle J. Nolan | | | IL Reg | istrat | ion #:035-00 | 03919 | | |
| Drilling Contractor: Roberts E | nv. Drilling Inc. | | Driller: | : <u>N</u> | <u>latt</u> | | | |
| Consulting Firm: Hanson Prof | essional Services Inc. | | Geolog | gist: _ | Rhonald W. | Hasenyage | er, LPG #196 | 5-000246 |
| Drilling Method: Hollow stem | auger | | Drilling | g Flui | id (Type): No | one | | |
| Logged By: Colin Winter | | | Date St | tarted | 1:1/13/20 | 21 Da | te Finished: _ | 1/14/2021 |
| Report Form Completed By:Co | lin Winter | | Date: | | 5/3/2021 | | | |
| ANNULAR SPA | CE DETAILS | | | | Elevations (MSL)* | Depths (BGS) | (0.0) | 1 ft.) |
| | | | | | 642.26 | -3.41 | Top of Prote | ective Casing |
| | | | | | 641.93 | 3.08 | Top of Rise | r Pipe |
| Type of Surface Seal: Concrete | | | | - - ~ | 638.85 | 0.00 | Ground Sur | face |
| | | | | | 638.05 | 0.80 | • | |
| Type of Annular Sealant: High-s | | | | | | | . 1 | |
| Installation Method: Tremie | : | | | | | | | |
| Setting Time: >24 hours | | | 7 | | | | Static Water (After Compl | |
| Type of Bentonite Seal Gran | | + | | - | | | | |
| Installation Method: Gravity | (choose one) | | | | 612.55 | 26.30 | Top of Seal | |
| Setting Time: 24 hours | | | | | 609.75 | 20.10 | Top of Sand | l Dools |
| | | | | | 009.73 | | Top or Sand | 11 dek |
| Type of Sand Pack: Quartz sand | | | | | 608.71 | 30.14 | Top of Scree | en |
| Grain Size: 10-20 (sign | | | | | | | . Top of Sere | |
| Installation Method: Gravity | / | | | | 603.92 | 34.93 | Bottom of S | creen |
| Type of Backfill Material: N/A | (if applicable) | | | | 603.57 | 35.28 | Bottom of V | Vell |
| Installation Method: | | | | | 602.85 | 36.00 | Bottom of B | Sorehole |
| | | | | | * Referenced to a | National Geode | tic Datum | |
| | | | | | CAS | ING MEA | SUREMEN | ΓS |
| WELL CONS | TRUCTION MATERIALS | | | Dia | meter of Boreho | ole | (in | ches) 8.0 |
| | type of material for each area) | | | | of Riser Pipe | | ` | ches) 2.0 |
| | | | | | tective Casing L | ength | | (feet) 5.0 |
| Protective Casing | SS304 SS316 PTFE PVC | OTHER: (St | teel | | er Pipe Length tom of Screen to | End Com | | (feet) 33.22 (feet) 0.35 |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC | | | | een Length (1s | | | (feet) 0.35 (feet) 4.79 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC | OTHER: | | | al Length of Cas | | | (feet) 4.79 (feet) 38.36 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Enviror | imental Prote | ection Agency | | | | Well | Comple | tion Report |
|---|---------------------------------|--------------------|-------------------------|-------------|------------------------|------------------------------|------------------------------|-----------------------------|
| Site #: | | County: <u>Mor</u> | itgomery | y | | | Well #: | XPW01 |
| Site Name: Coffeen Part 845 | Groundwater | | | | | F | Borehole #: | XPW01 |
| State Plane Coordinate: X 2,515,366 | | | | | | | | |
| Surveyed By: Kyle J. Nolan | | | | | | | | |
| Drilling Contractor: Roberts Er | nv. Drilling Inc. | | Driller: | Matt | | | | |
| Consulting Firm: Hanson Profe | essional Services In | nc. | Geolog | ist: Rho | onald W. | Hasenyage | er, LPG #196 | 6-000246 |
| Drilling Method: Hollow stem | auger | | Drilling | g Fluid (Ty | pe): <u>No</u> | one | | |
| Logged By: Colin Winter | | | Date St | tarted: | 2/8/20 | 21 Da | te Finished: _ | 2/8/2021 |
| Report Form Completed By:Co | lin Winter | | Date: _ | 5/3 | 3/2021 | | | |
| ANNULAR SPA | CE DETAILS | | | | vations (SL)* | Depths (BGS) | (0.0) | 1 ft.) |
| | | | | , | 34.92 | 3.07 | Top of Prote | ective Casing |
| | | | = | _63 | 34.57 | -2.72 | Top of Rise | r Pipe |
| Type of Surface Seal: Concrete | | | | 63 | 31.85 | 0.00 | Ground Sur | face |
| | | | | 63 | 31.15 | 0.70 | Top of Ann | ular Sealant |
| Type of Annular Sealant: Benton | | | 19 | | | | | |
| Installation Method: Gravity | , | | _ | | | | G W. | |
| Setting Time: >24 hours | | | <u> </u> | | | | Static Water (After Compl | |
| Type of Bentonite Seal Grant | ılar Pellet S | lurry | | | | | | |
| Installation Method: | | | $\overline{\mathbf{x}}$ | | n/a | n/a | Top of Seal | |
| Setting Time: | | | | _62 | 24.85 | 7.00 | Top of Sano | d Pack |
| Type of Sand Books | | | | | | | | |
| Type of Sand Pack: Quartz sand Grain Size: 10-20 (sie | | — <u> </u> | | 62 | 23.64 | 8.21 | Top of Scre | en |
| Installation Method: Gravity | | | | | | | | |
| installation Method. Gravity | | | | _61 | 18.87 | 12.98 | Bottom of S | Screen |
| Type of Backfill Material: N/A | (if applicable) | L | | _61 | 18.49 | 13.36 | Bottom of V | Well |
| Installation Method: | | | | _61 | 17.85 | 14.00 | Bottom of E | Borehole |
| | | | | * R6 | eferenced to a | National Geode | tic Datum | |
| | | | | | CAS | SING MEA | SUREMEN | TS |
| WELL CONG | TRUCTION MATI | EDIALC | | Diameter | of Boreh | ole | (ir | nches) 8.0 |
| | e type of material for each are | | | ID of Ris | | | ` | nches) 2.0 |
| | | | | | _ | Length | | (feet) 5.0 |
| Protective Casing | SS304 SS316 PT | FE PVC OTHER: (S | teel | | e Length | | | (feet) 10.93 |
| Riser Pipe Above W.T. | SS304 SS316 PT | | | | | o End Cap st slot to last sl | | (feet) 0.38 (feet) 4.77 |
| Riser Pipe Below W.T. | SS304 SS316 PT | | | | engun (1 ngth of Ca | | | (feet) 4.77 (feet) 16.08 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Illinois Environmental Protection Agency | Well Completion Rep | port |
|--|---|------|
| Site #: County: _Mc | ontgomery Well #: XPW02 | |
| Site Name: Coffeen Part 845 Groundwater | Borehole #: XPW02 | 2 |
| State Plane Coordinate: X 2,515,627.3 Y 871,987.1 (or) Latitude | | |
| Surveyed By: Kyle J. Nolan | | |
| Drilling Contractor: Roberts Env. Drilling Inc. | | |
| Consulting Firm: Hanson Professional Services Inc. | | |
| Drilling Method: Hollow stem auger | | |
| Logged By: Colin Winter | | |
| Report Form Completed By: Colin Winter | Date: 5/3/2021 | |
| ANNULAR SPACE DETAILS | Elevations Depths (0.01 ft.) | — |
| | (MSL)* (BGS) | |
| - | | g |
| | | |
| Type of Surface Seal: Concrete | 636.64 0.00 Ground Surface | |
| | | |
| Type of Annular Sealant: Bentonite chips | 4 | |
| Installation Method: Gravity | Static Water Level Static Water Level | |
| Setting Time:>24 hours | Static Water Level (After Completion) | |
| Type of Bentonite Seal Granular Pellet Slurry (choose one) | | |
| Installation Method: | n/aTop of Seal | |
| Setting Time: | 629.64 7.00 Top of Sand Pack | |
| Y Y | 7.00 Top of Sailed rack | |
| Type of Sand Pack: Quartz sand | 628.59 8.05 Top of Screen | |
| Grain Size: 10-20 (sieve size) | | |
| Installation Method: Gravity | | |
| Type of Backfill Material: N/A (if applicable) | | |
| Installation Method: | 618.44 18.20 Bottom of Borehole | |
| | * Referenced to a National Geodetic Datum | |
| | CASING MEASUREMENTS | |
| WELL CONCEDITORION MATERIALS | Diameter of Borehole (inches) 8. | .0 |
| WELL CONSTRUCTION MATERIALS (Choose one type of material for each area) | ID of Riser Pipe (inches) 2. | .0 |
| | 5 5 | .0 |
| Protective Coding | | .10 |
| Protective Casing SS304 SS316 PTFE PVC OTHER: Riser Pipe Above W.T. SS304 SS316 PTFE PVC OTHER: | Bottom of Screen to End Cap (leet) 0. | .35 |
| Riser Pipe Below W.T. SS304 SS316 PTFE PVC OTHER: | Screen Length (1st slot to last slot) (leet) 9. | .80 |

SS304

Well Completion Form (revised 02/06/02)

SS316

Total Length of Casing

**Hand-Slotted Well Screens Are Unacceptable

Screen Slot Size **

0.010

| Depit pn Wi Cpl.ti | Nlime AU mhLmti | v Sli LT | | | h læ | gtNrelmpti | PlrtU |
|-------------------------------------|---|---------------|------------|--------------------|--------------------|--------------------|--------|
| Site #: | C | ounty: Mon | tgomery | 7 | W | /ell #: <u>G2</u> | 75D |
| Site Name: Coffeen Part 845 | Groundwater | | | | В | orehole #:G | 275D |
| State Plane Coordinate: X 2,516,360 | 5.5 Y 874,285.3 (c | or) Latitude: | | | Longitud | e: | |
| Surveyed By: Michael J. Gran | | | | stration #:035-0 | | | |
| | | | Driller: | Matt | | | |
| Consulting Firm: Hanson Prof | | | | ist: Rhonald W | . Hasenyage | r, LPG #196-000 | 246 |
| Drilling Method: Hollow stem | auger | | Drilling | g Fluid (Type): N | lone | | |
| | | | | arted: 1/28/2 | | | |
| Report Form Completed By: Co | | | Date: | | | | - |
| v a a s I v P c Av | | | | Wel Compt in | | (0.01 ft.) | |
| v a a S I v I CIIv | gvikiyvii | | | (MSL)* | (BGS) | (0.01 1) | |
| | | | | _620.69_ | 3.17 | Top of Protective | Casing |
| | | | | 620.31 | 2.79 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | | | (17.50 | 0.00 | 0 10 0 | |
| ype of Surface Seat. Concrete | | | | 617.52 | 0.00 | Ground Surface | |
| Type of Annular Sealant: High-s | solids bentonite | _ | | 617.02 | 0.50 | Top of Annular S | ealant |
| Installation Method:Tremie | ; | | 17 | | | | |
| Setting Time: _ >24 hours | | _ \ | z | | | Static Water Leve | :1 |
| | | | | | | (After Completion) | |
| Type of Bentonite Seal Gran | Pellet Slurry (choose one) | | Y | | | | |
| Installation Method: Gravity | ` ' | | | 572.02 | 45.50 | Top of Seal | |
| Setting Time: 30 minutes | | | | | 46.50 | | |
| <u> </u> | | | X | _571.02_ | _46.50_ | Top of Sand Pack | |
| Type of Sand Pack: Quartz sand | I | _ | | | | | |
| Grain Size: 10-20 (sie | eve size) | | $\equiv $ | 567.76 | 49.76 | Top of Screen | |
| Installation Method: Gravity | ý | _ | | | | | |
| | | | ∄ | 557.97 | <u>59.55</u> | | |
| Type of Backfill Material: N/A | (if applicable) | _ _ | | _557.63_ | _59.89_ | Bottom of Well | |
| Installation Method: | | | | 517.82 | 99.70 | Bottom of Boreho | ole |
| | | | | * Referenced to | a National Geodeti | ic Datum | |
| | | | | CA | SING MEAS | SUREMENTS | |
| | | | | Diameter of Borel | nole | (inches) | 8.0 |
| | TRUCTION MATERIAL type of material for each area) | LS | | ID of Riser Pipe | | | 2.0 |
| | • | | | Protective Casing | Length | (feet) | 5.0 |
| | T | | | Riser Pipe Length | | (feet) | 52.55 |
| Protective Casing | | VC OTHER: S | teel) | Bottom of Screen | to End Cap | (feet) | 0.34 |
| Riser Pipe Above W.T. | | OTHER: | | Screen Length (| | ot) (feet) | 9.79 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE (F | OTHER: | | Total Length of Co | asing | (feet) | 62.68 |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

(inches)

SS304

Well Completion Form (revised 02/06/02)

| Depit pr Wi Cplt i Nli me Alt ml Inti v Sli | LT | | h læ | gtNrelmpti | PlrtU |
|---|---------------------------|-------------------------------------|-------------------------|--|---------|
| Site #: County: I | Montgomery | | W | Vell #: <u>G2</u> | 06D |
| Site Name: Coffeen Part 845 Groundwater | | | Bo | orehole #: | 6282D |
| State Plane Coordinate: $X = 2,514,684.6$ $Y = 875,111.4$ (or) Latitu | ıde: | | Longitude | e: | |
| Surveyed By: Michael J. Graminski | | | | | |
| Drilling Contractor: Roberts | | Matt | | | |
| Consulting Firm: Hanson Professional Services Inc. | Geologist: | Rhonald W. | Hasenyageı | r, LPG #196-000 |)246 |
| Drilling Method: Hollow stem auger | Drilling Fl | uid (Type): <u>No</u> | one | | |
| Logged By: Colin Winter | Date Starte | ed:1/25/20 | 21 Date | e Finished:1/2 | 25/2021 |
| Report Form Completed By: Colin Winter | | 5/3/2021 | | | |
| v a a s I v P c Av g WRWy v II c | | Wel Compt i n (MSL)* | RlrnEn (BGS) | (0.01 ft.) |) |
| _ | | 634.35 | 2.94 | Top of Protective | Casing |
| | | 634.14 | 2.73 | Top of Riser Pipe | e |
| Type of Surface Seal: Concrete | | 631.41 | 0.00 | Ground Surface | |
| | | 631.11 | 0.30 | Top of Annular S | Sealant |
| Type of Annular Sealant: High-solids bentonite | | | | Top of Aimulai C | calant |
| Installation Method: Tremie | | | | | |
| Setting Time:>24 hours | $ \overline{\Delta} $ | | | Static Water Lev (After Completion) | el |
| Type of Bentonite Seal Granular Pellet Slurry | | | | | |
| (choose one) Installation Method: Gravity | | 585.81 | 45.60 | Top of Seal | |
| | | _303.01_ | _43.00_ | rop or sear | |
| Setting Time: 15 hours | | 583.41 | _48.00_ | Top of Sand Pack | k |
| Type of Sand Pack: Quartz sand | | | | | |
| Grain Size: 10-20 (sieve size) | | _582.21_ | _49.20_ | Top of Screen | |
| Installation Method: Gravity | | | | | |
| Type of Backfill Material: N/A | | 572.41 572.02 | <u>59.00</u> 59.39 | Bottom of Screen Bottom of Well | 1 |
| (if applicable) | | _372.02 | | Bottom of Wen | |
| Installation Method: | | 571.41 * Referenced to a | 60.00 National Geodetic | | ole |
| | | | | | |
| | | | | SUREMENTS | |
| WELL CONSTRUCTION MATERIALS | | iameter of Boreho | | (inches) | 8.0 |
| (Choose one type of material for each area) | | of Riser Pipe rotective Casing L | ength | | 5.0 |
| | | iser Pipe Length | - | (feet) | 51.93 |
| Protective Casing SS304 SS316 PTFE PVC OTH | () | ottom of Screen to | | ` | 0.39 |
| Riser Pipe Above W.T. SS304 SS316 PTFE PVC OTH | | creen Length (1s | | | 9.77 |
| Riser Pipe Below W.T. SS304 SS316 PTFE PVC OTH | | otal Length of Cas | | (feet) | 62.09 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Depit pn WiCpLti | Nli meAU mhLm | ti v Sli LT | | | h læ | gtNrelmpti | PlrtU |
|-------------------------------------|---|----------------|------------------------------|--------------------------|---------------------|---|----------|
| Site #: | | County: Mor | itgomery | | W | Vell #: G2 | 283 |
| Site Name: Coffeen Part 845 | Groundwater | | | | В | orehole #: | G283 |
| State Plane Coordinate: X 2,516,503 | 3.0 Y 874,113.0 | (or) Latitude: | | | Longitud | e: | |
| Surveyed By: Michael J. Gran | ninski | | IL Regis | stration #: <u>035-0</u> | 03919 | | |
| - | | | Driller: | Matt | | | |
| Consulting Firm: <u>Hanson Prof</u> | essional Services Inc. | | Geologi | st: <u>Rhonald W.</u> | | | |
| Orilling Method: Hollow stem | auger | | Drilling | Fluid (Type): No | one | | |
| Logged By: Colin Winter | _ | | Date Sta | arted: 1/18/20 |)21 Dat | e Finished: 1/1 | 18/2021 |
| Report Form Completed By:Co | | | Date: | 5/3/2021 | | | |
| v a a s I v P cAv | | | | Wel Compt i n (MSL)* | | (0.01 ft.) | |
| | | | | 611.07 | 2.77 | Top of Protective | Casing |
| | | Te | | 610.75 | -2.45 | Top of Riser Pipe | ; |
| Type of Surface Seal: Concrete | | | | 608.30 | 0.00 | Ground Surface | |
| | | | | 607.70 | 0.60 | | ealant |
| Type of Annular Sealant: Benton | nite chips | _ 🕅 | | | | Top of Aimulai S | Calant |
| Installation Method: Gravity | ý | | | | | | |
| Setting Time: >24 hours | | | $\mathbb{Z} \mid \cdot \mid$ | | | Static Water Leve (After Completion) | el |
| Type of Bentonite Seal Gran | ular Pellet Slurry | | | | | | |
| Installation Method: | ` ' | | X X | n/a | n/a | Top of Seal | |
| Setting Time: | | | | 600.80 | 7.50 | Top of Sand Pack | C |
| | | | | | | 1 | |
| Type of Sand Pack: Quartz Sand | | | | 599.91 | 8.39 | Top of Screen | |
| Grain Size: 10-20 (sign | , | | | | | • | |
| Installation Method: Gravity | ý. | - | | _590.13_ | _18.17 | Bottom of Screen | |
| Type of Backfill Material: N/A | (if applicable) | [| | 589.94 | 18.36 | Bottom of Well | |
| Installation Method: | | | | 589.94 | 18.36 | Bottom of Boreho | ole |
| | | | | * Referenced to a | National Geodet | | |
| | | | | CAS | SING MEA | SUREMENTS | |
| ****** | TENT LOCAL A LA TENT A LA TENT A LA TENTA A L | T.G | | Diameter of Boreho | ole | (inches) | 8.0 |
| | TRUCTION MATERIA ne type of material for each area) | ALS | | ID of Riser Pipe | | (inches) | 2.0 |
| | | | - | Protective Casing L | ength | (feet) | 5.0 |
| | I | | | Riser Pipe Length | | (feet) | 10.84 |
| Protective Casing | SS304 SS316 PTFE | PVC OTHER: | Steel) | Bottom of Screen to | o End Cap | (feet) | 0.38 |
| Riser Pipe Above W.T. | | PVC OTHER: | | Screen Length (1s | st slot to last slo | ot) (feet) | 9.78 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE (| PVC OTHER: | | Total Length of Cas | sing | (feet) | 21.00 |

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

(inches)

SS304

Well Completion Form (revised 02/06/02)

| 🖴 Depitpa WiGhtiNlime AltmlLmptiv SliL | \mathbf{T} | | h læ | gtNrelmpti | PlrtU |
|--|--------------|--------------------------------------|----------------------------------|------------------------------------|--------------|
| Site #: County: Mo | ontgomery | | W | Vell #: G2 | 284 |
| Site Name: Coffeen Part 845 Groundwater | | | В | orehole #: | G284 |
| State Plane Coordinate: X_2,516,922.9 Y_874,423.6 (or) Latitude | e: | | Longitude | e: | |
| Surveyed By: Michael J. Graminski | | | | | |
| Drilling Contractor: Roberts | | Matt | | | |
| Consulting Firm: Hanson Professional Services Inc. | | | | r, LPG #196-000 | |
| Drilling Method: Hollow stem auger | Drilling Fl | uid (Type): No | one | | |
| Logged By: Colin Winter | | | | e Finished: 1/2 | |
| Report Form Completed By: Colin Winter | | 5/3/2021 | | | |
| v a a s I v P c Av g WRWy v II c | | Wel Compt in | | (0.01 ft.) | |
| vaasivi CAV g WRVy VIIC | | (MSL)* | (BGS) | (0.01 11.) | |
| | | 618.66 | 3.33 | Top of Protective | Casing |
| F | | 618.42 | 3.09 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | 61 7 00 | 0.00 | | |
| ype of surface seal. | | 615.33 | 0.00 | | |
| Type of Annular Sealant: Bentonite chips | | _614.33_ | 1.00 | Top of Annular S | ealant |
| Installation Method: Gravity | | | | | |
| Setting Time: >24 hours | ∇ | | | Static Water Leve | el |
| | | | | (After Completion) | |
| Type of Bentonite Seal Granular Pellet Slurry (choose one) | | | | | |
| Installation Method: | V V | n/a | n/a | Top of Seal | |
| Setting Time: | | 608.33 | 7.00 | Top of Sand Pack | - |
| | M | _000.55_ | | Top of Sand Faci | • |
| Type of Sand Pack: Quartz Sand | | 607.25 | 0 00 | Ton of Conon | |
| Grain Size:10-20 (sieve size) | | 607.25 | 8.08 | Top of Screen | |
| Installation Method: <u>Gravity</u> | | (02.49 | 12.05 | D. # | |
| Type of Backfill Material: N/A | | 602.48 602.10 | <u>12.85</u> <u>13.23</u> | Bottom of Screen Bottom of Well | |
| (if applicable) | | | | | |
| Installation Method: | | 601.33 * Referenced to a | <u>14.00</u> National Geodeti | | ole |
| | | | | | |
| | | | | SUREMENTS | |
| WELL CONSTRUCTION MATERIALS | | iameter of Boreho | | (inches) | 8.0 |
| (Choose one type of material for each area) | | of Riser Pipe | anath | | 2.0 |
| | | otective Casing L ser Pipe Length | - | | 5.0 11.17 |
| Protective Casing SS304 SS316 PTFE PVC OTHER | | ottom of Screen to | | ` / | 0.38 |
| Riser Pipe Above W.T. SS304 SS316 PTFE PVC OTHER | | reen Length (1s | | | 4.77 |
| Riser Pipe Below W.T. SS304 SS316 PTFE PVC OTHER | | otal Length of Cas | | (feet) | 16.32 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| 🖴 Depitpn WiGhtiNlime AltmlLmptiv Sli | IT | | h læ | gtNrelmpti | PlrtU |
|--|-------------|--|--------------------------|------------------------------------|--------------|
| Site #: County:] | Montgomery | | W | Vell #: G2 | 285 |
| Site Name: Coffeen Part 845 Groundwater | | | В | orehole #: | G285 |
| State Plane Coordinate: X_2,516,680.4 Y_874,795.0 (or) Latitu | ıde: | | Longitude | e: | |
| Surveyed By: Michael J. Graminski | | | | | |
| Drilling Contractor: Roberts | | Matt | | | |
| Consulting Firm: Hanson Professional Services Inc. | | | | r, LPG #196-000 | |
| Drilling Method: Hollow stem auger | Drilling Fl | uid (Type): No | one | | |
| Logged By: Colin Winter | _ | | | e Finished: 1/1 | |
| Report Form Completed By: Colin Winter | | 5/3/2021 | | | |
| v a a s I v P c Av g WRWy v II c | | Wel Comptin | | (0.01 ft.) | |
| The state of the s | | (MSL)* | (BGS) | (0.01 10) | |
| 5 | | 613.90 | 3.36 | Top of Protective | Casing |
| | | 613.52 | 2.98 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | (10.54 | 0.00 | C 10 C | |
| | | 610.54 | | | |
| Type of Annular Sealant: Bentonite chips | + | 610.24 | 0.30 | Top of Annular S | ealant |
| Installation Method: Gravity | | | | | |
| Setting Time: >24 hours | | | | Static Water Leve | el |
| | | | | (After Completion) | |
| Type of Bentonite Seal Granular Pellet Slurry (choose one) | 14 | | | | |
| Installation Method: | | n/a | n/a | Top of Seal | |
| Q v: TE: | | 598.24 | 12.30 | Top of Sand Pack | - |
| | | | | Top of Sunu Tues | • |
| Type of Sand Pack: Quartz Sand | | 596.86 | 13.68 | Top of Screen | |
| Grain Size: 10-20 (sieve size) | | | 13.06 | Top of Screen | |
| Installation Method: Gravity | | 507.00 | 22.45 | D 60 | |
| Type of Backfill Material: N/A | | <u>587.09</u> 586.71 | 23.45 23.83 | Bottom of Screen Bottom of Well | |
| (if applicable) | | | | | |
| Installation Method: | | | 26.00 National Geodetic | | ole |
| | | | | | |
| | | CAS | SING MEAS | SUREMENTS | |
| WELL CONSTRUCTION MATERIALS | | iameter of Boreho | ole | (inches) | 8.0 |
| (Choose one type of material for each area) | | O of Riser Pipe | .1 | | 2.0 |
| | | rotective Casing L | - | | 5.0 16.66 |
| Protective Casing SS304 SS316 PTFE PVC OTH | () | iser Pipe Length ottom of Screen to | | (feet) | 0.38 |
| Riser Pipe Above W.T. SS304 SS316 PTFE PVC OTH | T.D. | creen Length (1s | | | 9.77 |
| Riser Pipe Below W.T. SS304 SS316 PTFE PVC OTH | ED. | otal Length of Ca | | (feet) | 26.81 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| 🙆 Depit po WiCpltiNlimeAltmblnptivSlil | | | h læ | gtNrelmpti | PlrtU |
|--|-------------|---------------------------------------|----------------------------|---------------------|--------|
| Site #: County: _N | Montgomery_ | | W | Vell #: G28 | 36 |
| Site Name: Coffeen Part 845 Groundwater | | | В | orehole #:G | 286 |
| State Plane Coordinate: X 2,516,561.8 Y 875,072.2 (or) Latitud | de: | | Longitude | e: | |
| Surveyed By: Michael J. Graminski | | | | | |
| Drilling Contractor: Roberts | | Matt | | | |
| Consulting Firm: Hanson Professional Services Inc. | | | | r, LPG #196-0002 | |
| Drilling Method: Hollow stem auger | Drilling Fl | uid (Type): No | one | | |
| Logged By: Colin Winter | | | | e Finished: 1/19 | |
| Report Form Completed By: Colin Winter | | 5/3/2021 | | | |
| | Date | | | (0.01.0.) | |
| v a a s I v P cAv g WRWy v II c | | Wel Compt i n (MSL)* | (BGS) | (0.01 ft.) | |
| = | | 613.57 | 3.60 | Top of Protective C | Casing |
| | | 613.13 | 3.16 | Top of Riser Pipe | |
| Type of Surface Seal: Concrete | | 600.07 | 0.00 | | |
| ype of surface seam <u>econoreic</u> | | 609.97 | 0.00 | | |
| Type of Annular Sealant: Bentonite chips | | 609.47 | 0.50 | Top of Annular Se | alant |
| Installation Method: Gravity | | | | | |
| Setting Time: >24 hours | | | | Static Water Level | |
| | | | | (After Completion) | |
| Type of Bentonite Seal Granular Pellet Slurry (choose one) | 14 | | | | |
| Installation Method: | * ** | n/a | n/a | Top of Seal | |
| Setting Time: | M NM | 607.27 | 2.70 | Top of Sand Pack | |
| | | | | 1 | |
| Type of Sand Pack: Quartz Sand | | 606.60 | 3.37 | Top of Screen | |
| Grain Size: 10-20 (sieve size) | | | | 10p 01 2010011 | |
| Installation Method: <u>Gravity</u> | | 601.81 | 8.16 | Bottom of Screen | |
| Type of Backfill Material: N/A | | 601.47 | 8.50 | Bottom of Well | |
| (if applicable) | | | | | |
| Installation Method: | | | 10.00_ National Geodeti | | e |
| | | | | | |
| | | | | SUREMENTS | |
| WELL CONSTRUCTION MATERIALS | | iameter of Boreho | | (inches) | 8.0 |
| (Choose one type of material for each area) | | O of Riser Pipe rotective Casing L | ength | | 5.0 |
| | | iser Pipe Length | - | (feet) | 6.53 |
| Protective Casing SS304 SS316 PTFE PVC OTHE | _ (| ottom of Screen to | | ` | 0.34 |
| Riser Pipe Above W.T. SS304 SS316 PTFE PVC OTHE | | creen Length (1s | | | 4.79 |
| Riser Pipe Below W.T. SS304 SS316 PTFE PVC OTHE | | otal Length of Cas | | (feet) | 11.66 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Depit pn Wi Cplt | i Nli me AU: nhLnpti v S | li LT | | | h læ | gtNrelmpti | PlrtUn |
|------------------------------------|-------------------------------------|-------------------------|---------------|-------------------------------------|---------------------------|--|----------|
| Site #: | County: | Montg | gomery | | W | Vell #:G | 287 |
| Site Name: Coffeen Part 845 | Groundwater | | | | В | orehole #: | G287 |
| State Plane Coordinate: X 2,516,41 | .5.5 Y 875,442.8 (or) L | atitude: | | | Longitude | e: | |
| | minski | | | ration #:035-0 | | | |
| Drilling Contractor: Roberts | | | Driller: _ | Matt | | | |
| | fessional Services Inc. | | | : Rhonald W. | | | |
| _ | n auger | | | luid (Type): No | | | |
| _ | | | _ | | | | |
| | | | | ted: 1/18/20 | | e Finished:1/ | 18/2021 |
| Report Form Completed By:C | olin Winter | | Date: | 5/3/2021 | | | |
| v a a s I v P cAv | g WRWy v II c | | | Wel Compt in (MSL)* | RlrnEn (BGS) | (0.01 ft. |) |
| | | | | 617.88 | 3.54 | Top of Protective | e Casing |
| | | | 7 | 617.45 | 3.11 | Top of Riser Pip | e |
| Type of Surface Seal: Concrete | : | | | 614.34 | 0.00 | Ground Surface | |
| | | | | 613.74 | 0.60 | Top of Annular | Sealant |
| Type of Annular Sealant: Bento | onite chips | | | 013.74 | | Top of Amilular | Sealant |
| Installation Method: Gravi | ty | | | | | | |
| Setting Time: >24 hours | | | | | | Static Water Lev (After Completion) | |
| True of Doutonite Seel Co- | nular Pellet Slurry | | | | | (ritter completion) | |
| Type of Bentonite Seal Gra | nular Pellet Slurry (choose one) | | | | | | |
| Installation Method: | | $\overline{\mathbf{x}}$ | | n/a | n/a | Top of Seal | |
| Setting Time: | | | | 609.84 | 4.50 | Top of Sand Pac | k |
| T (C 1D 1 | | | | | | | |
| Type of Sand Pack: Quartz San | | | | 608.91 | 5.43 | Top of Screen | |
| Grain Size: 10-20 (s | | | | | | 1 | |
| Installation Method: <u>Gravi</u> | ty | | | 604.09 | 10.25 | Bottom of Screen | n |
| Type of Backfill Material: N/A | | |] | 603.75 | 10.59 | Bottom of Well | 11 |
| | (if applicable) | | | 602.54 | 11.00 | | |
| Installation Method: | | | | 602.54 * Referenced to a | 11.80 National Geodeti | Bottom of Boreh c Datum | ole |
| | | | | G.L.G | DIC ME L | | |
| | | | Г | | | SUREMENTS | 0.0 |
| | STRUCTION MATERIALS | | | Diameter of Boreho D of Riser Pipe | ole | (inches) | |
| (Choose o | one type of material for each area) | | | Protective Casing L | | ` ` | |
| | | | | Riser Pipe Length | _ | (feet) | 0.4 |
| Protective Casing | SS304 SS316 PTFE PVC | OTHER: Stee | $\overline{}$ | Bottom of Screen to | | • | |
| Riser Pipe Above W.T. | SS304 SS316 PTFE PVC | OTHER: | S | Screen Length (1s | st slot to last slo | t) (feet) | 4.82 |
| Riser Pipe Below W.T. | SS304 SS316 PTFE PVC | OTHER: | T | Total Length of Cas | sing | (feet) | 13.70 |

Well Completion Form (revised 02/06/02)

Screen Slot Size **

**Hand-Slotted Well Screens Are Unacceptable

0.010

| Iontgomery | | W | Vell #: G2 | 88 |
|---|---|--------------------|---------------------------------|--------------|
| | | B | orehole #: | G288 |
| le: | | Longitude | e: | |
| | | | | |
| | Matt | | | |
| Geologist: | | | | |
| Drilling Fl | uid (Type): No | one | | |
| | | | | |
| | | | | |
| | | | (0.01 ft.) | |
| | (MSL)* | (BGS) | (0.01 11.) | |
| | 620.37 | 3.29 | Top of Protective | Casing |
| | _620.07 | 2.99 | Top of Riser Pipe | |
| | (17.00 | 0.00 | | |
| | | 0.00 | | |
| | 616.78 | 0.30 | Top of Annular Se | ealant |
| | | | | |
| $\left \begin{array}{c} \overline{\Delta} \end{array} \right $ | | | Static Water Leve | 1 |
| | | | (After Completion) | |
| | | | | |
| | n/a | n/a | Top of Seal | |
| 1 N/M | 611.08 | 6.00 | Top of Sand Pack | |
| | 011.00 | | Top of Sand Lack | |
| | 600.40 | 7.50 | Ton of Comon | |
| | 009.49 | | Top of Screen | |
| | (04.92 | 12.26 | D. # | |
| | 604.82 | 12.75 | Bottom of Screen Bottom of Well | |
| | | | | |
| | 603.08 * Referenced to a | | | le |
| | | | | |
| | | | SUREMENTS | |
| | | ole | (inches) | 8.0 |
| | | | ` ′ | 2.0 |
| | _ | _ | | 5.0 10.58 |
| | | | ` | 0.49 |
| | | | | 4.67 |
| | _ | | | 15.74 |
| | le: IL Registr Driller: Geologist: Date Start Date: Date: | IL Registration #: | Be: | Borehole #: |

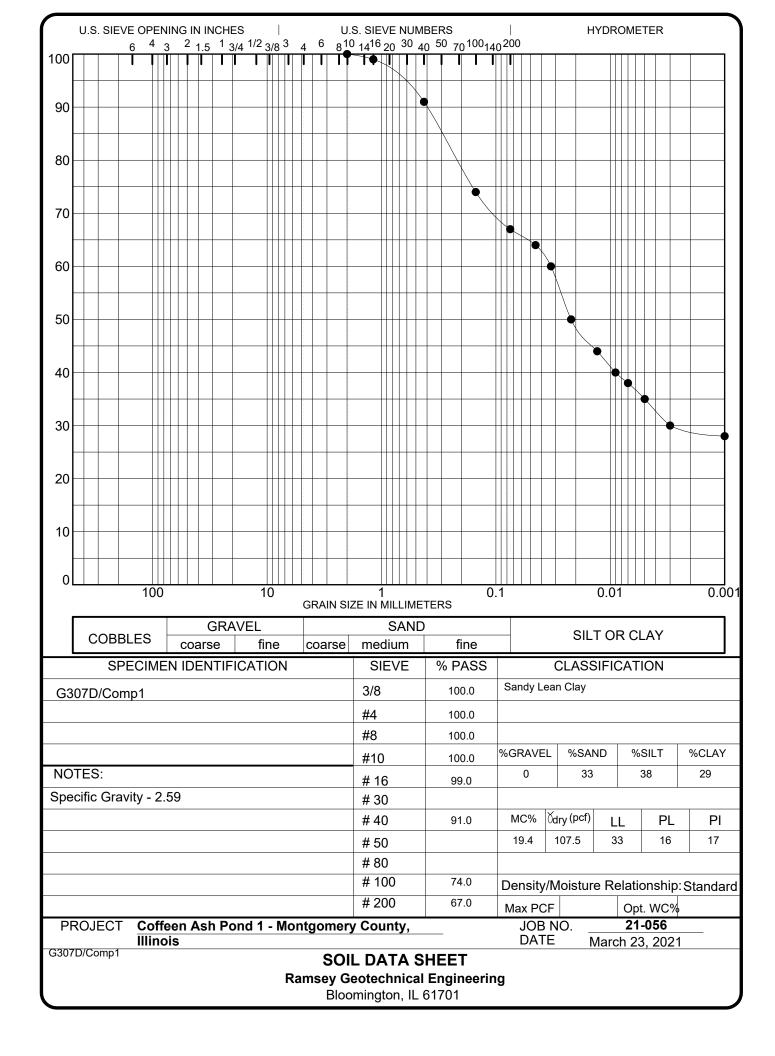
Well Completion Form (revised 02/06/02)

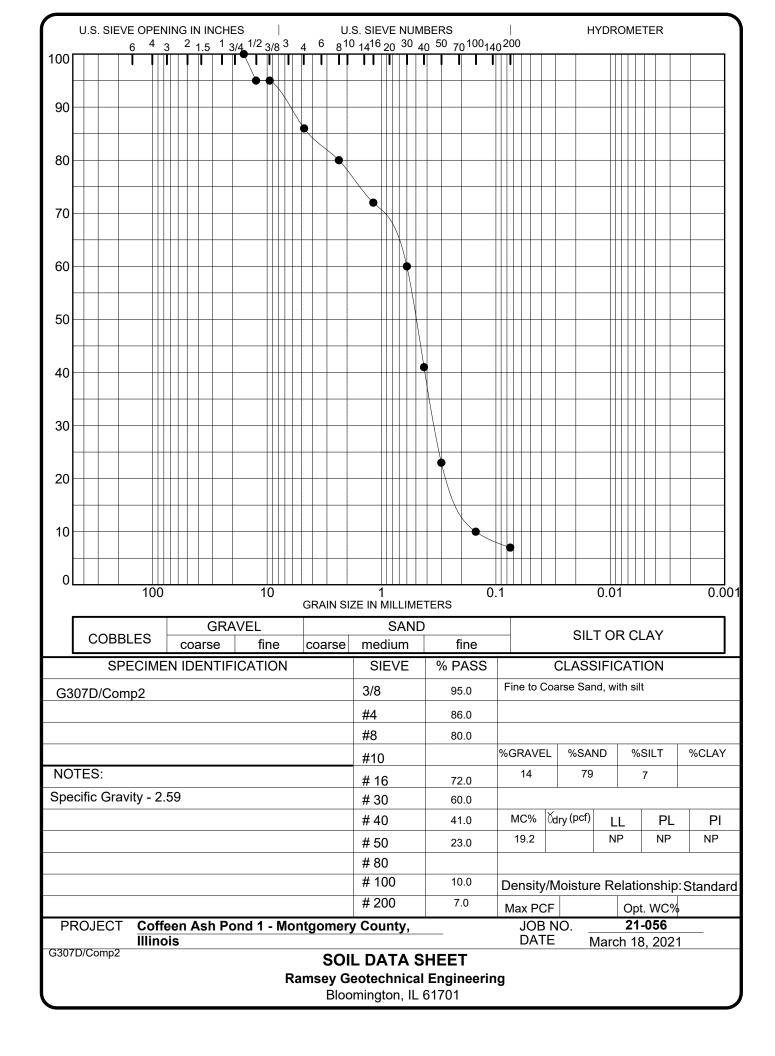
Screen Slot Size **

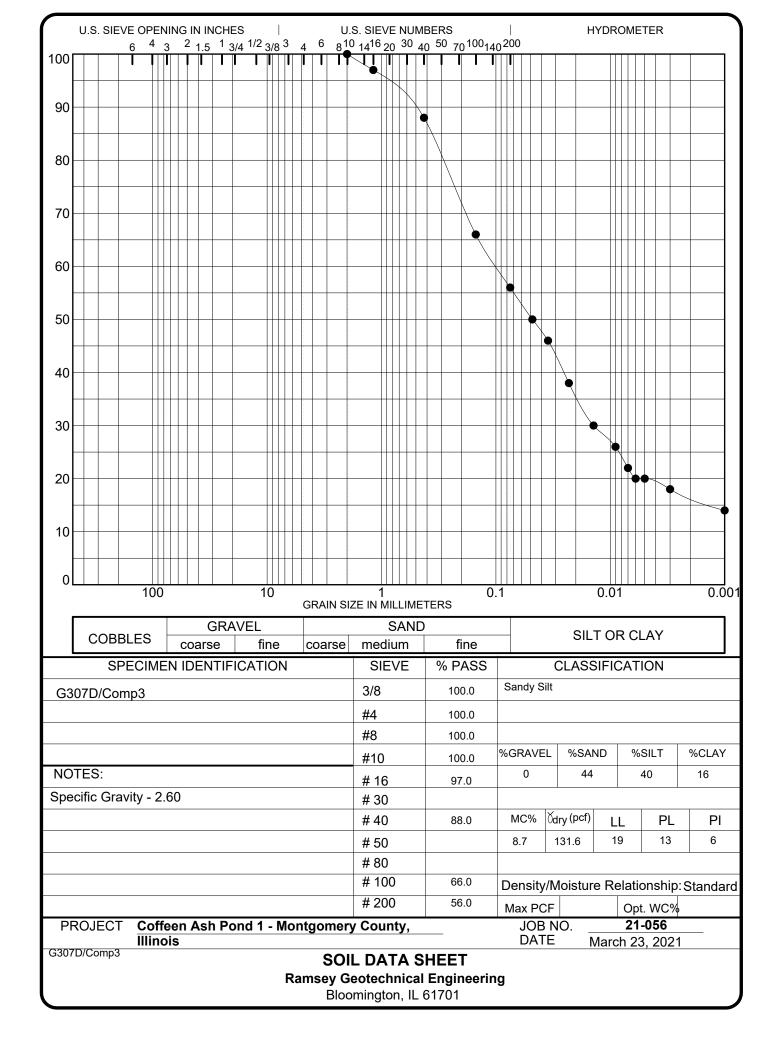
**Hand-Slotted Well Screens Are Unacceptable

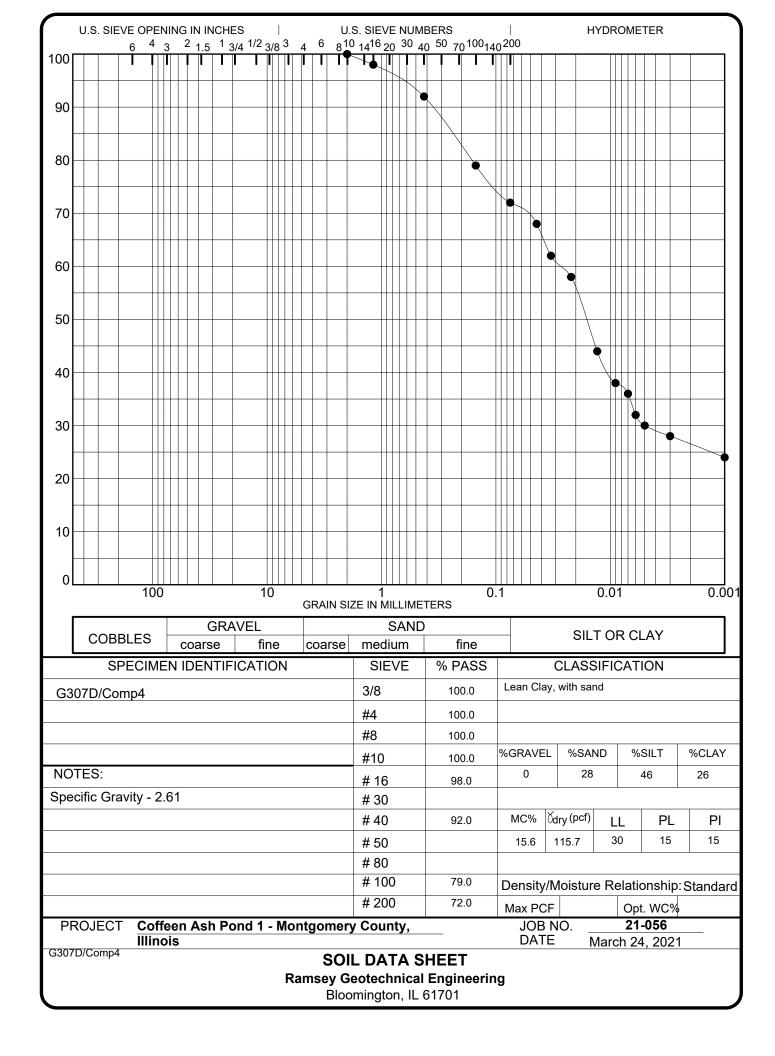
0.010

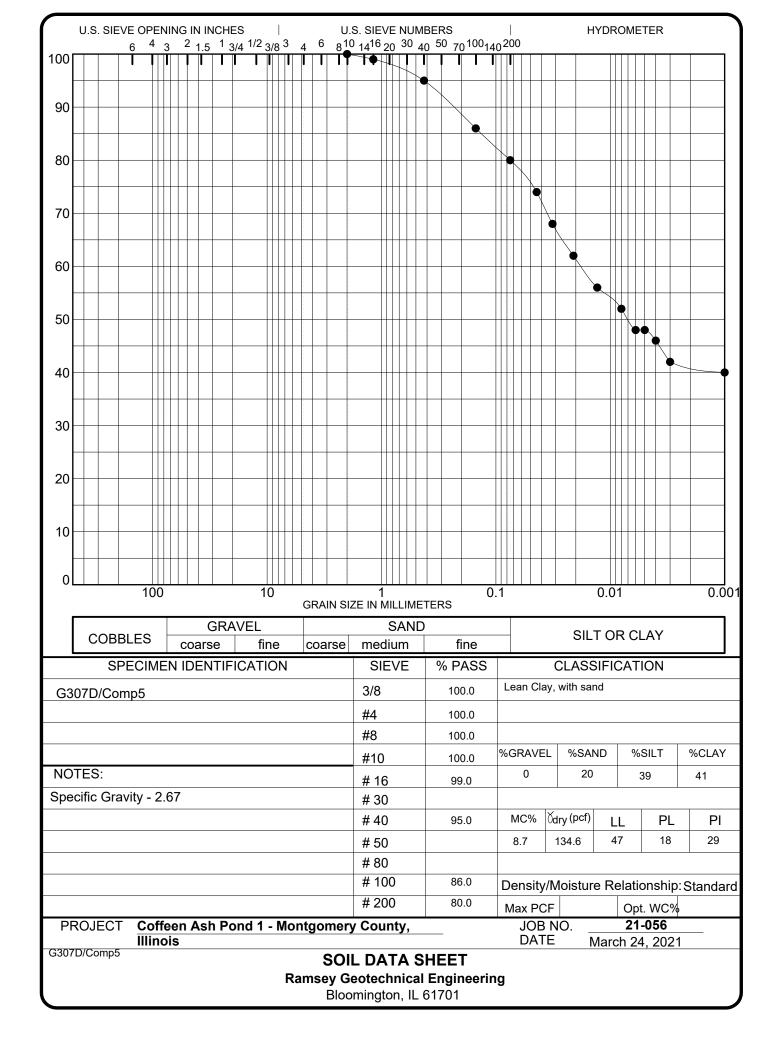
APPENDIX D GEOTECHNICAL LABORATORY REPORTS

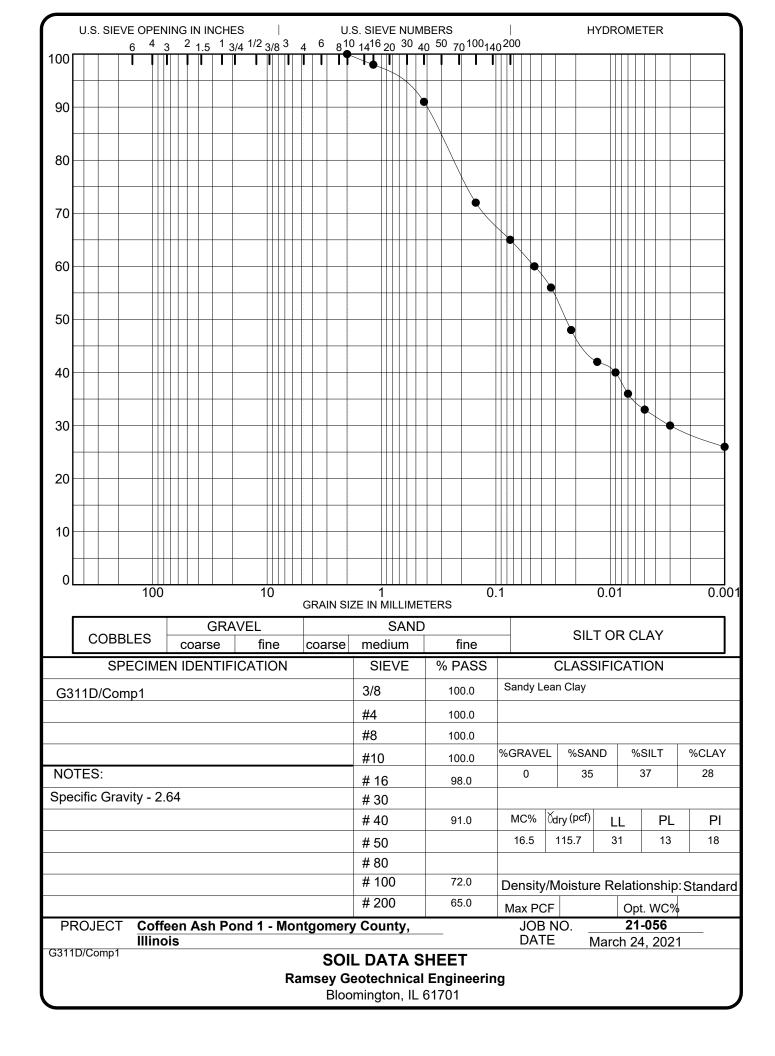


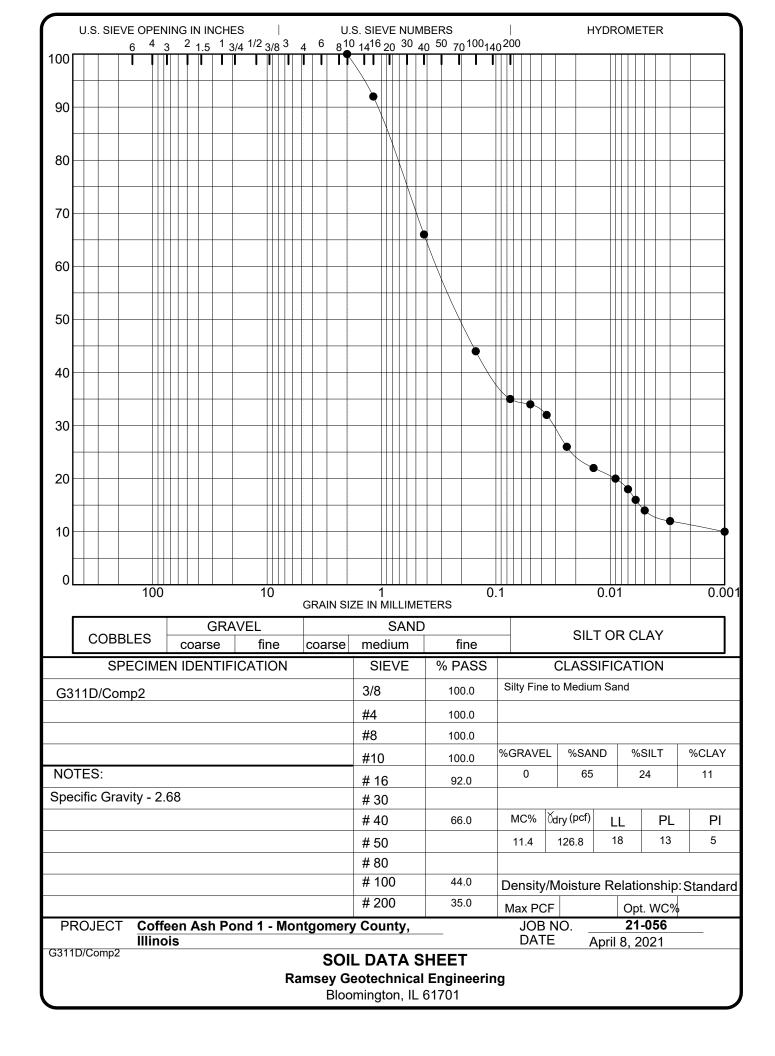


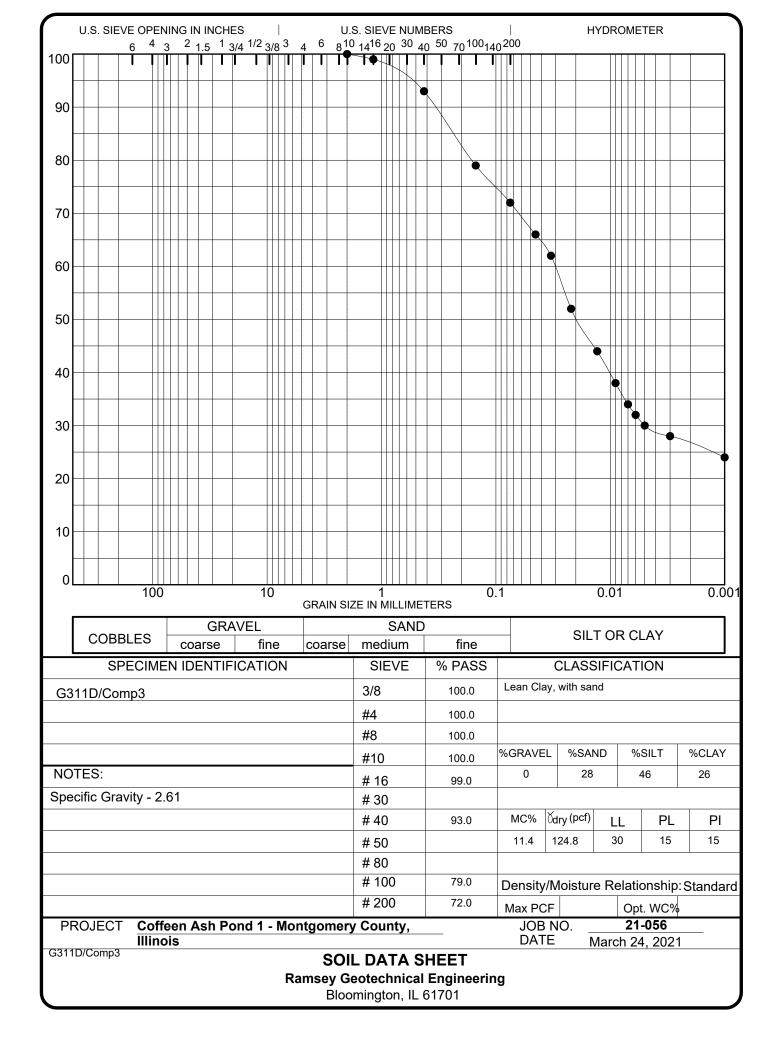


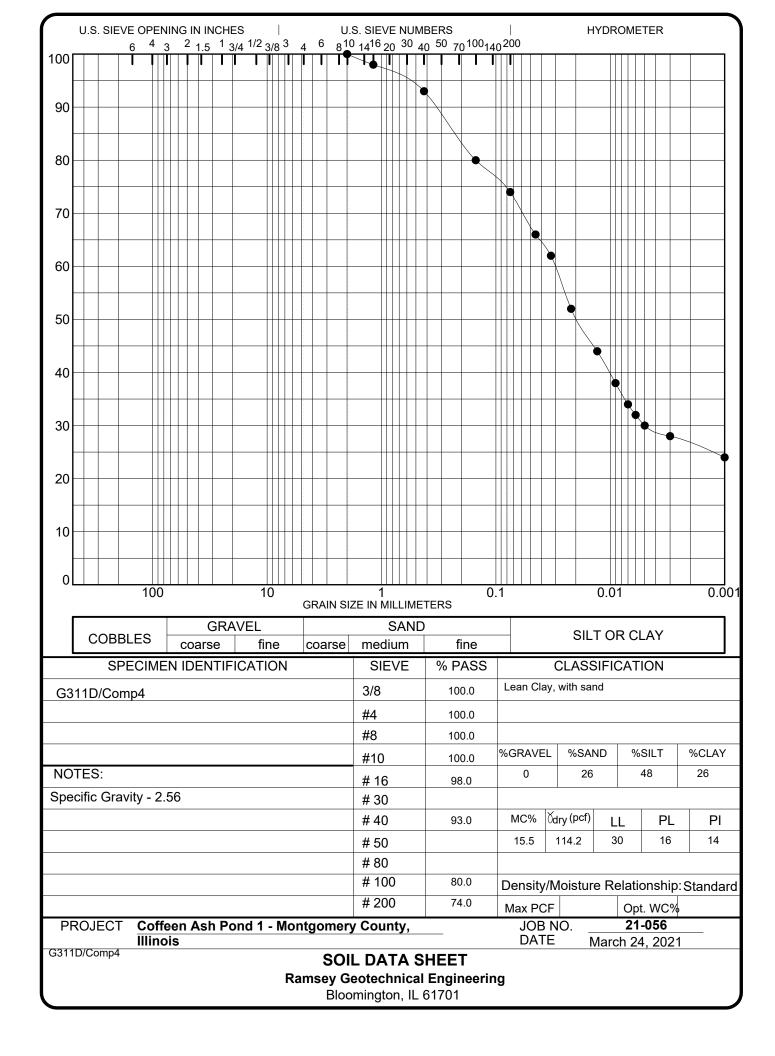


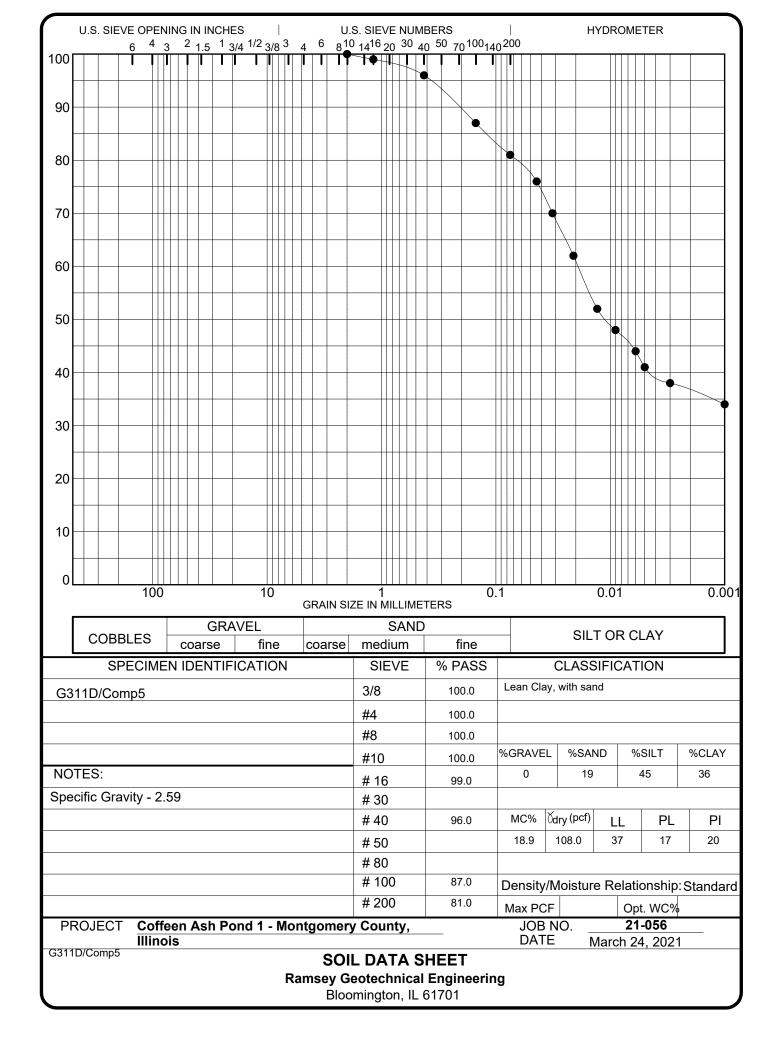


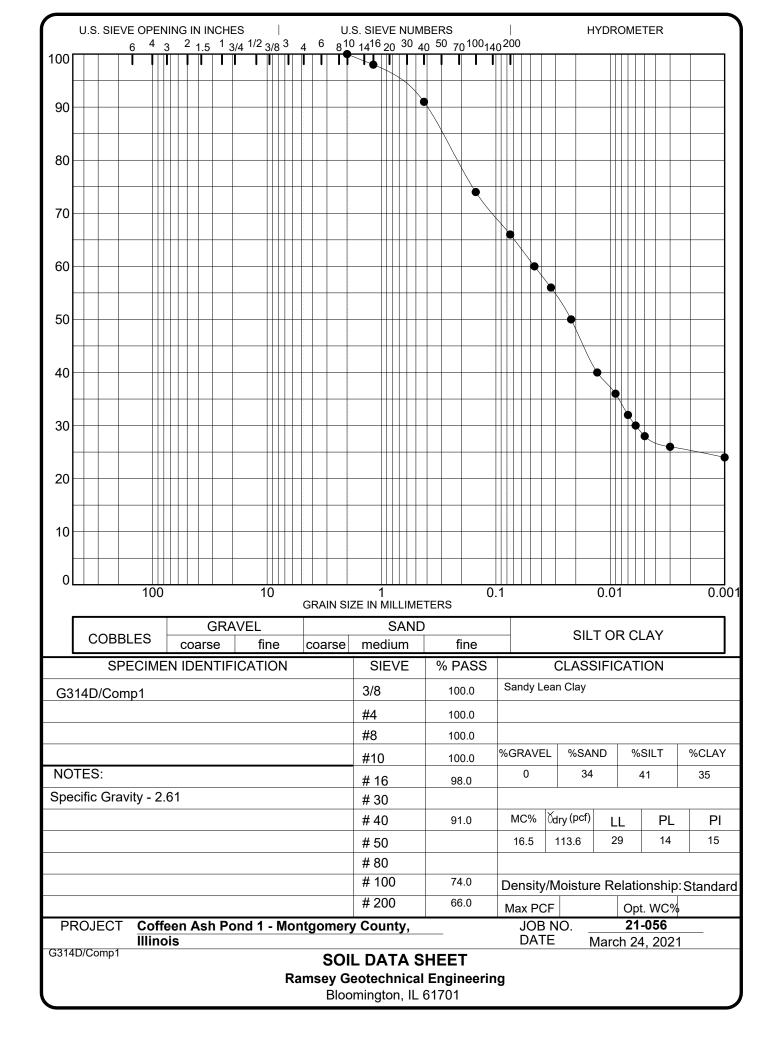


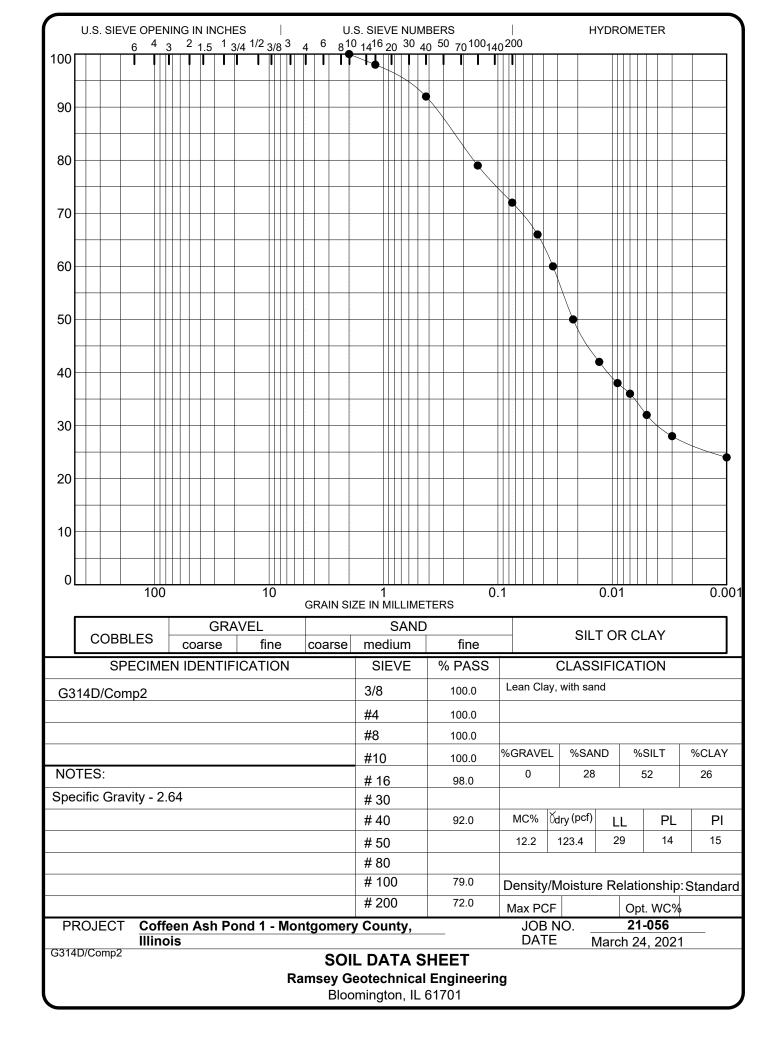


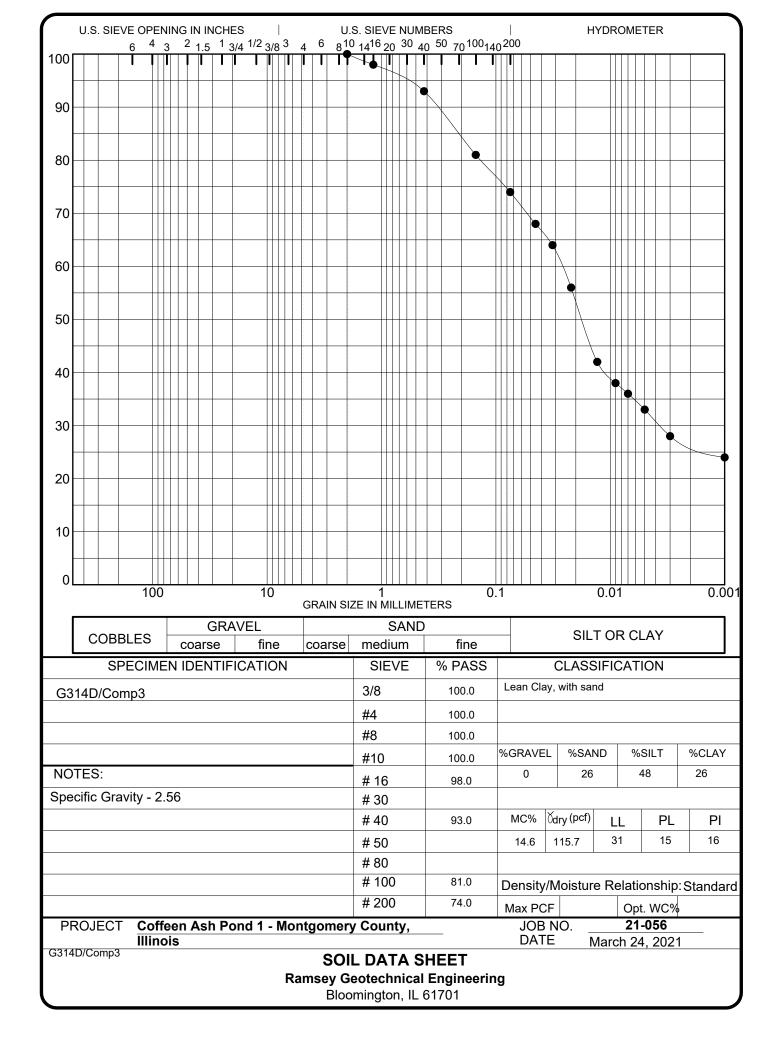


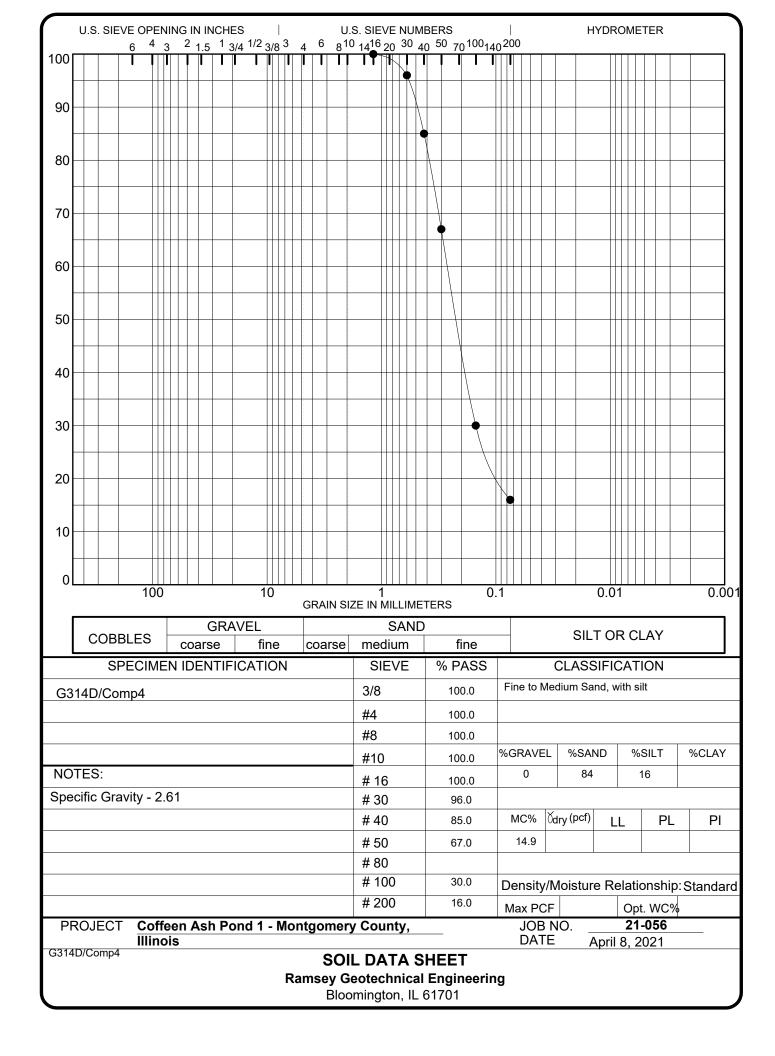


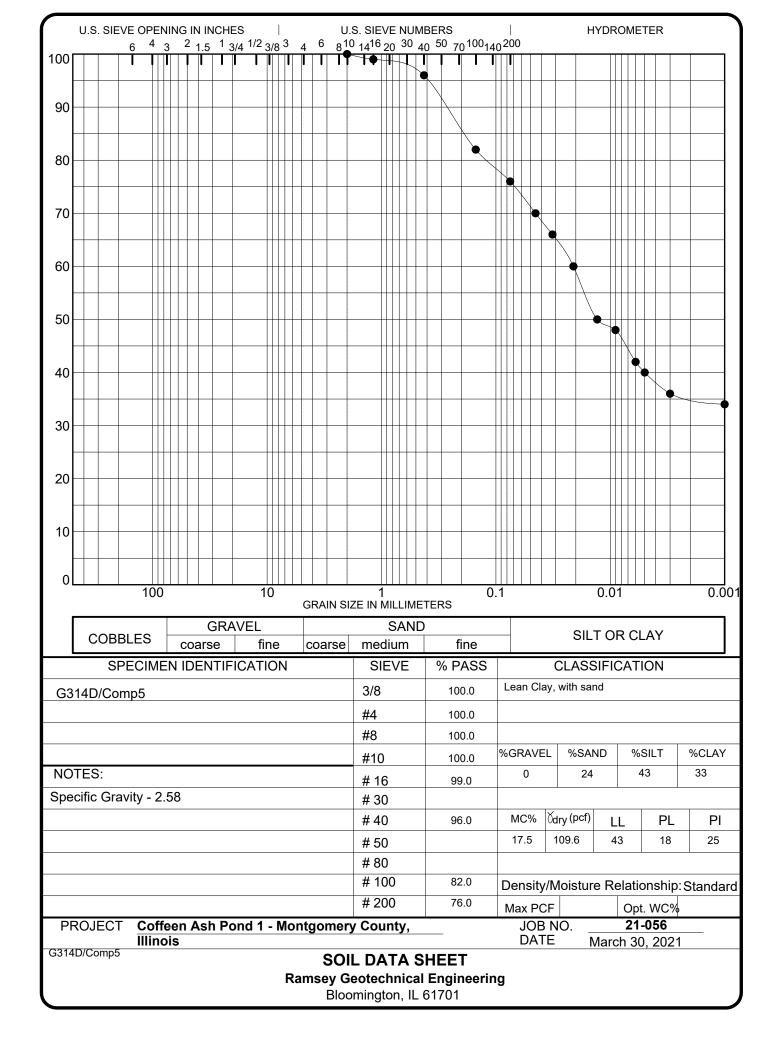


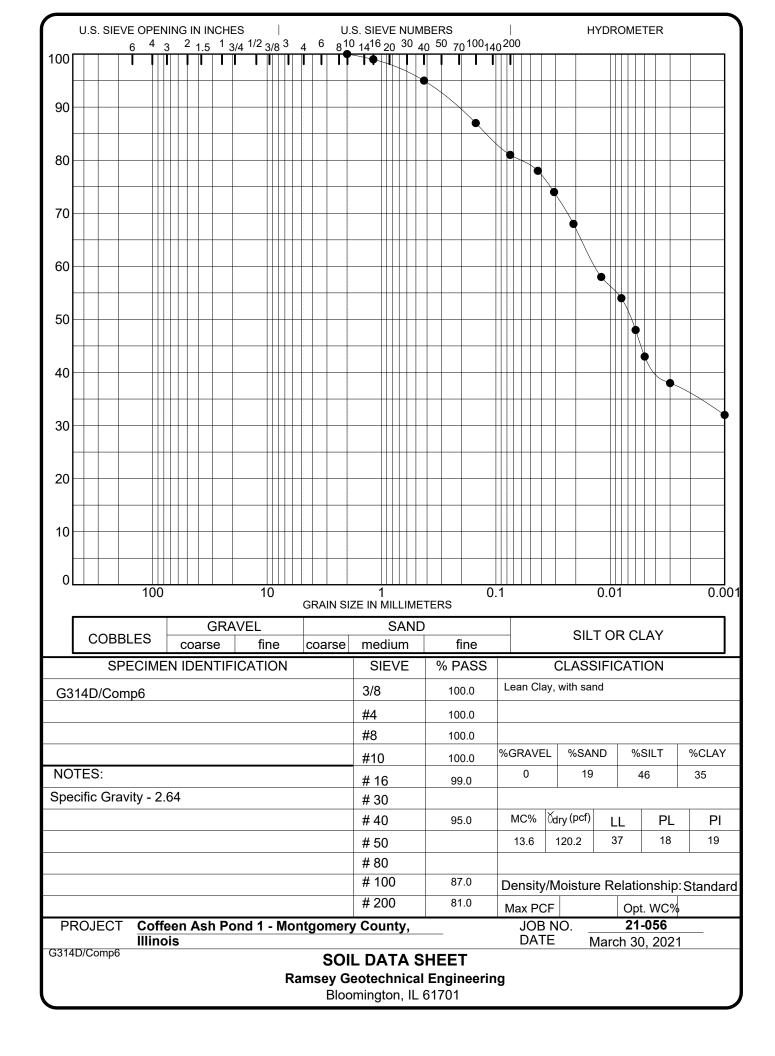


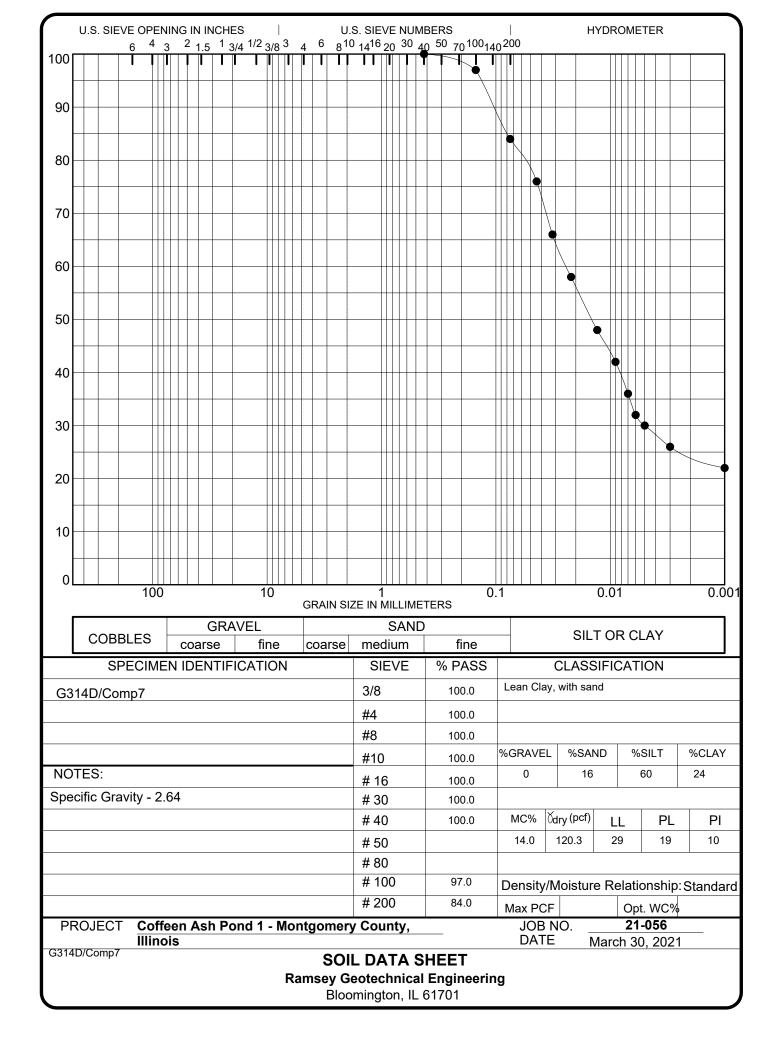


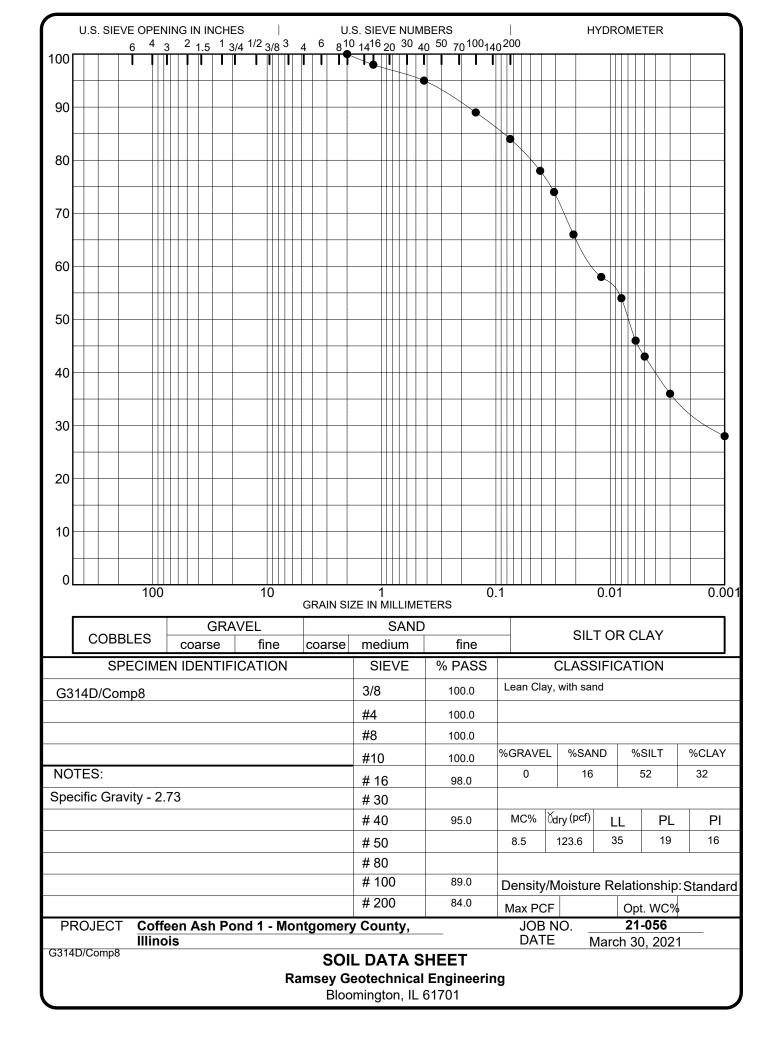














Via email: dramsey@ramgeoeng.com

April 5, 2021 J037264.01.6003

Mr. Douglas P. Ramsey, P.E. Ramsey Geotechnical Engineering 1701 W. Market Street Bloomington, Illinois 61701

Re: Coffeen Power Station

Ash Pond 1

Montgomery County, Illinois

Dear Mr. Ramsey:

Included in this report are the test results from five Shelby tubes and one bulk sample of bottom ash received in our laboratory on March 15, 2021. The samples were tested in general accordance with the test method listed below.

| Test to Determine | Method of Test |
|---|-------------------|
| Water (Moisture) Content of Soils | ASTM D2216 |
| Description and Identification of Soils (Visual-Manual) | ASTM D2488 |
| Hydraulic Conductivity of Soil | ASTM D5084 |
| Using Flexible Wall Permeameter | |
| Density (Unit Weight) of Soil Specimens | ASTM D7263 |

We trust this is the information you require. Please contact the undersigned if you have any questions regarding this report.

Respectfully submitted,

GEOTECHNOLOGY, INC.

Janet M. May

Illinois Laboratory Manager

JMM/LPH:jmm

Attachment: Test Result Summary

Hydraulic Conductivity Test Data Sheets Proctor Curve (Provided by Ramsey)

Shelby Tube Logs

Testing Assignment Sheets

11 French Village Industrial Park • Fairview Heights, IL 62208 • 618-345-4811 • Fax 618-345-5108 • geotechnology.com

Ramsey Geotechnical Engineering April 5, 2021 Page 2

TEST RESULT SUMMARY

Coffeen Power Station Ash Pond 1 Montgomery County, Illinois

| | | | ASTM D2216 | ASTM D7263 | ASTM D5084 | | | |
|------------------|------------------|----------------|------------------------|-------------------------|--------------------------------------|-----------------------------------|--|--|
| Boring Number | Sample Number | Depth, feet | Moisture Content, % | Dry Unit Weight, pcf | Hydraulic Conductivity, cm/sec | Range of Hydraulic Gradient | | |
| G307D | ST-5 | 8.0-10.0 | 21.6 | 105.0 | 4.8 x 10 ⁻⁸ | 1.3 - 12.9 | | |
| G307D | ST-22 | 42.0-44.0 | 15.0 | 118.8 | 3.7×10^{-7} | 5.5 - 20.7 | | |
| G311D | ST-4 | 6.0-8.0 | 19.7 | 107.5 | 2.9 x 10 ⁻⁸ | 11.9 - 22.7 | | |
| G311D | ST-14 | 26.0-28.0 | 16.2 | 116.7 | 5.5 x 10 ⁻⁸ | 1.4 - 1.5 | | |
| G314D | ST-18 | 34.0-36.0 | 16.6 | 115.0 | 3.0×10^{-7} | 0.9 - 6.7 | | |

| Sample Number/ Material | Optimum Moisture Content, % | Maximum Dry Unit Weight, pcf | Percent Compact | Moisture Content, % | Dry Unit Weight, pcf | Hydraulic Conductivity, cm/sec | Range of Hydraulic Gradient |
|-------------------------------|-----------------------------------|------------------------------------|--------------------|------------------------|-------------------------|--------------------------------------|-----------------------------------|
| LSN-3782/ Bottom Ash | 11.0 | 123.0 | 90.0 | 12.5 | 110.8 | 8.8 x 10 ⁻⁵ | 0.4 - 2.3 |

| | | | ASTM D2488 |
|------------------|------------------|-------------|--|
| Boring Number | Sample Number | Depth, feet | Material Description |
| G307D | ST-5 | 8.0-10.0 | Gray and yellow-brown, LEAN to FAT CLAY, some sand, trace gravel – CL/CH |
| G307D | ST-22 | 42.0-44.0 | Very dark gray-brown, LEAN CLAY with SAND, some gravel – CL |
| G311D | ST-4 | 6.0-8.0 | Gray-brown, LEAN CLAY with SAND, trace gravel - CL |
| G311D | ST-14 | 26.0-28.0 | Very dark gray-brown, LEAN CLAY, some sand, gravel – CL |
| G314D | ST-18 | 34.0-36.0 | Very dark gray, LEAN CLAY, trace sand, gravel – CL |

Notes and abbreviations:

% - Percent

cm/sec - Centimeters per second

| | | | | | | | Init | ial Unit Weigl | nt | | Unit Wei | ight as Te | sted |
|-------------|-----------------|-----------|-----------------|----------------|-----------------|-----------|------------|------------------|---------|-------------|--------------|------------|----------|
| JOB NO.: | J03 | 7264.01.6 | 002 | | | | WET UNIT V | WEIGHT, pcf: | 127.7 | W | ET UNIT WEIG | HT, pcf: | 127.4 |
| BORING NO | O.: | G307D | | | | | DRY UNIT V | WEIGHT, pcf: | 105.0 | D | RY UNIT WEIG | HT, pcf: | 104.0 |
| SAMPLE N | O.: ST- | -5; LSN-3 | 786 | | | | | | | | | | |
| DEPTH (Fee | et): | 8.0-10.0 | | | | | | | | | | | |
| | | Initial | As Tested** | | Initial | As Tested | INITIAL MO | ISTURE CONTE | NT | FINAL MOIST | URE CONTENT | | |
| LENGTH, is | | 4.779 | 4.793 | LENGTH, cn | | 12.174 | WET WT SP | | 1311.89 | WET WT SPLE | | 1319.74 | |
| DIAMETER | R, in.: | 2.876 | 2.887 | DIAMETER, | cn 7.305 | 7.333 | DRY WT SP | LE+TARE | 1126.94 | DRY WT SPLE | +TARE | 1126.94 | |
| WET WT., § | gms.: | 1040.57 | 1049.12 | • | | | TARE WEIG | HT | 271.38 | TARE WEIGH | Γ | 271.38 | |
| AREA, sq.ir | n.: | 6.496 | 6.546 | AREA, sq cm | : 41.912 | 42.233 | % MOISTU | RE | 21.6 | % MOISTURE | | 22.5 | |
| B VALUE (t | before Permeati | ion): | 95% | Cell / Back Pr | essure, psi: 75 | / 70 | | | | | | | |
| HEAD | DATE | | TIME | TEMP | ELAPSED | воттом | TOP | Q | K | HYDRAULIC | HYDRAULIC | HEAD | k |
| (PSI) | (YR,MO,DY) | | (HR,MN,SC) | <u>°C</u> | MINUTES | BURETTE | BURETTE | (CC) | CM/SEC | GRADIENT | HEAD | LOSS,% | (in/sec) |
| 0.0 | 16-Mar-21 | | 05:05 PM | 20.8 | 0 | 5.82 | 22.52 | | | 1.38 | 16.70 | | |
| 0.0 | 17-Mar-21 | | 08:23 AM | 21.1 | 918 | 5.93 | 22.35 | 0.11 | 4.6E-08 | 1.35 | 16.42 | 1.68 | 1.8E-08 |
| 0.0 | 17-Mar-21 | | 01:42 PM | 21.9 | 319 | 5.98 | 22.30 | 0.05 | 4.8E-08 | 1.34 | 16.32 | 0.61 | 1.9E-08 |
| 2.0 | 17-Mar-21 | | 02:20 PM | 21.9 | 0 | 6.10 | 22.29 | | | 12.92 | 156.79 | | |
| 2.0 | 17-Mar-21 | | 05:23 PM | 21.9 | 183 | 6.41 | 21.97 | 0.31 | 5.5E-08 | 12.86 | 156.16 | 0.40 | 2.2E-08 |
| 2.0 | 18-Mar-21 | | 08:23 AM | 21.1 | 900 | 7.81 | 20.71 | 1.40 | 4.8E-08 | 12.65 | 153.50 | 1.70 | 1.9E-08 |
| | | , | Average Temp. = | 21.5 | | | | AVERAGE K = | 5.0E-08 | | AVEI | RAGE K = | 2.0E-08 |
| | | _ | | ,- | | | | ted K for 20°C = | | | Corrected K | | 1.9E-08 |

^{**} Measurements at end of test

HYDRAULIC CONDUCTIVITY TEST DATA

(ASTM D 5084, Method F)

| | | | | | | | | Initial Unit Wei | ght | Unit Weight as Tested | | | |
|-----------------|-----------------|-----------------|---------------|----------------|---------------------|-----------|------------|-----------------------|---------|-----------------------|----------------|----------|--|
| JOB NO.: | J037264.01 | 1.6002 | | | | | WET UNIT W | VEIGHT, pcf: | 136.6 | WET UNIT W | EIGHT, pcf: | 136.3 | |
| BORING NO.: | G3071 | D | | | | | DRY UNIT W | DRY UNIT WEIGHT, pcf: | | DRY UNIT W | EIGHT, pcf: | 117.9 | |
| SAMPLE NO.: | ST-22; LSN | N-3787 | | | | | | | | | | | |
| DEPTH (Feet): | 42-44 | 1 | | | | | | | | | | | |
| | Turbitud. | A - T - 4 - 1** | | | 1 | A - T1 | DUTIAL MO | IGTUDE CONTENT | | EDIAL MOS | TUDE CONTENT | , | |
| LENGTH : | Initial | As Tested** | LENGTH | | Initial | As Tested | | ISTURE CONTENT | 1260.70 | | STURE CONTENT | | |
| LENGTH, in.: | 4.653 | 4.660 | LENGTH, c | | 11.819 | 11.836 | WET WT SPI | | 1360.70 | WET WT SPI | | 1366.19 | |
| DIAMETER, in. | | 2.884 | DIAMETER | <i>'</i> | 7.303 | 7.325 | DRY WT SPI | | 1219.23 | DRY WT SPI | | 1219.23 | |
| WET WT., gms. | | 1089.51 | AREA, sq c | m: | 41.883 | 42.145 | TARE WEIG | | 277.21 | TARE WEIGI | | 277.21 | |
| AREA, sq.in.: | 6.492 | 6.533 | | | | | % MOISTUI | RE | 15.0 | % MOISTUR | Е | 15.6 | |
| B VALUE (before | re Permeation): | 97% | Cell / Back I | Pressure, psi: | 45 / 4 | 40 | | | | | | | |
| | | M_1 | M_2 | | | | | | | | | | |
| Manometer Con | atanta | 0.0302 | 1.0410 | Com | nla Constant (I /A) | 0.2808 | | | | | | | |
| Manometer Con | stants | 0.0302 | 1.0410 | Sam | ple Constant (L/A) | υ.2808 | С | Т | | | | | |
| DATE | TIME | TEMP | ELAPSED | PIPET | ANNULUS | SPECIFIC | TEST | TRIAL | K | HYDRAULIC | HYDRAULIC | k | |
| (YR,MO,DY) | (HR,MN,SC) | <u>°C</u> | MINUTES | READING | READING | GRAVITY | CONSTANT | CONSTANT | CM/SEC | GRADIENT | HEAD | (in/sec) | |
| 17-Mar-21 | 09:03 AM | 22.1 | 0 | 19.29 | 0.72 | 12.570 | 0.000674 | 0.0561 | | 19.72 | 233.42 | | |
| 17-Mar-21 | 09:13 AM | 22.1 | 10 | 14.78 | 0.92 | 12.570 | 0.000674 | 0.0751 | 4.6E-07 | 14.72 | 174.22 | 1.8E-07 | |
| 17-Mar-21 | 09:35 AM | 22.1 | 22 | 10.37 | 0.61 | 12.570 | 0.000674 | 0.1067 | 3.2E-07 | 10.36 | 122.68 | 1.3E-07 | |
| 17-Mar-21 | 10:40 AM | 21.8 | 65 | 5.90 | 0.77 | 12.570 | 0.000674 | 0.2029 | 4.1E-07 | 5.45 | 64.48 | 1.6E-07 | |
| 17-Mar-21 | 02:55 PM | 21.5 | 0 | 20.15 | 0.66 | 12.570 | 0.000674 | 0.0534 | | 20.70 | 244.99 | | |
| 17-Mar-21 | 03:13 PM | 21.5 | 18 | 13.93 | 0.92 | 12.570 | 0.000674 | 0.0800 | 4.3E-07 | 13.82 | 163.54 | 1.7E-07 | |
| 17-Mar-21 | 04:33 PM | 21.9 | 80 | 8.13 | 1.18 | 12.570 | 0.000674 | 0.1498 | 2.9E-07 | 7.38 | 87.36 | 1.1E-07 | |
| | Average Temp. = | 21.9 | | | | | | AVERAGE K = | 3.8E-07 | A | VERAGE K = | 1.5E-07 | |
| | | | | | | | Corr | ected K for 20°C = | 3.7E-07 | | d K for 20°C = | 1.4E-07 | |

^{**} Measurements at end of test

HYDRAULIC CONDUCTIVITY TEST DATA

(ASTM D 5084, Method F)

| | | | | | | | | Initial Unit Wei | ght | Unit Weight as Tested | | |
|------------------|----------------|-------------|---------------|----------------|---|-----------|------------|-----------------------------|---------|------------------------------|----------------|----------|
| JOB NO.: | J037264.01 | 1.6002 | | | | | WET UNIT W | /EIGHT, pcf: | 128.7 | WET UNIT W | EIGHT, pcf: | 129.3 |
| BORING NO.: | G3111 | D | | | | | DRY UNIT W | DRY UNIT WEIGHT, pcf: 107.5 | | | EIGHT, pcf: | 107.3 |
| SAMPLE NO.: | ST-4; LSN | I-3788 | | | | | | | | | | |
| DEPTH (Feet): | 6.0-8. | 0 | | | | | | | | | | |
| | Initial | As Tested** | | | Initial | As Tested | INITIAL MO | ISTURE CONTENT | | EINIAI MOIS | STURE CONTENT | |
| LENGTH, in.: | 4.444 | 4.447 | LENGTH, c | | 11.288 | 11.295 | WET WT SPI | | 1271.15 | WET WT SPI | | 1277.34 |
| , | | | , | | | | | | | | | |
| DIAMETER, in.: | 2.879 | 2.881 | DIAMETER | <i>'</i> | 7.313 | 7.318 | DRY WT SPI | | 1110.30 | DRY WT SPI | | 1110.30 |
| WET WT., gms.: | 977.08 | 983.97 | AREA, sq c | m: | 41.999 | 42.058 | TARE WEIGI | | 294.07 | TARE WEIGI | | 294.07 |
| AREA, sq.in.: | 6.510 | 6.519 | | | | | % MOISTUI | КE | 19.7 | % MOISTUR | E | 20.5 |
| B VALUE (before) | Permeation): | 97% | Cell / Back F | Pressure, psi: | 45 / 4 | 40 | | | | | | |
| | | M_1 | M_2 | | | | | | | | | |
| Manometer Consta | ints | 0.0302 | 1.0410 | Sam | ple Constant (L/A) | 0.2686 | | | | | | |
| | | | | | , | γ | С | T | | | | |
| DATE | TIME | TEMP | ELAPSED | PIPET | ANNULUS | SPECIFIC | TEST | TRIAL | K | HYDRAULIC | HYDRAULIC | k |
| (YR,MO,DY) | (HR,MN,SC) | <u>°C</u> | MINUTES | READING | READING | GRAVITY | CONSTANT | CONSTANT | CM/SEC | GRADIENT | HEAD | (in/sec) |
| 22-Mar-21 | 08:47 AM | 19.5 | 0 | 21.23 | 0.88 | 12.570 | 0.000645 | 0.0512 | | 22.65 | 255.80 | |
| 22-Mar-21 | 09:04 AM | 19.7 | 17 | 20.25 | 0.91 | 12.570 | 0.000645 | 0.0538 | 3.4E-08 | 21.52 | 243.10 | 1.3E-08 |
| 22-Mar-21 | 09:30 AM | 19.8 | 26 | 19.07 | 0.96 | 12.570 | 0.000645 | 0.0575 | 2.9E-08 | 20.15 | 227.64 | 1.1E-08 |
| 22-Mar-21 | 10:12 AM | 19.8 | 42 | 17.48 | 1.03 | 12.570 | 0.000645 | 0.0633 | 2.7E-08 | 18.31 | 206.78 | 1.1E-08 |
| 22-Mar-21 | 10:57 AM | 20.0 | 45 | 16.03 | 1.10 | 12.570 | 0.000645 | 0.0697 | 2.5E-08 | 16.61 | 187.67 | 1.0E-08 |
| 22-Mar-21 | 12:10 PM | 20.4 | 73 | 13.98 | 1.17 | 12.570 | 0.000645 | 0.0813 | 2.7E-08 | 14.26 | 161.02 | 1.1E-08 |
| 22-Mar-21 | 01:36 PM | 20.5 | 86 | 11.93 | 1.26 | 12.570 | 0.000645 | 0.0976 | 2.8E-08 | 11.87 | 134.12 | 1.1E-08 |
| A - | verage Temp. = | 19.9 | | | | | | AVERAGE K = | 2.8E-08 | A | VERAGE K = | 1.1E-08 |
| A | verage remp. = | 17.7 | | | | | Corre | ected K for 20°C = | 2.9E-08 | | d K for 20°C = | 1.1E-08 |

^{**} Measurements at end of test

| | | | | | | | Initi | al Unit Weig | ht | | Unit Wei | ght as Te | sted |
|-----------|--------------------|-----------|-----------------|----------------|------------------|-----------|------------|-----------------|---------|-----------------------|--------------|------------|----------|
| JOB NO.: | J037 | 7264.01.6 | 002 | | | | WET UNIT V | VEIGHT, pcf: | 135.6 | W | ET UNIT WEIG | HT, pcf: | 136.2 |
| BORING 1 | NO.: | G311D | | | | | DRY UNIT W | /EIGHT, pcf: | 116.7 | DRY UNIT WEIGHT, pcf: | | | 117.1 |
| SAMPLE | NO.: ST-1 | 14; LSN-3 | 3789 | | | | | _ | | | | - | |
| DEPTH (F | eet): | 26.0-28.0 | | | | | | | | | | | |
| | Ī | Initial | As Tested** | | Initial | As Tested | INITIAL MO | ISTURE CONTI | ENT | FINAL MOIST | ΓURE CONTENT | | |
| LENGTH, | in.: | 5.010 | 4.991 | LENGTH, cı | n: 12.725 | 12.677 | WET WT SPI | LE+TARE | 1428.49 | WET WT SPLI | E+TARE | 1429.87 | |
| DIAMETE | ER, in.: | 2.873 | 2.874 | DIAMETER | , cm 7.297 | 7.300 | DRY WT SPI | LE+TARE | 1267.73 | DRY WT SPLE | E+TARE | 1267.73 | |
| WET WT., | , gms.: | 1155.90 | 1157.76 | | | | TARE WEIG | НТ | 272.59 | TARE WEIGH | T | 272.59 | |
| AREA, sq. | in.: | 6.483 | 6.487 | AREA, sq cn | n: 41.824 | 41.853 | % MOISTUI | RE | 16.2 | % MOISTURE | | 16.3 | |
| B VALUE | (before Permeation | on): | 98% | Cell / Back Pr | ressure, psi: 55 | / 50 | | | | | | | |
| HEAD | DATE | | TIME | TEMP | ELAPSED | воттом | ТОР | Q | К | HYDRAULIC | HYDRAULIC | HEAD | k |
| (PSI) | (YR,MO,DY) | | (HR,MN,SC) | <u>°C</u> | MINUTES | BURETTE | BURETTE | (CC) | CM/SEC | GRADIENT | HEAD | LOSS,% | (in/sec) |
| 0.0 | 21-Mar-21 | | 08:42 AM | 17.6 | 0 | 3.40 | 22.15 | | | 1.47 | 18.75 | | |
| 0.0 | 21-Mar-21 | | 12:52 PM | 19.0 | 250 | 3.45 | 22.11 | 0.05 | 5.1E-08 | 1.47 | 18.66 | 0.48 | 2.0E-08 |
| 0.0 | 22-Mar-21 | | 08:10 AM | 19.0 | 1158 | 3.67 | 21.90 | 0.22 | 5.3E-08 | 1.43 | 18.23 | 2.30 | 2.1E-08 |
| 0.0 | 22-Mar-21 | | 01:50 PM | 20.3 | 340 | 3.72 | 21.83 | 0.05 | 5.1E-08 | 1.42 | 18.11 | 0.66 | 2.0E-08 |
| 0.0 | 23-Mar-21 | | 07:01 AM | 20.3 | 1031 | 3.90 | 21.58 | 0.18 | 6.2E-08 | 1.39 | 17.68 | 2.37 | 2.4E-08 |
| | | 1 | Average Temp. = | 19.2 | | | | AVERAGE K = | 5.4E-08 | | AVER | RAGE K = | 2.1E-08 |
| | | | | | | | Correct | ed K for 20°C = | 5.5E-08 | | Corrected K | for 20°C = | 2.2E-08 |

^{**} Measurements at end of test

| | | | | | | | Initial Unit Weight | | Unit Weight as T | | | sted | |
|-----------|----------------|------------|-----------------|----------------|------------------|-----------|---------------------|------------------|------------------|-------------|--------------|------------|----------|
| JOB NO.: | J03 | 37264.01.6 | 5002 | | | | WET UNIT V | WEIGHT, pcf: | 134.1 | V | ET UNIT WEIG | HT, pcf: | 134.3 |
| BORING 1 | NO.: | G314D | | | | | DRY UNIT V | WEIGHT, pcf: | 115.0 | D | RY UNIT WEIG | HT, pcf: | 114.7 |
| SAMPLE | NO.: ST | -18; LSN- | 3790 | | | | | | | | | | |
| DEPTH (F | Feet): | 34.0-36.0 |) | | | | | | | | | | |
| | | Initial | As Tested** | | Initial | As Tested | INITIAL MC | DISTURE CONT | ENT | FINAL MOIS | TURE CONTENT | - | |
| LENGTH, | in.: | 5.097 | 5.105 | LENGTH, cn | n: 12.946 | 12.967 | WET WT SP | LE+TARE | 1467.69 | WET WT SPLI | E+TARE | 1471.60 | |
| DIAMETE | ER, in.: | 2.876 | 2.878 | DIAMETER, | er 7.305 | 7.310 | DRY WT SP | LE+TARE | 1301.35 | DRY WT SPLI | E+TARE | 1301.35 | |
| WET WT. | , gms.: | 1165.92 | 1170.56 | | | | TARE WEIG | HT | 301.77 | TARE WEIGH | T | 301.77 | |
| AREA, sq. | .in.: | 6.496 | 6.505 | AREA, sq cn | n: 41.912 | 41.970 | % MOISTU | RE | 16.6 | % MOISTURE | | 17.0 | |
| B VALUE | (before Permea | tion): | 98% | Cell / Back Pr | ressure, psi: 44 | 4 / 40 | | | | | | | |
| HEAD | DATE | | TIME | TEMP | ELAPSED | BOTTOM | TOP | Q | K | HYDRAULIC | HYDRAULIC | HEAD | k |
| (PSI) | (YR,MO,DY) | | (HR,MN,SC) | <u>°C</u> | MINUTES | BURETTE | BURETTE | (CC) | CM/SEC | GRADIENT | HEAD | LOSS,% | (in/sec) |
| 0.0 | 19-Mar-21 | | 10:12 AM | 19.4 | 0 | 6.03 | 22.64 | | | 1.28 | 16.61 | | |
| 0.0 | 21-Mar-21 | | 11:16 AM | 19.0 | 2944 | 8.13 | 20.01 | 2.10 | 3.1E-07 | 0.92 | 11.88 | 28.48 | 1.2E-07 |
| 1.0 | 21-Mar-21 | | 11:41 AM | 19.1 | 0 | 8.35 | 19.94 | | | 6.33 | 81.89 | | |
| 1.0 | 21-Mar-21 | | 12:51 PM | 19.4 | 70 | 8.73 | 19.65 | 0.38 | 3.2E-07 | 6.27 | 81.22 | 0.82 | 1.2E-07 |
| 1.0 | 22-Mar-21 | | 08:11 AM | 19.2 | 1160 | 13.80 | 14.76 | 5.07 | 3.0E-07 | 5.50 | 71.26 | 12.26 | 1.2E-07 |
| 1.0 | 22-Mar-21 | | 08:28 AM | 19.2 | 0 | 7.48 | 23.29 | | | 6.65 | 86.11 | | |
| 1.0 | 22-Mar-21 | | 11:59 AM | 20.3 | 211 | 8.40 | 22.33 | 0.92 | 2.8E-07 | 6.51 | 84.23 | 2.18 | 1.1E-07 |
| 1.0 | 22-Mar-21 | | 01:51 PM | 20.7 | 112 | 8.83 | 21.83 | 0.43 | 2.7E-07 | 6.43 | 83.30 | 1.10 | 1.1E-07 |
| | | | Average Temp. = | 19.5 | | | | AVERAGE K | = 3.0E-07 | | AVEI | RAGE K = | 1.2E-07 |
| | | | | | | | Correc | ted K for 20°C : | = 3.0E-07 | | Corrected K | for 20°C = | 1.2E-07 |

^{**} Measurements at end of test

| | | | | | | Initial Unit Weight | | | Unit Weight as Teste | | | sted |
|-----------|----------------------|-----------------|----------------|----------------------|-----------|----------------------------|------------------|------------|----------------------|--------------|------------|----------|
| JOB NO.: | J037264 | .01.6002 | ASTM D698 | Results | | WET UNIT V | WEIGHT, pcf: | 124.6 | W | ET UNIT WEIG | HT, pcf: | 132.0 |
| PROJECT: | Coffeen A | sh Pond 1 | Maximum Dr | y Unit Weight, pcf | 123.0 | DRY UNIT V | WEIGHT, pcf: | 110.8 | DRY UNIT WEIGHT, p | | HT, pcf: | 110.8 |
| SAMPLE 1 | NO.: LSN | -3782 | Optimum Wa | ter Content, % | 11.0 | Percent Con | npact: | 90.0% | | | | |
| MATERIA | L: Botto | m Ash | | | | | | | | | | |
| | | | | | | | | | | | | |
| | Initia | | | Initial | As Tested | - | DISTURE CONT | <u>ENT</u> | | TURE CONTENT | - | |
| LENGTH, | in.: 2 | .869 2.848 | LENGTH, cr | n: 7.287 | 7.234 | WET WT SP | LE+TARE | 896.23 | WET WT SPLI | E+TARE | 932.52 | |
| DIAMETE | R, in.: 2 | .884 2.895 | DIAMETER | , cn 7.325 | 7.353 | DRY WT SP | LE+TARE | 828.37 | DRY WT SPLE | E+TARE | 828.37 | |
| WET WT., | gms.: 61 | 2.77 649.36 | | | | TARE WEIG | HT | 283.46 | TARE WEIGH | Т | 283.46 | |
| AREA, sq. | in.: 6 | .533 6.582 | AREA, sq cn | n: 42.145 | 42.467 | % MOISTU | RE | 12.5 | % MOISTURE | | 19.1 | |
| | | | | | | | | | | | | |
| B VALUE | (before Permeation): | 95% | Cell / Back Pr | ressure, psi: 83 / 8 | 0 | Percent Wet | of Optimum: | 1.5 | | | | |
| HEAD | DATE | TIME | TEMP | ELAPSED | воттом | TOP | Q | K | HYDRAULIC | HYDRAULIC | HEAD | k |
| (PSI) | (YR,MO,DY) | (HR,MN,SC) | <u>°C</u> | MINUTES | BURETTE | BURETTE | (CC) | CM/SEC | GRADIENT | HEAD | LOSS,% | (in/sec) |
| 0.0 | 30-Mar-21 | 04:49 PM | 22.3 | 0 | 6.41 | 23.00 | | | 2.28 | 16.59 | | |
| 0.0 | 30-Mar-21 | 04:51 PM | 22.3 | 2 | 7.40 | 22.00 | 0.99 | 9.5E-05 | 2.00 | 14.60 | 12.00 | 3.7E-05 |
| 0.0 | 30-Mar-21 | 04:53 PM | 22.3 | 2 | 8.21 | 21.10 | 0.81 | 9.3E-05 | 1.77 | 12.89 | 11.71 | 3.7E-05 |
| 0.0 | 30-Mar-21 | 04:57 PM | 22.4 | 4 | 9.60 | 19.70 | 1.39 | 9.1E-05 | 1.39 | 10.10 | 21.64 | 3.6E-05 |
| 0.0 | 30-Mar-21 | 05:05 PM | 22.4 | 8 | 11.59 | 17.74 | 1.99 | 9.2E-05 | 0.84 | 6.15 | 39.11 | 3.6E-05 |
| 0.0 | 30-Mar-21 | 05:16 PM | 22.5 | 11 | 13.10 | 16.20 | 1.51 | 9.3E-05 | 0.43 | 3.10 | 49.59 | 3.7E-05 |
| | | A T | 22.4 | | | | AMEDACE | 0.2E 05 | | A = 7=1= | DACE IZ | 2.5E 05 |
| | | Average Temp. = | = 22.4 | | | | AVERAGE K | | | | RAGE K = | 3.7E-05 |
| | | | | | | Correc | ted K for 20°C : | - 0.0E-05 | | Corrected K | ior 20°C = | 3.5E-05 |

^{**} Measurements at end of test



| | | | | LSN-378 LSN-378 | | | ZOZI By: JMN to_10 | | | | | |
|-------------------------------|-----------------------------|---------------|---|---|-----------------------|------------|-----------------------|--|--|--|--|--|
| | 24 mag m | Shelby" | | | | | | | | | | |
| Tube [| Dimensions | S: Outside | Diameter (in): 3 | _ | Recovery | / (in): | - | | | | | |
| Tube Condition: Remarks | | End(s) not se | aled Other: | Sample 0 | Condition Good | d Fair | Poor Disturbed | | | | | |
| Tube Scale | Sample Use Test Type) | | Soil Identification and Processing Remarks (Draw lines to indicate top and botton of soil's surface and where sample was taken. Identify cut lines with: "Cut" "Date: m/d/y" "Your Initials") | | | | | | | | | |
| 2.0 | | Gray an | | LEAN TO FAT C trace gravel | | | | | | | | |
| 6.0 | | | - | | | Q | 0=2,75-654 | | | | | |
| 10.0 | K [†] | | | | | 5 | | | | | | |
| 14.0 | | | | | | | 20/54 | | | | | |
| 18.0 | | | | | | (Jp= | 2.0 tst | | | | | |
| 22.0 | | | / | | | | | | | | | |
| 24.0 Ave. H | Height (in.): | | Ave. Diame | eter (in.): | Specimen | n Wt. (gms |): | | | | | |
| | Tare | Number | Wet Mass + Tare (g) | atural Moisture Conter Dry Mass+ Tare (g) | t Tare Mass (g) | s W | /ater Content (%) | | | | | |
| | Wet t | Jnit Weight: | | pcf Dry Unit W | eight | | pcf | | | | | |
| 1 | d By: Date: | | | ted By: Date: /ersion.xls, 2.0-Scale | Checked By: Date: | | | | | | | |



| | Vo.: G3 | 307D | Sample N | LSN-378 10.: SH-22 | Depth | (ft): 4 | 2 to | 44 | | | | |
|--------------------------|-----------------------------|--------------|---|-----------------------|-----------|--------------|----------|---------------|--|--|--|--|
| Туре | X Std. " | Shelby" | Other: | | | | | | | | | |
| Tube D | imensions | s: Outside | Diameter (in):3 | _ | Re | covery (in): | /8 | | | | | |
| Tube | Dented | End(s) not s | ealed Other: | Sample (| Condition | Good Fa | air Poor | Disturbed | | | | |
| Remarks: | | | | | | | | | | | | |
| Tube Scale (in) (* | Sample Use Test Type) | | Soil Identification and Processing Remarks (Draw lines to indicate top and botton of soil's surface and where sample was taken. Identify cut lines with: "Cut" "Date: m/d/y" "Your Initials") | | | | | | | | | |
| .0 | | | | | | | | E u Kadis | | | | |
| .0 | | | 3" Clayen SAN | | | | | colored. | | | | |
| .0 | | very | dade gray-bi | 1-64 | carwi | HA SAN | 0, | | | | | |
| | | | 0 | | | | | SESA | | | | |
| .0 | -1 | | | | | 9/ | D-216 | 2001 | | | | |
| .0 | K | | | | | | | | | | | |
| 0.0 | | | | | | | | | | | | |
| 2.0 | | at . | | | | | | | | | | |
| 1.0 | | | | | | Qp | = 3.75 | stst | | | | |
| | | | | | | | | | | | | |
| 5.0 | | | | | | | | | | | | |
| 3.0 | | - | | | | | | | | | | |
| 0.0 | | 1 | | | | | | | | | | |
| 2.0 | | | | | | | | | | | | |
| 1.0 | | | | | | | | | | | | |
| Ave. H | eight (in.) | | Ave. Diame | eter (in.): | Sp | ecimen Wt. | (gms): | | | | | |
| | Tass | Number | N N | 14 | | | | | | | | |
| | rare | Number | Wet Mass + Tare (g) | Dry Mass+ Tare (g) | | Mass g) | | Content %) | | | | |
| | | | | | | | | | | | | |
| | Wet | Unit Weight: | | pcf Dry Unit W | eight | | pcf | | | | | |
| | By: | | Calculated By: Checked By: Date: Date: | | | | | | | | | |



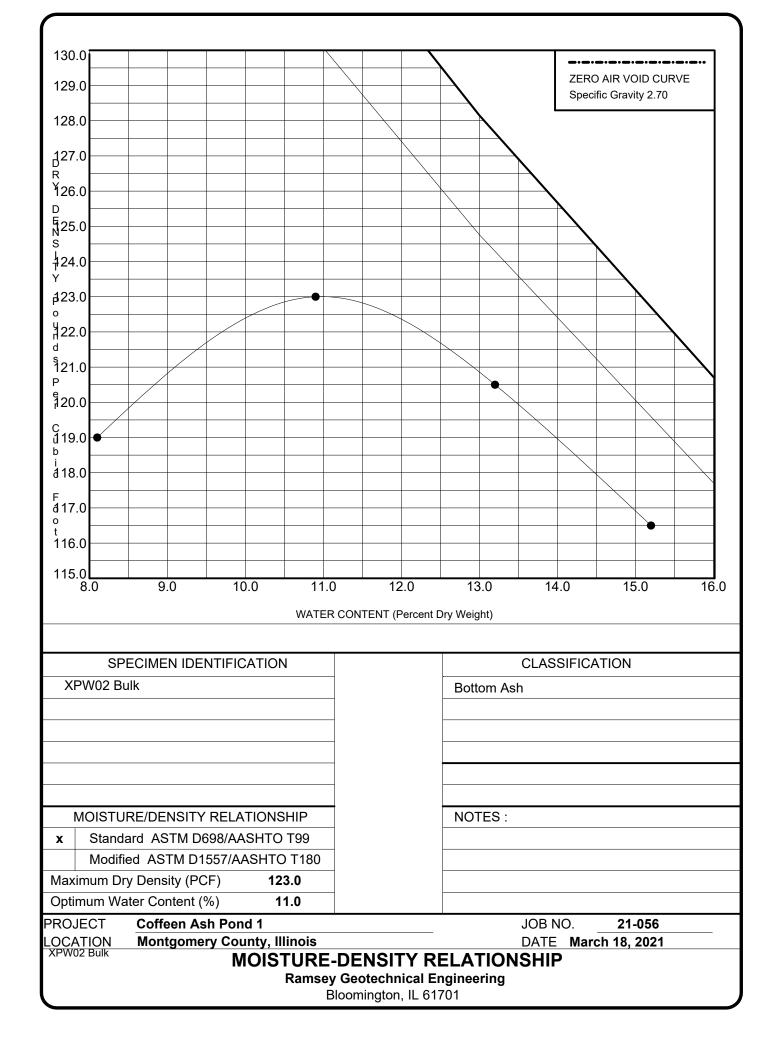
| Proj | ect No.: <u>//</u> | 13 72 | 64.01.0 | 6002 Proje | ect Name. | : Coff | <u>een</u> N-3788 | Date C | pened: | 3/1 | 8/202 | / By: <u>/ A</u> | M |
|-----------------------|----------------------------|---------|-------------|----------------|-------------|-------------------------|--|-----------|---------|---------|--------------|------------------|---|
| Bor | ing No.: _G | 311 | D | Sa | ample No. | | 4 | Depth | (ft): | 6 | to | 8 | |
| T | ype X Sto | d. "She | lby" [| Other: | | | | | | | | | |
| Tul | be Dimensi | ons: | Outside | Diameter (in): | 3 | 4 | | Re | covery | (in): | 24 | _ | |
| Tube | _ | Enc | l(s) not se | aled | Other: | | Sample Co | ondition | Good | Fair | Poor | Disturbed | |
| Condition | | | | | | | | | V | 7.34 | | 111101 | |
| Tube Scale (in) | Sample Use (Test Typ | | | (Draw lines to | indicate to | op and bo | tion and Pro tton of soil's n: "Cut" "Da | surface a | and whe | re sam | C I am man a | taken. | |
| 0.0 | | 6 | bray- | brown, LE | ANC | LAYWI | th SAVI | trac | e 91 | avel | -c | _ | |
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| 6.0 | | + | | | | | | | | (| Op= | 2.0-651 | |
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| 16.0 | | - | | | | | | | | m. | 7 | 044 | |
| 18.0 | | | | | | | | | | W.F | | otst | |
| 20.0 | | - | | | _/ | | | | | | | | |
| 22.0 | | 4 | | | / | | | | | | | | |
| 24.0 | | | | / | / | | | | | | | | |
| Av | e. Height (ii | n.): | | Ave | . Diamete | | | _ Spo | ecimen | Wt. (gm | ıs): | | ~ |
| | Та | re Nur | nber | Wet Mass + | | ural Moiste Dry Mass | ure Content s+ Tare | Tare | Mass | | Water C | Content | |
| | | | | (g) | | (g |) | (| g) | | (% | b) | |
| | | | | | | | | | | | | | |
| | We | et Unit | Weight: | | pc | ef [| Ory Unit Wei | ight | | | pcf | | |
| Tes | sted By: | | 2 | (| Calculated | d By: | | | Chec | ked By: | | | |
| 4.5 | Date: | | _ | 22/3/26/38 | | Date: | 25 Apr 43 - 235 | | | | | | |
| 102 | 2 (12/08/09 | 9) | | TubeLog | JMM Ver | rsion.xls, | 2.0-Scale | 6/15/201 | 17 | | | | |



| Proje | ect No.: <u>/</u> / | 237 | 264.01. | 6002 | Project Nan | ne.: <u>Cot</u> | Feen 2750 | 1 | | | | -/ By: JMM |
|-----------------------|---------------------------|-------------|-------------|--------------|--|-----------------|---|-----------|------------|---------|---------|--|
| Bori | ng No.: 6 | 3 | 110 | | Sample N | No.: 5H- | 5N-3789 - 14 | Depth | (ft): | 26 | to | 28 |
| Ту | pe X St | d. "S | helby" | Oth | ner: | | | | | | | |
| Tub | e Dimensi | ons: | Outside | Diame | ter (in):3 | | | Re | covery (| in):2 | 24 | _ |
| Tube | | E | nd(s) not s | ealed Other: | | | | | | Fair | Poor | Disturbed |
| Condition | | _ | | | | | | | V | | | |
| Tube Scale (in) | Sample Use (Test Ty | | | (Draw | lines to indicate | e top and b | ation and Prootton of soil's ith: "Cut" "Da | surface a | and whe | re sam | | taken. |
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| Ave | e. Height (i | n.): | | | Ave. Diamo | 40.14.1 | | <u> </u> | ecimen \ | Wt. (gm | ns): | |
| | Та | Tare Number | | | Mass + Tare (g) | Dry Ma | sture Content ss+ Tare g) | Tare | Mass g) | | Water 0 | AND THE RESERVE OF THE PARTY OF |
| | L | | | | | | | | | | | |
| | W | et Ur | nit Weight: | _ | | pcf | Dry Unit We | ight | | | pcf | |
| Tes | sted By: Date: | | | | Calculated By: Checked By: Date: Date: | | | | | | | |
| 102 | (12/08/0 | 9) | | To | thel og IMM V | /ereion vie | s 2 0-Scale | 6/15/20 | 17 | | | |



| Project | No.: <u>103</u> | 7264.01. | 10002 Project Nar | ne.: <u>Coffeen</u> LSN-379 | Date Opened: | 1/8/2021 By: IN | IM | | | | | |
|--------------------|-----------------------------|--------------|--|---|------------------|--------------------|-------|--|--|--|--|--|
| Boring I | No.: <u>G</u> 3 | 31412 | Sample I | No.: 5H-18 | Depth (ft): 3 | t to 36 | | | | | | |
| Туре | X Std. " | 'Shelby" | Other: | | | | | | | | | |
| Tube D | Dimensions | s: Outside | Diameter (in): 3 | _ | Recovery (in) | 220 | | | | | | |
| Tube Condition: | Dented | End(s) not s | ealed Other: | Sample 0 | Condition Good F | air Poor Disturbed | | | | | | |
| Remarks: | Bo 461 | n tube | sent, then woo | Idn't extrude | ; Tobe Cut | 2 10" from | botto | | | | | |
| Tube Scale | Sample Use Fest Type) | | Soil Identification and Processing Remarks (Draw lines to indicate top and botton of soil's surface and where sample was taken. Identify cut lines with: "Cut" "Date: m/d/y" "Your Initials") | | | | | | | | | |
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| 14.0 | | ×2" | Clayey Sane | Slam | | | | | | | | |
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| 24.0 | | | | | | | | | | | | |
| Ave. H | leight (in.) | | Ave. Diam | eter (in.): | Specimen Wt | (gms): | | | | | | |
| | Tare | Number | Wet Mass + Tare | latural Moisture Conten Dry Mass+ Tare | t Tare Mass | Water Content | | | | | | |
| | | | (g) | (g) | (g) | (%) | | | | | | |
| | Wet | Unit Weight: | | pcf Dry Unit W | eight | pcf | | | | | | |
| The state of | | | 200 | | | | | | | | | |
| | I By: Pate: | | Calcula | Date: | | By: | | | | | | |
| 102 (1 | 2/08/09) | | Tubel og JMM | Version.xls. 2.0-Scale | 6/15/2017 | | | | | | | |



21.05/0

Co feen Fly Ash

Hanson Professional Services Inc.

Subcontract Agreement: RGE2014 Task Order No. 20E0111A/2000A

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| Sample ID | Rimac Comp Strength | Visual-Manual Classification | Unified Classification | Moisture Content | Liquid / Plastic Limits | Particle Size < #200 | Particle Size - Sieves | Particle Size - Sieves + Hyd | Standard Compaction | Modified Compaction | Bulk Density | Unconfined Comp Strength | Consolidation Test | Specific Gravity | UU Triaxial Comp Strength | CU Traxail Comp Strength | CD Direct Shear Strength | Swell Test for Soil | Collapse Test for Soil | Permeability Granular Soil | Hyd Conduct Cohesive Soil | Shrinkafe Factor | Soil Resistivity | IBR and IBV of Soils | CBR Test | Elastic Moduli - Rock | Uniaxial Comp Str - Rock | Corrosivity | Hd | Chloride | Sulfate | Total Organic Content | Moisture, Ash & Organ Matter |
| 3307D | | | | 10 | | | | | V. | | | | 7 | 1 | | | | | | | | | | | | | | | | | | | |
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Note 1: All testing to be in accordance with Laboratory Testing Specifications.

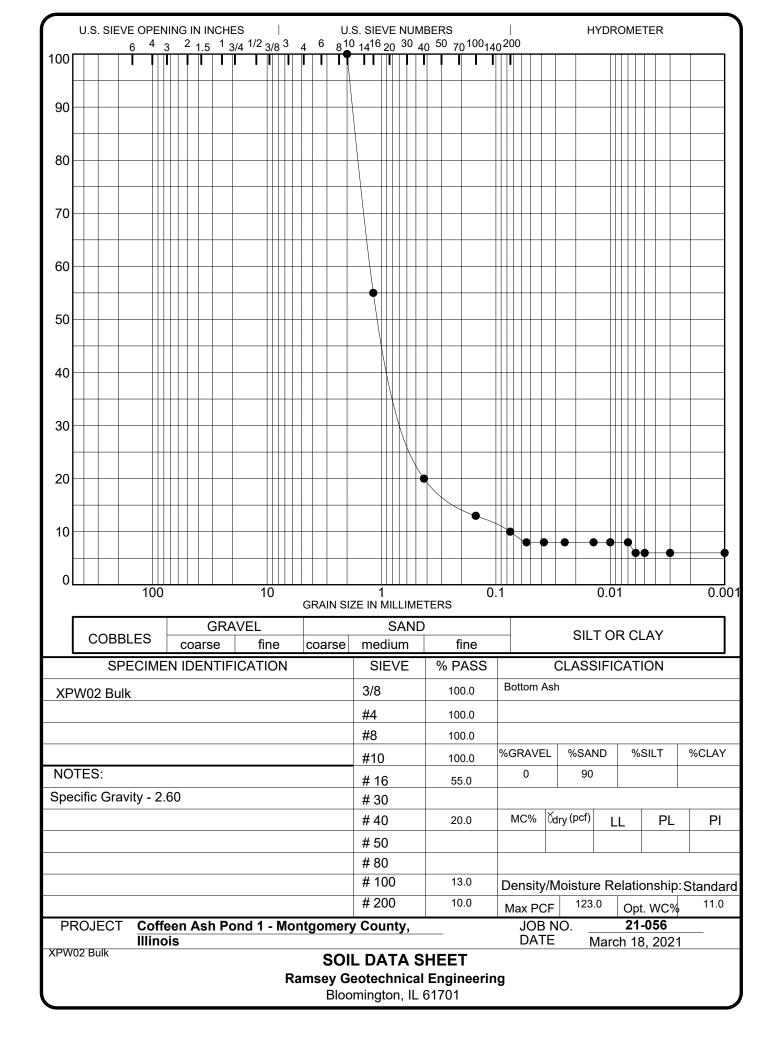
See Task Order or Attachment for any special instructions regarding scheduled testing.

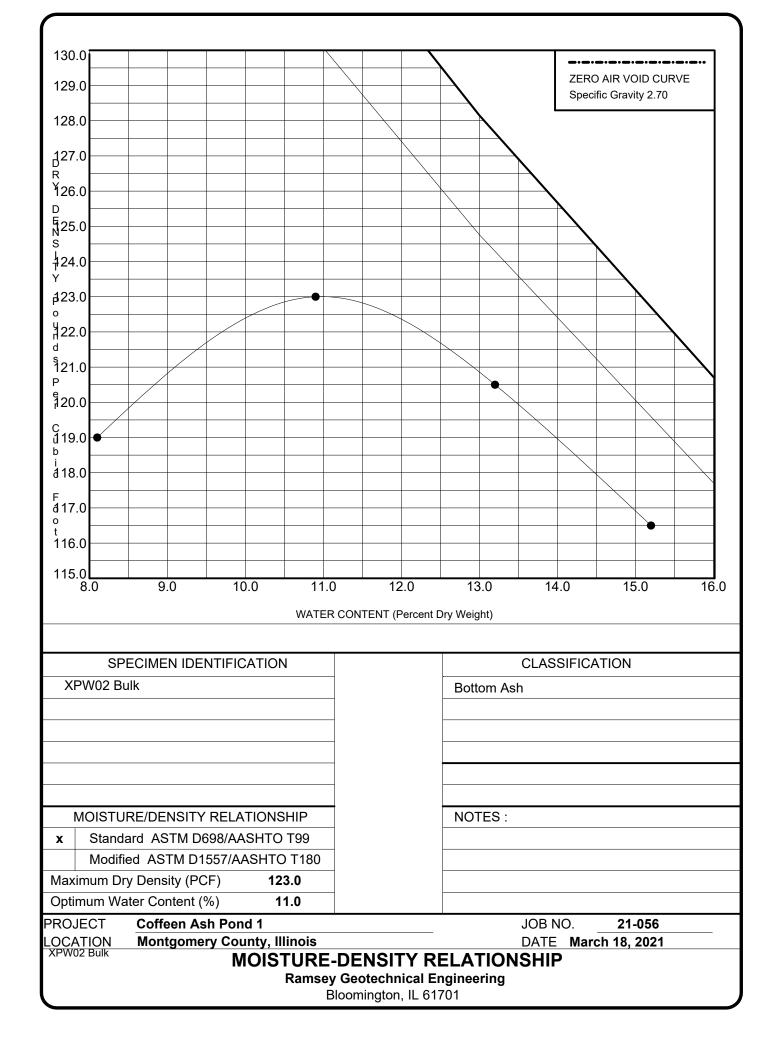
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| Sample ID | Rimac Comp Strength | Visual-Manual Classification | Unified Classification | Moisture Content | Liquid / Plastic Limits | Particle Size < #200 | Particle Size - Sieves | Particle Size - Sieves + Hyd | Standard Compaction | Modified Compaction | Bulk Density | Jnconfined Comp Strength | Consolidation Test | Specific Gravity | UU Triaxial Comp Strength | CU Traxail Comp Strength | CD Direct Shear Strength | Swell Test for Soil | Collapse Test for Soil | Permeability Granular Soil | Hyd Conduct Cohesive Soil | Shrinkafe Factor | Soil Resistivity | BR and IBV of Soils | CBR Test | Elastic Moduli - Rock | Uniaxial Comp Str - Rock | Corrosivity | | Chloride | Sulfate | Total Organic Content | Moisture, Ash & Organ Matter |
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| Sample ID | Rimac Comp Strength | Visual-Manual Classification | Unified Classification | Moisture Content | Liquid / Plastic Limits | Particle Size < #200 | Particle Size - Sieves | Particle Size - Sieves + Hyd | Standard Compaction | Modified Compaction | Bulk Density | Unconfined Comp Strength | Consolidation Test | Specific Gravity | UU Triaxial Comp Strength | CU Traxail Comp Strength | CD Direct Shear Strength | Swell Test for Soil | Collapse Test for Soil | Permeability Granular Soil | Hyd Conduct Cohesive Soil | Shrinkafe Factor | Soil Resistivity | IBR and IBV of Soils | CBR Test | Elastic Moduli - Rock | Uniaxial Comp Str - Rock | Corrosivity | Hd | Chloride | Sulfate | Total Organic Content | Moisture, Ash & Organ Matter |
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| Sample ID | Rimac Comp Strength | Visual-Manual Classification | Unified Classification | Moisture Content | Liquid / Plastic Limits | Particle Size < #200 | Particle Size - Sieves | Particle Size - Sieves + Hyd | Standard Compaction | Modified Compaction | Bulk Density | Unconfined Comp Strength | Consolidation Test | Specific Gravity | UU Triaxial Comp Strength | CU Traxail Comp Strength | CD Direct Shear Strength | Swell Test for Soil | Collapse Test for Soil | Permeability Granular Soil | Hyd Conduct Cohesive Soil | Shrinkafe Factor | Soil Resistivity | IBR and IBV of Soils | CBR Test | Elastic Moduli - Rock | Uniaxial Comp Str - Rock | Corrosivity | Hd | Chloride | Sulfate | Total Organic Content | Moisture, Ash & Organ Matter |
| 3314D | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| 16A | | | | T | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 17A | | | | | | | | | | | | | M | | | | | | | | | | | | | | | | | | | | |
| 19A | | | | | | | | | | | | | | | | | | | | | | 1 | | | | | | | | | | | |
| 20A | | | | | | | | | | | | = 1 | | | | | | | | | | | | | | | | | | | | | |
| 21A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| ST18 | | | | | | | | | | | | | | | | | | | | | X | | | | | | | | | | | | |
| 22A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Comp4 | | | | х | X | | | X | | | X | | | X | | | | | | | | | | | | | | | | | | | |
| 23A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | H | | |
| 24A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Comp5 | | | | х | х | | | x | | | х | | | х | | | | | | | | | | | | | | | | | | | |
| 25A | | | | | | | | | | | | | | | | | | | | | | | | - | | | | | | | | | |
| 26A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 27A | | | | | | | | | | | | | | | | | | | | | - | | | | | | | | | | | | |
| 28A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 29A | | | | | | 1 | 77 | | | | | | | | | | | П | | | | | | | | | | | | | | | |
| Comp6 | | | | x | X | | | X | | | X | | | x | | | | | | | | | | | | | | | | | | | |
| 35A | | | | | | | | | | | | | | | | | | | | | | | | - | | | | | | | | | |
| 36A | | | | | | | | | | | T | | | | | | | | | | | | | | | | | | | | | | |
| 37A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 38A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Comp7 | | | | x | x | | | X | | | x | | | x | | | | | | | | | | | | | | | | | | | |
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| Sample | Rimac Comp Strength | cation | Unified Classification | Moisture Content | Liquid / Plastic Limits | | Particle Size - Sieves | Particle Size - Sieves + Hyd | Standard Compaction | Modified Compaction | Bulk Density | Strength | est | | Ta. | CU Traxail Comp Strength | trength | Swell Test for Soil | Collapse Test for Soil | Permeability Granular Soil | Hyd Conduct Cohesive Soil | Shrinkafe Factor | Soil Resistivity | BR and IBV of Soils | CBR Test | Elastic Moduli - Rock | Uniaxial Comp Str - Rock | rosivity | | Chloride | Sulfate | Total Organic Content | Moisture, Ash & Organ Matter |
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| 44A | - | | | - | | - | - | | - | | | | | | Ε | | | | | | - | _ | | | | | _ | | | | | | - |
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| 47A | - | - | - | - | | | | | | | | | | | - | - | - | - | | | - | | - | _ | | | _ | | | | - | | - |
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| XPW01 | | | | | | | | | | + | | | | | | | | | | | | | | | - | | | | | | | - | |
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| 7A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| 3A | | M | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| 6A | 17 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| 8A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 9A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Comp2 | | | | X | X | | | X | | | X | | | X | | | | | | | | | | | | | | | | | | | |
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Hanson Professional Services Inc.

Subcontract Agreement: RGE2014 Task Order No. 20E0111A/2000A

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| | QC: KLT | QC: KLT | 1 | | | <u> </u> | ILL | | | | L/ \I | | | | /11 | | | 711 | 110 | _ | | | | | | | | | | | | | | | |
| | 7/21/21 | 7/21/21 | Ro | outii | ne T | es | ting | 1 | | | | | Сс | mp | lex | Τε | esti | ng | 1 | | | | | | | | | | Ar | aly | tica | al T | esti | ng | ı |
| Sample | Top Depth (Info taken from boring logs by | Bottom Depth (Info taken from boring logs by | Rimac Comp Strength | Visual-Manual Classification | Unified Classification | Moisture Content | Liquid / Plastic Limits | Particle Size < #200 | Particle Size - Sieves + Hvd | Standard Compaction | Modified Compaction | Bulk Density | Unconfined Comp Strength | Consolidation Test | Specific Gravity | _ | _ | | | Collapse Test for Soil | Permeability Granular Soil | Hyd Conduct Cohesive Soil | Shrinkafe Factor | Soil Resistivity | IBR and IBV of Soils | CBR Test | Elastic Moduli - Rock | Uniaxial Comp Str - Rock | Corrosivity | | Chloride | Sulfate | Total Organic Content | Moisture, Ash & Organ Matter | |
| ID | Ramboll) | Ramboll) | Ξ | Š | ٦, | Ĭ. | <u> </u> | 2 5 | 2 G | Š | Ĭ | B | J | ŏ | Sp | n | ರ | J | Š | Ö | Pe | Η | S | Sc | lВ | S | ΕĬ | ۲ | Ö | Hd | Ċ | S | 은 | Ĭ | |
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| 3A | 4 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | - |
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| Comp1 | <u>4</u> 8 | | | | | Х | Х | | Х | | | Х | | | Х | | | | | | | | | | | | | | | | | | | | ╁ |
| ST5 | 8 | 10 | | | | | | | | | | | | | | | | | | | | Х | | | | | | | | | | | | | \vdash |
| 7B | 12.8 | 14 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | \vdash |
| Comp2 | 12.8 | 14 | | | | х | х | | х | | | х | | | х | | | | | | | | | | | | | | | | | | | | T |
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| 10A | 18 | 20 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 11A | 20 | 22 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 12A | 22 | 24 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 13A | 24 | 26 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 14A | 26 | 28 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 15A | 28 | 30 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 16A | 30 | 32 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 17A | 32 | 34 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 18A | 34 | 34.9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Comp3 | 18 | 34.9 | | | | х | Х | | х | | | Х | | | х | | | | | | | | | | | | | | | | | | | | |
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| 21A | 40 | 42 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 22A | 42 | 44 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 23A | 44 | 46 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 24A | 46 | 48 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 25A | 48 | 50 | | | | | | | | | 1 | | | | | | | | | | | | | | | | | | | | | | | | L |
| 26A | 50 | 52 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 27A | 52 | 54 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Comp4 | 40 | 54 | | | | Х | Х | | х | | | Х | | | Х | | | | | | | | | | | | | | | | | | | | |
| ST22 | 42 | 44 | | | | | | | | | | | | | | | | | | | | х | | | | | | | | | | | | | |

Note 1: All testing to be in accordance with Laboratory Testing Specifications.

See Task Order or Attachment for any special instructions regarding scheduled testing.

| | | | | | SC | HE | Dι | JLE | 0 | FL | AE | 30 | RA | TC | R' | ΥT | ES | 1ITE | NG | | | | | | | | | | | | | | | | _ |
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| | QC: KLT 7/21/21 | QC: KLT 7/21/21 | Ro | utine | Те | stin | g | | | | | | Co | omp | olex | Te | esti | ng | | | | | | | | | | | Ar | nal | ytic | al 1 | Гest | ing | |
| Sample ID | Top Depth (Info taken from boring logs by Ramboll) | Bottom Depth (Info taken from boring logs by Ramboll) | Rimac Comp Strength | Visual-Manual Classification | Moisture Content | Liquid / Plastic Limits | Particle Size < #200 | Particle Size - Sieves | Particle Size - Sieves + Hyd | Standard Compaction | Modified Compaction | Bulk Density | Unconfined Comp Strength | Consolidation Test | Specific Gravity | UU Triaxial Comp Strength | CU Traxail Comp Strength | CD Direct Shear Strength | Swell Test for Soil | Collapse Test for Soil | Permeability Granular Soil | Hyd Conduct Cohesive Soil | Shrinkafe Factor | Soil Resistivity | IBR and IBV of Soils | CBR Test | Elastic Moduli - Rock | Uniaxial Comp Str - Rock | Corrosivity | , Ha | Chloride | Sulfate | Total Organic Content | Moisture, Ash & Organ Matter | |
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| 28A | 54 | 56 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 29A | 56 | 58 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 30A | 58 | 60 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Comp5 | 54 | 60 | | | Х | Х | | | Х | | | Х | | | Х | | | | | | | | | | | | | | 1 | | | | \downarrow | | |
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| 4A | 6 | 8 | | | + | | | | | | | | | | | | | | | | | | | | | | | \vdash | | | | | + | | |
| 5A | 8 | 10 | | | \dagger | | | | | | | | | | | | | | | | | | | | | | | \vdash | | | + | + | + | | |
| 6A | 10 | 12 | | | \dagger | | | | | | | | | | | | | | | | | | | | | | | \vdash | | | + | + | + | | |
| 11A | 20 | 22 | | | \dagger | | | | | | | | | | | | | | | | | | | | | | | \vdash | | | + | + | + | | |
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| 7A | 12 | 14 | | | | | | | | | | | | | | | | | | | | | | | | | | | | l | | | | | |
| Comp2 | 12 | 14 | | | х | Х | | | х | | | Х | | | х | | | | | | | | | | | | | | | | | | \bot | | |
| 10A | 18 | 20 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | + | | |
| 11A | 20 | 22 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 1 | | |
| 12A | 22 | 24 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 1 | | |
| 13A | 24 | 26 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 1 | | |
| 14A | 26 | 28 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 1 | | |
| 15A | 28 | 30 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | T | T | 1 | | |
| 16A | 30 | 32 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | T | T | 1 | | |
| 17A | 32 | 34 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 18A | 34 | 36 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | T | T | 1 | | |
| 19A | 36 | 38 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 20A | 38 | 40 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 21A | 40 | 42 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Comp3 | 18 | 42 | | | х | х | | | х | | | Х | | | х | | | | | | | | | | | | | | | | | | | | |
| ST14 | 28 | 30 | | | | | | | | | | | | | | | | | | | | Χ | | | | | | | | | | | | | |
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| | QC: KLT 7/21/21 | QC: KLT 7/21/21 | Ro | outii | ne T | es | ting | 1 | | | | | | Co | omp | olex | ι Τε | esti | ng | | | | | | | | | | | Ar | naly | /tica | al T | esti | ng |
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| G311D | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 23A | 44 | 46 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 24A | 46 | 48 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 25A | 48 | 50 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 26A | 50 | 52 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Comp4 | 44 | 52 | | | | х | Х | | | X | | | х | | | Х | | | | | | | | | | | | | | | | | | | |
| 074 | E0 | E 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 27A 28A | 52 54 | 54 56 | | | | \dashv | | | | | | | | - | | - | | - | - | | | | - | - | | - | | - | | - | | | | | |
| 28A 29A | 54 56 | 58 | - | - | | | | | | | | | | - | - | - | - | | | | | | - | - | - | | - | | | - | - | - | | | - |
| 30A | 58 | 60 | | | | \dashv | | | | | | | | | | | | - | - | | | | | | | | | - | | - | | | | | |
| Comp5 | 52 | 60 | | | | Х | х | | | Х | | | Х | | H | х | H | - | | | | | | | | | H | | | - | H | | | | |
| Compo | 32 | 00 | | | | ^ | ^ | | | ^ | | | ^ | | | ^ | | | | | | | | | | | | | | ļ | | | | | |
| G314D | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3A | 4.2 | 6.2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4A | 6.4 | 8.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 5A | 8.7 | 11.6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6A | 11.8 | 12.8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 7A | 13 | 15 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 8A | 15.5 | 17 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Comp1 | 4.2 | 17 | | | | х | Х | | | Х | | | Х | | | х | | | | | | | | | | | | | | | | | | | |
| 9A | 17.3 | 19.3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 10A | 19.6 | 21.6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Comp2 | 17.3 | 21.6 | | | | х | Х | | | Х | | | х | | | х | | | | | | | | | | | | | | | | | | | |
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| | | | | | | | | | | | | | | L | L | L | L | L | L | L | | | L | L | L | L | L | L | L | | | L | | | |
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| | | | | | SC | HE | Dι | JLE | 0 | FL | AE | 30 | RA | TC |)R` | ΥT | ES | STI | NG | i | | | | | | | | | | | | | | | |
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| | QC: KLT 7/21/21 | QC: KLT 7/21/21 | D. | utino | То | otin | ~ | | | | | | Co | mr | alox | , т. | o e ti | na | | | | | | | | | | | ۸۰ | , a ls | ıti or | J.T | ooti | ina | |
| | 1/21/21 | 1/21/21 | | utine | re | Sun | g I | | | | | | | | olex | 16 | รรแ | ng | | | | | | | | | | | ΑΠ | laly | llCa | al T | esu | | _ |
| Sample ID | Top Depth (Info taken from boring logs by Ramboll) | Bottom Depth (Info taken from boring logs by Ramboll) | Rimac Comp Strength | Visual-Manual Classification Unified Classification | Moisture Content | Liquid / Plastic Limits | Particle Size < #200 | Particle Size - Sieves | Particle Size - Sieves + Hyd | Standard Compaction | Modified Compaction | Bulk Density | Unconfined Comp Strength | Consolidation Test | Specific Gravity | UU Triaxial Comp Strength | CU Traxail Comp Strength | CD Direct Shear Strength | Swell Test for Soil | Collapse Test for Soil | Permeability Granular Soil | Hyd Conduct Cohesive Soil | Shrinkafe Factor | Soil Resistivity | IBR and IBV of Soils | CBR Test | Elastic Moduli - Rock | Uniaxial Comp Str - Rock | Corrosivity | Hd | Chloride | Sulfate | Total Organic Content | Moisture, Ash & Organ Matte | |
| G314D | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 11A | 21.8 | 23.8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 12A | 23.9 | 25.9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 13A | 26.1 | 28.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 14A | 28.3 | 30.3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 15A | 30.4 | 32.4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 16A | 32.6 | 34.6 | | | T | | | | | | | | | | | | | | | | | | | | | | | | | | | | П | | |
| 17A | 34.8 | 36.8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 19A | 39.1 | 41.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 20A | 41.3 | 43.3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 21A | 43.5 | 45.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Comp3 | 21.8 | 45.5 | | | х | х | | | Х | | | х | | | х | | | | | | | | | | | | | | | | | | | | |
| ST18 | 37 | 39 | | | | | | | | | | | | | | | | | | | | Х | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 22A | 46 | 47 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Comp4 | 46 | 47 | | | х | х | | | х | | | х | | | х | | | | | | | | | | | | | | | | | | | | |
| , | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 23A | 47.8 | 49.8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 24A | 50 | 52 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Comp5 | 47.8 | 52 | | | Х | х | | | Х | | | Х | | | х | | | | | | | | | | | | | | | | | | | | |
| , | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 25A | 52.2 | 54.2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 26A | 54.4 | 56.4 | H | | | | | | | | | | | | | | | | | | | | | | | | | | | | | - | | | |
| 27A | 56.5 | 58.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | T | | | |
| 28A | 58.7 | 60.7 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 29A | 60.9 | 62.9 | H | | | | | | | | | | | | | | | | | | | | | | | | | | | | | - | | | |
| Comp6 | 52.2 | 62.9 | | | Х | х | | | Х | | | х | | | х | | | | | | | | | | | | | | | | | | Н | | |
| | | | H | | † · · | † · · | | | | | | | | | <u> </u> | | | | | | | | | | | | | | | | | - | | | |
| 35A | 73.9 | 75.9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | - | - | | | |
| 36A | 76.1 | 78.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | <u> </u> | Н | | |
| 37A | 78.3 | 80.3 | | | | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | H | | |
| 38A | 80.5 | 82.5 | | + | - | \vdash | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Comp7 | 73.9 | 82.5 | | + | х | х | | | Х | | | х | | | Х | | | | | | | | | | | | | | | | | | | | |
| Joinpi | , 5.5 | 02.5 | | | ^ | ^ | | | ^ | | | ^ | | | ^ | | | | | | | | | | | | | | | | | | | | |
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|--------------|--|---|---------------------|--|------------------|-------------------------|----------------------|------------------------|------------------------------|---------------------|---------------------|--------------|--------------------------|--------------------|------------------|---------------------------|--------------------------|--------------------------|---------------------|------------------------|----------------------------|---------------------------|------------------|------------------|----------------------|----------|-----------------------|--------------------------|-------------|-----|----------|---------|-----------------------|------------------------------|---|
| | QC: KLT | QC: KLT | | | | | | | | | | | | | _ | | | | | | | | | | | | | | | | | | | | |
| | 7/21/21 | 7/21/21 | \vdash | utine | Tes | stin | g | | | | - | | Со | mp | lex | Τe | estii | ng | | | | | | | | | | | An | aly | tica | al T | esti | | |
| Sample ID | Top Depth (Info taken from boring logs by Ramboll) | Bottom Depth (Info taken from boring logs by Ramboll) | Rimac Comp Strength | Visual-Manual Classification Unified Classification | Moisture Content | Liquid / Plastic Limits | Particle Size < #200 | Particle Size - Sieves | Particle Size - Sieves + Hyd | Standard Compaction | Modified Compaction | Bulk Density | Unconfined Comp Strength | Consolidation Test | Specific Gravity | UU Triaxial Comp Strength | CU Traxail Comp Strength | CD Direct Shear Strength | Swell Test for Soil | Collapse Test for Soil | Permeability Granular Soil | Hyd Conduct Cohesive Soil | Shrinkafe Factor | Soil Resistivity | IBR and IBV of Soils | CBR Test | Elastic Moduli - Rock | Uniaxial Comp Str - Rock | Corrosivity | Hd | Chloride | Sulfate | Total Organic Content | Moisture, Ash & Organ Mattel | |
| G314D | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 44A | 93.5 | 93.9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 45A | 95.7 | 96.4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 46A | 97.9 | 98.8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 47A | 100 | 100.3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Comp8 | 93.5 | 100.3 | | | Х | Х | | | х | | | Х | | | Х | | | | | | | | | | | | | | | | | | | | |
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| XPW01 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1A | 0 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2A | 2 | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3A | 4 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4A | 6 | 8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Comp1 | 0 | 8 | | | х | х | | | Х | | | Χ | | | Х | | | | | | | | | | | | | | | | | | | | |
| ST3 | 4 | 6 | | | | | | | | | | | | | | | | | | | | Х | | | | | | | | | | | | | |
| 5A | 8 | 10 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6A | 10 | 12 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 7A | 12 | 12.8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Comp2 | 8 | 12.8 | | | х | Х | | | Х | | | Χ | | | Х | | | | | | | | | | | | | | | | | | | | |
| XPW02 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1A | 0 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2A | 2 | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3A | 4 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4A | 6 | 8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | Ĺ |
| Comp1 | 0 | 8 | | | Х | Х | | | Х | | | Х | | | Х | | | | | | | | | | | | | | | | | | | | |
| 5A | 8 | 10 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6A | 10 | 12 | | | İ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 7A | 12 | 14 | | | l | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 8A | 14 | 16 | | | İ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 9A | 16 | 17.7 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Comp2 | 8 | 17.7 | | | х | х | | | х | | | Х | | | Х | | | | | | | | | | | | | | | | | | | | |

APPENDIX E GROUNDWATER CONTOUR MAPS AND ELEVATIONS

GROUNDWATER CONTOUR MAPS

DRAWN BY/DATE: SDS 1/23/17 REVIEWED BY/DATE: TBN 1/25/17 APPROVED BY/DATE: JJW 2/7/17 COFFEEN ASH POND NO. 1 (UNIT ID: 101) AND COFFEEN ASH POND NO. 2 (UNIT ID: 102) UPPERMOST AQUIFER UNIT GROUNDWATER ELEVATION CONTOUR MAP ROUND 1: NOVEMBER 16, 2015

DYNEGY CCR RULE GROUNDWATER MONITORING COFFEEN POWER STATION COFFEEN, ILLINOIS PROJECT NO: 2285



DRAWN BY/DATE: SDS 1/23/17 REVIEWED BY/DATE: TBN 1/25/17 APPROVED BY/DATE: JJW 2/8/17 COFFEEN ASH POND NO. 1 (UNIT ID: 101) AND COFFEEN ASH POND NO. 2 (UNIT ID: 102) UPPERMOST AQUIFER UNIT GROUNDWATER ELEVATION CONTOUR MAP ROUND 2: FEBRUARY 8, 2016

DYNEGY CCR RULE GROUNDWATER MONITORING COFFEEN POWER STATION COFFEEN, ILLINOIS PROJECT NO: 2285



DRAWN BY/DATE: SDS 1/23/17 REVIEWED BY/DATE: TBN 1/25/17 APPROVED BY/DATE: JJW 2/8/17 COFFEEN ASH POND NO. 1 (UNIT ID: 101) AND COFFEEN ASH POND NO. 2 (UNIT ID: 102) UPPERMOST AQUIFER UNIT GROUNDWATER ELEVATION CONTOUR MAP ROUND 3: MAY 9, 2016

DYNEGY CCR RULE GROUNDWATER MONITORING COFFEEN POWER STATION COFFEEN, ILLINOIS PROJECT NO: 2285



DRAWN BY/DATE: SDS 1/23/17 REVIEWED BY/DATE: ANS 1/25/17 APPROVED BY/DATE: JJW 2/8/17 COFFEEN ASH POND NO. 1 (UNIT ID: 101) AND COFFEEN ASH POND NO. 2 (UNIT ID: 102) UPPERMOST AQUIFER UNIT GROUNDWATER ELEVATION CONTOUR MAP ROUND 4: JULY 25, 2016

DYNEGY CCR RULE GROUNDWATER MONITORING COFFEEN POWER STATION COFFEEN, ILLINOIS PROJECT NO: 2285

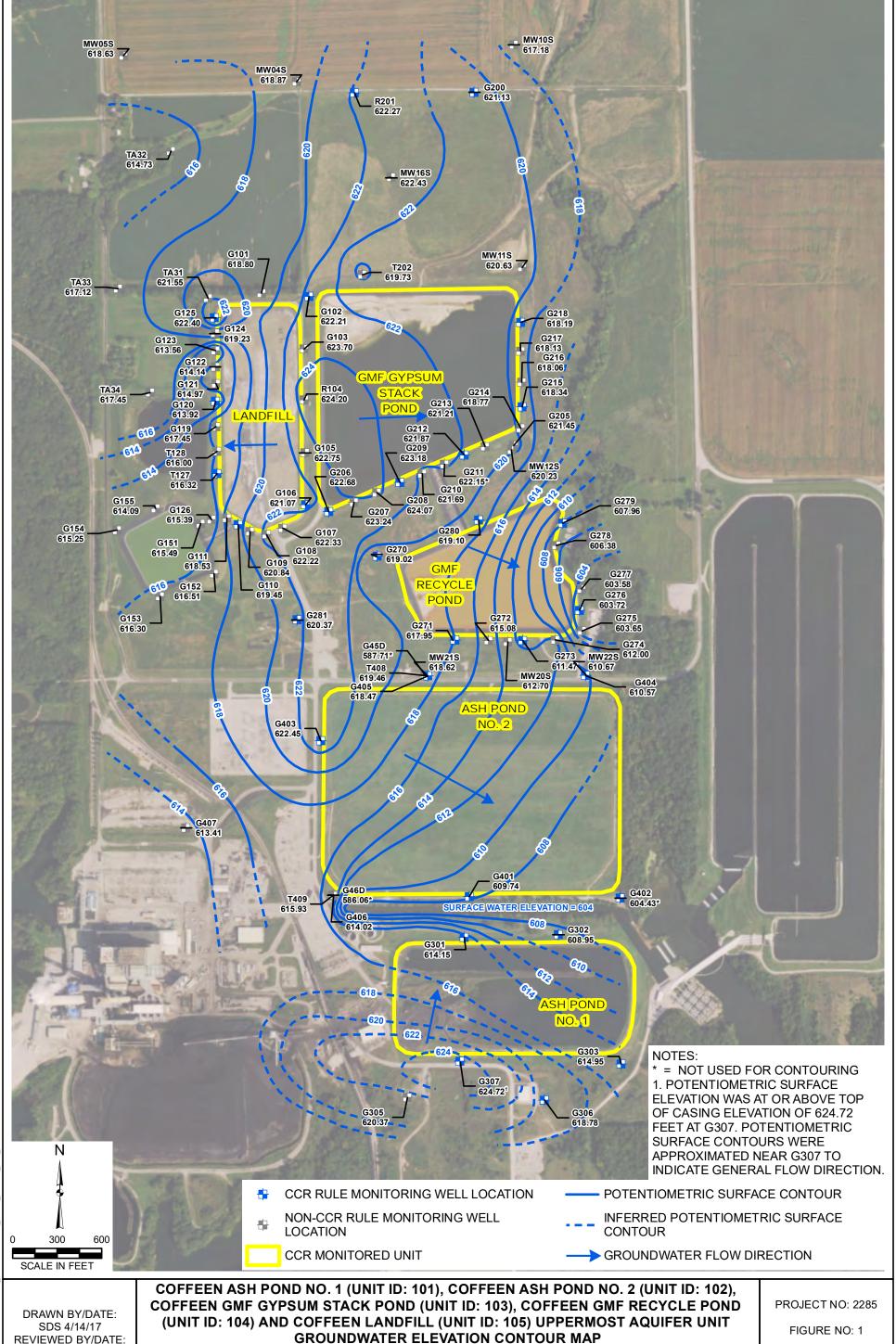


DRAWN BY/DATE: SDS 3/3/17 REVIEWED BY/DATE: TBN 3/3/17 APPROVED BY/DATE: JJW 8/30/17 COFFEEN ASH POND NO. 1 (UNIT ID: 101), COFFEEN ASH POND NO. 2 (UNIT ID: 102), COFFEEN GMF GYPSUM STACK POND (UNIT ID: 103), COFFEEN GMF RECYCLE POND (UNIT ID: 104) AND COFFEEN LANDFILL (UNIT ID: 105) UPPERMOST AQUIFER UNIT GROUNDWATER ELEVATION CONTOUR MAP

ROUND 5: NOVEMBER 12, 2016

DYNEGY CCR RULE GROUNDWATER MONITORING COFFEEN POWER STATION COFFEEN, ILLINOIS PROJECT NO: 2285 FIGURE NO: 1

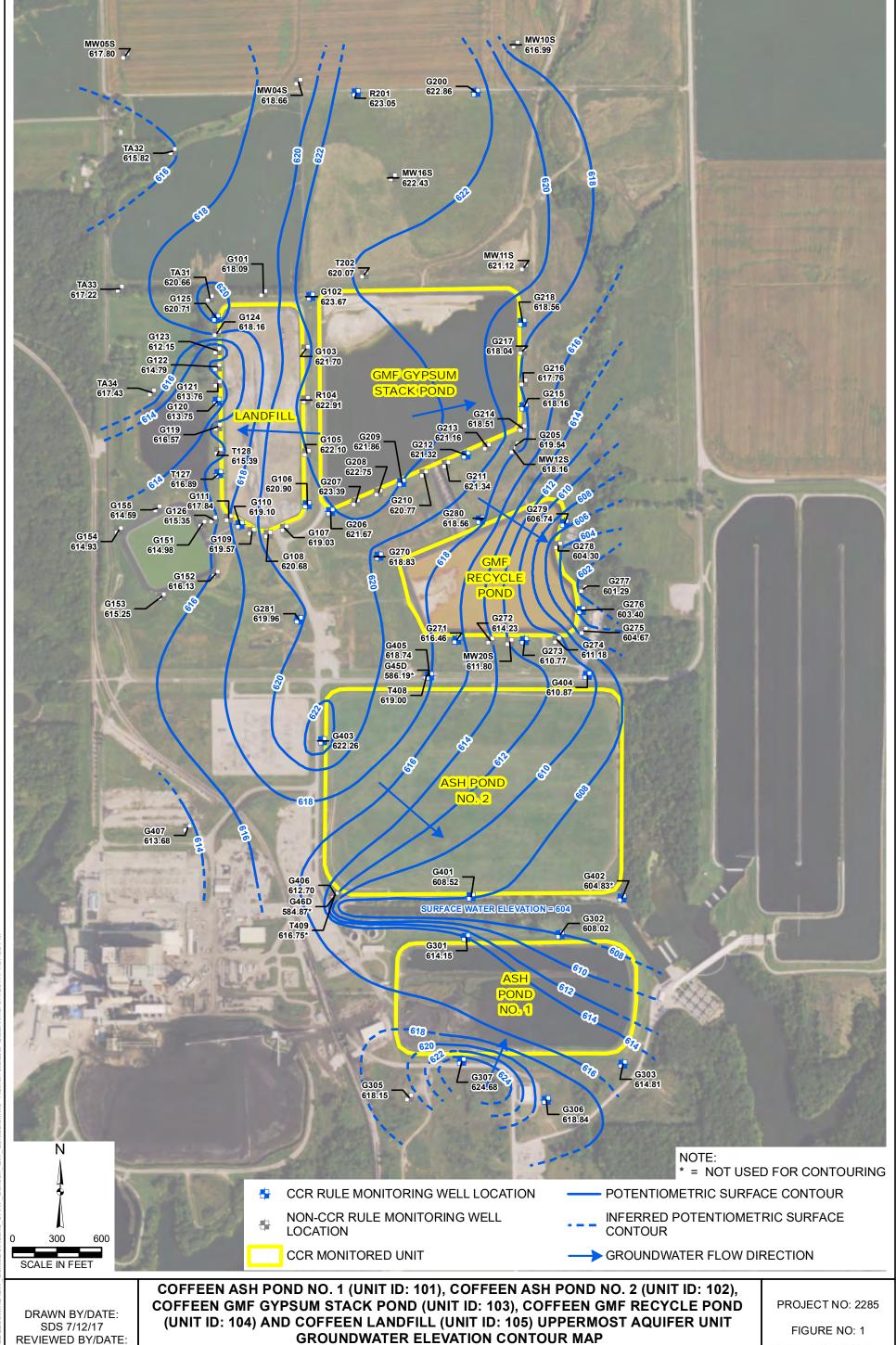




DRAWN BY/DATE: SDS 4/14/17 REVIEWED BY/DATE: TBN 4/14/17 APPROVED BY/DATE: JJW 8/30/17

ROUND 6: FEBRUARY 4, 2017

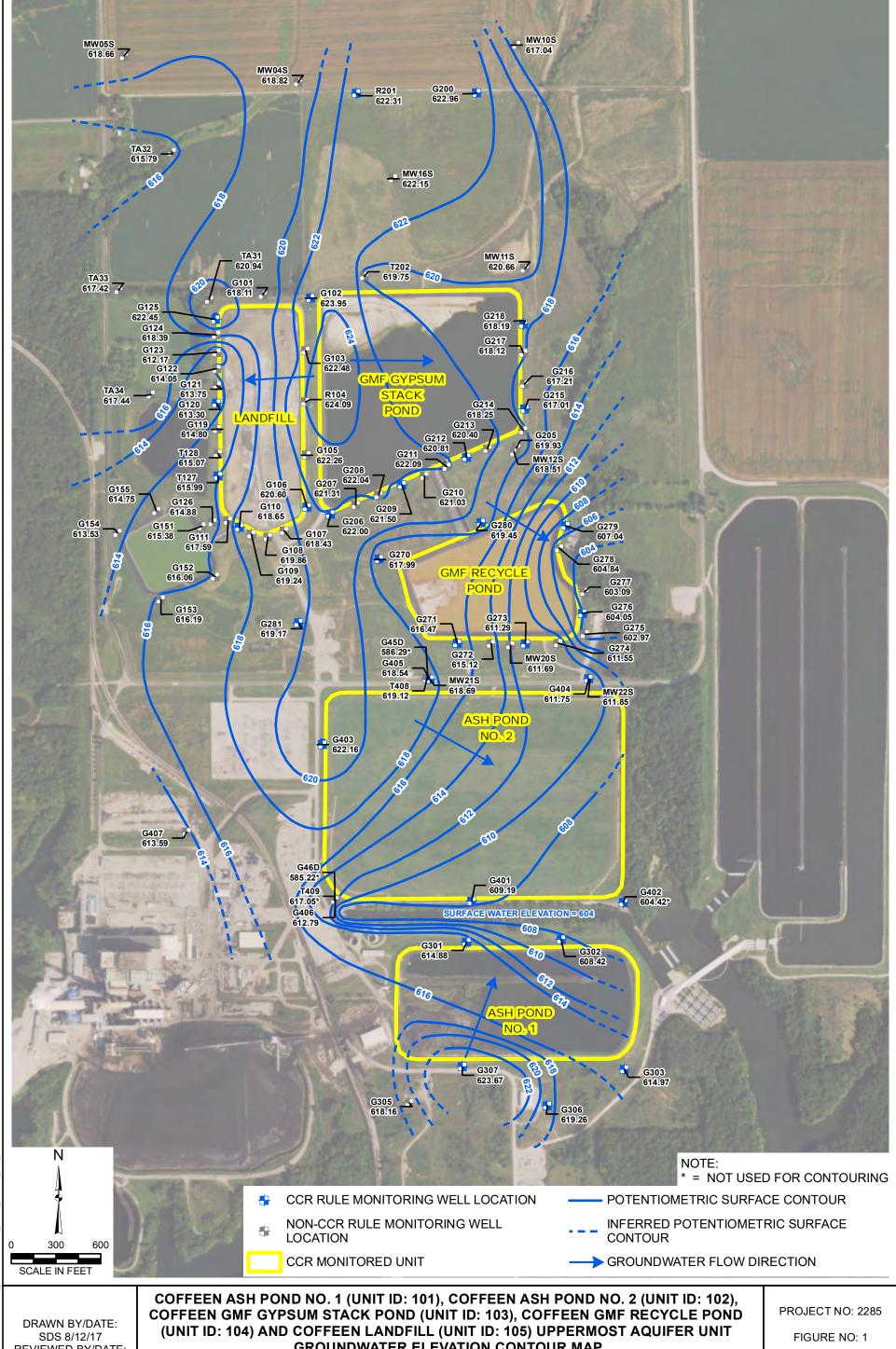




DRAWN BY/DATE: SDS 7/12/17 REVIEWED BY/DATE: TBN 7/12/17 APPROVED BY/DATE: JJW 8/30/17

ROUND 7: MAY 13, 2017



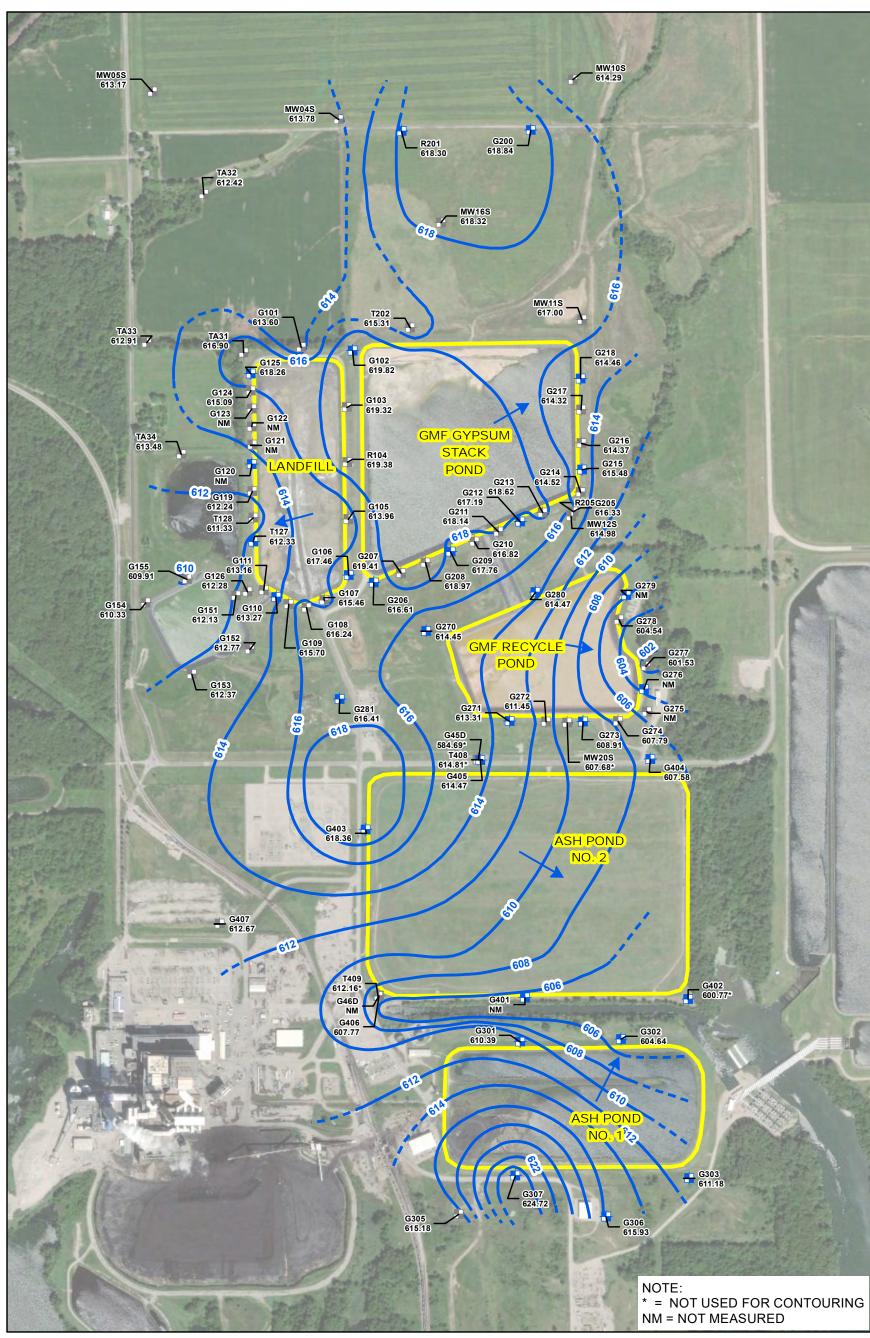


REVIEWED BY/DATE: TBN 8/10/17 APPROVED BY/DATE: JJW 8/30/17

GROUNDWATER ELEVATION CONTOUR MAP

ROUND 8: JULY 8, 2017





LEGEND

CCR RULE MONITORING WELL **LOCATION**

NON-CCR RULE MONITORING WELL **LOCATION GROUNDWATER ELEVATION**

CONTOUR (2-FT CONTOUR INTERVAL, NAVD88) INFERRED GROUNDWATER

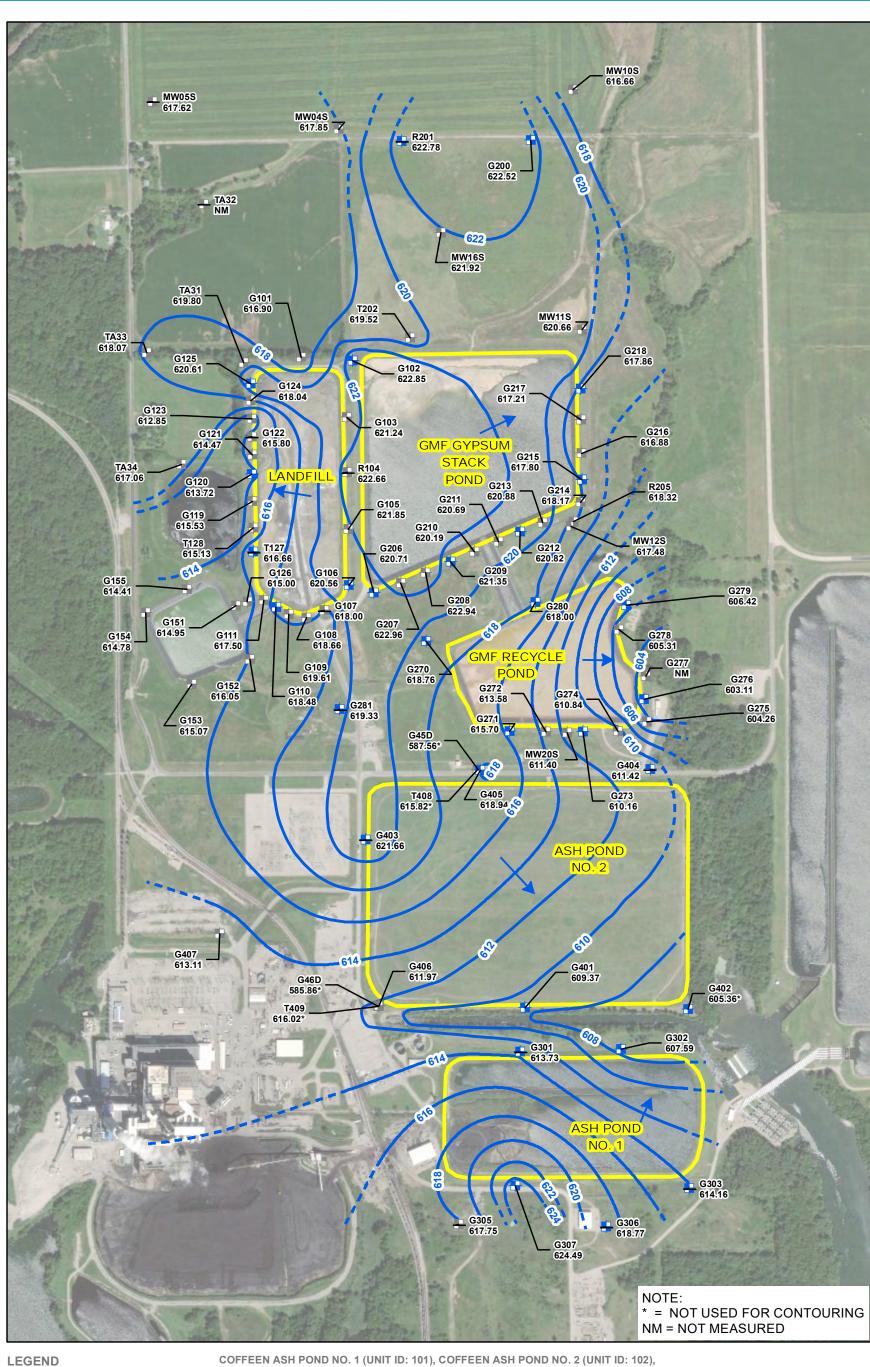
- - ELEVATION CONTOUR GROUNDWATER FLOW DIRECTION CCR MONITORED UNIT

COFFEEN ASH POND NO. 1 (UNIT ID: 101), COFFEEN ASH POND NO. 2 (UNIT ID: 102), COFFEEN GMF GYPSUM STACK POND (UNIT ID: 103), COFFEEN GMF RECYCLE POND (UNIT ID: 104) AND COFFEEN LANDFILL (UNIT ID: 105)
GROUNDWATER ELEVATION CONTOUR MAP

OCTOBER 21, 2017







- CCR RULE MONITORING WELL LOCATION
- NON-CCR RULE MONITORING WELL
- LOCATION
 GROUNDWATER ELEVATION
 CONTOUR (2-FT CONTOUR
- INTERVAL, NAVD88)

 INFERRED GROUNDWATER
 ELEVATION CONTOUR

CCR MONITORED UNIT

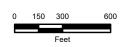
ELEVATION CONTOUR

GROUNDWATER FLOW DIRECTION

COFFEEN ASH POND NO. 1 (UNIT ID: 101), COFFEEN ASH POND NO. 2 (UNIT ID: 102), COFFEEN GMF GYPSUM STACK POND (UNIT ID: 103), COFFEEN GMF RECYCLE POND (UNIT ID: 104) AND COFFEEN LANDFILL (UNIT ID: 105)
GROUNDWATER ELEVATION CONTOUR MAP

GROUNDWATER ELEVATION CONTOUR MAP MAY 8, 2018

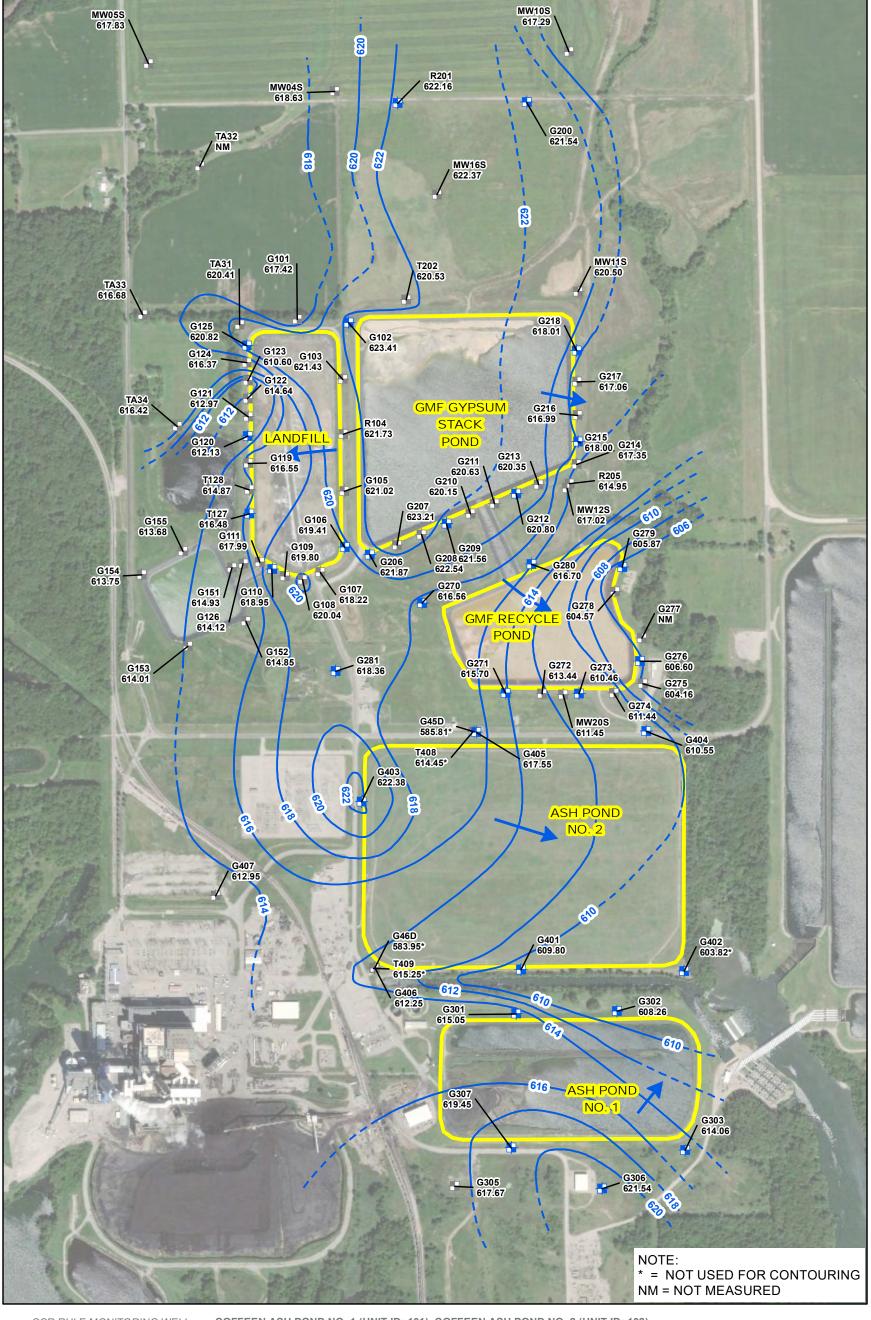
CCR RULE GROUNDWATER MONITORING COFFEEN POWER STATION COFFEEN, ILLINOIS

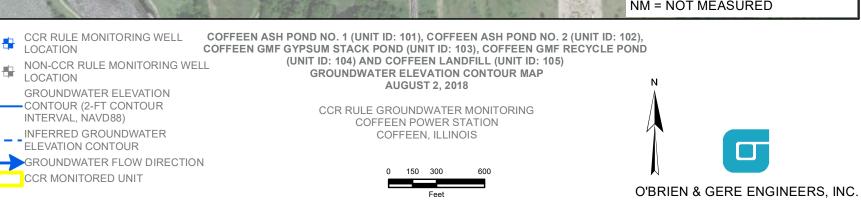


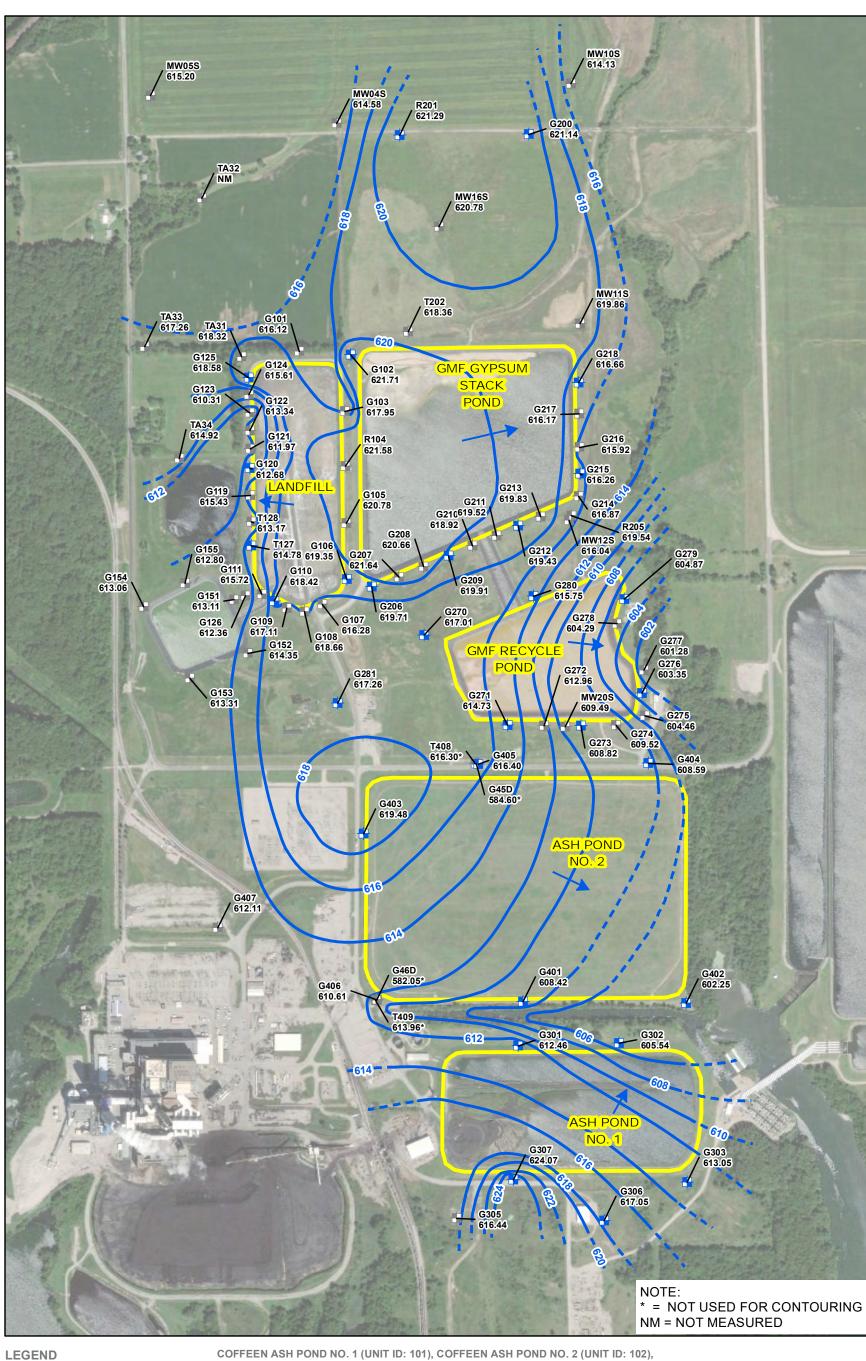


FILE_NO. 70099 DATE 8/1/2018

O'BRIEN & GERE ENGINEERS, INC.







- CCR RULE MONITORING WELL
 - LOCATION
- NON-CCR RULE MONITORING WELL LOCATION
 GROUNDWATER ELEVATION
- CONTOUR (2-FT CONTOUR INTERVAL, NAVD88)

 INFERRED GROUNDWATER ELEVATION CONTOUR

CCR MONITORED UNIT

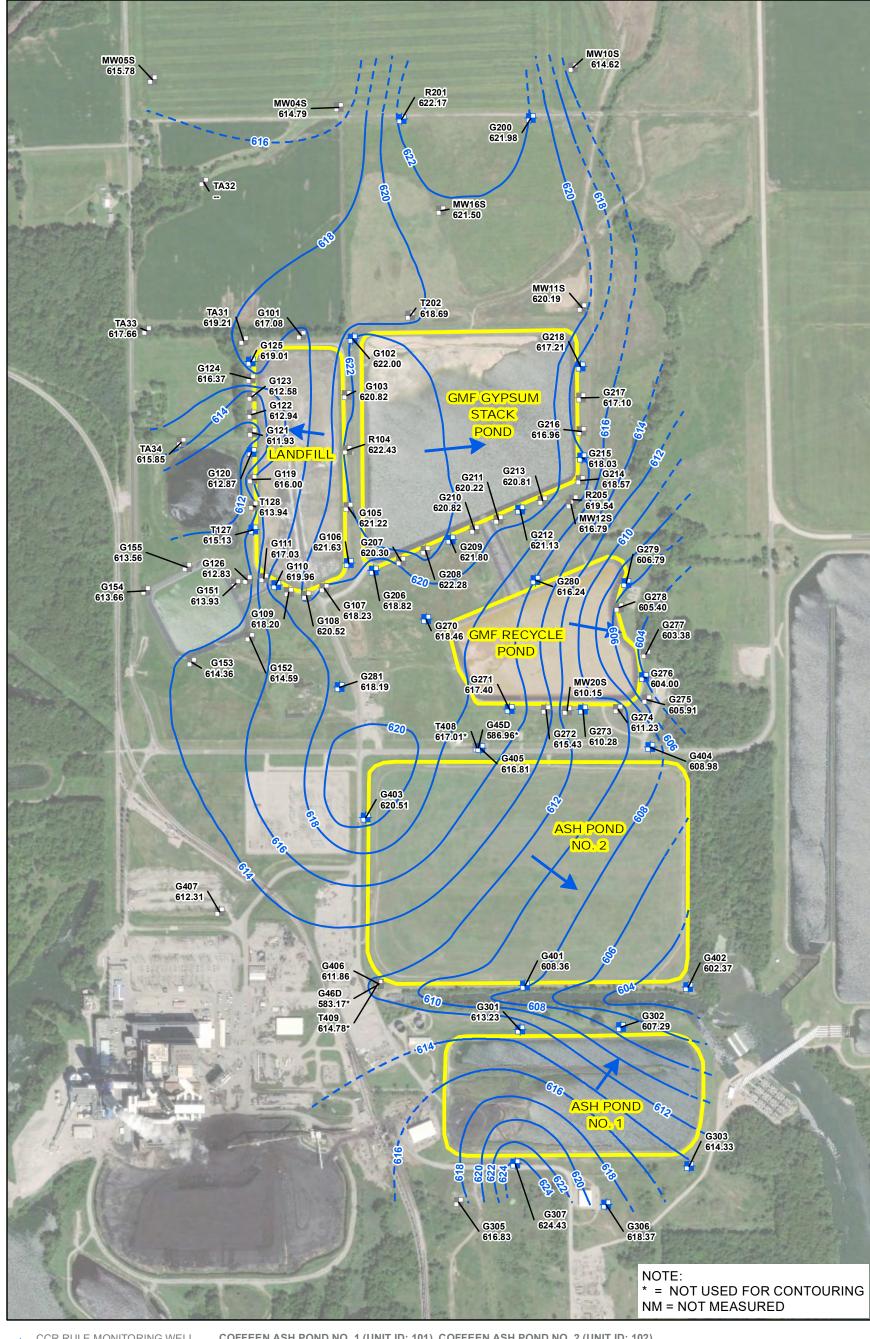
- ELEVATION CONTOUR

 GROUNDWATER FLOW DIRECTION
- COFFEEN ASH POND NO. 1 (UNIT ID: 101), COFFEEN ASH POND NO. 2 (UNIT ID: 102), COFFEEN GMF GYPSUM STACK POND (UNIT ID: 103), COFFEEN GMF RECYCLE POND (UNIT ID: 104) AND COFFEEN LANDFILL (UNIT ID: 105)
 GROUNDWATER ELEVATION CONTOUR MAP

OCTOBER 23, 2018









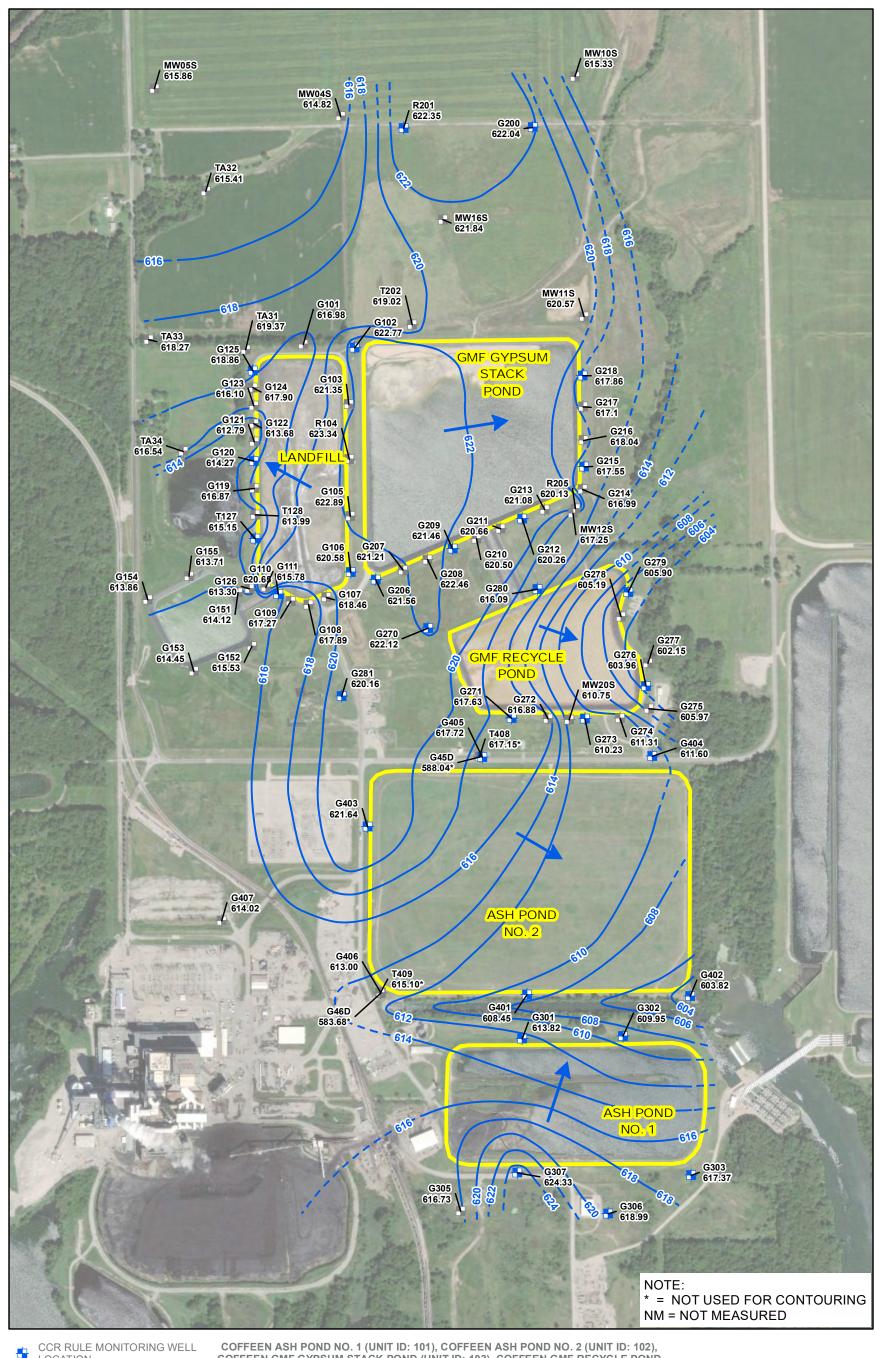
COFFEEN ASH POND NO. 1 (UNIT ID: 101), COFFEEN ASH POND NO. 2 (UNIT ID: 102), COFFEEN GMF GYPSUM STACK POND (UNIT ID: 103), COFFEEN GMF RECYCLE POND (UNIT ID: 104) AND COFFEEN LANDFILL (UNIT ID: 105)

GROUNDWATER ELEVATION CONTOUR MAP

JANUARY 15, 2019







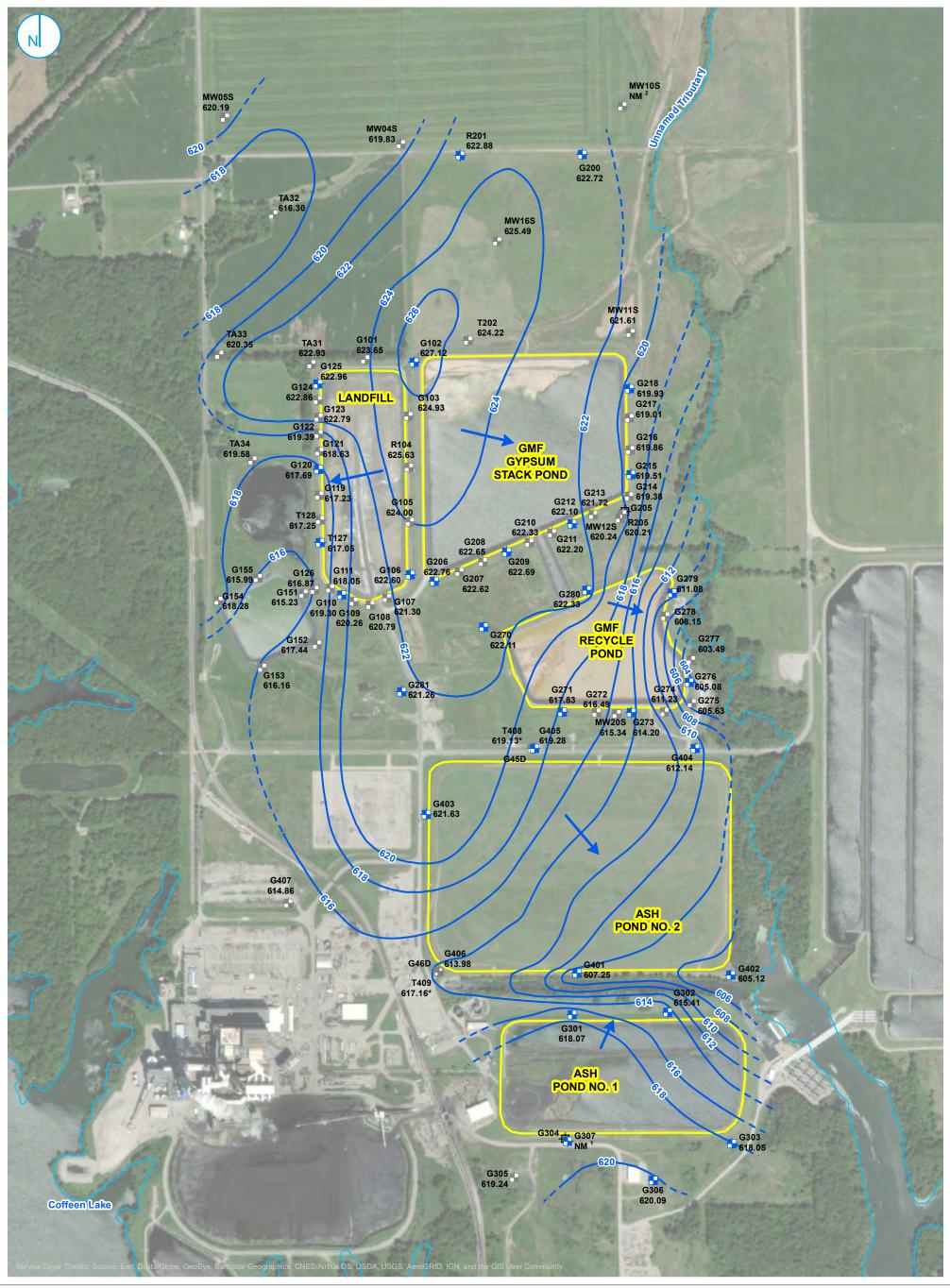


COFFEEN ASH POND NO. 1 (UNIT ID: 101), COFFEEN ASH POND NO. 2 (UNIT ID: 102), COFFEEN GMF GYPSUM STACK POND (UNIT ID: 103), COFFEEN GMF RECYCLE POND (UNIT ID: 104) AND COFFEEN LANDFILL (UNIT ID: 105)

GROUNDWATER ELEVATION CONTOUR MAP AUGUST 5, 2019







- CCR RULE MONITORING WELL LOCATION
- ♣ NON-CCR RULE MONITORING WELL LOCATION
- ABANDONED MONITORING WELL
- GROUNDWATER ELEVATION CONTOUR (2-FT CONTOUR INTERVAL, NAVD88)
- - INFERRED GROUNDWATER ELEVATION CONTOUR
- GROUNDWATER FLOW DIRECTION

CCR UNIT BOUNDARY

SURFACE WATER FEATURE

NOTE:
* = NOT USED FOR CONTOURING
NM = NOT MEASURED
1 G307 WAS FROZEN DURING THE
JANUARY 20, 2020 SAMPLING EVENT AND
WATER LEVEL COULD NOT BE
COLLECTED.
2 MANAGEM RAS DAMAGED DRIOR TO THE

² MW10S WAS DAMAGED PRIOR TO THE JANUARY 20, 2020 SAMPLING EVENT AND WATER LEVEL COULD NOT BE COLLECTED. GROUNDWATER ELEVATION CONTOUR MAP JANUARY 20, 2020

CCR RULE GROUNDWATER MONITORING

COFFEEN POWER STATION
COFFEEN, ILLINOIS

RAMBOLL US CORPORATION A RAMBOLL COMPANY



TABLE E-1. GROUNDWATER ELEVATIONS

| · | 1 | |
|-----------------|-------------|-----------------------------------|
| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
| G045D | 11/12/2016 | 584.91 |
| G045D | 02/04/2017 | 587.71 |
| G045D | 05/13/2017 | 586.19 |
| G045D | 07/08/2017 | 586.29 |
| G045D | 10/21/2017 | 584.69 |
| G045D | 05/08/2018 | 587.56 |
| G045D | 08/02/2018 | 585.81 |
| G045D | 10/23/2018 | 584.60 |
| G045D | 01/15/2019 | 586.96 |
| G045D | 08/05/2019 | 588.04 |
| G045D | 08/10/2020 | 614.21 |
| G045D | 01/20/2021 | 614.60 |
| G045D | 04/20/2021 | 614.32 |
| G045D | 07/26/2021 | 613.58 |
| G045D | 08/16/2021 | 613.83 |
| G046D | 11/12/2016 | 583.59 |
| G046D | 02/04/2017 | 586.06 |
| G046D | 05/13/2017 | 584.87 |
| G046D | 07/08/2017 | 585.22 |
| G046D | 05/08/2018 | 585.86 |
| G046D | 08/02/2018 | 583.95 |
| G046D | 10/23/2018 | 582.05 |
| G046D | 01/15/2019 | 583.17 |
| G046D | 08/05/2019 | 583.68 |
| G046D | 08/10/2020 | 609.00 |
| G046D | 01/20/2021 | 610.49 |
| G046D | 04/20/2021 | 611.06 |
| G046D | 07/26/2021 | 607.21 |
| G046D | 08/16/2021 | 608.17 |
| G101 | 01/20/2015 | 614.48 |
| G101 | 04/08/2015 | 618.87 |
| G101 | 07/23/2015 | 618.53 |
| G101 | 10/06/2015 | 617.15 |
| G101 | 11/16/2015 | 612.95 |
| G101 | 02/08/2016 | 618.46 |
| G101 | 05/09/2016 | 618.89 |
| G101 | 07/25/2016 | 618.44 |
| G101 | 11/12/2016 | 617.65 |
| G101 | 02/04/2017 | 618.80 |
| G101 | 05/13/2017 | 618.09 |
| G101 | 07/08/2017 | 618.11 |
| G101 | 10/21/2017 | 613.60 |
| G101 | 05/08/2018 | 616.90 |
| G101 | 08/02/2018 | 617.42 |
| G101 | 10/23/2018 | 616.12 |
| G101 | 01/15/2019 | 617.08 |
| L | 1 | |



| <u> </u> | | |
|-----------------|-------------|-----------------------------------|
| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
| G101 | 08/05/2019 | 616.98 |
| G101 | 01/20/2020 | 623.65 |
| G101 | 08/10/2020 | 616.70 |
| G101 | 10/15/2020 | 613.61 |
| G101 | 01/20/2021 | 617.20 |
| G101 | 01/28/2021 | 617.80 |
| G101 | 04/20/2021 | 622.85 |
| G101 | 07/26/2021 | 619.94 |
| G101 | 08/16/2021 | 619.95 |
| G102 | 01/20/2015 | 619.18 |
| G102 | 04/08/2015 | 622.06 |
| G102 | 10/06/2015 | 622.02 |
| G102 | 11/16/2015 | 618.96 |
| G102 | 02/08/2016 | 624.04 |
| G102 | 05/09/2016 | 625.34 |
| G102 | 07/25/2016 | 623.92 |
| G102 | 11/12/2016 | 623.39 |
| G102 | 02/04/2017 | 622.21 |
| G102 | 05/13/2017 | 623.67 |
| G102 | 07/08/2017 | 623.95 |
| G102 | 10/21/2017 | 619.82 |
| G102 | 01/26/2018 | 621.79 |
| G102 | 05/08/2018 | 622.85 |
| G102 | 08/02/2018 | 623.41 |
| G102 | 10/23/2018 | 621.71 |
| G102 | 01/15/2019 | 622.00 |
| G102 | 08/05/2019 | 622.77 |
| G102 | 01/20/2020 | 627.12 |
| G102 | 08/10/2020 | 621.72 |
| G102 | 10/15/2020 | 618.94 |
| G102 | 01/20/2021 | 619.79 |
| G102 | 01/26/2021 | 621.71 |
| G102 | 04/20/2021 | 623.86 |
| G102 | 05/03/2021 | 624.28 |
| G102 | 05/17/2021 | 623.83 |
| G102 | 06/09/2021 | 623.09 |
| G102 | 06/23/2021 | 621.22 |
| G102 | 07/12/2021 | 622.92 |
| G102 | 07/12/2021 | 622.97 |
| G102 | 08/16/2021 | 622.69 |
| G102 | 01/20/2015 | 620.82 |
| G103 | 04/08/2015 | 622.58 |
| G103 | 07/23/2015 | 621.70 |
| G103 | 10/06/2015 | 620.69 |
| G103 | 02/08/2016 | 621.68 |
| G103 | + | |
| G103 | 05/09/2016 | 623.26 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G103 | 07/25/2016 | 622.88 |
| G103 | 11/12/2016 | 621.21 |
| G103 | 02/04/2017 | 623.70 |
| G103 | 05/13/2017 | 621.70 |
| G103 | 07/08/2017 | 622.48 |
| G103 | 10/21/2017 | 619.32 |
| G103 | 05/08/2018 | 621.24 |
| G103 | 08/02/2018 | 621.43 |
| G103 | 10/23/2018 | 617.95 |
| G103 | 01/15/2019 | 620.82 |
| G103 | 08/05/2019 | 621.35 |
| G103 | 01/20/2020 | 624.93 |
| G103 | 08/10/2020 | 622.45 |
| G103 | 10/15/2020 | 618.91 |
| G103 | 01/20/2021 | 621.01 |
| G103 | 01/28/2021 | 621.38 |
| G103 | 04/20/2021 | 623.84 |
| G103 | 07/26/2021 | 624.14 |
| G103 | 08/16/2021 | 624.29 |
| G105 | 01/20/2015 | 621.95 |
| G105 | 04/08/2015 | 623.73 |
| G105 | 07/23/2015 | 622.72 |
| G105 | 10/06/2015 | 621.65 |
| G105 | 02/08/2016 | 623.03 |
| G105 | 05/09/2016 | 623.60 |
| G105 | 07/25/2016 | 622.08 |
| G105 | 11/12/2016 | 622.13 |
| G105 | 02/04/2017 | 622.75 |
| G105 | 05/13/2017 | 622.10 |
| G105 | 07/08/2017 | 622.26 |
| G105 | 10/21/2017 | 613.96 |
| G105 | 05/08/2018 | 621.85 |
| G105 | 08/02/2018 | 621.02 |
| G105 | 10/23/2018 | 620.78 |
| G105 | 01/15/2019 | 621.22 |
| G105 | 08/05/2019 | 622.89 |
| G105 | 01/20/2020 | 624.00 |
| G105 | 08/10/2020 | 623.11 |
| G105 | 10/15/2020 | 620.10 |
| G105 | 01/20/2021 | 622.21 |
| G105 | 01/28/2021 | 622.33 |
| G105 | 04/20/2021 | 623.23 |
| G105 | 07/26/2021 | 623.76 |
| G105 | 08/16/2021 | 623.70 |
| G106 | 01/20/2015 | 620.45 |
| G106 | 04/08/2015 | 622.19 |



| Γ | 1 | |
|-----------------|-------------|-----------------------------------|
| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
| G106 | 07/23/2015 | 621.43 |
| G106 | 10/06/2015 | 620.50 |
| G106 | 11/16/2015 | 619.32 |
| G106 | 02/08/2016 | 621.55 |
| G106 | 05/09/2016 | 622.11 |
| G106 | 07/25/2016 | 620.62 |
| G106 | 11/12/2016 | 620.65 |
| G106 | 02/04/2017 | 621.07 |
| G106 | 05/13/2017 | 620.90 |
| G106 | 07/08/2017 | 620.60 |
| G106 | 10/21/2017 | 617.46 |
| G106 | 05/08/2018 | 620.56 |
| G106 | 08/02/2018 | 619.41 |
| G106 | 10/23/2018 | 619.35 |
| G106 | 01/15/2019 | 621.63 |
| G106 | 08/05/2019 | 620.58 |
| G106 | 01/20/2020 | 622.60 |
| G106 | 08/10/2020 | 620.48 |
| G106 | 10/14/2020 | 618.19 |
| G106 | 01/20/2021 | 620.90 |
| G106 | 01/26/2021 | 620.90 |
| G106 | 04/20/2021 | 621.69 |
| G106 | 06/29/2021 | 621.95 |
| G106 | 07/26/2021 | 621.88 |
| G106 | 08/16/2021 | 621.90 |
| G107 | 01/20/2015 | 619.23 |
| G107 | 04/08/2015 | 620.85 |
| G107 | 07/23/2015 | 620.15 |
| G107 | 10/06/2015 | 619.10 |
| G107 | 02/08/2016 | 620.26 |
| G107 | 05/09/2016 | 620.78 |
| G107 | 07/25/2016 | 618.37 |
| G107 | 11/12/2016 | 618.72 |
| G107 | 02/04/2017 | 622.33 |
| G107 | 05/13/2017 | 619.03 |
| G107 | 07/08/2017 | 618.43 |
| G107 | 10/21/2017 | 615.46 |
| G107 | 05/08/2018 | 618.00 |
| G107 | 08/02/2018 | 618.22 |
| G107 | 10/23/2018 | 616.28 |
| G107 | 01/15/2019 | 618.23 |
| G107 | 08/05/2019 | 618.46 |
| G107 | 01/20/2020 | 621.30 |
| G107 | 08/10/2020 | 618.68 |
| G107 | 10/14/2020 | 616.56 |
| G107 | 01/20/2021 | 619.58 |
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| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|--------------------------|-----------------------------------|
| G107 | 01/28/2021 | 619.74 |
| G107 | 04/20/2021 | 620.19 |
| G107 | 07/26/2021 | 620.26 |
| G107 | 08/16/2021 | 620.39 |
| G108 | 01/19/2015 | 618.42 |
| G108 | 04/08/2015 | 620.31 |
| G108 | 07/24/2015 | 621.22 |
| G108 | 10/07/2015 | 618.92 |
| G108 | 02/08/2016 | 619.53 |
| G108 | 05/09/2016 | 620.15 |
| G108 | 07/25/2016 | 619.78 |
| G108 | 11/12/2016 | 620.46 |
| G108 | 02/04/2017 | 622.22 |
| G108 | 05/13/2017 | 620.68 |
| G108 | 07/08/2017 | 619.86 |
| G108 | 10/21/2017 | 616.24 |
| G108 | 05/08/2018 | 618.66 |
| G108 | 08/02/2018 | 620.04 |
| G108 | 10/23/2018 | 618.66 |
| G108 | 01/15/2019 | 620.52 |
| G108 | 08/05/2019 | 617.89 |
| G108 | 01/20/2020 | 620.79 |
| G108 | 08/10/2020 | 617.86 |
| G108 | 10/14/2020 | 616.02 |
| G108 | 01/20/2021 | 618.72 |
| G108 | 01/28/2021 | 618.82 |
| G108 | 04/20/2021 | 619.37 |
| G108 | 07/26/2021 | 619.40 |
| G108 | 08/16/2021 | 619.66 |
| G109 | 01/19/2015 | 617.78 |
| G109 | 04/08/2015 | 619.71 |
| G109 | 07/24/2015 | 620.41 |
| G109 G109 | 10/06/2015 02/08/2016 | 618.12 |
| G109 | 05/09/2016 | 619.56 |
| G109 G109 | 07/25/2016 | 619.11 |
| G109 | 11/12/2016 | 619.35 |
| G109 | 02/04/2017 | 620.84 |
| G109 G109 | 05/13/2017 | 619.57 |
| G109 G109 | 07/08/2017 | 619.24 |
| G109 | 10/21/2017 | 615.70 |
| G109 | 05/08/2018 | 619.61 |
| G109 | 08/02/2018 | 619.80 |
| G109 | 10/23/2018 | 617.11 |
| G109 | 01/15/2019 | 618.20 |
| G109 | 08/05/2019 | 617.27 |
| | -0, 00, 2019 | |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G109 | 01/20/2020 | 620.26 |
| G109 | 08/10/2020 | 617.16 |
| G109 | 10/14/2020 | 615.52 |
| G109 | 01/20/2021 | 617.91 |
| G109 | 01/28/2021 | 618.58 |
| G109 | 04/20/2021 | 618.59 |
| G109 | 07/26/2021 | 618.68 |
| G109 | 08/16/2021 | 618.96 |
| G110 | 01/19/2015 | 616.76 |
| G110 | 04/08/2015 | 618.60 |
| G110 | 07/24/2015 | 619.55 |
| G110 | 10/07/2015 | 617.70 |
| G110 | 11/16/2015 | 616.55 |
| G110 | 02/08/2016 | 617.88 |
| G110 | 05/09/2016 | 618.53 |
| G110 | 07/25/2016 | 617.64 |
| G110 | 11/12/2016 | 618.86 |
| G110 | 02/04/2017 | 619.45 |
| G110 | 05/13/2017 | 619.10 |
| G110 | 07/08/2017 | 618.65 |
| G110 | 10/21/2017 | 613.27 |
| G110 | 01/26/2018 | 616.74 |
| G110 | 05/08/2018 | 618.48 |
| G110 | 08/02/2018 | 618.95 |
| G110 | 10/23/2018 | 618.42 |
| G110 | 01/15/2019 | 619.96 |
| G110 | 08/05/2019 | 620.65 |
| G110 | 01/20/2020 | 619.30 |
| G110 | 08/10/2020 | 616.14 |
| G110 | 10/14/2020 | 614.90 |
| G110 | 01/20/2021 | 616.81 |
| G110 G110 | 01/20/2021 | 616.81 |
| G110 G110 | 04/20/2021 | 617.71 |
| G110 G110 | 07/26/2021 | 617.76 |
| G110 | 08/16/2021 | 617.97 |
| G110 G111 | 01/19/2015 | 615.93 |
| G111 | 04/08/2015 | 617.48 |
| | | |
| G111 | 07/24/2015 | 618.03 |
| G111 | 10/07/2015 | 616.79 |
| G111 | 02/08/2016 | 616.92 |
| G111 | 05/09/2016 | 617.52 |
| G111 | 07/25/2016 | 617.35 |
| G111 | 11/12/2016 | 617.61 |
| G111 | 02/04/2017 | 618.53 |
| G111 | 05/13/2017 | 617.84 |
| G111 | 07/08/2017 | 617.59 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G111 | 10/21/2017 | 613.16 |
| G111 | 05/08/2018 | 617.50 |
| G111 | 08/02/2018 | 617.99 |
| G111 | 10/23/2018 | 615.72 |
| G111 | 01/15/2019 | 617.03 |
| G111 | 08/05/2019 | 615.78 |
| G111 | 01/20/2020 | 618.05 |
| G111 | 08/10/2020 | 615.59 |
| G111 | 10/14/2020 | 614.40 |
| G111 | 01/20/2021 | 615.84 |
| G111 | 01/28/2021 | 616.67 |
| G111 | 04/20/2021 | 616.73 |
| G111 | 07/26/2021 | 616.84 |
| G111 | 08/16/2021 | 618.10 |
| G119 | 01/19/2015 | 615.64 |
| G119 | 04/08/2015 | 615.86 |
| G119 | 07/23/2015 | 616.55 |
| G119 | 10/06/2015 | 615.31 |
| G119 | 02/08/2016 | 615.83 |
| G119 | 05/09/2016 | 615.87 |
| G119 | 07/25/2016 | 614.73 |
| G119 | 11/12/2016 | 616.03 |
| G119 | 02/04/2017 | 617.45 |
| G119 | 05/13/2017 | 616.57 |
| G119 | 07/08/2017 | 614.80 |
| G119 | 10/21/2017 | 612.24 |
| G119 | 05/08/2018 | 615.53 |
| G119 | 08/02/2018 | 616.55 |
| G119 | 10/23/2018 | 615.43 |
| G119 | 01/15/2019 | 616.00 |
| G119 | 08/05/2019 | 616.87 |
| G119 | 01/20/2020 | 617.23 |
| G119 | 08/10/2020 | 616.02 |
| G119 | 10/13/2020 | 615.16 |
| G119 | 01/20/2021 | 616.09 |
| G119 | 01/28/2021 | 616.14 |
| G119 | 04/20/2021 | 616.80 |
| G119 | 07/26/2021 | 616.62 |
| G119 | 08/16/2021 | 616.75 |
| G120 | 01/19/2015 | 612.75 |
| G120 | 04/08/2015 | 613.43 |
| G120 | 07/23/2015 | 613.47 |
| G120 | 10/06/2015 | 612.94 |
| G120 | 11/16/2015 | 612.37 |
| G120 | 02/08/2016 | 613.06 |
| G120 | 05/09/2016 | 613.37 |
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|-----------------|-------------|-----------------------------------|
| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
| G120 | 07/25/2016 | 612.87 |
| G120 | 11/12/2016 | 613.45 |
| G120 | 02/04/2017 | 613.92 |
| G120 | 05/13/2017 | 613.75 |
| G120 | 07/08/2017 | 613.30 |
| G120 | 01/26/2018 | 612.69 |
| G120 | 05/08/2018 | 613.72 |
| G120 | 08/02/2018 | 612.13 |
| G120 | 10/23/2018 | 612.68 |
| G120 | 01/15/2019 | 612.87 |
| G120 | 05/03/2019 | 618.15 |
| G120 | 08/05/2019 | 614.27 |
| G120 | 01/20/2020 | 617.69 |
| G120 | 05/05/2020 | 618.23 |
| G120 | 08/10/2020 | 615.22 |
| G120 | 10/13/2020 | 614.39 |
| G120 | 01/20/2021 | 615.80 |
| G120 | 01/27/2021 | 615.80 |
| G120 | 04/20/2021 | 617.55 |
| G120 | 07/26/2021 | 616.95 |
| G120 | 08/16/2021 | 617.19 |
| G121 | 01/19/2015 | 613.63 |
| G121 | 04/08/2015 | 614.63 |
| G121 | 07/23/2015 | 614.09 |
| G121 | 10/06/2015 | 613.31 |
| G121 | 02/08/2016 | 614.10 |
| G121 | 05/09/2016 | 614.81 |
| G121 | 07/25/2016 | 613.62 |
| G121 | 11/12/2016 | 613.33 |
| G121 | 02/04/2017 | 614.97 |
| G121 | 05/13/2017 | 613.76 |
| G121 | 07/08/2017 | 613.75 |
| G121 | 05/08/2018 | 614.47 |
| G121 | 08/02/2018 | 612.97 |
| G121 | 10/23/2018 | 611.97 |
| G121 | 01/15/2019 | 611.93 |
| G121 | 08/05/2019 | 612.79 |
| G121 | 01/20/2020 | 618.63 |
| G121 | 08/10/2020 | 615.02 |
| G121 | 10/13/2020 | 613.69 |
| G121 | 01/20/2021 | 615.44 |
| G121 | 01/27/2021 | 616.14 |
| G121 | 04/20/2021 | 618.73 |
| G121 | 07/26/2021 | 616.79 |
| G121 | 08/16/2021 | 617.27 |
| G122 | 01/19/2015 | 610.79 |
| <u> </u> | 1 | |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G122 | 04/08/2015 | 615.94 |
| G122 | 07/23/2015 | 615.26 |
| G122 | 10/06/2015 | 614.39 |
| G122 | 02/08/2016 | 615.52 |
| G122 | 05/09/2016 | 616.84 |
| G122 | 07/25/2016 | 614.06 |
| G122 | 11/12/2016 | 614.64 |
| G122 | 02/04/2017 | 614.14 |
| G122 | 05/13/2017 | 614.79 |
| G122 | 07/08/2017 | 614.05 |
| G122 | 05/08/2018 | 615.80 |
| G122 | 08/02/2018 | 614.64 |
| G122 | 10/23/2018 | 613.34 |
| G122 | 01/15/2019 | 612.94 |
| G122 | 08/05/2019 | 613.68 |
| G122 | 01/20/2020 | 619.39 |
| G122 | 08/10/2020 | 613.48 |
| G122 | 10/13/2020 | 611.41 |
| G122 | 01/20/2021 | 613.99 |
| G122 | 01/27/2021 | 614.08 |
| G122 | 04/20/2021 | 620.41 |
| G122 | 07/26/2021 | 616.92 |
| G122 | 08/16/2021 | 617.28 |
| G123 | 01/19/2015 | 610.84 |
| G123 | 04/08/2015 | 612.41 |
| G123 | 07/23/2015 | 612.76 |
| G123 | 10/06/2015 | 611.89 |
| G123 | 02/08/2016 | 611.74 |
| G123 | 05/09/2016 | 611.73 |
| G123 | 07/25/2016 | 611.91 |
| G123 | 11/12/2016 | 612.03 |
| G123 | 02/04/2017 | 613.56 |
| G123 | 05/13/2017 | 612.15 |
| G123 | 07/08/2017 | 612.17 |
| G123 | 05/08/2018 | 612.85 |
| G123 | 08/02/2018 | 610.60 |
| G123 | 10/23/2018 | 610.31 |
| G123 | 01/15/2019 | 612.58 |
| G123 | 08/05/2019 | 616.10 |
| G123 | 01/20/2020 | 622.79 |
| G123 | 08/10/2020 | 615.96 |
| G123 | 10/14/2020 | 613.01 |
| G123 | 01/20/2021 | 615.92 |
| G123 | 01/27/2021 | 616.24 |
| G123 | 04/20/2021 | 622.41 |
| G123 | 07/26/2021 | 619.35 |



| COTTELIN, ILLINOIS | | |
|--------------------|-------------|-----------------------------------|
| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
| G123 | 08/16/2021 | 617.73 |
| G124 | 01/19/2015 | 615.27 |
| G124 | 04/08/2015 | 617.85 |
| G124 | 07/23/2015 | 618.25 |
| G124 | 10/06/2015 | 617.27 |
| G124 | 02/08/2016 | 616.47 |
| G124 | 05/09/2016 | 616.81 |
| G124 | 07/25/2016 | 618.27 |
| G124 | 11/12/2016 | 617.85 |
| G124 | 02/04/2017 | 619.23 |
| G124 | 05/13/2017 | 618.16 |
| G124 | 07/08/2017 | 618.39 |
| G124 | 10/21/2017 | 615.09 |
| G124 | 05/08/2018 | 618.04 |
| G124 | 08/02/2018 | 616.37 |
| G124 | 10/23/2018 | 615.61 |
| G124 | 01/15/2019 | 616.37 |
| G124 | 08/05/2019 | 617.90 |
| G124 | 01/20/2020 | 622.86 |
| G124 | 08/10/2020 | 615.53 |
| G124 | 10/14/2020 | 612.59 |
| G124 | 01/20/2021 | 615.96 |
| G124 | 01/27/2021 | 616.10 |
| G124 | 04/20/2021 | 622.44 |
| G124 | 07/26/2021 | 619.05 |
| G124 | 08/16/2021 | 619.43 |
| G125 | 01/19/2015 | 617.83 |
| G125 | 04/08/2015 | 620.45 |
| G125 | 07/23/2015 | 620.71 |
| G125 | 10/06/2015 | 619.66 |
| G125 | 11/16/2015 | 614.60 |
| G125 | 02/08/2016 | 619.95 |
| G125 | 05/09/2016 | 620.22 |
| G125 | 07/25/2016 | 621.53 |
| G125 | 11/12/2016 | 620.46 |
| G125 | 02/04/2017 | 622.40 |
| G125 | 05/13/2017 | 620.71 |
| G125 | 07/08/2017 | 622.45 |
| G125 | 10/21/2017 | 618.26 |
| G125 | 01/26/2018 | 613.88 |
| G125 | 05/08/2018 | 620.61 |
| G125 | 08/02/2018 | 620.82 |
| G125 | 10/23/2018 | 618.58 |
| G125 | 01/15/2019 | 619.01 |
| G125 | 08/05/2019 | 618.86 |
| G125 | 01/20/2020 | 622.96 |
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| COTTLEN, ILLINOIS | T | |
|-------------------|-------------|-----------------------------------|
| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
| G125 | 05/05/2020 | 623.39 |
| G125 | 08/10/2020 | 615.38 |
| G125 | 10/14/2020 | 612.46 |
| G125 | 01/20/2021 | 615.66 |
| G125 | 01/27/2021 | 615.66 |
| G125 | 04/20/2021 | 622.46 |
| G125 | 07/26/2021 | 619.11 |
| G125 | 08/16/2021 | 619.49 |
| G126 | 01/20/2015 | 615.22 |
| G126 | 04/08/2015 | 616.45 |
| G126 | 07/23/2015 | 616.34 |
| G126 | 10/07/2015 | 614.13 |
| G126 | 02/08/2016 | 616.12 |
| G126 | 05/09/2016 | 616.58 |
| G126 | 07/25/2016 | 614.82 |
| G126 | 11/12/2016 | 615.19 |
| G126 | 02/04/2017 | 615.39 |
| G126 | 05/13/2017 | 615.35 |
| G126 | 07/08/2017 | 614.88 |
| G126 | 10/21/2017 | 612.28 |
| G126 | 05/08/2018 | 615.00 |
| G126 | 08/02/2018 | 614.12 |
| G126 | 10/23/2018 | 612.36 |
| G126 | 01/15/2019 | 612.83 |
| G126 | 08/05/2019 | 613.30 |
| G126 | 01/20/2020 | 616.87 |
| G126 | 08/10/2020 | 614.91 |
| G126 | 10/14/2020 | 613.97 |
| G126 | 01/20/2021 | 614.95 |
| G126 | 01/29/2021 | 615.98 |
| G126 | 04/20/2021 | 615.68 |
| G126 | 07/26/2021 | 615.85 |
| G126 | 08/16/2021 | 616.05 |
| G151 | 07/23/2015 | 615.43 |
| G151 | 10/06/2015 | 614.86 |
| G151 | 11/12/2016 | 614.85 |
| G151 | 02/04/2017 | 615.49 |
| G151 | 05/13/2017 | 614.98 |
| G151 | 07/08/2017 | 615.38 |
| G151 | 10/21/2017 | 612.13 |
| G151 | 05/08/2018 | 614.95 |
| G151 | 08/02/2018 | 614.93 |
| G151 | 10/23/2018 | 613.11 |
| G151 | 01/15/2019 | 613.93 |
| G151 | 08/05/2019 | 614.12 |
| G151 | 01/20/2020 | 615.23 |
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| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G151 | 08/10/2020 | 614.11 |
| G151 | 10/13/2020 | 613.39 |
| G151 | 01/20/2021 | 613.86 |
| G151 | 02/01/2021 | 615.07 |
| G151 | 04/20/2021 | 614.53 |
| G151 | 07/26/2021 | 614.83 |
| G151 | 08/16/2021 | 615.06 |
| G152 | 07/23/2015 | 616.47 |
| G152 | 10/06/2015 | 614.06 |
| G152 | 11/12/2016 | 615.74 |
| G152 | 02/04/2017 | 616.51 |
| G152 | 05/13/2017 | 616.13 |
| G152 | 07/08/2017 | 616.06 |
| G152 | 10/21/2017 | 612.77 |
| G152 | 05/08/2018 | 616.05 |
| G152 | 08/02/2018 | 614.85 |
| G152 | 10/23/2018 | 614.35 |
| G152 | 01/15/2019 | 614.59 |
| G152 | 08/05/2019 | 615.53 |
| G152 | 01/20/2020 | 617.44 |
| G152 | 08/10/2020 | 614.46 |
| G152 | 10/13/2020 | 613.13 |
| G152 | 01/20/2021 | 614.87 |
| G152 | 02/01/2021 | 613.13 |
| G152 | 04/20/2021 | 615.34 |
| G152 | 07/26/2021 | 616.76 |
| G152 | 08/16/2021 | 615.30 |
| G153 | 07/23/2015 | 615.93 |
| G153 | 10/06/2015 | 614.45 |
| G153 | 11/12/2016 | 615.15 |
| G153 | 02/04/2017 | 616.30 |
| G153 | 05/13/2017 | 615.25 |
| G153 | 07/08/2017 | 616.19 |
| G153 | 10/21/2017 | 612.37 |
| G153 | 05/08/2018 | 615.07 |
| G153 | 08/02/2018 | 614.01 |
| G153 | 10/23/2018 | 613.31 |
| G153 | 01/15/2019 | 614.36 |
| G153 | 08/05/2019 | 614.45 |
| G153 G153 | 01/20/2020 | 616.16 |
| G153 G153 | 01/20/2020 | 613.72 |
| | | |
| G153 | 10/13/2020 | 612.16 |
| G153 | 01/20/2021 | 612.66 |
| G153 | 02/01/2021 | 613.18 |
| G153 | 04/20/2021 | 615.52 |
| G153 | 07/26/2021 | 613.97 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G153 | 08/16/2021 | 614.19 |
| G154 | 07/23/2015 | 614.85 |
| G154 | 10/06/2015 | 612.24 |
| G154 | 11/12/2016 | 614.68 |
| G154 | 02/04/2017 | 615.25 |
| G154 | 05/13/2017 | 614.93 |
| G154 | 07/08/2017 | 613.53 |
| G154 | 10/21/2017 | 610.33 |
| G154 | 05/08/2018 | 614.78 |
| G154 | 08/02/2018 | 613.75 |
| G154 | 10/23/2018 | 613.06 |
| G154 | 01/15/2019 | 613.66 |
| G154 | 08/05/2019 | 613.86 |
| G154 | 01/20/2020 | 618.28 |
| G154 | 08/10/2020 | 612.57 |
| G154 | 10/13/2020 | 610.84 |
| G154 | 01/20/2021 | 612.41 |
| G154 | 02/01/2021 | 617.01 |
| G154 | 04/20/2021 | 614.81 |
| G154 | 07/26/2021 | 615.21 |
| G154 | 08/16/2021 | 615.45 |
| G155 | 07/23/2015 | 614.45 |
| G155 | 10/06/2015 | 613.51 |
| G155 | 11/12/2016 | 613.93 |
| G155 | 02/04/2017 | 614.09 |
| G155 | 05/13/2017 | 614.59 |
| G155 | 07/08/2017 | 614.75 |
| G155 | 10/21/2017 | 609.91 |
| G155 | 05/08/2018 | 614.41 |
| G155 | 08/02/2018 | 613.68 |
| G155 | 10/23/2018 | 612.80 |
| G155 | 01/15/2019 | 613.56 |
| G155 | 08/05/2019 | 613.71 |
| G155 | 01/20/2020 | 615.99 |
| G155 | 08/10/2020 | 613.09 |
| G155 | 10/13/2020 | 612.10 |
| G155 | 01/20/2021 | 612.72 |
| G155 | 02/01/2021 | 614.59 |
| G155 | 04/20/2021 | 613.94 |
| G155 | 07/26/2021 | 613.81 |
| G155 G155 | 08/16/2021 | 614.01 |
| G200 | 10/05/2015 | 621.05 |
| G200 | 11/16/2015 | 621.66 |
| G200 | | |
| | 02/08/2016 | 623.29 |
| G200 | 05/09/2016 | 622.52 |
| G200 | 07/25/2016 | 622.82 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G200 | 11/12/2016 | 622.82 |
| G200 | 02/04/2017 | 621.13 |
| G200 | 05/13/2017 | 622.86 |
| G200 | 07/08/2017 | 622.96 |
| G200 | 10/21/2017 | 618.84 |
| G200 | 01/25/2018 | 620.39 |
| G200 | 05/08/2018 | 622.52 |
| G200 | 08/02/2018 | 621.54 |
| G200 | 10/23/2018 | 621.14 |
| G200 | 01/15/2019 | 621.98 |
| G200 | 08/05/2019 | 622.04 |
| G200 | 01/20/2020 | 622.72 |
| G200 | 08/10/2020 | 618.16 |
| G200 | 10/13/2020 | 615.63 |
| G200 | 01/20/2021 | 619.63 |
| G200 | 01/29/2021 | 619.63 |
| G200 | 03/29/2021 | 623.27 |
| G200 | 04/20/2021 | 621.86 |
| G200 | 04/21/2021 | 622.19 |
| G200 | 05/03/2021 | 622.69 |
| G200 | 05/06/2021 | 623.36 |
| G200 | 05/17/2021 | 622.10 |
| G200 | 06/09/2021 | 620.84 |
| G200 | 06/23/2021 | 619.38 |
| G200 | 07/12/2021 | 620.52 |
| G200 | 07/26/2021 | 619.74 |
| G200 | 07/28/2021 | 619.56 |
| G200 | 08/16/2021 | 619.88 |
| G205 | 02/08/2016 | 620.10 |
| G205 G205 | 05/09/2016 | 620.48 |
| G205 | 07/25/2016 | 619.81 |
| | | 620.04 |
| G205 | 11/12/2016 | |
| G205 | 02/04/2017 | 621.45 |
| G205 | 05/13/2017 | 619.54 |
| G205 | 07/08/2017 | 619.93 |
| G205 | 10/21/2017 | 616.33 |
| G206 | 10/07/2015 | 620.69 |
| G206 | 11/16/2015 | 619.27 |
| G206 | 02/08/2016 | 621.92 |
| G206 | 05/09/2016 | 622.30 |
| G206 | 06/27/2016 | 620.51 |
| G206 | 07/25/2016 | 621.71 |
| G206 | 11/12/2016 | 621.44 |
| G206 | 02/04/2017 | 622.68 |
| G206 | 05/13/2017 | 621.67 |
| G206 | 07/08/2017 | 622.00 |



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|-----------------|-------------|-----------------------------------|
| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
| G206 | 10/21/2017 | 616.61 |
| G206 | 05/08/2018 | 620.71 |
| G206 | 08/02/2018 | 621.87 |
| G206 | 10/23/2018 | 619.71 |
| G206 | 01/15/2019 | 618.82 |
| G206 | 08/05/2019 | 621.56 |
| G206 | 01/20/2020 | 622.76 |
| G206 | 05/05/2020 | 623.02 |
| G206 | 08/10/2020 | 619.92 |
| G206 | 10/13/2020 | 617.84 |
| G206 | 01/20/2021 | 621.50 |
| G206 | 01/27/2021 | 621.50 |
| G206 | 04/20/2021 | 622.07 |
| G206 | 05/03/2021 | 622.60 |
| G206 | 05/17/2021 | 622.31 |
| G206 | 06/09/2021 | 621.71 |
| G206 | 06/23/2021 | 620.54 |
| G206 | 07/12/2021 | 622.39 |
| G206 | 07/26/2021 | 622.00 |
| G206 | 08/16/2021 | 622.08 |
| G206D | 03/29/2021 | 583.94 |
| G206D | 03/30/2021 | 584.34 |
| G206D | 04/20/2021 | 585.96 |
| G206D | 04/22/2021 | 584.64 |
| G206D | 05/03/2021 | 587.42 |
| G206D | 05/05/2021 | 586.96 |
| G206D | 05/17/2021 | 587.81 |
| G206D | 05/18/2021 | 587.82 |
| G206D | 06/09/2021 | 584.19 |
| G206D | 06/23/2021 | 589.66 |
| G206D | 07/12/2021 | 590.72 |
| G206D | 07/26/2021 | 591.14 |
| G206D | 07/27/2021 | 591.15 |
| G206D | 08/16/2021 | 592.00 |
| G207 | 10/07/2015 | 620.72 |
| G207 | 02/08/2016 | 622.18 |
| G207 | 05/09/2016 | 622.56 |
| G207 | 07/25/2016 | 622.06 |
| G207 | 11/12/2016 | 622.54 |
| G207 | 02/04/2017 | 623.24 |
| G207 | 05/13/2017 | 623.39 |
| G207 | 07/08/2017 | 621.31 |
| G207 | 10/21/2017 | 619.41 |
| G207 | 05/08/2018 | 622.96 |
| G207 | 08/02/2018 | 623.21 |
| G207 | 10/23/2018 | 621.64 |
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|-----------------|-------------|-----------------------------------|
| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
| G207 | 01/15/2019 | 620.30 |
| G207 | 08/05/2019 | 621.21 |
| G207 | 01/20/2020 | 622.62 |
| G207 | 08/10/2020 | 619.71 |
| G207 | 10/13/2020 | 617.71 |
| G207 | 01/20/2021 | 621.85 |
| G207 | 01/28/2021 | 621.86 |
| G207 | 04/20/2021 | 622.30 |
| G207 | 07/26/2021 | 622.25 |
| G207 | 08/16/2021 | 622.36 |
| G208 | 10/07/2015 | 620.62 |
| G208 | 02/08/2016 | 622.19 |
| G208 | 05/09/2016 | 622.63 |
| G208 | 07/25/2016 | 622.20 |
| G208 | 11/12/2016 | 622.61 |
| G208 | 02/04/2017 | 624.07 |
| G208 | 05/13/2017 | 622.75 |
| G208 | 07/08/2017 | 622.04 |
| G208 | 10/21/2017 | 618.97 |
| G208 | 05/08/2018 | 622.94 |
| G208 | 08/02/2018 | 622.54 |
| G208 | 10/23/2018 | 620.66 |
| G208 | 01/15/2019 | 622.28 |
| G208 | 08/05/2019 | 622.46 |
| G208 | 01/20/2020 | 622.65 |
| G208 | 08/10/2020 | 619.56 |
| G208 | 10/13/2020 | 617.65 |
| G208 | 01/20/2021 | 622.09 |
| G208 | 01/27/2021 | 622.13 |
| G208 | 04/20/2021 | 622.37 |
| G208 | 07/26/2021 | 622.37 |
| G208 | 08/16/2021 | 622.50 |
| G209 | 10/07/2015 | 620.56 |
| G209 | 11/16/2015 | 620.06 |
| G209 | 02/08/2016 | 622.26 |
| G209 | 05/09/2016 | 622.74 |
| G209 | 07/25/2016 | 621.52 |
| G209 | 11/12/2016 | 621.65 |
| G209 | 02/04/2017 | 623.18 |
| G209 | 05/13/2017 | 621.86 |
| G209 | 07/08/2017 | 621.50 |
| G209 | 10/21/2017 | 617.76 |
| G209 | 01/25/2018 | 619.95 |
| G209 | 05/08/2018 | 621.35 |
| G209 | 08/02/2018 | 621.56 |
| G209 | 10/23/2018 | 619.91 |
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| G209 05/03/2019 621.80 G209 05/03/2019 623.09 G209 08/05/2019 621.46 G209 01/20/2020 622.69 G209 05/05/2020 622.69 G209 08/10/2020 619.59 G209 10/13/2020 619.59 G209 10/13/2020 617.69 G209 01/20/2021 621.94 G209 01/20/2021 622.40 G209 05/05/2021 622.40 G209 05/05/2021 622.82 G209 05/05/2021 622.82 G209 05/05/2021 622.82 G209 05/17/2021 622.51 G209 06/09/2021 622.03 G209 06/09/2021 622.03 G209 06/09/2021 622.03 G209 06/23/2021 622.82 G209 07/12/2021 622.03 G209 06/23/2021 622.03 G209 07/12/2021 622.08 G209 07/12/2021 622.08 G209 07/12/2021 622.08 G209 07/12/2021 622.08 G209 07/12/2021 622.08 G209 07/12/2021 622.08 G209 07/12/2021 622.08 G209 07/12/2021 622.08 G210 10/07/2015 619.83 G210 02/08/2016 621.72 G210 05/09/2016 622.50 G210 07/25/2016 620.94 G210 07/25/2016 620.94 G210 07/25/2016 621.05 G210 07/08/2017 621.69 G210 05/13/2017 621.69 G210 05/13/2017 621.03 G210 10/21/2017 616.82 G210 10/23/2018 620.15 G210 05/08/2018 620.15 G210 05/08/2018 620.15 G210 01/15/2019 620.82 G210 01/15/2019 620.88 G210 01/20/2020 622.33 G210 08/10/2020 619.97 G210 01/20/2021 622.18 G211 01/07/2015 619.00 G211 01/20/2021 622.18 G211 01/07/2015 619.00 G211 01/20/2021 622.18 G211 01/07/2015 619.00 G211 01/20/2021 622.18 G211 01/07/2015 619.00 G211 01/20/2021 622.18 G211 01/07/2015 622.18 G211 01/07/2015 622.18 G211 05/03/2017 622.15 G211 05/03/2017 622.15 | Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|---|-----------------|-------------|-----------------------------------|
| G209 08/05/2019 621.46 G209 01/20/2020 622.69 G209 05/05/2020 622.96 G209 08/10/2020 619.59 G209 10/13/2020 617.69 G209 01/20/2021 621.94 G209 01/27/2021 621.94 G209 04/20/2021 622.40 G209 05/03/2021 622.82 G209 05/03/2021 622.81 G209 06/03/2021 622.03 G209 06/23/2021 622.08 G209 07/12/2021 622.08 G209 07/25/2021 622.41 G209 08/16/2021 622.56 G210 10/07/2015 619.83 G210 02/08/2016 621.72 G210 05/09/2016 622.50 G210 07/25/2016 622.50 G210 07/25/2016 622.50 G210 07/25/2016 621.05 G210 07/08/2017 621.69 <td>G209</td> <td>01/15/2019</td> <td>621.80</td> | G209 | 01/15/2019 | 621.80 |
| G209 01/20/2020 622.69 G209 05/05/2020 622.96 G209 08/10/2020 619.59 G209 10/13/2020 617.69 G209 01/20/2021 621.94 G209 01/27/2021 621.94 G209 04/20/2021 622.40 G209 05/03/2021 622.82 G209 06/09/2021 622.03 G209 06/09/2021 622.03 G209 06/23/2021 622.08 G209 07/26/2021 622.08 G209 07/26/2021 622.41 G209 08/16/2021 622.56 G210 10/07/2015 619.83 G210 02/08/2016 621.72 G210 05/09/2016 622.50 G210 07/25/2016 622.50 G210 07/25/2016 622.09 G210 07/25/2016 621.05 G210 07/28/2017 621.69 G210 07/28/2017 621.03 <td>G209</td> <td>05/03/2019</td> <td>623.09</td> | G209 | 05/03/2019 | 623.09 |
| G209 05/05/2020 622.96 G209 08/10/2020 619.59 G209 10/13/2020 617.69 G209 01/20/2021 621.94 G209 01/27/2021 621.94 G209 04/20/2021 622.40 G209 05/03/2021 622.82 G209 06/09/2021 622.03 G209 06/23/2021 620.89 G209 07/26/2021 622.08 G209 07/26/2021 622.41 G209 08/16/2021 622.56 G210 10/07/2015 619.83 G210 02/08/2016 621.72 G210 05/09/2016 622.50 G210 07/25/2016 620.94 G210 07/25/2016 620.94 G210 07/25/2016 621.05 G210 07/08/2017 621.69 G210 07/08/2017 621.09 G210 07/08/2017 621.03 G210 05/08/2018 620.19 <td>G209</td> <td>08/05/2019</td> <td>621.46</td> | G209 | 08/05/2019 | 621.46 |
| G209 08/10/2020 619.59 G209 10/13/2020 617.69 G209 01/20/2021 621.94 G209 01/27/2021 621.94 G209 04/20/2021 622.40 G209 05/03/2021 622.82 G209 05/17/2021 622.03 G209 06/09/2021 622.03 G209 07/26/2021 622.08 G209 07/26/2021 622.41 G209 08/16/2021 622.56 G210 10/07/2015 619.83 G210 02/08/2016 621.72 G210 05/09/2016 622.50 G210 07/25/2016 622.50 G210 07/25/2016 621.05 G210 07/25/2016 621.05 G210 07/25/2016 621.05 G210 07/08/2017 621.69 G210 07/08/2017 621.69 G210 07/08/2017 621.03 G210 05/08/2018 620.19 <td>G209</td> <td>01/20/2020</td> <td>622.69</td> | G209 | 01/20/2020 | 622.69 |
| G209 10/13/2020 617.69 G209 01/20/2021 621.94 G209 01/27/2021 621.94 G209 04/20/2021 622.40 G209 05/03/2021 622.82 G209 06/09/2021 622.03 G209 06/09/2021 622.08 G209 07/26/2021 622.08 G209 07/26/2021 622.41 G209 07/26/2021 622.56 G210 10/07/2015 619.83 G210 02/08/2016 621.72 G210 02/08/2016 622.50 G210 07/25/2016 622.50 G210 07/25/2016 622.50 G210 07/25/2016 621.05 G210 07/25/2016 621.05 G210 07/25/2016 621.05 G210 07/08/2017 621.69 G210 07/08/2017 621.03 G210 07/08/2017 621.03 G210 08/02/2018 620.15 <td>G209</td> <td>05/05/2020</td> <td>622.96</td> | G209 | 05/05/2020 | 622.96 |
| G209 01/20/2021 621.94 G209 01/27/2021 621.94 G209 04/20/2021 622.40 G209 05/03/2021 622.82 G209 05/17/2021 622.51 G209 06/09/2021 622.08 G209 06/23/2021 622.08 G209 07/26/2021 622.41 G209 07/26/2021 622.41 G209 08/16/2021 622.56 G210 10/07/2015 619.83 G210 02/08/2016 621.72 G210 05/09/2016 622.50 G210 07/25/2016 622.50 G210 07/25/2016 622.50 G210 07/25/2016 621.05 G210 07/25/2016 621.05 G210 07/08/2017 621.69 G210 07/08/2017 621.69 G210 07/08/2017 621.03 G210 07/08/2017 621.03 G210 08/02/2018 620.19 <td>G209</td> <td>08/10/2020</td> <td>619.59</td> | G209 | 08/10/2020 | 619.59 |
| G209 01/27/2021 621.94 G209 04/20/2021 622.40 G209 05/03/2021 622.82 G209 05/17/2021 622.51 G209 06/09/2021 622.03 G209 06/23/2021 620.89 G209 07/26/2021 622.08 G209 07/26/2021 622.41 G209 08/16/2021 622.56 G210 10/07/2015 619.83 G210 02/08/2016 621.72 G210 05/09/2016 622.50 G210 07/25/2016 620.94 G210 07/25/2016 621.05 G210 07/25/2016 621.05 G210 07/25/2016 621.05 G210 07/25/2016 621.05 G210 07/08/2017 621.69 G210 07/08/2017 621.69 G210 07/08/2017 621.03 G210 07/20/2017 616.82 G210 05/08/2018 620.19 <td>G209</td> <td>10/13/2020</td> <td>617.69</td> | G209 | 10/13/2020 | 617.69 |
| G209 04/20/2021 622.40 G209 05/03/2021 622.82 G209 05/17/2021 622.51 G209 06/09/2021 622.03 G209 06/23/2021 620.89 G209 07/26/2021 622.08 G209 07/26/2021 622.41 G209 08/16/2021 622.56 G210 10/07/2015 619.83 G210 02/08/2016 621.72 G210 05/09/2016 622.50 G210 07/25/2016 622.94 G210 07/25/2016 622.094 G210 07/25/2016 621.05 G210 07/25/2016 621.05 G210 07/08/2017 621.69 G210 07/08/2017 621.69 G210 07/08/2017 621.03 G210 07/08/2017 621.03 G210 05/08/2018 620.19 G210 01/15/2019 620.82 G210 01/23/2018 618.92 <td>G209</td> <td>01/20/2021</td> <td>621.94</td> | G209 | 01/20/2021 | 621.94 |
| G209 05/03/2021 622.82 G209 05/17/2021 622.51 G209 06/09/2021 622.03 G209 06/23/2021 620.89 G209 07/12/2021 622.08 G209 07/26/2021 622.41 G209 08/16/2021 622.56 G210 10/07/2015 619.83 G210 02/08/2016 621.72 G210 05/09/2016 622.50 G210 07/25/2016 620.94 G210 07/25/2016 620.94 G210 11/12/2016 621.05 G210 07/08/2017 621.69 G210 07/08/2017 621.69 G210 05/13/2017 620.77 G210 07/08/2017 616.82 G210 07/08/2017 616.82 G210 05/08/2018 620.19 G210 08/02/2018 620.15 G210 01/15/2019 620.82 G210 01/20/2020 618.00 <td>G209</td> <td>01/27/2021</td> <td>621.94</td> | G209 | 01/27/2021 | 621.94 |
| G209 05/17/2021 622.51 G209 06/09/2021 622.03 G209 06/23/2021 620.89 G209 07/12/2021 622.08 G209 07/26/2021 622.41 G209 08/16/2021 622.56 G210 10/07/2015 619.83 G210 02/08/2016 621.72 G210 05/09/2016 622.50 G210 07/25/2016 620.94 G210 07/25/2016 620.94 G210 11/12/2016 621.05 G210 02/04/2017 621.69 G210 05/13/2017 620.77 G210 05/13/2017 620.77 G210 05/08/2018 620.19 G210 05/08/2018 620.19 G210 05/08/2018 620.19 G210 01/23/2018 618.92 G210 01/15/2019 620.82 G210 01/20/2020 622.33 G210 01/20/2020 618.00 <td>G209</td> <td>04/20/2021</td> <td>622.40</td> | G209 | 04/20/2021 | 622.40 |
| G209 06/09/2021 622.03 G209 06/23/2021 620.89 G209 07/12/2021 622.08 G209 07/26/2021 622.41 G209 08/16/2021 622.56 G210 10/07/2015 619.83 G210 02/08/2016 621.72 G210 05/09/2016 622.50 G210 07/25/2016 620.94 G210 07/25/2016 620.94 G210 11/12/2016 621.05 G210 02/04/2017 621.69 G210 05/13/2017 620.77 G210 05/13/2017 621.03 G210 07/08/2017 616.82 G210 05/08/2018 620.19 G210 05/08/2018 620.19 G210 08/02/2018 620.15 G210 10/23/2018 618.92 G210 01/15/2019 620.82 G210 01/20/2020 622.33 G210 01/20/2020 619.97 <td>G209</td> <td>05/03/2021</td> <td>622.82</td> | G209 | 05/03/2021 | 622.82 |
| G209 06/23/2021 620.89 G209 07/12/2021 622.08 G209 07/26/2021 622.41 G209 08/16/2021 622.56 G210 10/07/2015 619.83 G210 02/08/2016 621.72 G210 05/09/2016 622.50 G210 07/25/2016 620.94 G210 11/12/2016 621.05 G210 02/04/2017 621.69 G210 05/13/2017 620.77 G210 05/13/2017 620.77 G210 07/08/2017 621.03 G210 07/08/2017 616.82 G210 05/08/2018 620.19 G210 05/08/2018 620.19 G210 08/02/2018 620.15 G210 10/23/2018 618.92 G210 01/15/2019 620.82 G210 01/15/2019 620.82 G210 01/20/2020 618.00 G210 01/20/2020 618.00 <td>G209</td> <td>05/17/2021</td> <td>622.51</td> | G209 | 05/17/2021 | 622.51 |
| G209 07/12/2021 622.41 G209 07/26/2021 622.41 G209 08/16/2021 622.56 G210 10/07/2015 619.83 G210 05/09/2016 621.72 G210 05/09/2016 622.50 G210 07/25/2016 620.94 G210 11/12/2016 621.05 G210 02/04/2017 621.69 G210 05/13/2017 620.77 G210 05/13/2017 621.03 G210 07/08/2017 621.03 G210 07/08/2017 621.03 G210 05/08/2017 616.82 G210 05/08/2018 620.19 G210 08/02/2018 620.19 G210 08/02/2018 620.15 G210 10/23/2018 618.92 G210 01/15/2019 620.82 G210 08/05/2019 620.50 G210 01/20/2020 618.00 G210 01/20/2021 620.58 <td>G209</td> <td>06/09/2021</td> <td>622.03</td> | G209 | 06/09/2021 | 622.03 |
| G209 07/26/2021 622.41 G209 08/16/2021 622.56 G210 10/07/2015 619.83 G210 02/08/2016 621.72 G210 05/09/2016 622.50 G210 07/25/2016 620.94 G210 11/12/2016 621.05 G210 02/04/2017 621.69 G210 05/13/2017 620.77 G210 05/13/2017 620.77 G210 07/08/2017 621.03 G210 10/21/2017 616.82 G210 05/08/2018 620.19 G210 05/08/2018 620.19 G210 08/02/2018 620.15 G210 10/23/2018 618.92 G210 01/15/2019 620.82 G210 01/15/2019 620.82 G210 01/20/2020 622.33 G210 01/20/2020 619.97 G210 01/3/2020 618.00 G210 01/27/2021 620.58 | G209 | 06/23/2021 | 620.89 |
| G209 08/16/2021 622.56 G210 10/07/2015 619.83 G210 02/08/2016 621.72 G210 05/09/2016 621.72 G210 05/09/2016 622.50 G210 07/25/2016 620.94 G210 11/12/2016 621.05 G210 02/04/2017 621.69 G210 05/13/2017 620.77 G210 07/08/2017 621.03 G210 10/21/2017 616.82 G210 10/21/2017 616.82 G210 05/08/2018 620.19 G210 05/08/2018 620.19 G210 08/02/2018 620.15 G210 10/23/2018 618.92 G210 01/15/2019 620.82 G210 01/25/2019 620.82 G210 01/20/2020 622.33 G210 01/20/2020 618.00 G210 01/20/2021 620.58 G210 01/27/2021 620.58 <td>G209</td> <td>07/12/2021</td> <td>622.08</td> | G209 | 07/12/2021 | 622.08 |
| G210 10/07/2015 619.83 G210 02/08/2016 621.72 G210 05/09/2016 622.50 G210 07/25/2016 620.94 G210 11/12/2016 621.05 G210 02/04/2017 621.69 G210 05/13/2017 620.77 G210 07/08/2017 621.03 G210 10/21/2017 616.82 G210 05/08/2018 620.19 G210 05/08/2018 620.19 G210 10/23/2018 620.15 G210 10/23/2018 618.92 G210 01/15/2019 620.82 G210 01/25/2019 620.50 G210 01/20/2020 622.33 G210 01/20/2020 619.97 G210 10/13/2020 618.00 G210 01/20/2021 620.58 G210 01/20/2021 622.18 G210 07/26/2021 622.18 G210 08/16/2021 622.18 <td>G209</td> <td>07/26/2021</td> <td>622.41</td> | G209 | 07/26/2021 | 622.41 |
| G210 02/08/2016 621.72 G210 05/09/2016 622.50 G210 07/25/2016 620.94 G210 11/12/2016 621.05 G210 02/04/2017 621.69 G210 05/13/2017 621.69 G210 05/13/2017 620.77 G210 07/08/2017 621.03 G210 10/21/2017 616.82 G210 05/08/2018 620.19 G210 08/02/2018 620.19 G210 08/02/2018 620.15 G210 10/23/2018 618.92 G210 01/15/2019 620.82 G210 01/15/2019 620.82 G210 01/20/2020 622.33 G210 01/20/2020 619.97 G210 01/13/2020 618.00 G210 01/20/2021 620.58 G210 01/27/2021 620.40 G210 04/20/2021 622.18 G210 07/26/2021 622.18 <td>G209</td> <td>08/16/2021</td> <td>622.56</td> | G209 | 08/16/2021 | 622.56 |
| G210 05/09/2016 622.50 G210 07/25/2016 620.94 G210 11/12/2016 621.05 G210 02/04/2017 621.69 G210 05/13/2017 620.77 G210 07/08/2017 621.03 G210 10/21/2017 616.82 G210 05/08/2018 620.19 G210 08/02/2018 620.15 G210 10/23/2018 618.92 G210 10/23/2018 618.92 G210 01/15/2019 620.82 G210 08/05/2019 620.50 G210 01/20/2020 622.33 G210 01/20/2020 619.97 G210 01/13/2020 618.00 G210 01/20/2021 620.58 G210 01/27/2021 620.40 G210 04/20/2021 622.18 G210 07/26/2021 622.18 G211 10/07/2015 619.00 G211 02/08/2016 622.28 <td>G210</td> <td>10/07/2015</td> <td>619.83</td> | G210 | 10/07/2015 | 619.83 |
| G210 07/25/2016 620.94 G210 11/12/2016 621.05 G210 02/04/2017 621.69 G210 05/13/2017 620.77 G210 07/08/2017 621.03 G210 10/21/2017 616.82 G210 05/08/2018 620.19 G210 08/02/2018 620.19 G210 10/23/2018 618.92 G210 10/23/2018 618.92 G210 01/15/2019 620.82 G210 01/25/2019 620.50 G210 01/20/2020 622.33 G210 01/20/2020 619.97 G210 10/13/2020 618.00 G210 01/20/2021 620.58 G210 01/27/2021 620.40 G210 01/27/2021 620.40 G210 07/26/2021 622.18 G210 07/26/2021 622.18 G211 10/07/2015 619.00 G211 02/08/2016 622.08 <td>G210</td> <td>02/08/2016</td> <td>621.72</td> | G210 | 02/08/2016 | 621.72 |
| G210 11/12/2016 621.05 G210 02/04/2017 621.69 G210 05/13/2017 620.77 G210 07/08/2017 621.03 G210 10/21/2017 616.82 G210 05/08/2018 620.19 G210 08/02/2018 620.15 G210 10/23/2018 618.92 G210 10/23/2019 620.82 G210 01/15/2019 620.82 G210 08/05/2019 620.50 G210 01/20/2020 622.33 G210 01/20/2020 619.97 G210 10/13/2020 618.00 G210 01/20/2021 620.58 G210 01/27/2021 620.40 G210 01/27/2021 622.18 G210 07/26/2021 622.18 G210 07/26/2021 622.18 G210 08/16/2021 622.28 G211 10/07/2015 619.00 G211 02/08/2016 622.45 <td>G210</td> <td>05/09/2016</td> <td>622.50</td> | G210 | 05/09/2016 | 622.50 |
| G210 02/04/2017 621.69 G210 05/13/2017 620.77 G210 07/08/2017 621.03 G210 10/21/2017 616.82 G210 05/08/2018 620.19 G210 08/02/2018 620.15 G210 10/23/2018 618.92 G210 10/15/2019 620.82 G210 08/05/2019 620.50 G210 08/05/2019 620.50 G210 01/20/2020 619.97 G210 01/30/2020 619.97 G210 10/13/2020 618.00 G210 01/20/2021 620.58 G210 01/27/2021 620.58 G210 04/20/2021 622.18 G210 04/20/2021 622.18 G210 07/26/2021 622.18 G211 10/07/2015 619.00 G211 02/08/2016 622.08 G211 05/09/2016 622.45 G211 07/25/2016 621.81 <td>G210</td> <td>07/25/2016</td> <td>620.94</td> | G210 | 07/25/2016 | 620.94 |
| G210 05/13/2017 620.77 G210 07/08/2017 621.03 G210 10/21/2017 616.82 G210 05/08/2018 620.19 G210 08/02/2018 620.15 G210 10/23/2018 618.92 G210 01/15/2019 620.82 G210 08/05/2019 620.50 G210 01/20/2020 622.33 G210 01/20/2020 619.97 G210 10/13/2020 618.00 G210 01/20/2021 620.58 G210 01/27/2021 620.58 G210 01/27/2021 620.40 G210 04/20/2021 622.18 G210 07/26/2021 622.18 G210 08/16/2021 622.18 G211 10/07/2015 619.00 G211 02/08/2016 622.08 G211 05/09/2016 622.45 G211 07/25/2016 621.81 G211 02/04/2017 622.15 <td>G210</td> <td>11/12/2016</td> <td>621.05</td> | G210 | 11/12/2016 | 621.05 |
| G210 07/08/2017 621.03 G210 10/21/2017 616.82 G210 05/08/2018 620.19 G210 08/02/2018 620.15 G210 10/23/2018 618.92 G210 01/15/2019 620.82 G210 08/05/2019 620.50 G210 01/20/2020 622.33 G210 01/20/2020 619.97 G210 10/13/2020 618.00 G210 10/13/2020 618.00 G210 01/20/2021 620.58 G210 01/27/2021 620.58 G210 01/27/2021 620.40 G210 04/20/2021 622.18 G210 07/26/2021 622.18 G211 10/07/2015 619.00 G211 02/08/2016 622.08 G211 05/09/2016 622.08 G211 07/25/2016 621.81 G211 11/12/2016 621.28 G211 02/04/2017 622.15 <td>G210</td> <td>02/04/2017</td> <td>621.69</td> | G210 | 02/04/2017 | 621.69 |
| G210 10/21/2017 616.82 G210 05/08/2018 620.19 G210 08/02/2018 620.15 G210 10/23/2018 618.92 G210 01/15/2019 620.82 G210 08/05/2019 620.50 G210 01/20/2020 622.33 G210 08/10/2020 619.97 G210 10/13/2020 618.00 G210 01/20/2021 620.58 G210 01/27/2021 620.40 G210 01/27/2021 620.40 G210 04/20/2021 622.18 G210 07/26/2021 622.18 G210 08/16/2021 622.28 G211 10/07/2015 619.00 G211 02/08/2016 622.08 G211 05/09/2016 622.45 G211 07/25/2016 621.81 G211 11/12/2016 621.28 G211 02/04/2017 622.15 | G210 | 05/13/2017 | 620.77 |
| G210 05/08/2018 620.19 G210 08/02/2018 620.15 G210 10/23/2018 618.92 G210 01/15/2019 620.82 G210 08/05/2019 620.50 G210 01/20/2020 622.33 G210 08/10/2020 619.97 G210 10/13/2020 618.00 G210 01/20/2021 620.58 G210 01/27/2021 620.58 G210 04/20/2021 622.18 G210 04/20/2021 622.18 G210 07/26/2021 622.18 G210 08/16/2021 622.28 G211 10/07/2015 619.00 G211 02/08/2016 622.08 G211 05/09/2016 622.45 G211 07/25/2016 621.81 G211 11/12/2016 621.28 G211 02/04/2017 622.15 | G210 | 07/08/2017 | 621.03 |
| G210 08/02/2018 620.15 G210 10/23/2018 618.92 G210 01/15/2019 620.82 G210 08/05/2019 620.50 G210 01/20/2020 622.33 G210 08/10/2020 619.97 G210 10/13/2020 618.00 G210 01/20/2021 620.58 G210 01/27/2021 620.40 G210 04/20/2021 622.18 G210 07/26/2021 622.18 G210 07/26/2021 622.18 G210 08/16/2021 622.28 G211 10/07/2015 619.00 G211 02/08/2016 622.08 G211 05/09/2016 622.45 G211 07/25/2016 621.81 G211 11/12/2016 621.28 G211 02/04/2017 622.15 | G210 | 10/21/2017 | 616.82 |
| G210 10/23/2018 618.92 G210 01/15/2019 620.82 G210 08/05/2019 620.50 G210 01/20/2020 622.33 G210 08/10/2020 619.97 G210 10/13/2020 618.00 G210 01/20/2021 620.58 G210 01/27/2021 620.40 G210 04/20/2021 622.18 G210 07/26/2021 622.18 G210 08/16/2021 622.28 G211 10/07/2015 619.00 G211 02/08/2016 622.08 G211 05/09/2016 622.45 G211 07/25/2016 621.81 G211 11/12/2016 621.28 G211 02/04/2017 622.15 | G210 | 05/08/2018 | 620.19 |
| G210 01/15/2019 620.82 G210 08/05/2019 620.50 G210 01/20/2020 622.33 G210 08/10/2020 619.97 G210 10/13/2020 618.00 G210 01/20/2021 620.58 G210 01/27/2021 620.40 G210 04/20/2021 622.18 G210 07/26/2021 622.18 G210 08/16/2021 622.28 G211 10/07/2015 619.00 G211 02/08/2016 622.08 G211 05/09/2016 622.45 G211 07/25/2016 621.81 G211 11/12/2016 621.28 G211 02/04/2017 622.15 | G210 | 08/02/2018 | 620.15 |
| G210 08/05/2019 620.50 G210 01/20/2020 622.33 G210 08/10/2020 619.97 G210 10/13/2020 618.00 G210 01/20/2021 620.58 G210 01/27/2021 620.40 G210 04/20/2021 622.18 G210 07/26/2021 622.18 G210 08/16/2021 622.28 G211 10/07/2015 619.00 G211 02/08/2016 622.08 G211 05/09/2016 622.45 G211 07/25/2016 621.81 G211 11/12/2016 621.28 G211 02/04/2017 622.15 | G210 | 10/23/2018 | 618.92 |
| G210 01/20/2020 622.33 G210 08/10/2020 619.97 G210 10/13/2020 618.00 G210 01/20/2021 620.58 G210 01/27/2021 620.40 G210 04/20/2021 622.18 G210 07/26/2021 622.18 G210 08/16/2021 622.28 G211 10/07/2015 619.00 G211 02/08/2016 622.08 G211 05/09/2016 622.45 G211 07/25/2016 621.81 G211 11/12/2016 621.28 G211 02/04/2017 622.15 | G210 | 01/15/2019 | 620.82 |
| G210 08/10/2020 619.97 G210 10/13/2020 618.00 G210 01/20/2021 620.58 G210 01/27/2021 620.40 G210 04/20/2021 622.18 G210 07/26/2021 622.18 G210 08/16/2021 622.28 G211 10/07/2015 619.00 G211 02/08/2016 622.08 G211 05/09/2016 622.45 G211 07/25/2016 621.81 G211 11/12/2016 621.28 G211 02/04/2017 622.15 | G210 | 08/05/2019 | 620.50 |
| G210 10/13/2020 618.00 G210 01/20/2021 620.58 G210 01/27/2021 620.40 G210 04/20/2021 622.18 G210 07/26/2021 622.18 G210 08/16/2021 622.28 G211 10/07/2015 619.00 G211 02/08/2016 622.08 G211 05/09/2016 622.45 G211 07/25/2016 621.81 G211 11/12/2016 621.28 G211 02/04/2017 622.15 | G210 | 01/20/2020 | 622.33 |
| G210 01/20/2021 620.58 G210 01/27/2021 620.40 G210 04/20/2021 622.18 G210 07/26/2021 622.18 G210 08/16/2021 622.28 G211 10/07/2015 619.00 G211 02/08/2016 622.08 G211 05/09/2016 622.45 G211 07/25/2016 621.81 G211 11/12/2016 621.28 G211 02/04/2017 622.15 | G210 | 08/10/2020 | 619.97 |
| G210 01/27/2021 620.40 G210 04/20/2021 622.18 G210 07/26/2021 622.18 G210 08/16/2021 622.28 G211 10/07/2015 619.00 G211 02/08/2016 622.08 G211 05/09/2016 622.45 G211 07/25/2016 621.81 G211 11/12/2016 621.28 G211 02/04/2017 622.15 | G210 | 10/13/2020 | 618.00 |
| G210 04/20/2021 622.18 G210 07/26/2021 622.18 G210 08/16/2021 622.28 G211 10/07/2015 619.00 G211 02/08/2016 622.08 G211 05/09/2016 622.45 G211 07/25/2016 621.81 G211 11/12/2016 621.28 G211 02/04/2017 622.15 | G210 | 01/20/2021 | 620.58 |
| G210 07/26/2021 622.18 G210 08/16/2021 622.28 G211 10/07/2015 619.00 G211 02/08/2016 622.08 G211 05/09/2016 622.45 G211 07/25/2016 621.81 G211 11/12/2016 621.28 G211 02/04/2017 622.15 | G210 | 01/27/2021 | 620.40 |
| G210 08/16/2021 622.28 G211 10/07/2015 619.00 G211 02/08/2016 622.08 G211 05/09/2016 622.45 G211 07/25/2016 621.81 G211 11/12/2016 621.28 G211 02/04/2017 622.15 | G210 | 04/20/2021 | 622.18 |
| G211 10/07/2015 619.00 G211 02/08/2016 622.08 G211 05/09/2016 622.45 G211 07/25/2016 621.81 G211 11/12/2016 621.28 G211 02/04/2017 622.15 | G210 | 07/26/2021 | 622.18 |
| G211 02/08/2016 622.08 G211 05/09/2016 622.45 G211 07/25/2016 621.81 G211 11/12/2016 621.28 G211 02/04/2017 622.15 | G210 | 08/16/2021 | 622.28 |
| G211 05/09/2016 622.45 G211 07/25/2016 621.81 G211 11/12/2016 621.28 G211 02/04/2017 622.15 | G211 | 10/07/2015 | 619.00 |
| G211 07/25/2016 621.81 G211 11/12/2016 621.28 G211 02/04/2017 622.15 | G211 | 02/08/2016 | 622.08 |
| G211 11/12/2016 621.28 G211 02/04/2017 622.15 | G211 | 05/09/2016 | 622.45 |
| G211 02/04/2017 622.15 | G211 | 07/25/2016 | 621.81 |
| | G211 | 11/12/2016 | 621.28 |
| G211 05/13/2017 621.34 | G211 | 02/04/2017 | 622.15 |
| • | G211 | 05/13/2017 | 621.34 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G211 | 07/08/2017 | 622.09 |
| G211 | 10/21/2017 | 618.14 |
| G211 | 05/08/2018 | 620.69 |
| G211 | 08/02/2018 | 620.63 |
| G211 | 10/23/2018 | 619.52 |
| G211 | 01/15/2019 | 620.22 |
| G211 | 08/05/2019 | 620.66 |
| G211 | 01/20/2020 | 622.20 |
| G211 | 08/10/2020 | 619.83 |
| G211 | 10/13/2020 | 617.77 |
| G211 | 01/20/2021 | 620.22 |
| G211 | 01/27/2021 | 620.50 |
| G211 | 04/20/2021 | 622.04 |
| G211 | 07/26/2021 | 621.82 |
| G211 | 08/16/2021 | 621.91 |
| G212 | 10/07/2015 | 620.76 |
| G212 | 11/16/2015 | 618.54 |
| G212 | 02/08/2016 | 621.99 |
| G212 | 05/09/2016 | 622.04 |
| G212 | 07/25/2016 | 620.89 |
| G212 | 11/12/2016 | 621.00 |
| G212 | 02/04/2017 | 621.87 |
| G212 | 05/13/2017 | 621.32 |
| G212 | 07/08/2017 | 620.81 |
| G212 | 10/21/2017 | 617.19 |
| G212 | 05/08/2018 | 620.82 |
| G212 | 08/02/2018 | 620.80 |
| G212 | 10/23/2018 | 619.43 |
| G212 | 01/15/2019 | 621.13 |
| G212 | 08/05/2019 | 620.26 |
| G212 | 01/20/2020 | 622.10 |
| G212 | 08/10/2020 | 619.14 |
| G212 | 10/13/2020 | 616.90 |
| G212 | 01/20/2021 | 620.08 |
| G212 | 01/26/2021 | 620.08 |
| G212 | 04/20/2021 | 621.60 |
| G212 | 05/03/2021 | 622.12 |
| G212 | 05/17/2021 | 621.74 |
| G212 | 06/09/2021 | 621.19 |
| G212 | 06/23/2021 | 619.96 |
| G212 | 06/29/2021 | 620.08 |
| G212 | 07/12/2021 | 620.55 |
| G212 | 07/26/2021 | 621.13 |
| G212 | 08/16/2021 | 621.41 |
| G213 | 10/07/2015 | 620.21 |
| G213 | 02/08/2016 | 621.20 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G213 | 05/09/2016 | 621.69 |
| G213 | 07/25/2016 | 620.36 |
| G213 | 11/12/2016 | 620.78 |
| G213 | 02/04/2017 | 621.21 |
| G213 | 05/13/2017 | 621.16 |
| G213 | 07/08/2017 | 620.40 |
| G213 | 10/21/2017 | 618.62 |
| G213 | 05/08/2018 | 620.88 |
| G213 | 08/02/2018 | 620.35 |
| G213 | 10/23/2018 | 619.83 |
| G213 | 01/15/2019 | 620.81 |
| G213 | 08/05/2019 | 621.08 |
| G213 | 01/20/2020 | 621.72 |
| G213 | 08/10/2020 | 618.66 |
| G213 | 10/13/2020 | 616.56 |
| G213 | 01/20/2021 | 619.61 |
| G213 | 01/27/2021 | 619.97 |
| G213 | 04/20/2021 | 621.28 |
| G213 | 07/26/2021 | 620.96 |
| G213 | 08/16/2021 | 621.20 |
| G214 | 10/07/2015 | 617.56 |
| G214 | 02/08/2016 | 618.11 |
| G214 | 05/09/2016 | 619.39 |
| G214 | 07/25/2016 | 617.75 |
| G214 | 11/12/2016 | 618.16 |
| G214 | 02/04/2017 | 618.77 |
| G214 | 05/13/2017 | 618.51 |
| G214 | 07/08/2017 | 618.25 |
| G214 | 10/21/2017 | 614.52 |
| G214 | 05/08/2018 | 618.17 |
| G214 | 08/02/2018 | 617.35 |
| G214 | 10/23/2018 | 616.87 |
| G214 | 01/15/2019 | 618.57 |
| G214 | 08/05/2019 | 616.99 |
| G214 | 01/20/2020 | 619.38 |
| G214 | 08/10/2020 | 616.32 |
| G214 | 10/13/2020 | 614.47 |
| G214 | 01/20/2021 | 616.45 |
| G214 | 01/27/2021 | 616.64 |
| G214 | 04/20/2021 | 618.60 |
| G214 | 07/26/2021 | 618.39 |
| G214 | 08/16/2021 | 618.55 |
| G215 | 10/07/2015 | 616.56 |
| G215 | 11/16/2015 | 616.38 |
| G215 | 02/08/2016 | 618.31 |
| G215 | 05/09/2016 | 619.45 |
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| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G215 | 07/25/2016 | 617.10 |
| G215 | 11/12/2016 | 617.91 |
| G215 | 02/04/2017 | 618.34 |
| G215 | 05/13/2017 | 618.16 |
| G215 | 07/08/2017 | 617.01 |
| G215 | 10/21/2017 | 615.48 |
| G215 | 05/08/2018 | 617.80 |
| G215 | 08/02/2018 | 618.00 |
| G215 | 10/23/2018 | 616.26 |
| G215 | 01/15/2019 | 618.03 |
| G215 | 08/05/2019 | 617.55 |
| G215 | 01/20/2020 | 619.51 |
| G215 | 08/10/2020 | 617.11 |
| G215 | 10/14/2020 | 618.58 |
| G215 | 01/20/2021 | 617.19 |
| G215 | 01/26/2021 | 617.19 |
| G215 | 04/20/2021 | 618.83 |
| G215 | 05/03/2021 | 619.20 |
| G215 | 05/17/2021 | 619.10 |
| G215 | 06/09/2021 | 618.65 |
| G215 | 06/23/2021 | 617.45 |
| G215 | 06/29/2021 | 617.72 |
| G215 | 07/12/2021 | 618.24 |
| G215 | 07/26/2021 | 618.79 |
| G215 | 08/16/2021 | 618.91 |
| G216 | 10/07/2015 | 616.66 |
| G216 | 02/08/2016 | 618.74 |
| G216 | 05/09/2016 | 619.81 |
| G216 | 07/25/2016 | 617.68 |
| G216 | 11/12/2016 | 617.68 |
| G216 | 02/04/2017 | 618.06 |
| G216 | 05/13/2017 | 617.76 |
| G216 | 07/08/2017 | 617.21 |
| G216 | 10/21/2017 | 614.37 |
| G216 | 05/08/2018 | 616.88 |
| G216 | 08/02/2018 | 616.99 |
| G216 | 10/23/2018 | 615.92 |
| G216 | 01/15/2019 | 616.96 |
| G216 | 08/05/2019 | 618.04 |
| G216 | 01/20/2020 | 619.86 |
| G216 | 08/10/2020 | 617.54 |
| G216 G216 | 10/14/2020 | 615.85 |
| G216 G216 | 01/20/2021 | 617.65 |
| G216 G216 | | |
| | 01/28/2021 | 617.48 |
| G216 | 04/20/2021 | 619.25 |
| G216 | 07/26/2021 | 619.20 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G216 | 08/16/2021 | 619.30 |
| G217 | 10/07/2015 | 616.71 |
| G217 | 02/08/2016 | 618.25 |
| G217 | 05/09/2016 | 619.13 |
| G217 | 07/25/2016 | 617.81 |
| G217 | 11/12/2016 | 617.81 |
| G217 | 02/04/2017 | 618.13 |
| G217 | 05/13/2017 | 618.04 |
| G217 | 07/08/2017 | 618.12 |
| G217 | 10/21/2017 | 614.32 |
| G217 | 05/08/2018 | 617.21 |
| G217 | 08/02/2018 | 617.06 |
| G217 | 10/23/2018 | 616.17 |
| G217 | 01/15/2019 | 617.10 |
| G217 | 08/05/2019 | 617.10 |
| G217 | 01/20/2020 | 619.01 |
| G217 | 08/10/2020 | 616.20 |
| G217 | 10/14/2020 | 614.57 |
| G217 | 01/20/2021 | 616.74 |
| G217 | 01/28/2021 | 616.84 |
| G217 | 04/20/2021 | 618.45 |
| G217 | 07/26/2021 | 617.93 |
| G217 | 08/16/2021 | 618.04 |
| G218 | 10/07/2015 | 616.93 |
| G218 | 11/16/2015 | 617.11 |
| G218 | 02/08/2016 | 619.05 |
| G218 | 05/09/2016 | 620.10 |
| G218 | 07/25/2016 | 618.01 |
| G218 | 11/12/2016 | 618.39 |
| G218 | 02/04/2017 | 618.19 |
| G218 | 05/13/2017 | 618.56 |
| G218 | 07/08/2017 | 618.19 |
| G218 | 10/21/2017 | 614.46 |
| G218 | 01/26/2018 | 616.46 |
| G218 | 05/08/2018 | 617.87 |
| G218 | 08/02/2018 | 618.01 |
| G218 | 10/23/2018 | 616.66 |
| G218 | 01/15/2019 | 617.21 |
| G218 | 08/05/2019 | 617.86 |
| G218 | 01/20/2020 | 619.93 |
| G218 | 08/10/2020 | 617.42 |
| G218 | 10/14/2020 | 615.65 |
| G218 | 01/20/2021 | 617.53 |
| G218 | 01/26/2021 | 617.53 |
| G218 | 04/20/2021 | 619.53 |
| G218 | 05/03/2021 | 619.90 |



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|-----------------|-------------|-----------------------------------|
| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
| G218 | 05/17/2021 | 619.72 |
| G218 | 06/09/2021 | 619.32 |
| G218 | 06/23/2021 | 617.87 |
| G218 | 07/12/2021 | 618.60 |
| G218 | 07/26/2021 | 619.11 |
| G218 | 08/16/2021 | 619.33 |
| G270 | 10/05/2015 | 616.07 |
| G270 | 11/16/2015 | 621.06 |
| G270 | 02/08/2016 | 622.94 |
| G270 | 05/09/2016 | 622.77 |
| G270 | 07/25/2016 | 617.73 |
| G270 | 11/12/2016 | 618.31 |
| G270 | 02/04/2017 | 619.02 |
| G270 | 05/13/2017 | 618.83 |
| G270 | 07/08/2017 | 617.99 |
| G270 | 10/21/2017 | 614.45 |
| G270 | 05/08/2018 | 618.76 |
| G270 | 08/02/2018 | 616.56 |
| G270 | 10/23/2018 | 617.01 |
| G270 | 01/15/2019 | 618.46 |
| G270 | 08/05/2019 | 622.12 |
| G270 | 01/20/2020 | 622.11 |
| G270 | 08/10/2020 | 618.11 |
| G270 | 10/14/2020 | 616.17 |
| G270 | 01/20/2021 | 622.51 |
| G270 | 01/21/2021 | 622.57 |
| G270 | 03/29/2021 | 623.38 |
| G270 | 03/30/2021 | 623.44 |
| G270 | 04/20/2021 | 622.74 |
| G270 | 04/21/2021 | 622.85 |
| G270 | 05/03/2021 | 623.08 |
| G270 | 05/06/2021 | 623.27 |
| G270 | 05/17/2021 | 622.87 |
| G270 | 05/19/2021 | 623.30 |
| G270 | 06/09/2021 | 621.75 |
| G270 | 06/15/2021 | 620.09 |
| G270 | 06/23/2021 | 619.06 |
| G270 | 06/29/2021 | 621.69 |
| G270 | 07/12/2021 | 622.56 |
| G270 | 07/26/2021 | 622.39 |
| G270 | 07/27/2021 | 622.30 |
| G270 | 08/16/2021 | 622.54 |
| G271 | 10/08/2015 | 614.12 |
| G271 | 11/16/2015 | 613.77 |
| G271 | 02/08/2016 | 615.87 |
| G271 | 05/09/2016 | 616.05 |
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|-----------------|-------------|-----------------------------------|
| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
| G271 | 07/25/2016 | 616.62 |
| G271 | 11/12/2016 | 616.49 |
| G271 | 02/04/2017 | 617.95 |
| G271 | 05/13/2017 | 616.46 |
| G271 | 07/08/2017 | 616.47 |
| G271 | 07/17/2017 | 616.47 |
| G271 | 10/21/2017 | 613.31 |
| G271 | 05/08/2018 | 615.70 |
| G271 | 08/02/2018 | 615.70 |
| G271 | 10/23/2018 | 614.73 |
| G271 | 01/15/2019 | 617.40 |
| G271 | 08/05/2019 | 617.63 |
| G271 | 01/20/2020 | 617.83 |
| G271 | 08/10/2020 | 614.18 |
| G271 | 08/13/2020 | 614.18 |
| G271 | 10/14/2020 | 612.90 |
| G271 | 01/20/2021 | 613.91 |
| G271 | 02/01/2021 | 613.91 |
| G271 | 04/20/2021 | 615.51 |
| G271 | 05/03/2021 | 615.96 |
| G271 | 05/17/2021 | 615.78 |
| G271 | 06/09/2021 | 615.52 |
| G271 | 06/23/2021 | 615.02 |
| G271 | 07/12/2021 | 615.57 |
| G271 | 07/26/2021 | 615.67 |
| G271 | 08/16/2021 | 615.78 |
| G272 | 10/08/2015 | 612.56 |
| G272 | 02/08/2016 | 614.93 |
| G272 | 05/09/2016 | 614.96 |
| G272 | 07/25/2016 | 614.79 |
| G272 | 11/12/2016 | 614.34 |
| G272 | 02/04/2017 | 615.08 |
| G272 | 05/13/2017 | 614.23 |
| G272 | 07/08/2017 | 615.12 |
| G272 | 10/21/2017 | 611.45 |
| G272 | 05/08/2018 | 613.58 |
| G272 | 08/02/2018 | 613.44 |
| G272 | 10/23/2018 | 612.96 |
| G272 | 01/15/2019 | 615.43 |
| G272 | 08/05/2019 | 616.88 |
| G272 | 01/20/2020 | 616.49 |
| G272 | 08/10/2020 | 613.19 |
| G272 | 10/14/2020 | 611.89 |
| G272 | 01/20/2021 | 613.01 |
| G272 | 02/01/2021 | 616.48 |
| G272 | 04/20/2021 | 614.50 |
| <u> </u> | 1 | |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G272 | 07/26/2021 | 614.44 |
| G272 | 08/16/2021 | 614.47 |
| G273 | 10/08/2015 | 610.41 |
| G273 | 11/16/2015 | 611.82 |
| G273 | 02/08/2016 | 613.26 |
| G273 | 05/09/2016 | 612.83 |
| G273 | 07/25/2016 | 611.27 |
| G273 | 11/12/2016 | 610.83 |
| G273 | 02/04/2017 | 611.47 |
| G273 | 05/13/2017 | 610.77 |
| G273 | 07/08/2017 | 611.29 |
| G273 | 07/17/2017 | 611.29 |
| G273 | 10/21/2017 | 608.91 |
| G273 | 05/08/2018 | 610.16 |
| G273 | 08/02/2018 | 610.46 |
| G273 | 10/23/2018 | 608.82 |
| G273 | 01/15/2019 | 610.28 |
| G273 | 08/05/2019 | 610.23 |
| G273 | 01/20/2020 | 614.20 |
| G273 | 08/10/2020 | 611.52 |
| G273 | 08/13/2020 | 611.52 |
| G273 | 10/14/2020 | 610.31 |
| G273 | 01/20/2021 | 611.52 |
| G273 | 02/01/2021 | 611.52 |
| G273 | 04/20/2021 | 612.42 |
| G273 | 05/03/2021 | 612.90 |
| G273 | 05/17/2021 | 612.63 |
| G273 | 06/09/2021 | 612.24 |
| G273 | 06/23/2021 | 611.79 |
| G273 | 07/12/2021 | 612.22 |
| G273 | 07/26/2021 | 612.35 |
| G273 | 08/16/2021 | 613.52 |
| G274 | 10/08/2015 | 610.06 |
| G274 | 02/08/2016 | 610.22 |
| G274 | 05/09/2016 | 609.97 |
| G274 | 07/25/2016 | 611.06 |
| G274 | 11/12/2016 | 610.86 |
| G274 | 02/04/2017 | 612.00 |
| G274 | 05/13/2017 | 611.18 |
| G274 | 07/08/2017 | 611.55 |
| G274 | 10/21/2017 | 607.79 |
| G274 | 05/08/2018 | 610.84 |
| G274 | 08/02/2018 | 611.44 |
| G274 | 10/23/2018 | 609.52 |
| G274 | 01/15/2019 | 611.23 |
| G274 G274 | 08/05/2019 | 611.31 |
| J2/4 | 00/03/2019 | 011.31 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G274 | 01/20/2020 | 611.23 |
| G274 | 08/10/2020 | 609.29 |
| G274 | 10/14/2020 | 608.49 |
| G274 | 01/20/2021 | 610.36 |
| G274 | 02/01/2021 | 611.18 |
| G274 | 04/20/2021 | 609.89 |
| G274 | 07/26/2021 | 609.82 |
| G274 | 08/16/2021 | 609.88 |
| G275 | 02/08/2016 | 604.71 |
| G275 | 05/09/2016 | 604.76 |
| G275 | 07/25/2016 | 603.17 |
| G275 | 11/12/2016 | 604.28 |
| G275 | 02/04/2017 | 603.65 |
| G275 | 05/13/2017 | 604.67 |
| G275 | 07/08/2017 | 602.97 |
| G275 | 05/08/2018 | 604.26 |
| G275 | 08/02/2018 | 604.16 |
| G275 | 10/23/2018 | 604.46 |
| G275 | 01/15/2019 | 605.91 |
| G275 | 08/05/2019 | 605.97 |
| G275 | 01/20/2020 | 605.63 |
| G275 | 08/10/2020 | 604.95 |
| G275 | 01/20/2021 | 605.02 |
| G275 | 04/20/2021 | 605.00 |
| G275 | 07/13/2021 | 605.63 |
| G275 | 07/26/2021 | 605.05 |
| G275 | 08/16/2021 | 605.09 |
| G275D | 03/30/2021 | 570.32 |
| G275D | 04/20/2021 | 570.98 |
| G275D | 04/22/2021 | 568.33 |
| G275D | 05/03/2021 | 569.75 |
| G275D | 05/05/2021 | 570.26 |
| G275D | 05/17/2021 | 568.67 |
| G275D | 05/18/2021 | 569.00 |
| G275D | 06/09/2021 | 570.31 |
| G275D | 06/23/2021 | 569.71 |
| G275D | 07/12/2021 | 570.43 |
| G275D | 07/26/2021 | 570.35 |
| G275D | 07/28/2021 | 570.68 |
| G275D | 08/16/2021 | 571.48 |
| G276 | 11/16/2015 | 603.25 |
| G276 | 02/08/2016 | 603.71 |
| G276 | 05/09/2016 | 604.71 |
| G276 | 07/25/2016 | 604.92 |
| | 11/12/2016 | |
| G276 | | 603.60 |
| G276 | 02/04/2017 | 603.72 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G276 | 05/13/2017 | 603.40 |
| G276 | 07/08/2017 | 604.05 |
| G276 | 07/18/2017 | 604.05 |
| G276 | 05/08/2018 | 603.11 |
| G276 | 08/02/2018 | 606.60 |
| G276 | 10/23/2018 | 603.35 |
| G276 | 01/15/2019 | 604.00 |
| G276 | 08/05/2019 | 603.96 |
| G276 | 01/20/2020 | 605.08 |
| G276 | 08/10/2020 | 604.63 |
| G276 | 08/12/2020 | 604.63 |
| G276 | 10/14/2020 | 603.59 |
| G276 | 01/20/2021 | 603.71 |
| G276 | 04/20/2021 | 604.65 |
| G276 | 05/03/2021 | 604.71 |
| G276 | 05/17/2021 | 604.88 |
| G276 | 06/09/2021 | 604.93 |
| G276 | 06/23/2021 | 604.53 |
| G276 | 06/28/2021 | 604.58 |
| G276 | 07/12/2021 | 604.55 |
| G276 | 07/26/2021 | 604.68 |
| G276 | 08/16/2021 | 604.73 |
| G277 | 02/08/2016 | 602.98 |
| G277 | 05/09/2016 | 603.79 |
| G277 | 07/25/2016 | 602.08 |
| G277 | 11/12/2016 | 601.23 |
| G277 | 02/04/2017 | 603.58 |
| G277 | 05/13/2017 | 601.29 |
| G277 | 07/08/2017 | 603.09 |
| G277 | 10/21/2017 | 601.53 |
| G277 | 10/23/2018 | 601.28 |
| G277 | 01/15/2019 | 603.38 |
| G277 | 08/05/2019 | 602.15 |
| G277 | 01/20/2020 | 603.49 |
| G277 | 08/10/2020 | 603.29 |
| G277 | 04/20/2021 | 603.33 |
| G277 | 07/26/2021 | 603.33 |
| G278 | 02/08/2016 | 606.56 |
| G278 | 05/09/2016 | 607.00 |
| G278 | 07/25/2016 | 604.57 |
| G278 | 11/12/2016 | 604.29 |
| G278 | 02/04/2017 | 606.38 |
| G278 | 05/13/2017 | 604.30 |
| G278 | 07/08/2017 | 604.84 |
| G278 | 10/21/2017 | 604.54 |
| G278 | 05/08/2018 | 605.31 |
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| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G278 | 08/02/2018 | 604.57 |
| G278 | 10/23/2018 | 604.29 |
| G278 | 01/15/2019 | 605.40 |
| G278 | 08/05/2019 | 605.19 |
| G278 | 01/20/2020 | 608.15 |
| G278 | 08/10/2020 | 606.83 |
| G278 | 10/14/2020 | 605.55 |
| G278 | 01/20/2021 | 605.18 |
| G278 | 04/20/2021 | 606.47 |
| G278 | 07/26/2021 | 607.49 |
| G278 | 08/16/2021 | 607.62 |
| G279 | 10/08/2015 | 608.14 |
| G279 | 11/16/2015 | 607.80 |
| G279 | 02/08/2016 | 609.16 |
| G279 | 05/09/2016 | 610.17 |
| G279 | 07/25/2016 | 606.94 |
| G279 | 11/12/2016 | 606.93 |
| G279 | 02/04/2017 | 607.96 |
| G279 | 05/13/2017 | 606.74 |
| G279 | 07/08/2017 | 607.04 |
| G279 | 07/18/2017 | 607.04 |
| G279 | 05/08/2018 | 606.42 |
| G279 | 08/02/2018 | 605.87 |
| G279 | 10/23/2018 | 604.87 |
| G279 | 01/15/2019 | 606.79 |
| G279 | 08/05/2019 | 605.90 |
| G279 | 01/20/2020 | 611.08 |
| G279 | 08/10/2020 | 607.17 |
| G279 | 08/12/2020 | 607.17 |
| G279 | 10/14/2020 | 605.54 |
| G279 | 01/20/2021 | 607.07 |
| G279 | 01/28/2021 | 607.07 |
| G279 | 04/20/2021 | 608.97 |
| G279 G279 | 05/03/2021 | 609.38 |
| G279 G279 | 05/03/2021 | 609.22 |
| G279 G279 | 06/09/2021 | 599.69 |
| G279 G279 | 06/09/2021 | 607.74 |
| | | |
| G279 | 07/12/2021 | 608.18 |
| G279 | 07/26/2021 | 608.57 |
| G279 | 08/16/2021 | 608.95 |
| G280 | 10/08/2015 | 614.54 |
| G280 | 11/16/2015 | 618.45 |
| G280 | 02/08/2016 | 621.37 |
| G280 | 05/09/2016 | 621.94 |
| G280 | 07/25/2016 | 618.21 |
| G280 | 11/12/2016 | 618.46 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|--------------------------|-----------------------------------|
| G280 | 02/04/2017 | 619.10 |
| G280 | 05/13/2017 | 618.56 |
| G280 | 07/08/2017 | 619.45 |
| G280 | 07/18/2017 | 619.45 |
| G280 | 10/21/2017 | 614.47 |
| G280 | 05/08/2018 | 618.00 |
| G280 | 08/02/2018 | 616.70 |
| G280 | 10/23/2018 | 615.75 |
| G280 | 01/15/2019 | 616.24 |
| G280 | 08/05/2019 | 616.09 |
| G280 | 01/20/2020 | 622.33 |
| G280 | 08/10/2020 | 619.50 |
| G280 | 08/11/2020 | 619.50 |
| G280 | 10/14/2020 | 617.45 |
| G280 | 01/20/2021 | 618.20 |
| G280 | 01/28/2021 | 618.70 |
| G280 | 03/29/2021 | 620.61 |
| G280 | 03/30/2021 | 621.22 |
| G280 | 04/20/2021 | 619.76 |
| G280 | 04/22/2021 | 620.13 |
| G280 | 05/03/2021 | 620.21 |
| G280 | 05/06/2021 | 620.89 |
| G280 | 05/17/2021 | 619.98 |
| G280 | 05/19/2021 | 620.72 |
| G280 | 06/09/2021 | 619.75 |
| G280 | 06/23/2021 | 618.93 |
| G280 | 06/28/2021 | 619.02 |
| G280 | 07/12/2021 | 619.26 |
| G280 | 07/12/2021 | 619.50 |
| G280 | 07/13/2021 | 619.75 |
| G280 | 07/20/2021 | 619.66 |
| | + | |
| G280 | 08/16/2021 | 620.00 |
| G281 G281 | 11/16/2015 02/08/2016 | 619.56 |
| | + | |
| G281 | 05/09/2016 | 620.93 |
| G281 | 07/25/2016 | 620.30 |
| G281 | 11/12/2016 | 620.01 |
| G281 | 02/04/2017 | 620.37 |
| G281 | 05/13/2017 | 619.96 |
| G281 | 07/08/2017 | 619.17 |
| G281 | 10/21/2017 | 616.41 |
| G281 | 05/08/2018 | 619.33 |
| G281 | 08/02/2018 | 618.36 |
| G281 | 10/23/2018 | 617.26 |
| G281 | 01/15/2019 | 618.19 |
| G281 | 08/05/2019 | 620.16 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G281 | 01/20/2020 | 621.26 |
| G281 | 08/10/2020 | 619.26 |
| G281 | 01/20/2021 | 619.36 |
| G281 | 01/29/2021 | 619.36 |
| G281 | 03/29/2021 | 621.68 |
| G281 | 03/31/2021 | 621.29 |
| G281 | 04/20/2021 | 619.62 |
| G281 | 04/21/2021 | 619.77 |
| G281 | 05/03/2021 | 620.60 |
| G281 | 05/05/2021 | 620.85 |
| G281 | 05/17/2021 | 620.13 |
| G281 | 06/09/2021 | 619.65 |
| G281 | 06/14/2021 | 619.46 |
| G281 | 06/23/2021 | 618.71 |
| G281 | 06/28/2021 | 619.77 |
| G281 | 07/12/2021 | 620.23 |
| G281 | 07/26/2021 | 620.02 |
| G281 | 07/27/2021 | 619.92 |
| G281 | 08/16/2021 | 619.81 |
| G283 | 03/29/2021 | 607.80 |
| G283 | 03/31/2021 | 607.34 |
| G283 | 04/20/2021 | 606.34 |
| G283 | 04/22/2021 | 606.09 |
| G283 | 05/03/2021 | 606.81 |
| G283 | 05/06/2021 | 606.79 |
| G283 | 05/17/2021 | 606.30 |
| G283 | 05/18/2021 | 606.54 |
| G283 | 06/09/2021 | 605.13 |
| G283 | 06/15/2021 | 604.95 |
| G283 | 06/23/2021 | 604.56 |
| G283 | 06/29/2021 | 605.29 |
| G283 | 07/12/2021 | 605.50 |
| G283 | 07/13/2021 | 605.82 |
| G283 | 07/26/2021 | 605.18 |
| G283 | 07/27/2021 | 605.08 |
| G283 | 08/16/2021 | 605.12 |
| G284 | 03/29/2021 | 611.14 |
| G284 | 03/30/2021 | 610.95 |
| G284 | 04/20/2021 | 608.16 |
| G284 | 04/21/2021 | 607.65 |
| G284 | 05/03/2021 | 609.33 |
| G284 | 05/06/2021 | 610.72 |
| G284 | 05/17/2021 | 608.16 |
| G284 | 05/18/2021 | 609.49 |
| G284 | 06/09/2021 | 607.07 |
| G284 | 06/14/2021 | 606.95 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G284 | 06/23/2021 | 606.17 |
| G284 | 06/28/2021 | 608.02 |
| G284 | 07/12/2021 | 607.68 |
| G284 | 07/13/2021 | 607.69 |
| G284 | 07/26/2021 | 607.11 |
| G284 | 07/27/2021 | 606.95 |
| G284 | 08/16/2021 | 606.98 |
| G285 | 03/29/2021 | 608.62 |
| G285 | 03/30/2021 | 608.81 |
| G285 | 04/20/2021 | 608.13 |
| G285 | 04/22/2021 | 603.79 |
| G285 | 05/03/2021 | 606.99 |
| G285 | 05/06/2021 | 607.57 |
| G285 | 05/17/2021 | 607.47 |
| G285 | 05/18/2021 | 607.51 |
| G285 | 06/09/2021 | 607.39 |
| G285 | 06/15/2021 | 607.08 |
| G285 | 06/23/2021 | 604.33 |
| G285 | 06/28/2021 | 604.93 |
| G285 | 07/12/2021 | 604.80 |
| G285 | 07/13/2021 | 604.92 |
| G285 | 07/26/2021 | 605.27 |
| G285 | 07/27/2021 | 605.37 |
| G285 | 08/16/2021 | 606.28 |
| G286 | 03/29/2021 | 609.08 |
| G286 | 03/31/2021 | 608.22 |
| G286 | 04/20/2021 | 606.63 |
| G286 | 04/22/2021 | 606.15 |
| G286 | 05/03/2021 | 606.97 |
| G286 | 05/06/2021 | 608.56 |
| G286 | 05/17/2021 | 606.44 |
| G286 | 05/18/2021 | 606.57 |
| G286 | 06/09/2021 | 604.68 |
| G286 | 06/15/2021 | 602.98 |
| G286 | 07/12/2021 | 605.90 |
| G286 | 07/13/2021 | 606.00 |
| G287 | 03/29/2021 | 610.22 |
| G287 | 04/20/2021 | 608.67 |
| G287 | 04/20/2021 | 608.03 |
| G287 | 05/03/2021 | 609.28 |
| G287 | 05/05/2021 | 610.29 |
| G287 | 05/06/2021 | 608.41 |
| G287 G287 | 05/17/2021 | 609.32 |
| G287 G287 | 06/09/2021 | 607.59 |
| | | |
| G287 | 06/14/2021 | 617.45 |
| G287 | 07/12/2021 | 610.83 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G287 | 07/13/2021 | 607.78 |
| G287 | 08/16/2021 | 607.76 |
| G288 | 03/29/2021 | 616.32 |
| G288 | 03/30/2021 | 615.89 |
| G288 | 04/20/2021 | 613.90 |
| G288 | 04/21/2021 | 613.56 |
| G288 | 05/03/2021 | 614.51 |
| G288 | 05/06/2021 | 616.00 |
| G288 | 05/17/2021 | 613.87 |
| G288 | 05/18/2021 | 616.15 |
| G288 | 06/09/2021 | 612.90 |
| G288 | 06/15/2021 | 612.47 |
| G288 | 06/23/2021 | 611.90 |
| G288 | 06/28/2021 | 612.91 |
| G288 | 07/12/2021 | 613.59 |
| G288 | 07/13/2021 | 615.11 |
| G288 | 07/26/2021 | 612.85 |
| G288 | 07/27/2021 | 612.75 |
| G288 | 08/16/2021 | 612.98 |
| G301 | 11/16/2015 | 616.51 |
| G301 | 02/08/2016 | 617.21 |
| G301 | 05/09/2016 | 616.75 |
| G301 | 07/25/2016 | 614.65 |
| G301 | 11/12/2016 | 614.08 |
| G301 | 02/04/2017 | 614.15 |
| G301 | 05/13/2017 | 614.15 |
| G301 | 07/08/2017 | 614.88 |
| G301 | 10/21/2017 | 610.39 |
| G301 | 05/08/2018 | 613.73 |
| G301 | 08/02/2018 | 615.05 |
| G301 | 10/23/2018 | 612.46 |
| G301 G301 | 01/15/2019 | 613.23 |
| G301 G301 | 08/05/2019 | 613.82 |
| G301 G301 | 01/20/2020 | 618.07 |
| G301 G301 | 08/10/2020 | 615.16 |
| G301 G301 | 08/10/2020 | 616.03 |
| G301 G301 | 01/20/2021 | 616.03 |
| | | |
| G301 | 04/20/2021 | 616.05 |
| G301 | 05/03/2021 | 616.12 |
| G301 | 05/17/2021 | 615.99 |
| G301 | 06/09/2021 | 615.63 |
| G301 | 06/23/2021 | 615.02 |
| G301 | 07/12/2021 | 615.79 |
| G301 | 07/26/2021 | 615.31 |
| G301 | 08/16/2021 | 615.45 |
| G302 | 11/16/2015 | 610.74 |



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|-----------------|-------------|-----------------------------------|
| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
| G302 | 02/08/2016 | 613.14 |
| G302 | 05/09/2016 | 614.60 |
| G302 | 07/25/2016 | 608.16 |
| G302 | 11/12/2016 | 607.92 |
| G302 | 02/04/2017 | 608.95 |
| G302 | 05/13/2017 | 608.02 |
| G302 | 07/08/2017 | 608.42 |
| G302 | 10/21/2017 | 604.64 |
| G302 | 05/08/2018 | 607.59 |
| G302 | 08/02/2018 | 608.26 |
| G302 | 10/23/2018 | 605.54 |
| G302 | 01/15/2019 | 607.29 |
| G302 | 08/05/2019 | 609.95 |
| G302 | 01/20/2020 | 615.41 |
| G302 | 08/10/2020 | 608.05 |
| G302 | 01/20/2021 | 609.99 |
| G302 | 01/27/2021 | 609.99 |
| G302 | 04/20/2021 | 611.85 |
| G302 | 05/03/2021 | 612.07 |
| G302 | 05/17/2021 | 612.06 |
| G302 | 06/09/2021 | 610.29 |
| G302 | 06/23/2021 | 608.79 |
| G302 | 07/12/2021 | 611.79 |
| G302 | 07/26/2021 | 610.98 |
| G302 | 08/16/2021 | 611.77 |
| G303 | 11/16/2015 | 616.70 |
| G303 | 02/08/2016 | 617.87 |
| G303 | 05/09/2016 | 617.97 |
| G303 | 07/25/2016 | 614.92 |
| G303 | 11/12/2016 | 614.38 |
| G303 | 02/04/2017 | 614.95 |
| G303 | 05/13/2017 | 614.81 |
| G303 | 07/08/2017 | 614.97 |
| G303 | 10/21/2017 | 611.18 |
| G303 | 05/08/2018 | 614.16 |
| G303 | 08/02/2018 | 614.06 |
| G303 | 10/23/2018 | 613.05 |
| G303 | 01/15/2019 | 614.33 |
| G303 | 08/05/2019 | 617.37 |
| G303 | 01/20/2020 | 618.05 |
| G303 | 08/10/2020 | 615.16 |
| G303 | 01/20/2021 | 616.17 |
| G303 | 01/26/2021 | 616.17 |
| G303 | 04/20/2021 | 617.27 |
| G303 | 05/03/2021 | 618.02 |
| G303 | 05/03/2021 | 617.37 |
| 3303 | 03/1//2021 | 017.37 |



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|-----------------|-------------|-----------------------------------|
| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
| G303 | 06/09/2021 | 616.52 |
| G303 | 06/23/2021 | 614.92 |
| G303 | 07/12/2021 | 617.15 |
| G303 | 07/26/2021 | 616.44 |
| G303 | 08/16/2021 | 616.58 |
| G304 | 11/16/2015 | 623.78 |
| G304 | 02/08/2016 | 624.07 |
| G304 | 05/09/2016 | 623.91 |
| G304 | 07/25/2016 | 626.72 |
| G305 | 05/09/2016 | 618.48 |
| G305 | 07/01/2016 | 616.28 |
| G305 | 07/25/2016 | 618.24 |
| G305 | 09/29/2016 | 617.33 |
| G305 | 11/12/2016 | 618.06 |
| G305 | 02/04/2017 | 620.49 |
| G305 | 05/13/2017 | 618.27 |
| G305 | 07/08/2017 | 618.28 |
| G305 | 10/21/2017 | 615.30 |
| G305 | 05/08/2018 | 617.87 |
| G305 | 08/02/2018 | 617.79 |
| G305 | 10/23/2018 | 616.56 |
| G305 | 01/15/2019 | 616.95 |
| G305 | 08/05/2019 | 616.85 |
| G305 | 01/20/2020 | 619.36 |
| G305 | 08/10/2020 | 617.02 |
| G305 | 01/20/2021 | 618.63 |
| G305 | 04/20/2021 | 618.77 |
| G305 | 05/03/2021 | 619.11 |
| G305 | 05/17/2021 | 618.90 |
| G305 | 06/09/2021 | 618.04 |
| G305 | 06/23/2021 | 616.94 |
| G305 | 07/12/2021 | 618.55 |
| G305 | 07/26/2021 | 618.18 |
| G305 | 08/16/2021 | 618.31 |
| G306 | 05/09/2016 | 619.74 |
| G306 | 07/01/2016 | 615.11 |
| G306 | 07/25/2016 | 619.26 |
| G306 | 09/29/2016 | 617.64 |
| G306 | 11/12/2016 | 618.77 |
| G306 | 02/04/2017 | 618.97 |
| G306 | 05/13/2017 | 619.03 |
| G306 | 07/08/2017 | 619.45 |
| G306 | 10/21/2017 | 616.12 |
| G306 | 05/08/2018 | 618.96 |
| G306 | 08/02/2018 | 621.73 |
| G306 | 10/23/2018 | 617.24 |
| 3300 | 10/23/2010 | V1/12T |



| _ | 1 | |
|-----------------|-------------|-----------------------------------|
| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
| G306 | 01/15/2019 | 618.56 |
| G306 | 08/05/2019 | 619.18 |
| G306 | 01/20/2020 | 620.28 |
| G306 | 08/10/2020 | 617.26 |
| G306 | 01/20/2021 | 619.17 |
| G306 | 01/26/2021 | 618.98 |
| G306 | 03/29/2021 | 620.42 |
| G306 | 04/20/2021 | 619.30 |
| G306 | 04/21/2021 | 619.53 |
| G306 | 05/03/2021 | 619.96 |
| G306 | 05/05/2021 | 620.27 |
| G306 | 05/17/2021 | 619.44 |
| G306 | 05/18/2021 | 619.56 |
| G306 | 06/09/2021 | 618.04 |
| G306 | 06/15/2021 | 617.29 |
| G306 | 06/23/2021 | 616.32 |
| G306 | 06/28/2021 | 618.31 |
| G306 | 07/12/2021 | 620.59 |
| G306 | 07/14/2021 | 620.17 |
| G306 | 07/26/2021 | 618.84 |
| G306 | 07/27/2021 | 618.70 |
| G306 | 08/16/2021 | 618.92 |
| G307 | 07/25/2016 | 624.30 |
| G307 | 09/29/2016 | 623.85 |
| G307 | 11/12/2016 | 624.44 |
| G307 | 02/04/2017 | 624.60 |
| G307 | 05/13/2017 | 624.56 |
| G307 | 07/08/2017 | 623.55 |
| G307 | 10/21/2017 | 624.60 |
| G307 | 05/08/2018 | 624.37 |
| G307 | 08/02/2018 | 619.33 |
| G307 | 10/23/2018 | 623.95 |
| G307 | 01/15/2019 | 624.31 |
| G307 | 08/05/2019 | 624.21 |
| G307 | 05/06/2020 | 624.72 |
| G307 | 08/10/2020 | 624.36 |
| G307 | 01/20/2021 | 624.10 |
| G307 | 01/27/2021 | 624.10 |
| G307 | 04/20/2021 | 624.50 |
| G307 | 05/17/2021 | 624.45 |
| G307 | 07/12/2021 | 624.45 |
| G307 | 08/16/2021 | 624.46 |
| G307D | 03/29/2021 | 622.43 |
| G307D | 04/20/2021 | 622.48 |
| G307D | 04/21/2021 | 622.46 |
| G307D | 05/03/2021 | 622.47 |
| | | |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G307D | 05/04/2021 | 622.44 |
| G307D | 05/17/2021 | 622.44 |
| G307D | 05/18/2021 | 622.46 |
| G307D | 06/09/2021 | 622.43 |
| G307D | 06/15/2021 | 622.42 |
| G307D | 06/23/2021 | 622.42 |
| G307D | 07/12/2021 | 622.59 |
| G307D | 07/26/2021 | 622.26 |
| G307D | 07/27/2021 | 622.51 |
| G307D | 08/16/2021 | 621.49 |
| G308 | 03/29/2021 | 621.03 |
| G308 | 04/20/2021 | 619.67 |
| G308 | 04/21/2021 | 620.15 |
| G308 | 05/03/2021 | 620.04 |
| G308 | 05/05/2021 | 621.01 |
| G308 | 05/17/2021 | 619.93 |
| G308 | 06/09/2021 | 619.17 |
| G308 | 06/14/2021 | 619.06 |
| G308 | 06/23/2021 | 618.54 |
| G308 | 06/28/2021 | 620.44 |
| G308 | 07/12/2021 | 620.22 |
| G308 | 07/14/2021 | 620.67 |
| G308 | 07/26/2021 | 619.68 |
| G308 | 07/27/2021 | 619.44 |
| G308 | 08/16/2021 | 619.45 |
| G309 | 03/29/2021 | 621.09 |
| G309 | 04/20/2021 | 618.88 |
| G309 | 04/21/2021 | 618.88 |
| G309 | 04/22/2021 | 618.88 |
| G309 | 05/03/2021 | 619.04 |
| G309 | 05/05/2021 | 619.84 |
| G309 | 05/17/2021 | 618.83 |
| G309 | 06/09/2021 | 618.43 |
| G309 | 06/14/2021 | 618.25 |
| G309 | 06/23/2021 | 617.89 |
| G309 G309 | 06/23/2021 | 618.95 |
| G309 G309 | 07/12/2021 | 619.31 |
| | | |
| G309 | 07/13/2021 | 620.17 |
| G309 | 07/26/2021 | 618.88 |
| G309 | 07/27/2021 | 618.78 |
| G309 | 08/16/2021 | 618.91 |
| G310 | 03/29/2021 | 617.27 |
| G310 | 04/20/2021 | 614.41 |
| G310 | 04/22/2021 | 614.40 |
| G310 | 05/03/2021 | 614.61 |
| G310 | 05/04/2021 | 615.01 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G310 | 05/17/2021 | 614.47 |
| G310 | 05/19/2021 | 616.01 |
| G310 | 06/09/2021 | 613.83 |
| G310 | 06/15/2021 | 613.54 |
| G310 | 06/23/2021 | 613.20 |
| G310 | 06/28/2021 | 614.15 |
| G310 | 07/12/2021 | 614.81 |
| G310 | 07/13/2021 | 615.88 |
| G310 | 07/26/2021 | 614.13 |
| G310 | 07/28/2021 | 614.00 |
| G310 | 08/16/2021 | 614.29 |
| G311 | 03/29/2021 | 616.54 |
| G311 | 03/30/2021 | 616.21 |
| G311 | 04/20/2021 | 613.75 |
| G311 | 04/22/2021 | 613.68 |
| G311 | 05/03/2021 | 614.01 |
| G311 | 05/04/2021 | 615.13 |
| G311 | 05/17/2021 | 613.86 |
| G311 | 05/19/2021 | 615.78 |
| G311 | 06/09/2021 | 613.13 |
| G311 | 06/15/2021 | 612.78 |
| G311 | 06/23/2021 | 612.45 |
| G311 | 06/29/2021 | 613.31 |
| G311 | 07/12/2021 | 613.75 |
| G311 | 07/14/2021 | 615.37 |
| G311 | 07/26/2021 | 613.05 |
| G311 | 07/27/2021 | 612.94 |
| G311 | 08/16/2021 | 613.30 |
| G311D | 03/29/2021 | 575.42 |
| G311D | 03/30/2021 | 575.73 |
| G311D | 04/20/2021 | 575.29 |
| G311D | 04/22/2021 | 575.74 |
| G311D | 05/03/2021 | 573.09 |
| G311D | 05/04/2021 | 573.23 |
| G311D | 05/17/2021 | 572.40 |
| G311D | 05/19/2021 | 572.91 |
| G311D | 06/09/2021 | 573.85 |
| G311D | 06/15/2021 | 575.25 |
| G311D G311D | 06/23/2021 | 571.74 |
| G311D G311D | 07/12/2021 | 571.63 |
| G311D G311D | 07/12/2021 | 569.74 |
| | | |
| G311D | 07/28/2021 | 569.98 |
| G311D | 08/16/2021 | 570.34 |
| G312 | 03/29/2021 | 612.19 |
| G312 | 03/30/2021 | 611.97 |
| G312 | 04/20/2021 | 609.11 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G312 | 04/22/2021 | 608.97 |
| G312 | 05/03/2021 | 609.47 |
| G312 | 05/04/2021 | 610.07 |
| G312 | 05/17/2021 | 609.27 |
| G312 | 05/19/2021 | 610.89 |
| G312 | 06/09/2021 | 608.31 |
| G312 | 06/15/2021 | 607.64 |
| G312 | 06/23/2021 | 606.99 |
| G312 | 06/29/2021 | 608.07 |
| G312 | 07/12/2021 | 608.70 |
| G312 | 07/13/2021 | 610.23 |
| G312 | 07/26/2021 | 608.56 |
| G312 | 07/27/2021 | 608.47 |
| G312 | 08/16/2021 | 609.09 |
| G313 | 03/29/2021 | 611.78 |
| G313 | 03/30/2021 | 611.75 |
| G313 | 04/20/2021 | 611.46 |
| G313 | 04/22/2021 | 611.41 |
| G313 | 05/03/2021 | 611.68 |
| G313 | 05/04/2021 | 611.66 |
| G313 | 05/17/2021 | 611.62 |
| G313 | 05/18/2021 | 611.66 |
| G313 | 06/09/2021 | 611.57 |
| G313 | 06/14/2021 | 611.55 |
| G313 | 06/23/2021 | 611.29 |
| G313 | 06/28/2021 | 611.58 |
| G313 | 07/12/2021 | 611.70 |
| G313 | 07/13/2021 | 611.81 |
| G313 | 07/26/2021 | 611.71 |
| G313 | 07/27/2021 | 611.73 |
| G313 | 08/16/2021 | 611.90 |
| G314 | 03/29/2021 | 596.40 |
| G314 | 03/30/2021 | 597.11 |
| G314 | 04/20/2021 | 603.16 |
| G314 | 04/21/2021 | 603.48 |
| G314 | 05/03/2021 | 604.66 |
| G314 | 05/04/2021 | 604.64 |
| G314 | 05/17/2021 | 605.61 |
| G314 | 06/09/2021 | 607.54 |
| G314 | 06/14/2021 | 608.16 |
| G314 | 06/23/2021 | 605.19 |
| G314 | 06/28/2021 | 606.45 |
| G314 | 07/12/2021 | 605.32 |
| G314 | 07/13/2021 | 605.60 |
| G314 | 07/26/2021 | 606.66 |
| G314 | 07/27/2021 | 606.84 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G314 | 08/16/2021 | 608.60 |
| G314D | 03/29/2021 | 572.75 |
| G314D | 03/30/2021 | 573.05 |
| G314D | 04/20/2021 | 571.76 |
| G314D | 04/21/2021 | 571.95 |
| G314D | 05/03/2021 | 568.77 |
| G314D | 05/04/2021 | 568.95 |
| G314D | 05/17/2021 | 566.84 |
| G314D | 05/19/2021 | 566.84 |
| G314D | 06/09/2021 | 567.45 |
| G314D | 06/14/2021 | 568.60 |
| G314D | 06/23/2021 | 566.77 |
| G314D | 07/12/2021 | 566.88 |
| G314D | 07/26/2021 | 566.65 |
| G314D | 07/28/2021 | 566.75 |
| G314D | 08/16/2021 | 567.28 |
| G315 | 03/29/2021 | 621.24 |
| G315 | 03/30/2021 | 621.20 |
| G315 | 04/20/2021 | 621.05 |
| G315 | 04/22/2021 | 621.12 |
| G315 | 05/03/2021 | 621.13 |
| G315 | 05/05/2021 | 621.25 |
| G315 | 05/17/2021 | 621.14 |
| G315 | 05/18/2021 | 621.34 |
| G315 | 06/09/2021 | 620.24 |
| G315 | 06/15/2021 | 619.70 |
| G315 | 06/23/2021 | 619.17 |
| G315 | 06/29/2021 | 621.04 |
| G315 | 07/12/2021 | 620.91 |
| G315 | 07/14/2021 | 621.13 |
| G315 | 07/26/2021 | 620.42 |
| G315 | 07/28/2021 | 620.44 |
| G315 | 08/16/2021 | 620.29 |
| G316 | 03/29/2021 | 591.63 |
| G316 | 03/30/2021 | 591.55 |
| G316 | 04/20/2021 | 591.23 |
| G316 | 04/22/2021 | 591.31 |
| G316 | 05/03/2021 | 591.39 |
| G316 | 05/05/2021 | 591.63 |
| G316 | 05/03/2021 | 591.28 |
| G316 | 06/09/2021 | 581.54 |
| G316 G316 | 06/09/2021 | 590.61 |
| G316 G316 | 06/14/2021 | 590.06 |
| | 06/23/2021 | |
| G316 | 1 | 591.40 |
| G316 | 07/12/2021 | 591.16 |
| G316 | 07/13/2021 | 591.50 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G316 | 07/26/2021 | 590.73 |
| G316 | 07/27/2021 | 590.68 |
| G316 | 08/16/2021 | 590.59 |
| G317 | 03/29/2021 | 610.40 |
| G317 | 03/30/2021 | 610.89 |
| G317 | 04/20/2021 | 610.94 |
| G317 | 04/22/2021 | 610.84 |
| G317 | 05/03/2021 | 611.75 |
| G317 | 05/05/2021 | 611.15 |
| G317 | 05/17/2021 | 611.65 |
| G317 | 05/18/2021 | 611.57 |
| G317 | 06/09/2021 | 610.59 |
| G317 | 06/15/2021 | 609.63 |
| G317 | 06/23/2021 | 606.57 |
| G317 | 06/28/2021 | 608.25 |
| G317 | 07/12/2021 | 607.93 |
| G317 | 07/13/2021 | 607.92 |
| G317 | 07/26/2021 | 608.27 |
| G317 | 07/28/2021 | 608.11 |
| G317 | 08/16/2021 | 608.46 |
| G401 | 11/16/2015 | 607.82 |
| G401 | 02/08/2016 | 608.14 |
| G401 | 05/09/2016 | 608.00 |
| G401 | 07/25/2016 | 608.47 |
| G401 | 11/12/2016 | 607.84 |
| G401 | 02/04/2017 | 609.74 |
| G401 | 05/13/2017 | 608.52 |
| G401 | 07/08/2017 | 609.19 |
| G401 | 05/08/2018 | 609.37 |
| G401 | 08/02/2018 | 609.80 |
| G401 | 10/23/2018 | 608.42 |
| G401 | 01/15/2019 | 608.36 |
| G401 | 08/05/2019 | 608.45 |
| G401 | 01/20/2020 | 607.25 |
| G401 | 05/06/2020 | 607.02 |
| G401 | 08/10/2020 | 606.77 |
| G401 | 01/29/2021 | 604.22 |
| G401 | 04/20/2021 | 604.14 |
| G401 G401 | 07/26/2021 | 603.94 |
| G401 G401 | 08/16/2021 | 604.04 |
| G401 G402 | 11/16/2015 | 604.02 |
| | 02/08/2016 | |
| G402 | · · | 604.90 |
| G402 | 05/09/2016 | 605.18 |
| G402 | 07/25/2016 | 604.33 |
| G402 | 11/12/2016 | 604.24 |
| G402 | 02/04/2017 | 604.43 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| | | |
| G402 | 05/13/2017 | 604.83 |
| G402 | 07/08/2017 | 604.42 |
| G402 | 10/21/2017 | 600.77 |
| G402 | 05/08/2018 | 605.36 |
| G402 | 08/02/2018 | 603.82 |
| G402 | 10/23/2018 | 602.25 |
| G402 | 01/15/2019 | 602.37 |
| G402 | 08/05/2019 | 603.82 |
| G402 | 01/20/2020 | 605.12 |
| G402 | 08/10/2020 | 602.09 |
| G402 | 01/20/2021 | 603.01 |
| G402 | 01/28/2021 | 603.01 |
| G402 | 04/20/2021 | 603.78 |
| G402 | 07/26/2021 | 602.83 |
| G402 | 08/16/2021 | 603.29 |
| G403 | 11/16/2015 | 621.81 |
| G403 | 02/08/2016 | 621.78 |
| G403 | 05/09/2016 | 621.76 |
| G403 | 07/25/2016 | 622.16 |
| G403 | 11/12/2016 | 621.80 |
| G403 | 02/04/2017 | 622.45 |
| G403 | 05/13/2017 | 622.26 |
| G403 | 07/08/2017 | 622.16 |
| G403 | 10/21/2017 | 618.36 |
| G403 | 05/08/2018 | 621.66 |
| G403 | 08/02/2018 | 622.38 |
| G403 | 10/23/2018 | 619.48 |
| G403 | 01/15/2019 | 620.51 |
| G403 | 08/05/2019 | 621.64 |
| G403 | 01/20/2020 | 621.63 |
| G403 | 08/10/2020 | 621.14 |
| G403 | 01/20/2021 | 619.88 |
| G403 | 01/21/2021 | 619.88 |
| G403 | 04/20/2021 | 619.41 |
| G403 | 07/26/2021 | 619.56 |
| G403 | 08/16/2021 | 619.27 |
| G404 | 11/16/2015 | 611.67 |
| G404 | 02/08/2016 | 611.58 |
| G404 | 05/09/2016 | 611.46 |
| G404 | 07/25/2016 | 611.67 |
| G404 | 11/12/2016 | 610.58 |
| G404 | 02/04/2017 | 610.57 |
| G404 | 05/13/2017 | 610.87 |
| G404 | 07/08/2017 | 611.75 |
| G404 | 10/21/2017 | 607.58 |
| G404 | 05/08/2018 | 611.42 |
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| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G404 | 08/02/2018 | 610.55 |
| G404 | 10/23/2018 | 608.59 |
| G404 | 01/15/2019 | 608.98 |
| G404 | 08/05/2019 | 611.60 |
| G404 | 01/20/2020 | 612.14 |
| G404 | 08/10/2020 | 610.37 |
| G404 | 01/20/2021 | 611.63 |
| G404 | 01/21/2021 | 611.63 |
| G404 | 04/20/2021 | 611.51 |
| G404 | 07/26/2021 | 611.29 |
| G404 | 08/16/2021 | 610.95 |
| G405 | 11/16/2015 | 618.85 |
| G405 | 02/08/2016 | 618.90 |
| G405 | 05/09/2016 | 618.99 |
| G405 | 07/25/2016 | 618.51 |
| G405 | 11/12/2016 | 618.48 |
| G405 | 02/04/2017 | 618.47 |
| G405 | 05/13/2017 | 618.74 |
| G405 | 07/08/2017 | 618.54 |
| G405 | 10/21/2017 | 614.47 |
| G405 | 05/08/2018 | 618.94 |
| G405 | 08/02/2018 | 617.55 |
| G405 | 10/23/2018 | 616.40 |
| G405 | 01/15/2019 | 616.81 |
| G405 | 08/05/2019 | 617.72 |
| G405 | 01/20/2020 | 619.28 |
| G405 | 08/10/2020 | 617.62 |
| G405 | 01/20/2021 | 617.12 |
| G405 | 01/21/2021 | 617.12 |
| G405 | 04/20/2021 | 617.13 |
| G405 | 07/26/2021 | 617.37 |
| G405 | 08/16/2021 | 617.28 |
| G406 | 11/12/2016 | 616.01 |
| G406 | 02/04/2017 | 617.52 |
| G406 | 05/13/2017 | 616.20 |
| G406 | 07/08/2017 | 616.29 |
| G406 | 10/21/2017 | 611.27 |
| | | |
| G406 | 05/08/2018 | 615.47 |
| G406 | 08/02/2018 | 615.75 |
| G406 | 10/23/2018 | 614.11 |
| G406 | 01/15/2019 | 615.36 |
| G406 | 08/05/2019 | 616.50 |
| G406 | 01/20/2020 | 617.48 |
| G406 | 08/10/2020 | 615.54 |
| G406 | 01/20/2021 | 612.97 |
| G406 | 04/20/2021 | 613.78 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| G406 | 07/26/2021 | 614.20 |
| G406 | 08/16/2021 | 613.82 |
| G407 | 11/12/2016 | 613.27 |
| G407 | 02/04/2017 | 613.41 |
| G407 | 05/13/2017 | 613.68 |
| G407 | 07/08/2017 | 613.59 |
| G407 | 10/21/2017 | 612.67 |
| G407 | 05/08/2018 | 613.11 |
| G407 | 08/02/2018 | 612.95 |
| G407 | 10/23/2018 | 612.11 |
| G407 | 01/15/2019 | 612.31 |
| G407 | 08/05/2019 | 614.02 |
| G407 | 01/20/2020 | 614.86 |
| G407 | 08/10/2020 | 613.74 |
| G407 | 01/20/2021 | 614.70 |
| G407 | 04/20/2021 | 614.49 |
| G407 | 07/26/2021 | 614.38 |
| G407 | 08/16/2021 | 614.41 |
| G410 | 10/23/2018 | 610.41 |
| G410 | 01/15/2019 | 610.91 |
| G410 | 08/05/2019 | 611.75 |
| G410 | 01/20/2020 | 612.70 |
| G410 | 08/10/2020 | 610.88 |
| G410 | 01/20/2021 | 610.91 |
| G410 | 04/20/2021 | 611.38 |
| G410 | 07/26/2021 | 611.51 |
| G410 | 08/16/2021 | 611.29 |
| G411 | 10/23/2018 | 613.20 |
| G411 | 01/15/2019 | 613.82 |
| G411 | 08/05/2019 | 614.25 |
| G411 | 01/20/2020 | 617.53 |
| G411 | 08/10/2020 | 615.51 |
| G411 | 01/20/2021 | 615.91 |
| G411 | 04/20/2021 | 616.12 |
| G411 | 07/26/2021 | 616.20 |
| G411 | 08/16/2021 | 616.03 |
| MW03D | 04/20/2021 | 597.90 |
| MW03D | 05/03/2021 | 598.18 |
| MW03D | 05/17/2021 | 598.06 |
| MW03D | 06/09/2021 | 598.13 |
| MW03D | 06/23/2021 | 598.09 |
| MW03D | 07/12/2021 | 598.09 |
| MW03D MW03D | 07/12/2021 | 598.12 |
| MW03D MW03D | 08/16/2021 | 598.09 |
| | | |
| MW04S | 02/08/2016 | 621.62 |
| MW04S | 05/09/2016 | 620.45 |



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|-----------------|-------------|-----------------------------------|
| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
| MW04S | 07/25/2016 | 618.84 |
| MW04S | 11/12/2016 | 618.66 |
| MW04S | 02/04/2017 | 618.97 |
| MW04S | 05/13/2017 | 618.76 |
| MW04S | 07/08/2017 | 618.92 |
| MW04S | 10/21/2017 | 613.88 |
| MW04S | 05/08/2018 | 617.95 |
| MW04S | 08/02/2018 | 618.73 |
| MW04S | 10/23/2018 | 614.68 |
| MW04S | 01/15/2019 | 614.89 |
| MW04S | 08/05/2019 | 614.92 |
| MW04S | 01/20/2020 | 619.93 |
| MW04S | 08/10/2020 | 617.74 |
| MW04S | 01/20/2021 | 620.63 |
| MW04S | 04/20/2021 | 619.39 |
| MW04S | 07/26/2021 | 618.55 |
| MW04S | 08/16/2021 | 618.50 |
| MW05S | 02/08/2016 | 620.92 |
| MW05S | 05/09/2016 | 620.53 |
| MW05S | 07/25/2016 | 618.20 |
| MW05S | 11/12/2016 | 617.38 |
| MW05S | 02/04/2017 | 618.78 |
| MW05S | 05/13/2017 | 617.95 |
| MW05S | 07/08/2017 | 618.81 |
| MW05S | 10/21/2017 | 613.32 |
| MW05S | 05/08/2018 | 617.77 |
| MW05S | 08/02/2018 | 617.98 |
| MW05S | 10/23/2018 | 615.35 |
| MW05S | 01/15/2019 | 615.93 |
| MW05S | 08/05/2019 | 616.01 |
| MW05S | 01/20/2020 | 620.34 |
| MW05S | 08/10/2020 | 617.09 |
| MW05S | 01/20/2021 | 618.33 |
| MW05S | 04/20/2021 | 619.07 |
| MW05S | 07/26/2021 | 618.14 |
| MW05S | 08/16/2021 | 617.84 |
| MW10S | 02/08/2016 | 620.43 |
| MW10S | 05/09/2016 | 619.47 |
| MW10S | 07/25/2016 | 617.69 |
| MW10S | 11/12/2016 | 616.69 |
| MW10S | 02/04/2017 | 617.41 |
| MW10S | 05/13/2017 | 617.22 |
| MW10S | 07/08/2017 | 617.27 |
| MW10S | 10/21/2017 | 614.52 |
| MW10S | 05/08/2018 | 616.89 |
| MW10S | 08/02/2018 | 617.52 |
| | . , | |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| MW10S | 10/23/2018 | 614.36 |
| MW10S | 01/15/2019 | 614.85 |
| MW10S | 08/05/2019 | 615.56 |
| MW10S | 08/10/2020 | 617.11 |
| MW10S | 01/20/2021 | 619.48 |
| MW10S | 04/20/2021 | 619.03 |
| MW10S | 07/26/2021 | 617.74 |
| MW10S | 08/16/2021 | 617.35 |
| MW11S | 02/08/2016 | 621.30 |
| MW11S | 05/09/2016 | 622.19 |
| MW11S | 07/25/2016 | 620.99 |
| MW11S | 11/12/2016 | 620.92 |
| MW11S | 02/04/2017 | 620.82 |
| MW11S | 05/13/2017 | 621.31 |
| MW11S | 07/08/2017 | 620.85 |
| MW11S | 10/21/2017 | 617.19 |
| MW11S | 05/08/2018 | 620.85 |
| MW11S | 08/02/2018 | 620.69 |
| MW11S | 10/23/2018 | 620.05 |
| MW11S | 01/15/2019 | 620.38 |
| MW11S | 08/05/2019 | 620.76 |
| MW11S | 01/20/2020 | 621.80 |
| MW11S | 08/10/2020 | 618.12 |
| MW11S | 01/20/2021 | 619.64 |
| MW11S | 04/20/2021 | 621.76 |
| MW11S | 05/03/2021 | 622.01 |
| MW11S | 05/17/2021 | 621.94 |
| MW11S | 06/09/2021 | 621.45 |
| MW11S | 06/23/2021 | 618.83 |
| MW11S | 07/12/2021 | 620.54 |
| MW11S | 07/26/2021 | 620.97 |
| MW11S | 08/16/2021 | 621.49 |
| MW11D | 04/20/2021 | 621.13 |
| MW11D | 05/03/2021 | 621.36 |
| MW11D | 05/17/2021 | 621.27 |
| MW11D | 06/09/2021 | 620.96 |
| MW11D | 06/23/2021 | 618.72 |
| MW11D | 07/12/2021 | 619.88 |
| MW11D MW11D | 07/12/2021 | 620.57 |
| MW11D MW11D | 08/16/2021 | 621.01 |
| | | |
| MW12S | 02/08/2016 | 620.37 |
| MW12S | 05/09/2016 | 620.48 |
| MW12S | 07/25/2016 | 618.53 |
| MW12S | 11/12/2016 | 617.97 |
| MW12S | 02/04/2017 | 620.33 |
| MW12S | 05/13/2017 | 618.26 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| MW12S | 07/08/2017 | 618.61 |
| MW12S | 10/21/2017 | 615.08 |
| MW12S | 05/08/2018 | 617.58 |
| MW12S | 08/02/2018 | 617.12 |
| MW12S | 10/23/2018 | 616.14 |
| MW12S | 01/15/2019 | 616.89 |
| MW12S | 08/05/2019 | 617.35 |
| MW12S | 01/20/2020 | 620.34 |
| MW12S | 08/10/2020 | 615.69 |
| MW12S | 01/20/2021 | 611.42 |
| MW12S | 04/20/2021 | 618.96 |
| MW12S | 05/03/2021 | 619.66 |
| MW12S | 05/17/2021 | 619.23 |
| MW12S | 06/09/2021 | 618.20 |
| MW12S | 06/23/2021 | 616.52 |
| MW12S | 07/12/2021 | 619.35 |
| MW12S | 07/26/2021 | 618.43 |
| MW12S | 08/16/2021 | 618.79 |
| MW12D | 04/20/2021 | 611.97 |
| MW12D | 05/03/2021 | 611.87 |
| MW12D | 05/17/2021 | 611.95 |
| MW12D | 06/09/2021 | 611.87 |
| MW12D | | 611.79 |
| | 06/23/2021 | |
| MW12D | 07/12/2021 | 611.55 |
| MW12D | 07/26/2021 | 611.50 |
| MW12D | 08/16/2021 | 611.51 |
| MW16S | 02/08/2016 | 625.29 |
| MW16S | 05/09/2016 | 624.54 |
| MW16S | 07/25/2016 | 622.13 |
| MW16S | 11/12/2016 | 622.26 |
| MW16S | 02/04/2017 | 622.53 |
| MW16S | 05/13/2017 | 622.53 |
| MW16S | 07/08/2017 | 622.25 |
| MW16S | 10/21/2017 | 618.42 |
| MW16S | 05/08/2018 | 622.02 |
| MW16S | 08/02/2018 | 622.47 |
| MW16S | 10/23/2018 | 620.88 |
| MW16S | 01/15/2019 | 621.60 |
| MW16S | 08/05/2019 | 621.94 |
| MW16S | 01/20/2020 | 625.59 |
| MW16S | 08/10/2020 | 618.52 |
| MW16S | 01/20/2021 | 618.34 |
| MW16S | 04/20/2021 | 623.78 |
| MW16S | 05/03/2021 | 624.58 |
| MW16S | 05/17/2021 | 623.87 |
| MW16S | 06/09/2021 | 622.57 |
| | | |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| MW16S | 06/23/2021 | 620.48 |
| MW16S | 07/12/2021 | 620.58 |
| MW16S | 07/26/2021 | 620.68 |
| MW16S | 08/16/2021 | 620.65 |
| MW16D | 04/20/2021 | 615.42 |
| MW16D | 05/03/2021 | 615.92 |
| MW16D | 05/17/2021 | 616.36 |
| MW16D | 06/09/2021 | 616.87 |
| MW16D | 06/23/2021 | 616.90 |
| MW16D | 07/12/2021 | 616.76 |
| MW16D | 07/26/2021 | 616.63 |
| MW16D | 08/16/2021 | 616.35 |
| MW20S | 02/08/2016 | 614.36 |
| MW20S | 05/09/2016 | 614.09 |
| MW20S | 07/25/2016 | 611.61 |
| MW20S | 11/12/2016 | 611.51 |
| MW20S | 02/04/2017 | 612.76 |
| MW20S | 05/13/2017 | 611.86 |
| MW20S | 07/08/2017 | 611.75 |
| MW20S | 10/21/2017 | 607.74 |
| MW20S | 05/08/2018 | 611.46 |
| MW20S | 08/02/2018 | 611.51 |
| MW20S | 10/23/2018 | 609.55 |
| MW20S | 01/15/2019 | 610.21 |
| MW20S | 08/05/2019 | 610.81 |
| MW20S | 01/20/2020 | 615.40 |
| MW20S | 08/10/2020 | 612.37 |
| MW20S | 01/20/2021 | 612.27 |
| MW20S | 04/20/2021 | 613.45 |
| MW20S | 07/26/2021 | 613.35 |
| MW20S | 08/16/2021 | 612.31 |
| R104 | 01/20/2015 | 623.03 |
| R104 | 04/08/2015 | 624.77 |
| R104 | 10/06/2015 | 621.69 |
| R104 | 11/16/2015 | 621.34 |
| R104 | 02/08/2016 | 624.11 |
| R104 | 05/09/2016 | 624.89 |
| | | |
| R104 | 07/25/2016 | 623.65 |
| R104 | 11/12/2016 | 623.49 |
| R104 | 02/04/2017 | 624.20 |
| R104 | 05/13/2017 | 622.91 |
| R104 | 07/08/2017 | 624.09 |
| R104 | 10/21/2017 | 619.38 |
| R104 | 05/08/2018 | 622.66 |
| R104 | 08/02/2018 | 621.73 |
| R104 | 10/23/2018 | 621.58 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| R104 | 01/15/2019 | 622.43 |
| R104 | 08/05/2019 | 623.34 |
| R104 | 01/20/2020 | 625.63 |
| R104 | 08/10/2020 | 624.56 |
| R104 | 10/15/2020 | 621.10 |
| R104 | 01/20/2021 | 623.31 |
| R104 | 01/28/2021 | 620.57 |
| R104 | 04/20/2021 | 624.95 |
| R104 | 07/26/2021 | 625.41 |
| R104 | 08/16/2021 | 625.92 |
| R201 | 10/05/2015 | 619.94 |
| R201 | 11/16/2015 | 622.44 |
| R201 | 02/08/2016 | 623.40 |
| R201 | 05/09/2016 | 622.81 |
| R201 | 07/25/2016 | 622.36 |
| R201 | 11/12/2016 | 622.82 |
| R201 | 02/04/2017 | 622.27 |
| R201 | 05/13/2017 | 623.05 |
| R201 | 07/08/2017 | 622.31 |
| R201 | 10/21/2017 | 618.30 |
| R201 | 01/25/2018 | 622.00 |
| R201 | 05/08/2018 | 622.78 |
| R201 | 08/02/2018 | 622.16 |
| R201 | 10/23/2018 | 621.29 |
| R201 | 01/15/2019 | 622.17 |
| R201 | 08/05/2019 | 622.35 |
| R201 | 01/20/2020 | 622.88 |
| R201 | 08/10/2020 | 618.89 |
| R201 | 10/13/2020 | 616.57 |
| R201 | 01/20/2021 | 620.52 |
| R201 | 01/29/2021 | 620.52 |
| R201 | 03/29/2021 | 623.52 |
| R201 | 04/20/2021 | 622.16 |
| R201 | 04/20/2021 | 622.59 |
| R201 | 05/03/2021 | 622.91 |
| R201 | 05/03/2021 | 623.40 |
| R201 R201 | 05/06/2021 | 622.68 |
| | | |
| R201 | 06/09/2021 | 621.12 |
| R201 | 06/14/2021 | 620.63 |
| R201 | 06/23/2021 | 619.92 |
| R201 | 06/29/2021 | 621.16 |
| R201 | 07/12/2021 | 621.34 |
| R201 | 07/13/2021 | 621.36 |
| R201 | 07/26/2021 | 620.37 |
| R201 | 07/28/2021 | 620.16 |
| R201 | 08/16/2021 | 620.61 |



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|-----------------|-------------|-----------------------------------|
| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
| R205 | 05/08/2018 | 618.32 |
| R205 | 08/02/2018 | 614.95 |
| R205 | 10/23/2018 | 618.85 |
| R205 | 01/15/2019 | 619.54 |
| R205 | 08/05/2019 | 620.13 |
| R205 | 01/20/2020 | 620.21 |
| R205 | 08/10/2020 | 615.92 |
| R205 | 10/14/2020 | 613.87 |
| R205 | 01/20/2021 | 617.80 |
| R205 | 01/28/2021 | 618.45 |
| R205 | 04/20/2021 | 619.12 |
| R205 | 07/26/2021 | 618.66 |
| R205 | 08/16/2021 | 618.99 |
| T127 | 01/19/2015 | 615.65 |
| T127 | 04/08/2015 | 616.04 |
| T127 | 07/23/2015 | 616.04 |
| T127 | 10/06/2015 | 615.66 |
| T127 | 11/16/2015 | 615.91 |
| T127 | 02/08/2016 | 616.04 |
| T127 | 05/09/2016 | 616.15 |
| T127 | 07/25/2016 | 615.96 |
| T127 | 11/12/2016 | 616.73 |
| T127 | 02/04/2017 | 616.32 |
| T127 | 05/13/2017 | 616.89 |
| T127 | 07/08/2017 | 615.99 |
| T127 | 10/21/2017 | 612.33 |
| T127 | 01/27/2018 | 611.06 |
| T127 | 05/08/2018 | 616.66 |
| T127 | 08/02/2018 | 616.48 |
| T127 | 10/23/2018 | 614.78 |
| T127 | 01/15/2019 | 615.13 |
| T127 | 05/03/2019 | 617.26 |
| T127 | 08/05/2019 | 615.15 |
| T127 | 01/20/2020 | 617.05 |
| T127 | 05/05/2020 | 617.02 |
| T127 | 08/10/2020 | 615.90 |
| T127 | 10/14/2020 | 615.08 |
| T127 | 01/20/2021 | 615.89 |
| T127 | 01/29/2021 | 615.89 |
| T127 | 04/20/2021 | 616.54 |
| T127 | 06/29/2021 | 616.72 |
| T127 | 07/26/2021 | 616.53 |
| T127 | 08/16/2021 | 616.65 |
| T128 | 01/19/2015 | 614.73 |
| T128 | 04/08/2015 | 614.89 |
| T128 | 07/23/2015 | 615.40 |
| | 1 | |



| | , | |
|-----------------|--------------|-----------------------------------|
| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
| T128 | 10/06/2015 | 614.67 |
| T128 | 02/08/2016 | 614.90 |
| T128 | 05/09/2016 | 615.01 |
| T128 | 07/25/2016 | 614.75 |
| T128 | 11/12/2016 | 614.95 |
| T128 | 02/04/2017 | 616.00 |
| T128 | 05/13/2017 | 615.39 |
| T128 | 07/08/2017 | 615.07 |
| T128 | 10/21/2017 | 611.33 |
| T128 | 05/08/2018 | 615.13 |
| T128 | 08/02/2018 | 614.87 |
| T128 | 10/23/2018 | 613.17 |
| T128 | 01/15/2019 | 613.94 |
| T128 | 08/05/2019 | 613.99 |
| T128 | 01/20/2020 | 617.25 |
| T128 | 08/10/2020 | 616.15 |
| T128 | 10/14/2020 | 615.36 |
| T128 | 01/20/2021 | 616.20 |
| T128 | 01/28/2021 | 616.33 |
| T128 | 04/20/2021 | 616.94 |
| T128 | 07/26/2021 | 616.81 |
| T128 | 08/16/2021 | 616.93 |
| T202 | 02/08/2016 | 622.82 |
| T202 | 05/09/2016 | 623.66 |
| T202 | 07/25/2016 | 619.49 |
| T202 | 11/12/2016 | 619.88 |
| T202 | 02/04/2017 | 619.73 |
| T202 | 05/13/2017 | 620.07 |
| T202 | 07/08/2017 | 619.75 |
| T202 | 10/21/2017 | 615.31 |
| T202 | 05/08/2018 | 619.52 |
| T202 | 08/02/2018 | 620.53 |
| T202 | 10/23/2018 | 618.36 |
| T202 | 01/15/2019 | 618.69 |
| T202 | 08/05/2019 | 619.02 |
| T202 | 01/20/2020 | 624.22 |
| T202 | 08/10/2020 | 620.39 |
| T202 | 01/20/2021 | 620.08 |
| T202 | 04/20/2021 | 623.43 |
| T202 | 07/26/2021 | 622.64 |
| T202 | 08/16/2021 | 622.69 |
| T408 | 11/12/2016 | 618.58 |
| T408 | 02/04/2017 | 619.46 |
| T408 | 05/13/2017 | 619.00 |
| T408 | 07/08/2017 | 619.12 |
| T408 | 10/21/2017 | 614.81 |
| | -,,, | |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| T408 | 05/08/2018 | 615.82 |
| T408 | 08/02/2018 | 614.45 |
| T408 | 10/23/2018 | 616.30 |
| T408 | 01/15/2019 | 617.01 |
| T408 | 08/05/2019 | 617.15 |
| T408 | 01/20/2020 | 619.13 |
| T408 | 08/10/2020 | 617.38 |
| T408 | 01/20/2021 | 616.85 |
| T408 | 04/20/2021 | 616.65 |
| T408 | 07/26/2021 | 617.21 |
| T408 | 08/16/2021 | 617.22 |
| T409 | 11/12/2016 | 615.98 |
| T409 | 02/04/2017 | 615.93 |
| T409 | 05/13/2017 | 616.75 |
| T409 | 07/08/2017 | 617.05 |
| T409 | 10/21/2017 | 612.16 |
| T409 | 05/08/2018 | 616.02 |
| T409 | 08/02/2018 | 615.25 |
| T409 | 10/23/2018 | 613.96 |
| T409 | 01/15/2019 | 614.78 |
| T409 | 08/05/2019 | 615.10 |
| T409 | 01/20/2020 | 617.16 |
| T409 | 08/10/2020 | 615.43 |
| T409 | 01/20/2021 | 614.41 |
| T409 | 04/20/2021 | 615.33 |
| T409 | 07/26/2021 | 615.72 |
| T409 | 08/16/2021 | 615.42 |
| TA31 | 02/08/2016 | 621.56 |
| TA31 | 05/09/2016 | 621.32 |
| TA31 | 07/25/2016 | 620.63 |
| TA31 | 11/12/2016 | 620.50 |
| TA31 | 02/04/2017 | 621.55 |
| TA31 | 05/13/2017 | 620.66 |
| TA31 | 07/08/2017 | 620.94 |
| TA31 | 10/21/2017 | 616.90 |
| TA31 | 05/08/2018 | 619.80 |
| TA31 | 08/02/2018 | 620.41 |
| TA31 | 10/23/2018 | 618.32 |
| TA31 | 01/15/2019 | 619.21 |
| TA31 | 08/05/2019 | 619.37 |
| TA31 | 01/20/2020 | 622.93 |
| TA31 | 08/10/2020 | 614.89 |
| TA31 | 01/20/2021 | 615.79 |
| TA31 | 04/20/2021 | 622.14 |
| TA31 | 07/26/2021 | 618.76 |
| | + | |



| Samula Lacation | Samula Data | Crown durates Flouration (# NAVDOO) |
|-----------------|-------------|-------------------------------------|
| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
| TA32 | 02/08/2016 | 615.46 |
| TA32 | 05/09/2016 | 616.02 |
| TA32 | 07/25/2016 | 615.61 |
| TA32 | 11/12/2016 | 615.53 |
| TA32 | 02/04/2017 | 614.73 |
| TA32 | 05/13/2017 | 615.82 |
| TA32 | 07/08/2017 | 615.79 |
| TA32 | 10/21/2017 | 612.42 |
| TA32 | 08/05/2019 | 615.41 |
| TA32 | 01/20/2020 | 616.30 |
| TA33 | 02/08/2016 | 619.67 |
| TA33 | 05/09/2016 | 619.75 |
| TA33 | 07/25/2016 | 616.91 |
| TA33 | 11/12/2016 | 616.81 |
| TA33 | 02/04/2017 | 617.12 |
| TA33 | 05/13/2017 | 617.22 |
| TA33 | 07/08/2017 | 617.42 |
| TA33 | 10/21/2017 | 612.91 |
| TA33 | 05/08/2018 | 618.07 |
| TA33 | 08/02/2018 | 616.68 |
| TA33 | 10/23/2018 | 617.26 |
| TA33 | 01/15/2019 | 617.66 |
| TA33 | 08/05/2019 | 618.27 |
| TA33 | 01/20/2020 | 620.35 |
| TA33 | 08/10/2020 | 614.10 |
| TA33 | 01/20/2021 | 614.34 |
| TA33 | 04/20/2021 | 619.07 |
| TA33 | 07/26/2021 | 616.82 |
| TA33 | 08/16/2021 | 616.86 |
| TA34 | 02/08/2016 | 619.29 |
| TA34 | 05/09/2016 | 619.35 |
| TA34 | 07/25/2016 | 617.37 |
| TA34 | 11/12/2016 | 617.40 |
| TA34 | 02/04/2017 | 617.45 |
| TA34 | 05/13/2017 | 617.43 |
| TA34 | 07/08/2017 | 617.44 |
| TA34 | 10/21/2017 | 613.48 |
| TA34 | 05/08/2018 | 617.06 |
| TA34 | 08/02/2018 | 616.42 |
| TA34 | 10/23/2018 | 614.92 |
| TA34 | 01/15/2019 | 615.85 |
| TA34 | 08/05/2019 | 616.54 |
| TA34 | 01/20/2020 | 619.58 |
| TA34 | 08/10/2020 | 615.68 |
| TA34 | 01/20/2021 | 616.16 |
| TA34 | 04/20/2021 | 618.74 |
| | - | - |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|------------------|--------------------------|-----------------------------------|
| TA34 | 07/26/2021 | 617.18 |
| TA34 | 08/16/2021 | 617.42 |
| TR32 | 08/05/2019 | 615.67 |
| TR32 | 01/20/2020 | 616.56 |
| TR32 | 08/10/2020 | 614.92 |
| TR32 | 01/20/2021 | 614.50 |
| TR32 | 04/20/2021 | 615.59 |
| TR32 | 07/26/2021 | 616.09 |
| TR32 | 08/16/2021 | 616.18 |
| XPW01 | 03/29/2021 | 630.23 |
| XPW01 | 03/30/2021 | 630.19 |
| XPW01 | 04/20/2021 | 629.83 |
| XPW01 | 04/22/2021 | 629.84 |
| XPW01 | 05/03/2021 | 629.83 |
| XPW01 | 05/05/2021 | 630.00 |
| XPW01 | 05/17/2021 | 629.85 |
| XPW01 | 05/18/2021 | 630.11 |
| XPW01 | 06/09/2021 | 629.67 |
| XPW01 | 06/14/2021 | 629.57 |
| XPW01 | 06/23/2021 | 629.27 |
| XPW01 | 07/12/2021 | 629.90 |
| XPW01 | 07/26/2021 | 629.73 |
| XPW01 | 07/27/2021 | 629.65 |
| XPW01 | 08/16/2021 | 629.87 |
| XPW02 | 03/29/2021 | 630.19 |
| XPW02 | 03/30/2021 | 630.17 |
| XPW02 | 04/20/2021 | 629.87 |
| XPW02 | 04/22/2021 | 629.88 |
| XPW02 | 05/03/2021 | 629.87 |
| XPW02 | 05/05/2021 | 629.98 |
| XPW02 | 05/17/2021 | 629.86 |
| XPW02 | 05/19/2021 | 630.00 |
| XPW02 | 06/09/2021 | 629.72 |
| XPW02 | 06/14/2021 | 629.64 |
| XPW02 | 06/23/2021 | 629.37 |
| XPW02 | 07/12/2021 | 629.71 |
| XPW02 | 07/26/2021 | 629.78 |
| XPW02 | 07/27/2021 | 629.72 |
| XPW02 | 08/16/2021 | 629.91 |
| XSG-01 | 03/29/2021 | 630.06 |
| XSG-01 | 04/20/2021 | 630.28 |
| XSG-01 | 05/03/2021 | 629.86 |
| | 05/17/2021 | 629.88 |
| XSG-01 | | |
| XSG-01 XSG-01 | 06/09/2021 | 629.74 |
| | 06/09/2021 06/23/2021 | 629.74 629.38 |



| Sample Location | Sample Date | Groundwater Elevation (ft NAVD88) |
|-----------------|-------------|-----------------------------------|
| XSG-01 | 07/26/2021 | 629.79 |
| XSG-01 | 08/16/2021 | 629.92 |
| SG-02 | 03/29/2021 | 598.75 |
| SG-02 | 04/20/2021 | 598.56 |
| SG-02 | 05/03/2021 | 598.74 |
| SG-02 | 05/17/2021 | 598.56 |
| SG-02 | 06/09/2021 | 598.37 |
| SG-02 | 06/23/2021 | 598.34 |
| SG-02 | 07/12/2021 | 598.75 |
| SG-02 | 07/26/2021 | 598.44 |
| SG-02 | 08/16/2021 | 598.39 |
| SG-03 | 04/20/2021 | 589.81 |
| SG-03 | 05/03/2021 | 589.84 |
| SG-03 | 05/17/2021 | 589.84 |
| SG-03 | 06/09/2021 | 589.65 |
| SG-03 | 06/23/2021 | 589.51 |
| SG-03 | 07/12/2021 | 589.97 |
| SG-03 | 07/26/2021 | 589.77 |
| SG-03 | 08/16/2021 | 589.70 |
| SG-04 | 04/20/2021 | 592.99 |
| SG-04 | 05/03/2021 | 592.93 |
| SG-04 | 05/17/2021 | 593.00 |
| SG-04 | 06/09/2021 | 592.82 |
| SG-04 | 06/23/2021 | 592.72 |
| SG-04 | 07/12/2021 | 591.94 |
| SG-04 | 07/26/2021 | 592.83 |
| SG-04 | 08/16/2021 | 593.01 |

Notes:

ft NAVD88 = feet relative to the North American Vertical Datum 1988, GEOID 12A $_{generated\ 10/12/2021,\ 9:26:51\ AM\ CDT}$



| ADDITIONAL VERTICAL HYDRAULIC GRADIENTS | |
|---|--|
| | |
| | |

VERTICAL HYDRAULIC GRADIENTS

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT GYPSUM MANAGEMENT FACILITY GYPSUM STACK POND COFFEEN, ILLINOIS

| Date | G206 Groundwater Elevation (ft NAVD88) UA | G206D Groundwater Elevation (ft NAVD88) DA (PMP) | Head Change (ft) | Distance Change ¹ (ft) | Vertical H Gradio (dh/ | ent ² |
|-----------|---|--|----------------------------------|---|------------------------------|------------------|
| 3/29/2021 | | 583.94 | | | | |
| 4/20/2021 | 622.07 | 585.96 | 36.11 | 33.51 | 1.08 | down |
| 5/3/2021 | 622.60 | 587.42 | 35.18 | 33.51 | 1.05 | down |
| 5/17/2021 | 622.31 | 587.81 | 34.50 | 33.51 | 1.03 | down |
| 6/9/2021 | 621.71 | 584.19 | 37.52 | 33.51 | 1.12 | down |
| 6/23/2021 | 620.54 | 589.66 | 30.88 | 33.51 | 0.92 | down |
| 7/12/2021 | 622.39 | 590.72 | 31.67 | 33.51 | 0.95 | down |
| 7/26/2021 | 622.00 | 591.14 | 30.86 | 33.51 | 0.92 | down |
| | _ | | Middle of screen elevation G206 | | | 610.8 |
| | | | Middle of screen elevation G206D | | | 577.3 |

[O: KLT 6/4/21, C:YMD 6/7/21][U:KLT 8/25/21, C:EDP 8/31/21]

Notes:

DA = deep aquifer

dh = head change

dl = distance change

ft = foot/feet

NAVD88 = North American Vertical Datum of 1988

PMP = potential migration pathway

UA = uppermost aquifer



¹ Distance change was calculated using the midpoint of the piezometer screen and water table surface. If the water table surface was above the top of the monitoring well screen, then distance change was calculated using the midpoint of both screens.

 $^{^2}$ Vertical gradients between ± 0.0015 are considered flat, and typically have less than 0.02 foot difference in groundwater elevation between wells.

^{-- =} no data collected on date / no vertical gradient calculated

VERTICAL HYDRAULIC GRADIENTS

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT GYPSUM MANAGEMENT FACILITY RECYCLE POND COFFEEN, ILLINOIS

| Date | G405 Groundwater Elevation (ft NAVD88) UA | T408 Groundwater Elevation (ft NAVD88) LCU (upper) | Head Change (ft) | Distance Change ¹ (ft) | Vertical Hydraulic Gradient ² (dh/dl) | |
|------------|---|--|--|---|--|-------|
| 2/4/2017 | 618.47 | 619.46 | -0.99 | 12.00 | -0.08 | up |
| 5/13/2017 | 618.74 | 619.00 | -0.26 | 12.00 | -0.02 | up |
| 7/8/2017 | 618.54 | 619.12 | -0.58 | 12.00 | -0.05 | up |
| 10/21/2017 | 614.47 | 614.81 | -0.34 | 12.00 | -0.03 | up |
| 5/8/2018 | 618.94 | 615.82 | 3.12 | 12.00 | 0.26 | down |
| 8/2/2018 | 617.55 | 614.45 | 3.10 | 12.00 | 0.26 | down |
| 10/23/2018 | 616.40 | 616.30 | 0.10 | 12.00 | 0.01 | down |
| 1/15/2019 | 616.81 | 617.01 | -0.20 | 12.00 | -0.02 | up |
| 8/5/2019 | 617.72 | 617.15 | 0.57 | 12.00 | 0.05 | down |
| 1/20/2020 | 619.28 | 619.13 | 0.15 | 12.00 | 0.01 | down |
| 8/10/2020 | 617.62 | 617.38 | 0.24 | 12.00 | 0.02 | down |
| 1/20/2021 | 617.12 | 616.85 | 0.27 | 12.00 | 0.02 | down |
| 4/20/2021 | 617.13 | 616.65 | 0.48 | 12.00 | 0.04 | down |
| 7/26/2021 | 617.37 | 617.21 | 0.16 | 12.00 | 0.01 | down |
| | | | Middle of screen elevation G405D 610.0 | | | 610.0 |
| | | | Middle of screen elevation T408 598.0 | | | 598.0 |

| Date | G275 Groundwater Elevation (ft NAVD88) UA | G275D Groundwater Elevation (ft NAVD88) DA (PMP) | Head Change (ft) | Distance Change ¹ (ft) | Hydraulic | ertical c Gradient ² h/dl) | |
|-----------------|---|--|---------------------------------|---|-----------|---|--|
| 4/20/21-4/21/20 | 605.00 | 568.33 | 36.67 | 42.14 | 0.87 | down | |
| 7/12/21-7/13/21 | 605.63 | 570.43 | 35.20 | 42.77 | 0.82 | down | |
| 7/26/2021 | 605.05 | 570.35 | 34.70 | 42.18 | 0.82 | down | |
| | | | Middle of screen elevation G275 | | | 605.7 | |
| | | Middle of screen elevation G275D | | | 562.9 | | |



VERTICAL HYDRAULIC GRADIENTS

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT GYPSUM MANAGEMENT FACILITY RECYCLE POND COFFEEN, ILLINOIS

| Date | T408 Groundwater Elevation (ft NAVD88) LCU (upper) | G45D Groundwater Elevation (ft NAVD88) LCU (lower) | Head Change (ft) | Distance Change ¹ (ft) | Vertical Hydraulic Gradient ² (dh/dl) | |
|------------|--|--|---------------------------------|---|--|-------|
| 2/4/2017 | 619.46 | 587.71 | 31.75 | 13.78 | 2.30 | down |
| 5/13/2017 | 619.00 | 586.19 | 32.81 | 13.78 | 2.38 | down |
| 7/8/2017 | 619.12 | 586.29 | 32.83 | 13.78 | 2.38 | down |
| 10/21/2017 | 614.81 | 584.69 | 30.12 | 13.78 | 2.19 | down |
| 5/8/2018 | 615.82 | 587.56 | 28.26 | 13.78 | 2.05 | down |
| 8/2/2018 | 614.45 | 585.81 | 28.64 | 13.78 | 2.08 | down |
| 10/23/2018 | 616.30 | 584.60 | 31.70 | 13.78 | 2.30 | down |
| 1/15/2019 | 617.01 | 586.96 | 30.05 | 13.78 | 2.18 | down |
| 8/5/2019 | 617.15 | 588.04 | 29.11 | 13.78 | 2.11 | down |
| 8/10/2020 | 617.38 | 614.21 | 3.17 | 13.78 | 0.23 | down |
| 1/20/2021 | 616.85 | 614.60 | 2.25 | 13.78 | 0.16 | down |
| 4/20/2021 | 616.65 | 614.32 | 2.33 | 13.78 | 0.17 | down |
| 7/26/2021 | 617.21 | 613.58 | 3.63 | 13.78 | 0.26 | down |
| | | | Middle of | screen elevation | n T408 | 598.0 |
| | | | Middle of screen elevation G45D | | | 584.2 |

[O: KLT 6/4/21, C:YMD 6/7/21][U:KLT 8/25/21, C:EDP 8/31/21]

Notes:

DA = deep aguifer

dh = head change

dl = distance change

ft = foot/feet

LCU (lower) = lower confining unit (Smithboro)

LCU (upper) = lower confining unit (Vandalia)

NAVD88 = North American Vertical Datum of 1988

PMP = potential migration pathway

UA = uppermost aquifer

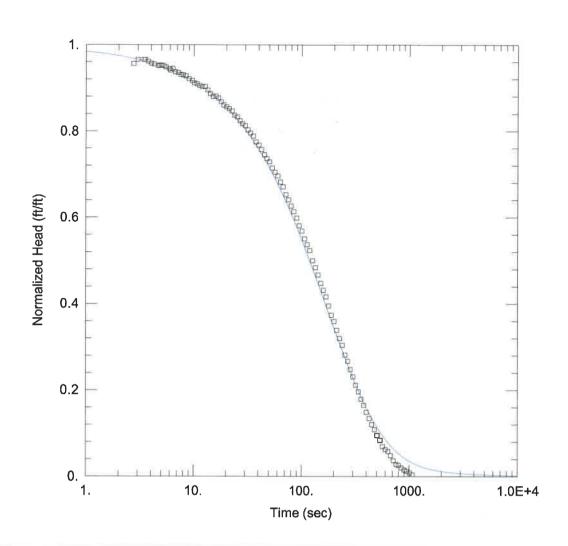


¹ Distance change was calculated using the midpoint of the piezometer screen and water table surface. If the water table surface was above the top of the monitoring well screen, then distance change was calculated using the midpoint of both screens.

 $^{^{2}}$ Vertical gradients between ± 0.0015 are considered flat, and typically have less than 0.02 foot difference in groundwater elevation between wells.

^{-- =} no data collected on date / no vertical gradient calculated

HYDRAULIC CONDUCTIVITY TEST DATA



G301 FALLING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G301-fh.aqt

Date: 06/03/21

Time: 15:37:26

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G301 Test Date: 3/10/2021

AQUIFER DATA

Saturated Thickness: 2.5 ft

WELL DATA (G301)

Initial Displacement: 1.78 ft

Total Well Penetration Depth: 11.54 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 11.79 ft

Screen Length: 4.65 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

SOLUTION

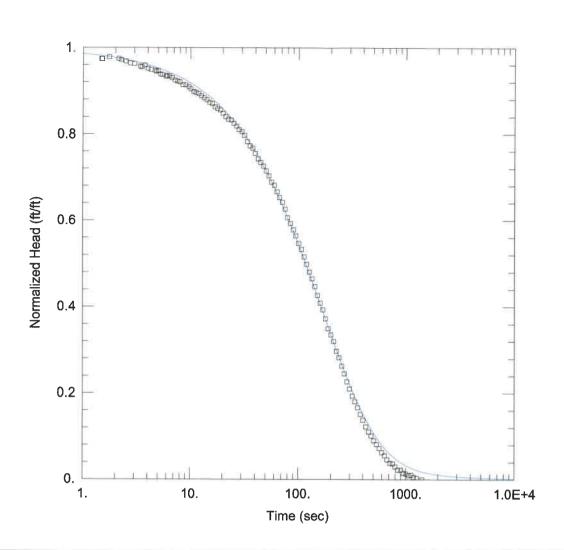
Aquifer Model: Confined

Kr = 0.0011 cm/sec

 $Kz/Kr = \overline{1}$.

Solution Method: KGS Model

Ss = $0.00093 \, \text{ft}^{-1}$



G301 RISING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G301-rh.aqt

Date: 06/03/21

Time: 15:37:28

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G301 Test Date: 3/10/2021

AQUIFER DATA

Saturated Thickness: 2.5 ft

WELL DATA (G301)

Initial Displacement: 1.86 ft

Total Well Penetration Depth: 11.54 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 11.79 ft

Screen Length: 4.65 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

SOLUTION

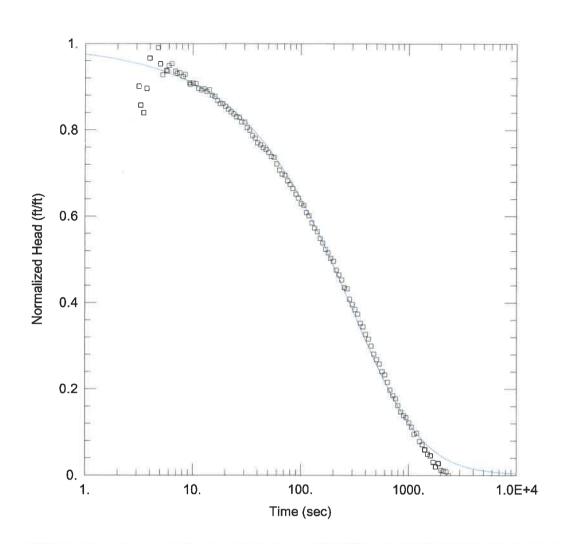
Aguifer Model: Confined

Kr = 0.0012 cm/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss = 0.00051 ft^{-1}



G303 FALLING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G303-fh.aqt

Date: 06/03/21

Time: 15:37:29

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G303 Test Date: 3/11/2021

AQUIFER DATA

Saturated Thickness: 5. ft

WELL DATA (G303)

Initial Displacement: 1.08 ft

Total Well Penetration Depth: 17.45 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 17.85 ft

Screen Length: 10. ft
Well Radius: 0.08333 ft
Gravel Pack Porosity: 0.

SOLUTION

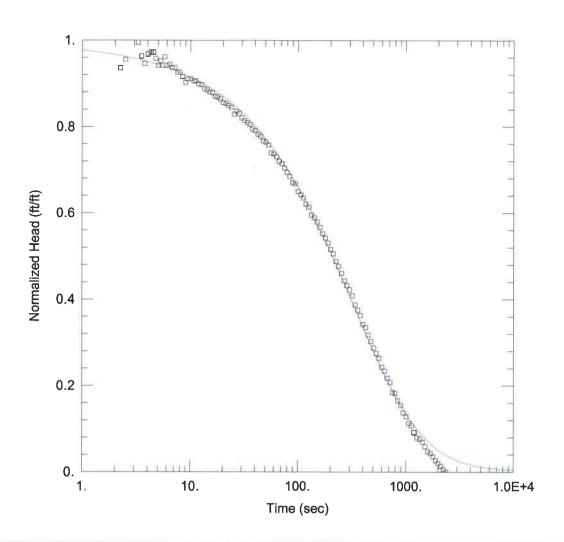
Aquifer Model: Confined

Kr = 0.00028 cm/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss = 0.011 ft^{-1}



G303 RISING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G303-rh.aqt

Date: 06/03/21

Time: 15:37:31

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G303 Test Date: 3/11/2021

AQUIFER DATA

Saturated Thickness: 5. ft

WELL DATA (G303)

Initial Displacement: 7.78 ft

Total Well Penetration Depth: 17.45 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 17.85 ft

Screen Length: 10. ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

SOLUTION

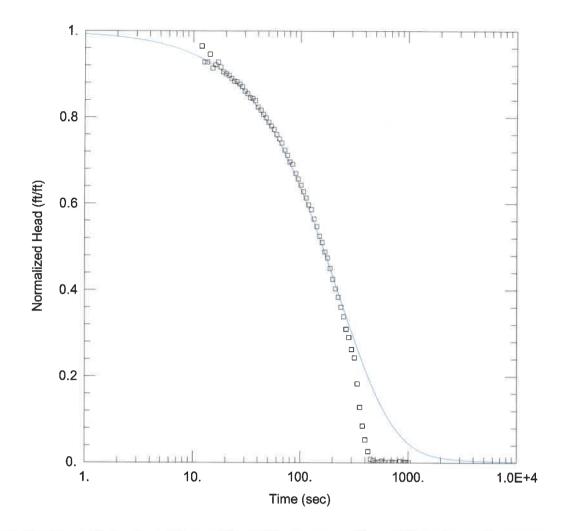
Aquifer Model: Confined

Kr = 0.00026 cm/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss = $0.01 \, \text{ft}^{-1}$



G307D FALLING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G307D-fh.aqt

Date: 06/03/21 Time: 15:37:32

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A
Location: Coffeen, IL
Test Well: G307D
Test Date: 3/12/2021

AQUIFER DATA

Saturated Thickness: 10. ft

WELL DATA (G307D)

Initial Displacement: 1.65 ft

Total Well Penetration Depth: 58.72 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 59.57 ft

Screen Length: 9.77 ft
Well Radius: 0.08333 ft
Gravel Pack Porosity: 0.

SOLUTION

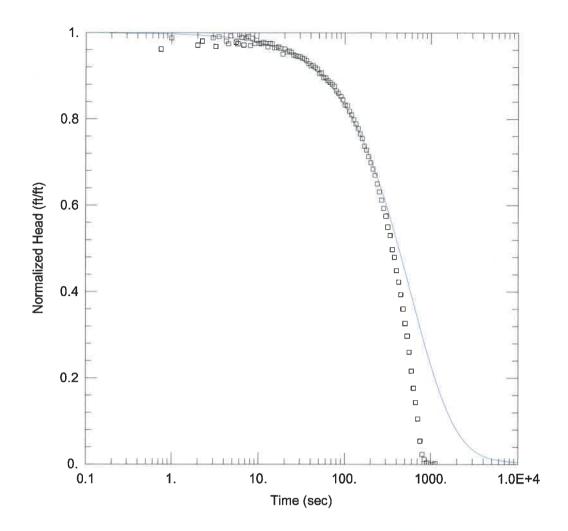
Aquifer Model: Confined

Kr = 0.00032 cm/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss = $1.0E-6 \text{ ft}^{-1}$



G307D RISING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G307D-rh.aqt

Date: 06/04/21 Time: 08:21:32

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G307D Test Date: 3/12/2021

AQUIFER DATA

Saturated Thickness: 10. ft

WELL DATA (G307D)

Initial Displacement: 1.55 ft

Total Well Penetration Depth: 58.72 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 59.57 ft

Screen Length: 9.77 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

SOLUTION

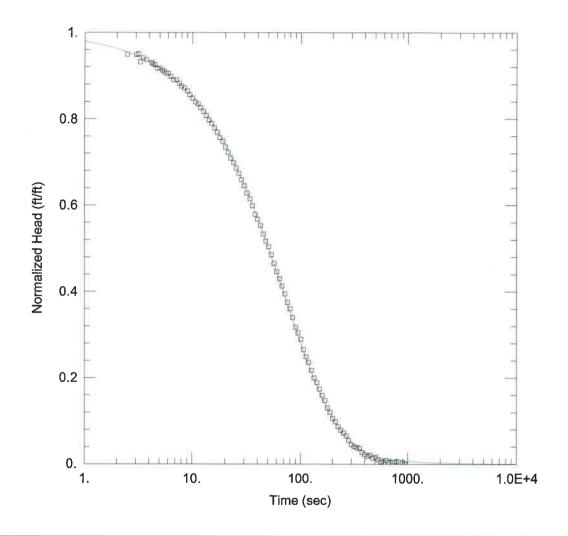
Aquifer Model: Confined

Kr = 0.00012 cm/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss = $1.0E-6 \text{ ft}^{-1}$



G308 FALLING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G308-fh.aqt

Date: 06/03/21

Time: 15:37:35

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G308 Test Date: 3/11/2021

AQUIFER DATA

Saturated Thickness: 1.7 ft

WELL DATA (G308)

Initial Displacement: 1.73 ft

Total Well Penetration Depth: 13.97 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 14.29 ft

Screen Length: 4.79 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

SOLUTION

Aquifer Model: Confined

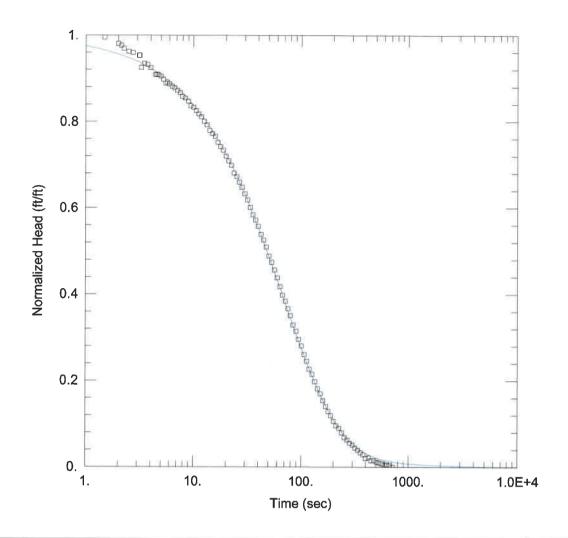
= 0.0055 cm/sec

Kz/Kr = 1.

Kr

Solution Method: KGS Model

Ss = $0.0001 \, \text{ft}^{-1}$



G308 RISING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G308-rh.aqt

Date: 06/03/21

Time: 15:37:37

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G308 Test Date: 3/11/2021

AQUIFER DATA

Saturated Thickness: 5. ft

WELL DATA (G308)

Initial Displacement: 11.9 ft

Total Well Penetration Depth: 13.97 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 14.29 ft

Screen Length: 4.79 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

SOLUTION

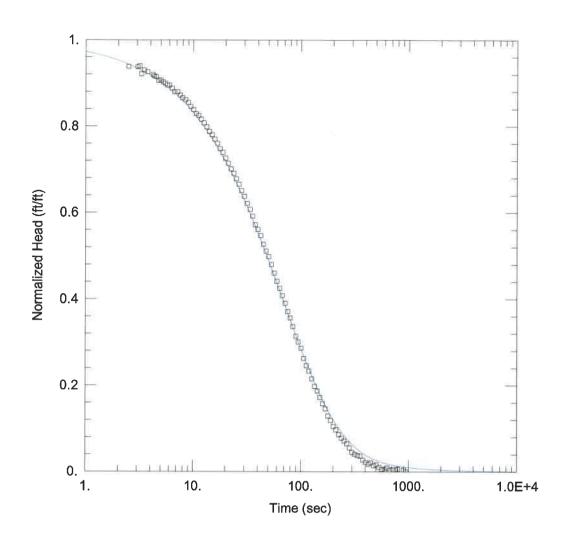
Aquifer Model: Confined

(r = 0.0016 cm/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss = $0.0001 \, \text{ft}^{-1}$



G309 FALLING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G309-fh.aqt

Date: 06/03/21

Time: 15:37:38

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G309 Test Date: 3/11/2021

AQUIFER DATA

Saturated Thickness: 0.7 ft

WELL DATA (G309)

Initial Displacement: 1.75 ft

Total Well Penetration Depth: 14.38 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 14.73 ft

Screen Length: 4.78 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

SOLUTION

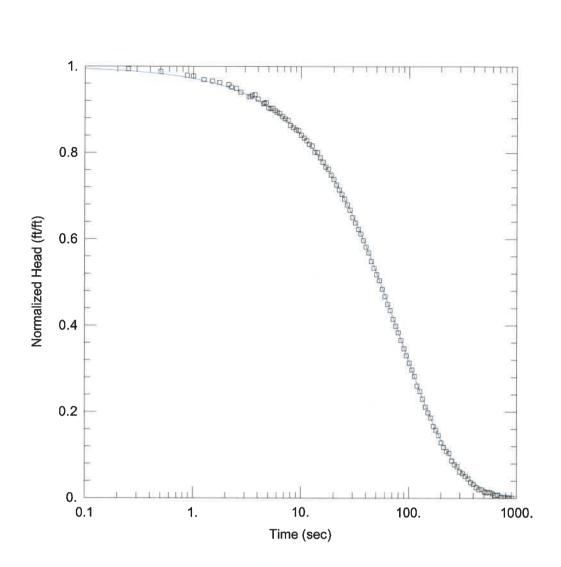
Aquifer Model: Confined

Kr = 0.0091 cm/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss = 0.0025 ft^{-1}



G309 RISING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G309-rh.aqt

Date: 06/04/21 Time: 08:22:05

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G309 Test Date: 3/11/2021

AQUIFER DATA

Saturated Thickness: 14.73 ft

WELL DATA (G309)

Initial Displacement: 1.575 ft

Total Well Penetration Depth: 14.38 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 14.73 ft

Screen Length: 4.78 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

SOLUTION

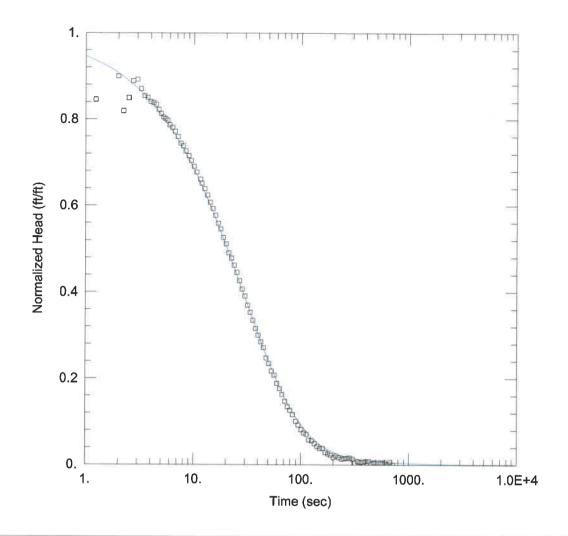
Aquifer Model: Confined

Kr = 0.00088 cm/sec

Solution Method: KGS Model

Ss = 0.00035 ft^{-1}

Kz/Kr = 1.



G310 FALLING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G310-fh.aqt

Date: 06/03/21

Time: 15:37:42

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G310 Test Date: 3/10/2021

AQUIFER DATA

Saturated Thickness: 2. ft

WELL DATA (G310)

Initial Displacement: 1.61 ft

Total Well Penetration Depth: 10.53 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 10.88 ft

Screen Length: 4.79 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

SOLUTION

Aquifer Model: Confined

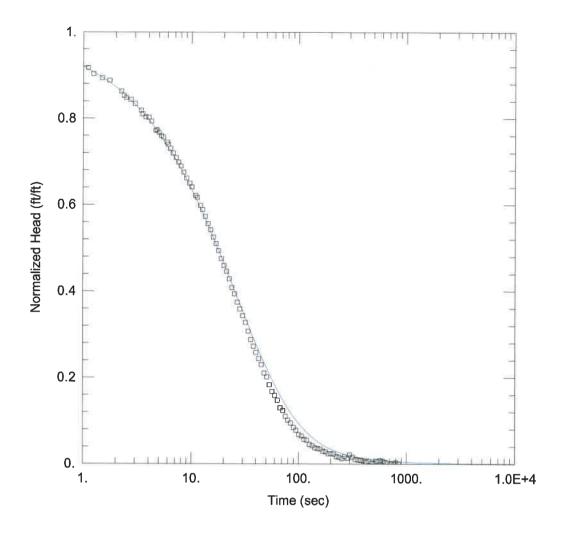
= 0.0075 cm/sec

Kz/Kr = 1.

Kr

Solution Method: KGS Model

Ss = $0.0005 \, \text{ft}^{-1}$



G310 RISING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G310-rh.aqt

Date: 06/03/21

Time: 15:37:43

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G310 Test Date: 3/10/2021

AQUIFER DATA

Saturated Thickness: 2. ft

WELL DATA (G310)

Initial Displacement: 1.67 ft

Total Well Penetration Depth: 10.53 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 10.88 ft

Screen Length: 4.79 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

SOLUTION

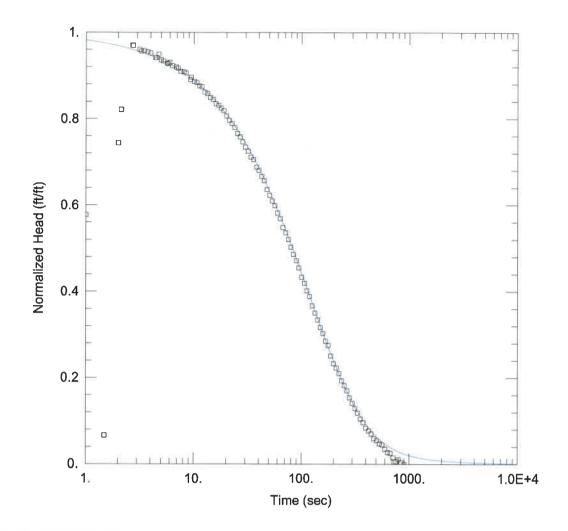
Aquifer Model: Confined

Kr = 0.0059 cm/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss = 0.006 ft^{-1}



G311D FALLING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G311D-fh.aqt

Date: 06/03/21 Time: 15:38:30

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G311D Test Date: 3/10/2021

AQUIFER DATA

Saturated Thickness: 10. ft

WELL DATA (G311D)

Initial Displacement: 1.625 ft

Total Well Penetration Depth: 10.21 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 10.69 ft

Screen Length: 9.94 ft Well Radius: 0.08333 ft

Gravel Pack Porosity: 0.

SOLUTION

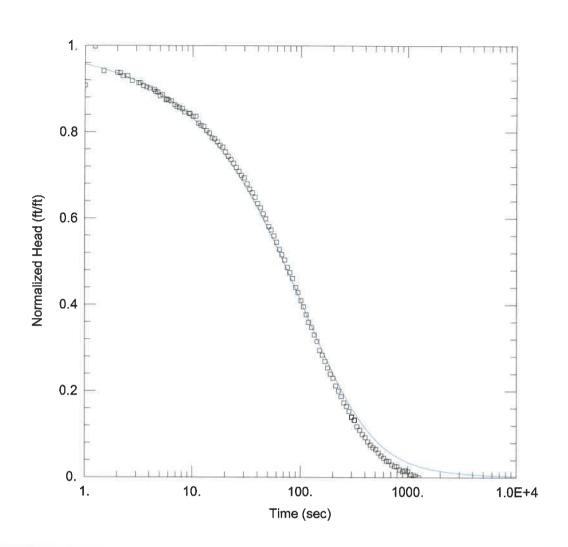
Aquifer Model: Confined

Kr = 0.00038 cm/sec

Kz/Kr = 1.

Solution Method: KGS Model

 $= 4.7E-5 \text{ ft}^{-1}$ Ss



G311D RISING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G311D-rh.agt

Date: 06/03/21 Time: 15:38:31

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G311D Test Date: 3/10/2021

AQUIFER DATA

Saturated Thickness: 10. ft

WELL DATA (G311D)

Initial Displacement: 1.72 ft

Total Well Penetration Depth: 10.21 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 10.69 ft

Screen Length: 9.94 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

SOLUTION

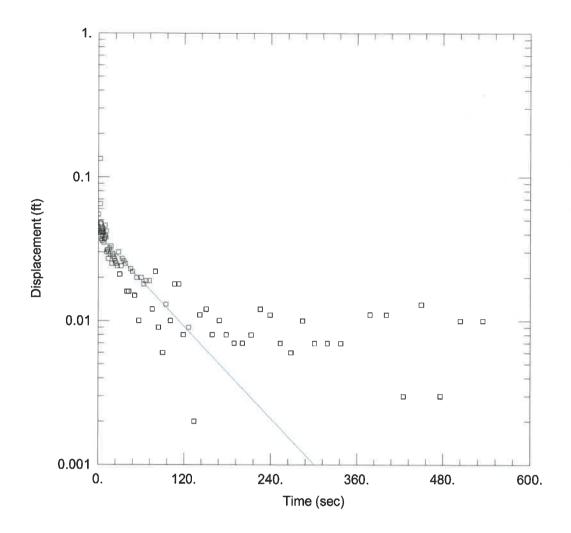
Aquifer Model: Confined

Kr = 0.00021 cm/sec

 $Kz/Kr = \overline{1}$.

Solution Method: KGS Model

Ss = 0.0027 ft^{-1}





Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G311-fh.aqt

Date: 06/03/21

Time: 15:38:33

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G311 Test Date: 3/10/2021

AQUIFER DATA

Saturated Thickness: 3. ft

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (G311)

Initial Displacement: 0.055 ft

Total Well Penetration Depth: 10.32 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 10.68 ft

Screen Length: 4.77 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

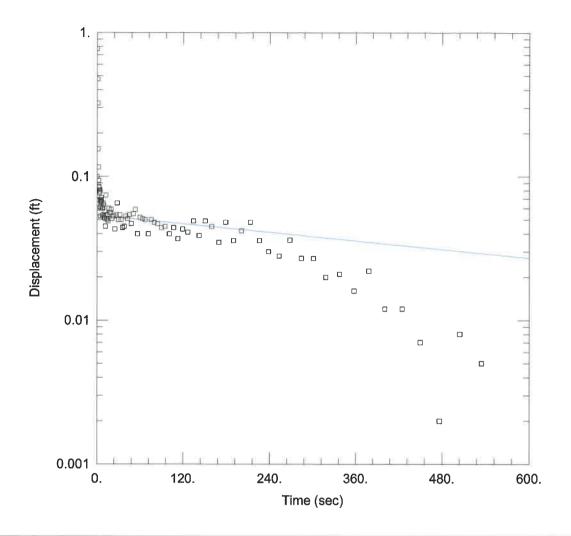
SOLUTION

Aquifer Model: Confined

Solution Method: Bouwer-Rice

K = 0.0015 cm/sec

y0 = 0.04 ft



G311 RISING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G311-rh.aqt

Date: 06/03/21 Time: 15:38:35

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G311 Test Date: 3/10/2021

AQUIFER DATA

Saturated Thickness: 3. ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (G311)

Initial Displacement: 0.1 ft

Total Well Penetration Depth: 10.32 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 10.68 ft

Screen Length: 4.77 ft
Well Radius: 0.08333 ft
Gravel Pack Porosity: 0.

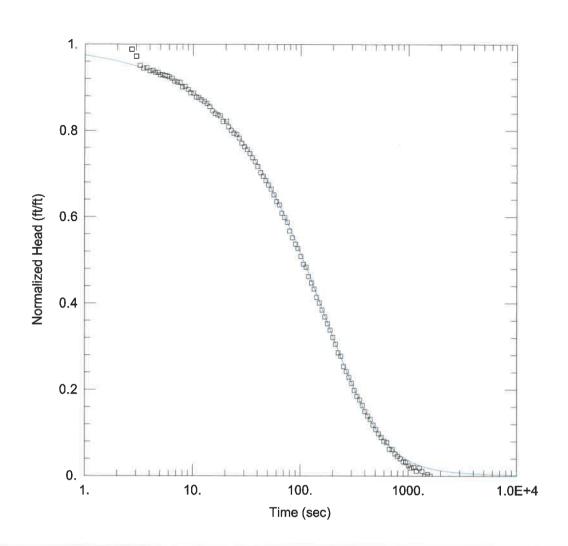
SOLUTION

Aquifer Model: Confined

K = 0.00014 cm/sec

Solution Method: Bouwer-Rice

y0 = 0.054 ft



G312 FALLING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G312-fh.aqt

Date: 06/03/21

Time: 15:38:36

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G312 Test Date: 3/10/2021

AQUIFER DATA

Saturated Thickness: 2.3 ft

WELL DATA (G312)

Initial Displacement: 1.29 ft

Total Well Penetration Depth: 7.8 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 8.15 ft

Screen Length: 4.79 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

SOLUTION

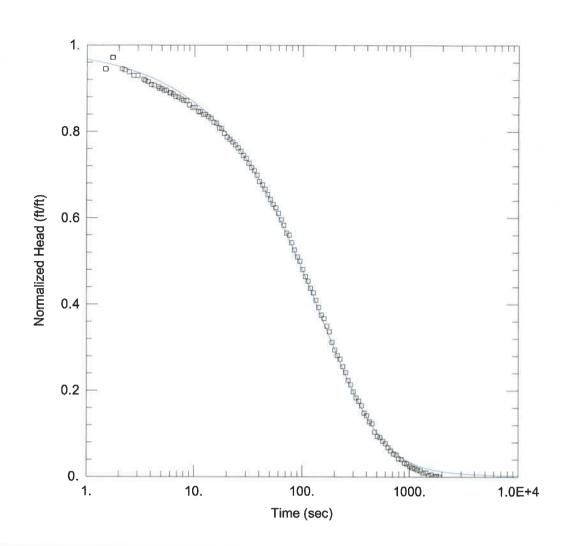
Aquifer Model: Confined

Kr = 0.0011 cm/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss = 0.0066 ft^{-1}



G312 RISING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G312-rh.aqt

Date: 06/03/21

Time: 15:38:38

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G312 Test Date: 3/10/2021

AQUIFER DATA

Saturated Thickness: 2.3 ft

WELL DATA (G312)

Initial Displacement: 1.4 ft

Total Well Penetration Depth: 7.8 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 8.15 ft

Screen Length: 4.79 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

SOLUTION

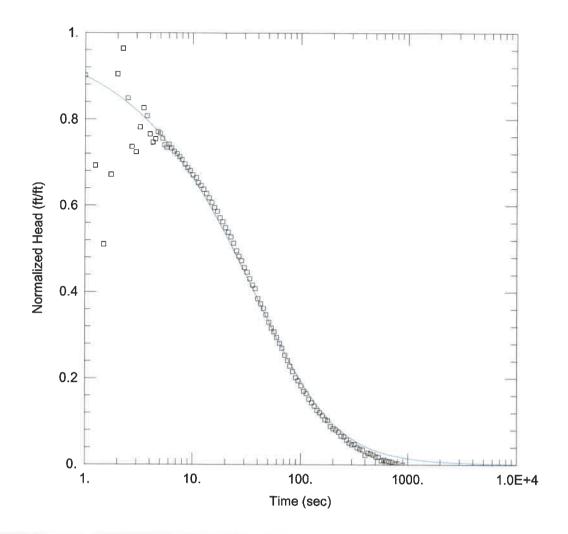
Aquifer Model: Confined

Kr = 0.0011 cm/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss = 0.013 ft^{-1}



G313 FALLING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G313-fh.aqt

Date: 06/03/21

Time: 15:38:40

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G313 Test Date: 3/10/2021

AQUIFER DATA

Saturated Thickness: 1.5 ft

WELL DATA (G313)

Initial Displacement: 1.7 ft

Total Well Penetration Depth: 10.9 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 11.25 ft

Screen Length: 4.81 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

SOLUTION

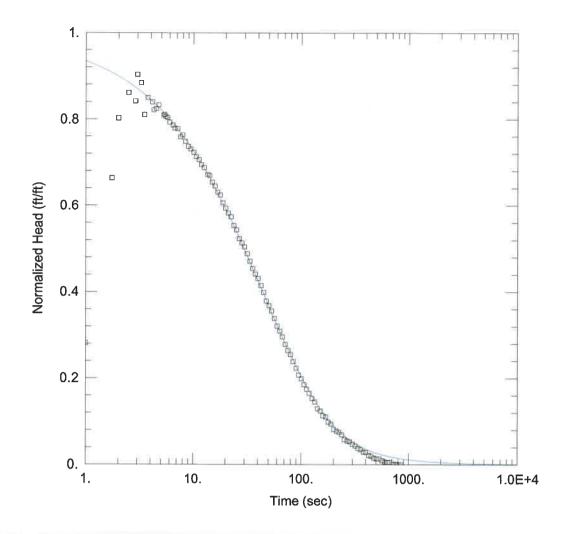
Aquifer Model: Confined

Kr = 0.0027 cm/sec

 $Kz/Kr = \overline{1}$.

Solution Method: KGS Model

Ss = $0.07 \, \text{ft}^{-1}$



G313 RISING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G313-rh.aqt

Date: 06/03/21 Time: 15:38:41

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G313 Test Date: 3/10/2021

AQUIFER DATA

Saturated Thickness: 1.5 ft

WELL DATA (G313)

Initial Displacement: 1.65 ft

Total Well Penetration Depth: 10.9 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 11.25 ft

Screen Length: 4.81 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

SOLUTION

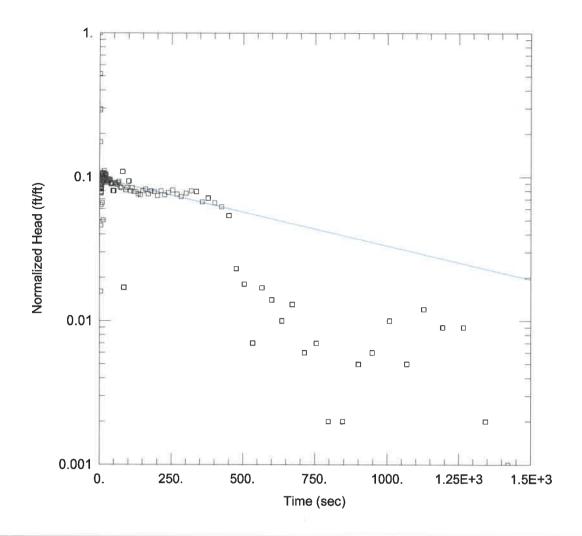
Aquifer Model: Confined

Kr = 0.0035 cm/sec

 $Kz/Kr = \overline{1}$.

Solution Method: KGS Model

Ss = $0.015 \, \text{ft}^{-1}$



G314D FALLING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G314D-fh.aqt

Date: 06/03/21 Time: 15:38:43

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G314D Test Date: 3/10/2021

AQUIFER DATA

Saturated Thickness: 1. ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (G314D)

Initial Displacement: 1. ft

Total Well Penetration Depth: 9.77 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 6.3 ft

Screen Length: 9.77 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

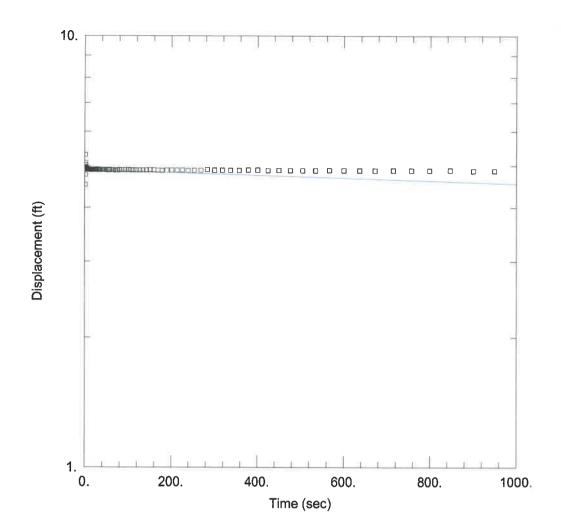
SOLUTION

Aquifer Model: Confined

K = 0.00033 cm/sec

Solution Method: Bouwer-Rice

y0 = 0.098 ft



G314D RISING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G314D-rh.aqt

Date: 06/03/21 Time: 15:38:45

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G314D Test Date: 3/10/2021

AQUIFER DATA

Saturated Thickness: 1. ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (G314D)

Initial Displacement: 4.95 ft

Total Well Penetration Depth: 9.77 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 6.3 ft

Screen Length: 9.77 ft
Well Radius: 0.08333 ft
Gravel Pack Porosity: 0.

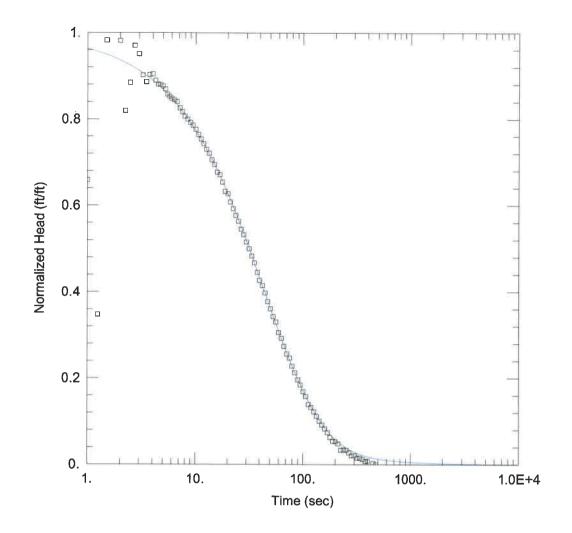
SOLUTION

Aquifer Model: Confined

K = 2.3E-5 cm/sec

Solution Method: Bouwer-Rice

y0 = 4.9 ft



G315 FALLING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G315-fh.aqt

Date: 06/03/21

Time: 15:38:46

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G315 Test Date: 3/12/2021

AQUIFER DATA

Saturated Thickness: 1.6 ft

WELL DATA (G315)

Initial Displacement: 1.35 ft

Total Well Penetration Depth: 14.77 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 12.56 ft

Screen Length: 4.79 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

SOLUTION

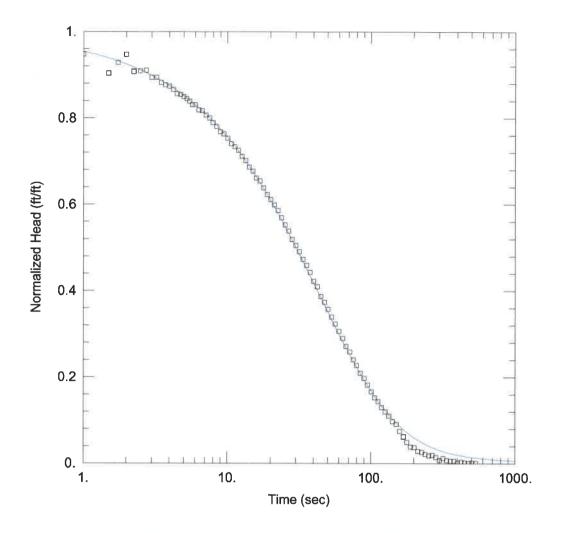
Aquifer Model: Confined

Kr = 0.0066 cm/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss = 0.0007 ft^{-1}



G315 RISING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G315-rh.agt

Date: 06/03/21 Time: 16:40:34

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G315 Test Date: 3/12/2021

AQUIFER DATA

Saturated Thickness: 1.6 ft

WELL DATA (G315)

Initial Displacement: 1.77 ft

Total Well Penetration Depth: 14.77 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 12.56 ft

Screen Length: 4.79 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

SOLUTION

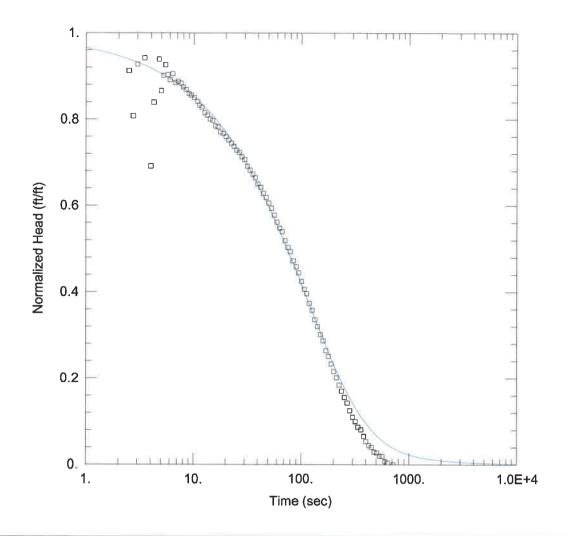
Aquifer Model: Confined

= 0.0058 cm/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss $= 0.003 \text{ ft}^{-1}$



G316 FALLING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G316-fh.aqt

Date: 06/03/21

Time: 15:38:50

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G316 Test Date: 3/11/2021

AQUIFER DATA

Saturated Thickness: 1.4 ft

WELL DATA (G316)

Initial Displacement: 1.51 ft

Total Well Penetration Depth: 6.69 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 4.08 ft

Screen Length: 4.8 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

SOLUTION

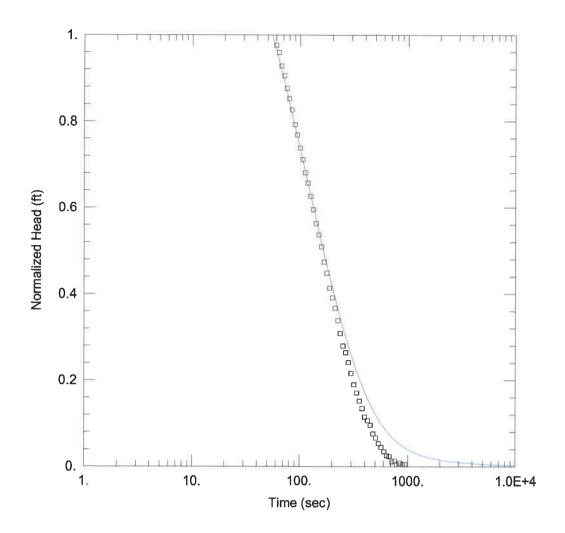
Aquifer Model: Confined

Kr = 0.0023 cm/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss = $0.02 \, \text{ft}^{-1}$



G316 RISING HEAD TEST

Data Set: I:\20jobs\20E0111A\Admin\13-Calculations\Slug Tests\Coffeen\G316-rh.aqt

Date: 06/03/21

Time: 15:38:51

PROJECT INFORMATION

Client: Coffeen Power Station

Project: 20E0111A Location: Coffeen, IL Test Well: G316 Test Date: 3/11/2021

AQUIFER DATA

Saturated Thickness: 1.4 ft

WELL DATA (G316)

Initial Displacement: 1.62 ft

Total Well Penetration Depth: 6.69 ft

Casing Radius: 0.08333 ft

Static Water Column Height: 4.08 ft

Screen Length: 4.8 ft Well Radius: 0.08333 ft Gravel Pack Porosity: 0.

SOLUTION

Aquifer Model: Confined

= 0.0023 cm/sec

Kz/Kr = 1.

Solution Method: KGS Model

Ss = 0.0085 ft^{-1}

ADDITIONAL FIELD HYDRAULIC CONDUCTIVITIES

FIELD HYDRAULIC CONDUCTIVITIES

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT GMF GYPSUM STACK POND COFFEEN, ILLINOIS

| Well ID | Gradient Position | Bottom of Screen Elevation (ft NAVD88) | Screen Length ¹ (ft) | Field Identified Screened Material | Slug Type | Analysis Method | Falling Head (Slug In) Hydraulic Conductivity (cm/s) | Rising Head (Slug Out) Hydraulic Conductivity (cm/s) | Minimum Hydraulic Conductivity (cm/s) | Maximum Hydraulic Conductivity (cm/s) | Hydraulic Conductivity Geometric Mean (cm/s) |
|----------|----------------------|--|------------------------------------|---------------------------------------|-----------|--------------------------|--|--|--|--|---|
| Uppermos | t Aquiter | | | | | | 1 | | | | _ |
| G206 | D | 608.61 | 4.41 | SM, s(CL), CL | solid | Kansas Geological Survey | 5.0E-04 | 4.9E-04 | | | |
| G209 | D | 608.29 | 4.54 | CL | solid | Kansas Geological Survey | | 2.5E-04 | | | |
| G212 | D | 609.30 | 4.55 | SM, s(CL), CL | solid | Kansas Geological Survey | 2.1E-03 | 1.8E-03 | 2.5E-04 | 4.0E-03 | 1.4E-03 |
| G215 | D | 606.68 | 4.39 | SM, s(CL), ML | solid | Kansas Geological Survey | 4.0E-03 | 3.5E-03 | | | |
| G218 | D | 605.87 | 4.44 | SM, SC, CL | solid | Kansas Geological Survey | 2.6E-03 | 2.4E-03 | | | |
| | | | • | | | • | | | | [(|): KLT, C:EDP 8/31/21] |

Notes:

1. All wells are constructed from 2 inch PVC with 0.01 inch slotted screens.

- - = Test not analyzed/performed

cm/s = centimeters per second

D = downgradient ft = foot/feet

NAVD88 = North American Vertical Datum of 1988

PVC = polyvinyl chloride

USCS = Unified Soil Classification System

CL = Lean Clay
s(CL) = Sandy Lean Clay
ML = Silt
SC = Clayey Sand
SM = Silty Sand



FIELD HYDRAULIC CONDUCTIVITIES

HYDROGEOLOGIC SITE CHARACTERIZATION REPORT COFFEEN POWER PLANT GMF RECYCLE POND COFFEEN, ILLINOIS

| Well ID | Gradient Position | Bottom of Screen Elevation (ft NAVD88) | Screen Length ¹ (ft) | Field Identified Screened Material | Slug Type | Analysis Method | Falling Head (Slug In) Hydraulic Conductivity (cm/s) | Rising Head (Slug Out) Hydraulic Conductivity (cm/s) | Minimum Hydraulic Conductivity (cm/s) | Maximum Hydraulic Conductivity (cm/s) | Hydraulic Conductivity Geometric Mean (cm/s) |
|-----------|----------------------|--|---------------------------------|---------------------------------------|-----------|--------------------------|--|--|--|--|---|
| Uppermos | t Aquifer | | | | | | | | | | |
| G272 | D | 606.74 | 4.87 | SP to ML, (CL)s | solid | Kansas Geological Survey | 1.7E-03 | | | | |
| G284 | D | 602.48 | 4.77 | ML | solid | Kansas Geological Survey | 1.2E-03 | 7.8E-04 | 7.8E-04 | 1.7E-03 | 1.1E-03 |
| G286 | D | 601.81 | 4.79 | SP, ML, CL | solid | Kansas Geological Survey | 1.2E-03 | | 7.0E-04 | 1.76-03 | 1.16-03 |
| G287 | D | 604.09 | 4.82 | SP, ML, CL | solid | Kansas Geological Survey | 1.1E-03 | 1.1E-03 | | | |
| Lower Con | fining Unit | (PMP) | | | | | | | | | |
| G283 | D | 590.13 | 9.78 | SP, ML | solid | Kansas Geological Survey | 4.2E-03 | 4.5E-03 | 2.75.04 | 4.55.00 | 1 25 02 |
| G285 | D | 587.09 | 9.77 | CL | solid | Bouwer-Rice | 2.7E-04 | 4.3E-04 | 2.7E-04 | 4.5E-03 | 1.2E-03 |
| - | | | | | | | • | • | • | [(| D: KLT, C:EDP 8/31/21] |

Notes:

1. All wells are constructed from 2 inch PVC with 0.01 inch slotted screens.

- - = Test not analyzed/performed

cm/s = centimeters per second

D = downgradient

ft = foot/feet

NAVD88 = North American Vertical Datum of 1988

PVC = polyvinyl chloride

PMP = potential migration pathway

USCS = Unified Soil Classification System

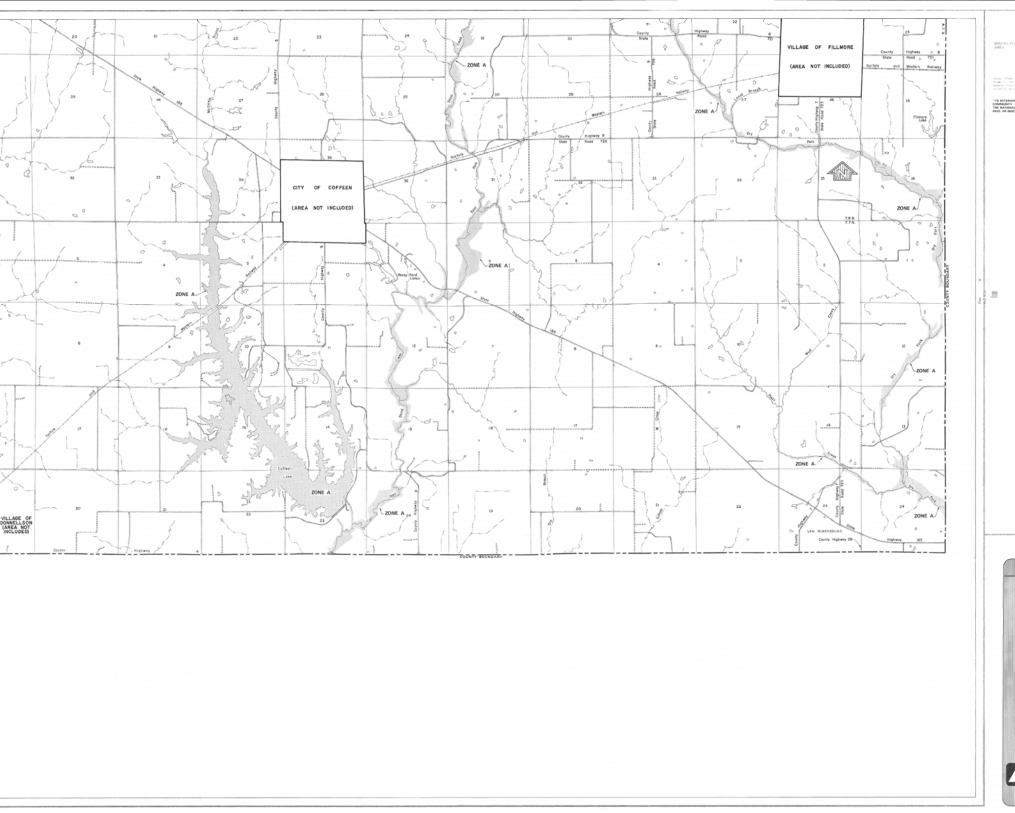
CL = Lean Clay

(CL)s = Lean Clay with Sand ML = Silt

SP = Poorly-Graded Sand



APPENDIX G FEMA FLOOD HAZARD MAP



NATIONAL FLO FHBN FLOOD HAZA

MONT COUN ILLIN UNINCOR

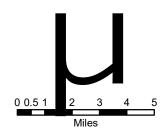
PANEL 9 0

COMMU



This map illustrates stream reaches at risk for potential flooding that were not designated as Special Flood Hazard Areas (SFHAs) and were not shown on Federal Emergency Management Agency (FEMA) Flood Insurance Rate Maps as of July 1, 2007. Also shown are areas of Risk Class A (high), B (medium), and C (low) adopted by FEMA Region 5. Streams lacking a SFHA designation and draining more than one square mile in a Risk Class A area or draining more than 10 square miles in a Risk Class B or C area are shown with red lines.

A table associated with this map lists streams with unmapped potential flood risk, their names, and the number of miles not within a Special Flood Hazard Area.



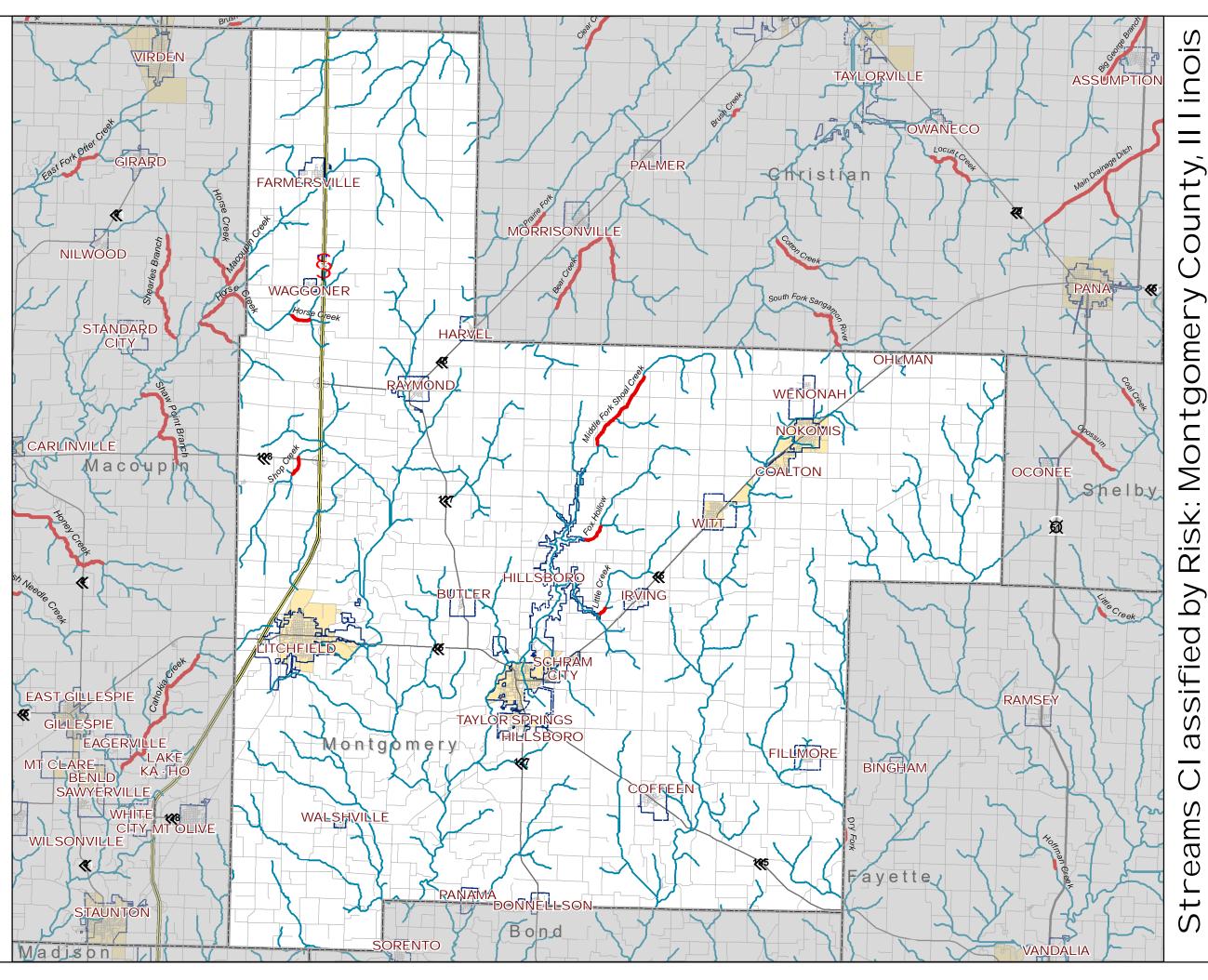
Legend

Streams without SFHAs
Streams
Municipal Boundaries
County Boundaries
Interstate Hwy
US Highways
State Routes
Roads
Risk CI asses

A - High Risk

C - Low Risk

B - Medium Risk



ATTACHMENT I

Intended for

Illinois Power Generating Company

Date

October 25, 2021

Project No.

1940100806-002

GROUNDWATER MONITORING PLAN

ASH POND NO. 1 COFFEEN POWER PLANT COFFEEN, ILLINOIS



GROUNDWATER MONITORING PLAN COFFEEN POWER PLANT ASH POND NO. 1

Project Name Coffeen Power Plant Ash Pond No. 1

Project No. **1940100806-002**

Recipient Illinois Power Generating Company

Document Type Groundwater Monitoring Plan

Revision FINAL

Date October 25, 2021

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LICENSED PROFESSIONAL CERTIFICATIONS

35 I.A.C. § 845.630 Groundwater Monitoring Systems (PE)

I, Eric J. Tlachac, a qualified professional engineer in good standing in the State of Illinois, certify that the groundwater monitoring system described in this document (Groundwater Monitoring Plan, Coffeen Power Plant Ash Pond No. 1), has been designed and constructed to meet the requirements of 35 I.A.C. § 845.630. The monitoring system was developed based on information included in the Hydrogeologic Site Characterization Report (Ramboll 2021; included in the Operating Permit to which this Groundwater Monitoring Plan is attached).

Eric J. Tla¢hac

Qualified Professional Engineer

062-063091 Illinois

Date: October 25, 2021



35 I.A.C. § 845.630 Groundwater Monitoring Systems (PG)

I, Brian G. Hennings, a qualified professional geologist in good standing in the State of Illinois, certify that the groundwater monitoring system described in this document (Groundwater Monitoring Plan, Coffeen Power Plant Ash Pond No. 1), has been designed and constructed to meet the requirements of 35 I.A.C. § 845.630. The monitoring system was developed based on information included in the Hydrogeologic Site Characterization Report (Ramboll 2021; included in the Operating Permit to which this Groundwater Monitoring Plan is attached).

Brian G. Hennings

Professional Geologist

196.001482 Illinois

Date: October 25, 2021

BRIAN G. HENNINGS GO 196.001482

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APPENDICES

Appendix A Statistical Analysis Plan

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ACRONYMS AND ABBREVIATIONS

35 I.A.C. Title 35 of the Illinois Administrative Code 40 C.F.R. Title 40 of the Code of Federal Regulations

AP1 Ash Pond No. 1

ASD Alternate Source Demonstration

bgs below ground surface
CCR coal combustion residuals
cm/s centimeters per second
CPP Coffeen Power Plant

DA deep aquifer

DCU deep confining unit

GMP Groundwater Monitoring Plan GWPS Groundwater Protection Standard

HCR Hydrogeologic Site Characterization Report

ID identification

IEPA Illinois Environmental Protection Agency
IPGC Illinois Power Generating Company

LCU lower confining unit mg/L milligrams per liter

NID National Inventory of Dams

NA not applicable No. number

NRT/OBG Natural Resources Technology, an OBG Company

Part 845 Residuals in Surface Impoundments: Title 35 of the Illinois Administrative Code §

845

PMP potential migration pathway
QA/QC quality assurance/quality control

Ramboll Ramboll Americas Engineering Solutions, Inc.

RL reporting limit

SI surface impoundment
TDS total dissolved solids
UA uppermost aquifer
UCU upper confining unit

USEPA United States Environmental Protection Agency

WLO water level only

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1. INTRODUCTION

1.1 Overview

In accordance with requirements of the Standards for the Disposal of Coal Combustion Residuals (CCR) in Surface Impoundments (SIs): Title 35 of the Illinois Administrative Code (35 I.A.C.) § 845 (Part 845) (Illinois Environmental Protection Agency [IEPA], April 15, 2021), Ramboll Americas Engineering Solutions, Inc. (Ramboll) has prepared this Groundwater Monitoring Plan (GMP) on behalf of Coffeen Power Plant (CPP), operated by Illinois Power Generating Company (IPGC). This report will apply specifically to the CCR Unit referred to as the Ash Pond Number (No.) 1 (AP1), Vistra identification (ID) No. 101, IEPA ID No. W1350150004-01, and National Inventory of Dams (NID) No. IL50722. This GMP includes Part 845 content requirements specific to 35 I.A.C. § 845.630 (Groundwater Monitoring System), 35 I.A.C. § 845.640 (Groundwater Sampling and Analysis), and 35 I.A.C. § 845.650 (Groundwater Monitoring Program) for AP1 at the CPP.

A checklist which identifies the specific requirements of 35 I.A.C. § 845.630, 35 I.A.C. § 845.640, and 35 I.A.C. § 845.650 is included in **Table 1-1**. The table provides references to sections, tables, and figures included in this document to locate the information that meets specific requirements of 35 I.A.C. § 845.630, 35 I.A.C. § 845.640, and 35 I.A.C. § 845.650.

1.2 Site Location and Background

The CPP is located approximately two miles south of the city of Coffeen, Illinois and approximately eight miles southeast of the city of Hillsboro, Illinois (**Figure 1-1**). AP1 is located in Montgomery County, in central Illinois, within Section 11, Township 7 North, and Range 7 East. The CPP is located between the two lobes of Coffeen Lake to the west, east, and south, and is bordered by agricultural land to the north. The CPP operated as a coal-fired power plant from 1964 to November 2019 and has five CCR management units. The approximately 1,100-acre Coffeen Lake was built by damming the McDavid Branch of the East Fork of Shoal Creek in 1963 for use as an artificial cooling lake for the CPP. Historically coal mines were operated at depth in the vicinity of the CPP as well as a US Minerals processing facility located to the north. Mine shafts, processing facilities, and historic coal storage associated with these historic operations were located south of AP1. IPGC ceased receipt of waste to AP1 prior to April 11, 2021.

Coffeen AP1 (**Figure 1-2**) is a 23-acre, unlined SI used to manage CCR (bottom ash) and non-CCR waste streams at the CPP. Its total storage capacity is approximately 300 acre-feet. AP1 (also known as the Bottom Ash/Recycle Pond) is a reclaimed ash pond that was constructed utilizing the existing earthen berms with reinforcement, as provided by Water Pollution Control Permit 1978-EA-389 issued by the Agency on May 26, 1978. AP1 (existing unlined SI) covers an area of approximately 23-acres, has berms up to 41 feet above the surrounding land surface, and a capacity of 300-acre-foot. Several years ago, air heater wash and boiler chemical cleaning wastes were directed to AP1, but this practice was discontinued. The bottom ash is periodically removed from AP1 for beneficial uses by a third-party contractor. Sluicing of waste to API ceased prior to November 4, 2019.

1.3 Conceptual Model

Significant site investigation has been completed at the CPP to characterize the geology, hydrogeology, and groundwater quality. Based on extensive investigation and monitoring, the

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CPP has been well characterized and detailed in the Hydrogeologic Site Characterization Report (HCR [Ramboll, 2021]; included in the Operating Permit to which this Plan is attached). A site conceptual model has been developed and is discussed below.

In addition to the CCR present at AP1, there are five principal layers of unlithified material present above the bedrock, which are categorized into hydrostratigraphic units below (from surface downward) based on stratigraphic relationships and common hydrogeologic characteristics.

- **Upper Confining Unit (UCU):** Composed of the Roxana and Peoria Silts (Loess Unit) and the upper clayey portion of the Hagarstown member which are classified as silts to clayey silts and gravelly clay below the surficial soil. The UCU has been eroded east of AP1, near the Unnamed Tributary.
- **Uppermost Aquifer:** The uppermost aquifer is the Hagarstown Member which is classified as primarily sandy to gravelly silts and clays with thin beds of sands. Similar to the Loess Unit, the Hagarstown is absent in some locations near the Unnamed Tributary.
- Lower Confining Unit (LCU): Comprised of the Vandalia Member, Mulberry Grove Member, and Smithboro Member. These units include a sandy to silty till with thin, discontinuous sand lenses, a discontinuous and limited extent sandy silt which has infilled prior erosional features, and silty to clayey diamicton, respectively. This unit has been identified as a potential migration pathway (PMP) because downward vertical gradients indicate that there is the potential for impacts to migrate within this unit.
- **Deep Aquifer (DA):** Sand and sandy silt/clay units of the Yarmouth Soil, which include accretionary deposits of fine sediment and organic materials, typically less than five feet thick and discontinuous across the CPP. This unit is also identified as a PMP, because it is the first permeable unit below the uppermost aquifer.
- **Deep Confining Unit (DCU):** Comprised of the Banner Formation, generally consists of clays, silts, and sands. The Lierle Clay Member is the upper layer of the Banner Formation which was encountered at the Site.

Bedrock of the Bond Formation, which consists of limestone and calcareous clays and shale, was not encountered in the borings advanced on CPP.

Flow of groundwater from central portions of the CPP to Coffeen Lake or the Unnamed Tributary through the uppermost aquifer are the primary pathways for contaminant migration. The LCU and DA underlying the uppermost aquifer have been identified as PMPs. Groundwater elevations are primarily controlled by surface topography, geologic unit topography, and water levels within Coffeen Lake and the Unnamed Tributary. A groundwater divide trending north-south is observed running through the approximate center of the CPP (**Figure 1-3**). Phreatic surfaces or water elevations within the SIs are generally consistent and have not been observed to fluctuate with groundwater elevations indicating limited hydraulic connection with the SIs.

Part 845 parameters were monitored in uppermost aquifer monitoring wells at AP1 as part of the Title 40 of the Code of Federal Regulations (40 C.F.R.) § 257 monitoring program beginning in 2015. These data were supplemented with sampling of additional locations in 2021. The results indicate that the following parameters were detected at concentrations greater than the applicable 35 I.A.C. § 845.600 groundwater protection standards (GWPSs) and are considered potential exceedances:

• Arsenic in downgradient uppermost aquifer wells G302, G303, and G304/G307. Arsenic was also detected in upgradient uppermost aquifer well G306.

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- Boron in downgradient uppermost aquifer wells G301, G302, G303, G304/G307, G305, G308, G311, and G313. Boron was also detected in upgradient uppermost aquifer well G306.
- Cadmium in downgradient uppermost aquifer well G304/G307.
- Chromium in downgradient uppermost aquifer well G304/G307.
- Cobalt in downgradient uppermost aquifer wells G301, G302, G303, G304/G307, and G305; and in downgradient LCU well G314. Cobalt was also detected in upgradient uppermost aquifer well G306.
- Lead in downgradient uppermost aquifer wells G301, G302, G303, G304/G307 and G305; and in downgradient LCU well G316. Lead was also detected in upgradient uppermost aquifer well G306.
- Lithium in downgradient uppermost aquifer wells G303 and G304/G307.
- pH (lower limit) in downgradient uppermost aquifer wells G301 and G312.
- Radium 226 and 228 combined in downgradient LCU well G316.
- Sulfate in downgradient uppermost aquifer wells G301, G302, G303, G304/G307, G305, G308, G309, G310, G311, G312, G313, G315, and G317; in downgradient LCU wells G307D, G314, and G316; and in downgradient DA well G314D. Sulfate was also detected at concentrations greater than the GWPS in upgradient uppermost aquifer well G306.
- Total dissolved solids (TDS) in downgradient uppermost aquifer wells G301, G302, G303, G304/G307, G305, G308, G309, G310, G311, G312, G313, G315, and G317; in downgradient LCU wells G307D, G314, and G316; and in downgradient DA well G314D. Sulfate was also detected at concentrations greater than the GWPS in upgradient uppermost aquifer well G306.

Concentration results for the above parameters were compared directly to 35 I.A.C. § 845.600 GWPS, without an evaluation of background concentrations. Evaluation of background groundwater quality has been completed as part of this GMP, and compliance with Part 845 will be determined following the first round of groundwater sampling. The first round of groundwater sampling for compliance will be completed the quarter following issuance of the Operating Permit and in accordance with this GMP.

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2. GROUNDWATER MONITORING SYSTEMS

2.1 Existing Monitoring Well Network and Analysis

This GMP is being provided to propose a groundwater monitoring network and monitoring program specific to AP1 that will comply with Part 845. Monitoring networks and programs that apply to other units are not discussed in this GMP. Those programs will continue to be performed as specified in IEPA approvals. Any future modifications will be proposed and submitted to IEPA for approval in a separate document. The remaining discussion in this document will include only these networks and monitoring programs that are applicable and specific to the AP1, specifically the 40 C.F.R. § 257 network and the proposed Part 845 monitoring network.

2.1.1 40 C.F.R. § 257 Monitoring Program

The 40 C.F.R. § 257 well network for AP1 consists of six monitoring wells installed nearby or adjacent to AP1 within the uppermost aquifer. The AP1 40 C.F.R. § 257 well network consists of two background monitoring wells (G281 and G306) and four compliance monitoring wells (G301, G302, G303, and G307). The boring logs, well construction forms, and other related monitoring well forms are available in the Operating Records as required by 40 C.F.R. § 257.91 for each monitored CCR Unit or CCR Multi-Unit, and are included in Appendix C of the HCR (included in the Operating Permit to which this Plan is attached).

Assessment monitoring in accordance with 40 C.F.R. § 257.95 was initiated on April 9, 2018. Details on the procedures and techniques used to fulfill the groundwater sampling and analysis program requirements are found in the Sampling and Analysis Plan for AP1 (Natural Resource Technology, an OBG Company [NRT/OBG], 2017).

Groundwater samples are collected semiannually and analyzed for the laboratory and field parameters from Appendix III and Appendix IV of 40 C.F.R. § 257, summarized in **Table A** below.

Table A. 40 C.F.R. § 257 Groundwater Monitoring Program Parameters

| Field Parameters ¹ | | | | | | | |
|---|-------------|------------|-----------------------------|--|--|--|--|
| Groundwater Elevation | рH | | | | | | |
| Appendix III Parameters (Total, except TDS) | | | | | | | |
| Boron | Chloride | Sulfate | | | | | |
| Calcium | Fluoride | TDS | | | | | |
| Appendix IV Paramete | ers (Total) | | | | | | |
| Antimony | Cadmium | Lithium | Selenium | | | | |
| Arsenic | Chromium | Mercury | Thallium | | | | |
| Barium | Cobalt | Molybdenum | Radium 226 and 228 combined | | | | |
| Beryllium | Lead | | | | | | |

¹Dissolved oxygen, temperature, specific conductance, oxidation/reduction potential, and turbidity are recorded during sample collection.

Results and analysis of groundwater sampling are reported annually by January 31 of the following year and made available on the CCR public website as required by 40 C.F.R. § 257.

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2.1.2 Part 845 Well Installation and Monitoring

In 2021, 13 additional monitoring wells (G307D, G308, G309, G310, G311, G311D, G312, G313, G314, G314D, G315, G316, and G317) were installed along the perimeter of AP1 to assess the vertical and horizontal lithology, stratigraphy, chemical properties, and physical properties of geologic layers to a minimum of 100 feet below ground surface (bgs) as specified in 35 I.A.C. § 845.620(b). Additionally, two leachate monitoring wells (XPW01 and XPW02) were installed within the AP1 unit to characterize the CCR materials.

Prospective Part 845 monitoring wells were sampled for eight rounds from March to August 2021 and the results were assessed for selection of the AP1 Part 845 monitoring well network. Groundwater samples were collected and analyzed for 35 I.A.C. § 845.600 parameters as summarized in **Table B** below.

Table B. Part 845 Groundwater Monitoring Program Parameters

| Field Parameters ¹ | | | | | | |
|--------------------------------|----------|-----------|------------|--|--|--|
| Groundwater Elevation | pН | Turbidity | | | | |
| Metals (Total) | | | | | | |
| Antimony | Boron | Cobalt | Molybdenum | | | |
| Arsenic | Cadmium | Lead | Selenium | | | |
| Barium | Calcium | Lithium | Thallium | | | |
| Beryllium | Chromium | Mercury | | | | |
| Inorganics (Total, except TDS) | | | | | | |
| Fluoride | Sulfate | Chloride | TDS | | | |
| Other (Total) | | | | | | |
| Radium 226 and 228 combined | | | | | | |

¹ Dissolved oxygen, temperature, specific conductance, and oxidation/reduction potential were recorded during sample collection.

Data and results from the Part 845 background monitoring were included in the water quality discussion included in the HCR (included in the Operating Permit to which this Plan is attached). The data collected from background locations during the Part 845 monitoring were used to evaluate and calculate background concentrations for AP1. The evaluation and discussion are included in **Section 3.2** of this report.

Data collected from the 40 C.F.R. § 257 monitoring network from 2015 to 2021, and from the Part 845 background monitoring were used for selection of the Part 845 monitoring well network proposed in **Section 2.2**.

2.2 Proposed Part 845 Monitoring Well Network

The groundwater monitoring network proposed in this plan will include 12 monitoring wells screened in the uppermost aquifer (G281, G301, G302, G303, G305, G306, G307, G308, G310, G312, G313, and G315), three monitoring wells screened in the LCU (G307D, G314, and G316), one well screened in the DA (G314D), and three temporary water level only surface water staff gages (SG-02, SG-03, and XSG-01). The proposed network is summarized in **Table C** below and displayed on **Figure 2-1.** Sixteen wells (two background and 14 compliance) will be used to monitor groundwater concentrations within the hydrostratigraphic units.

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The groundwater samples collected from the 16 wells will be used to monitor and evaluate groundwater quality and demonstrate compliance with the groundwater quality standards listed in 35 I.A.C. § 845.600(a). The proposed monitoring wells will yield groundwater samples that represent the quality of downgradient groundwater at the CCR boundary (as required in 35 I.A.C. § 845.630(a)(2)). Monitoring well depths and construction details are listed in **Table 2-1** and summarized in **Table C** below.

Table C. Proposed Part 845 Monitoring Well Network

| Tuble Cittopes | ed Part 843 Monitoring Wen Ne | | |
|------------------------|-------------------------------|---------------------------------------|------------|
| Well ID | Monitored Unit | Well Screen Interval (feet bgs) | Well Type¹ |
| G281 | UA | 15.5 - 20.2 | Background |
| G301 | UA | 11.3 - 16.0 | Compliance |
| G302 | UA | 13.2 - 17.9 | Compliance |
| G303 | UA | 10.0 - 20.0 | Compliance |
| G305 | UA | 13.4 - 18.3 | Compliance |
| G306 | UA | 13.1 - 17.7 | Background |
| G307 | UA | 13.0 - 17.8 | Compliance |
| G307D | LCU | 49.0 - 58.8 | Compliance |
| G308 | UA | 10.1 - 14.9 | Compliance |
| G310 | UA | 10.2 - 15.0 | Compliance |
| G312 | UA | 9.8 - 14.6 | Compliance |
| G313 | UA | 6.3 - 11.1 | Compliance |
| G314 | LCU | 14.6 - 19.6 | Compliance |
| G314D | DA | 39.3 - 49.1 | Compliance |
| G315 | UA | 9.7 - 14.5 | Compliance |
| G316 | LCU | 10.0 - 14.8 | Compliance |
| XSG-01 ^{2, 3} | CCR | NA | WLO |
| SG-02 ^{2, 3} | Surface Water | NA | WLO |
| SG-03 ^{2, 3} | Surface Water | NA | WLO |

¹ Well type refers to the role of the well in the monitoring network.

2.3 Well Abandonment

No wells are currently proposed for abandonment.

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 $^{^{\}rm 2}\,\text{Surface}$ water level measuring points.

³ Location is temporary pending implementation of impoundment closure per an approved Construction Permit Application.

NA = Not Applicable

UA = uppermost aquifer

WLO = water level only

3. APPLICABLE GROUNDWATER QUALITY STANDARDS

3.1 Groundwater Classification

Groundwater within the uppermost aquifer at AP1 meets the definition of Class I – Potable Resource Groundwater (35 I.A.C. § 620.210), based on the following criteria:

- The groundwater is located more than 10 feet bgs; and
- Field hydraulic conductivity tests performed in the uppermost aquifer resulted in an overall (geometric mean) horizontal hydraulic conductivity of 2.0×10^{-3} centimeters per second (cm/s), exceeding the 1×10^{-4} cm/s criterion.

3.2 Statistical Evaluation of Background Groundwater Data

A Statistical Analysis Plan (**Appendix A**) has been developed to describe procedures that will be used to establish background conditions and implement compliance monitoring as necessary and required by 35 I.A.C. § 845.640 and 35 I.A.C. § 845.650. The Statistical Analysis Plan was prepared in accordance with the requirements of 35 I.A.C. § 845.640(f), with reference to the acceptable statistical procedures provided in United States Environmental Protection Agency's (USEPA) *Statistical Analysis of Groundwater Monitoring Data at RCRA Facilities, Unified Guidance* (*Unified Guidance*, March 2009), and is intended to provide a logical process and framework for conducting the statistical analysis of the data obtained during groundwater monitoring.

In accordance with 35 I.A.C. § 845.640(f)(1), the statistical method chosen for analysis of background groundwater quality was either the tolerance interval or the prediction interval procedure for each constituent listed in 35 I.A.C. § 845.600(a)(1) at this CCR unit per 35 I.A.C. § 845.640(f)(1)(C). A comparison of the statistical background concentrations and groundwater quality standards listed in 35 I.A.C. § 845.600(a)(1) and the resulting GWPSs are summarized in **Table 3-1**.

3.3 Applicable Groundwater Protection Standards

The applicable GWPS will be established in accordance with 35 I.A.C. § 845.600(a) (greater of the background concentration or numerical limit specified in 35 I.A.C. § 845.600(a)(1)). The results of the statistical analysis of background groundwater data (**Table 3-1**) indicate that most background concentrations in the uppermost aquifer and PMP are less than the groundwater quality standards listed in 35 I.A.C. § 845.600(a)(1). Therefore, for these parameters, the groundwater quality standards listed in 35 I.A.C. § 845.600(a)(1) will be applied to the results from the proposed groundwater monitoring network. The only exception being boron, where the background concentration is greater than the 35 I.A.C. § 845.600(a)(1) standard (3.2 milligrams per liter [mg/L] versus 2 mg/L). In this instance, the GWPS will be the background concentration.

Under most circumstances, the GWPS will be compared to the lower confidence limit for the observed concentrations for each constituent in each compliance well. Exceptions are when there are high percentages (greater than 50 percent) of non-detects in compliance well data, for which a future mean (for 50 to 70 percent non-detects) or median (for greater than 70 percent non-detects) will be compared to the GWPS. Consistent with the *Unified Guidance*, the same general statistical method of confidence interval testing against a fixed GWPS is recommended in compliance and corrective action programs. Confidence intervals provide a flexible and statistically accurate method to test how a parameter estimated from a single sample compares

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to a fixed numerical limit. Confidence intervals explicitly account for variation and uncertainty in the sample data used to construct them.

Evaluation of the applicable standards will occur in conjunction with the analysis of groundwater quality results. Background calculations and the resulting concentrations may be updated as appropriate, in accordance with the Statistical Analysis Plan included in **Appendix A.**

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4. GROUNDWATER MONITORING PLAN

The groundwater monitoring plan will monitor and evaluate groundwater quality to demonstrate compliance with the groundwater quality standards included in 40 C.F.R. § 257.94(e), 40 C.F.R. § 257.95(h), and 35 I.A.C. § 845.600(a). The groundwater monitoring program will include sampling and analysis procedures that are consistent and that provide an accurate representation of groundwater quality at the background and compliance wells as required by 35 I.A.C. § 845.630. As discussed in **Section 2**, two monitoring programs specific to AP1 exist: the 40 C.F.R. § 257 monitoring program and the proposed Part 845 monitoring program. These networks will continue to be monitored until USEPA approves Part 845. It is expected that upon USEPA approval of Part 845, the 40 C.F.R. § 257 monitoring program and reporting will be eliminated, and the proposed Part 845 monitoring and reporting included in this Plan will continue until requirements of Part 845 have been achieved.

4.1 Monitoring Networks and Parameters

4.1.1 40 C.F.R. § 257 Groundwater Monitoring

The existing 40 C.F.R. § 257 monitoring program was discussed in detail in **Section 2.1.1**. Six wells (two background and four compliance) are sampled for Appendix III and Appendix IV parameters on a semi-annual frequency. No changes are proposed to this monitoring network. Well locations and parameters will continue to be monitored and reported as required by 40 C.F.R. § 257 until USEPA approves Part 845.

4.1.2 Part 845 Groundwater Monitoring

The proposed Part 845 Monitoring Network will consist of two background monitoring wells (G281 and G306), 14 compliance monitoring wells (G301, G302, G303, G305, G307, G307D, G308, G310, G312, G313, G314, G314D, G315, and G316), and three temporary water level only surface water staff gages (SG-02, SG-03, and XSG-01) to monitor potential impacts from AP1 (**Figure 2-1**). These monitoring wells are screened within the uppermost aquifer (G281, G301, G302, G303, G305, G306, G307, G308, G310, G312, G313, G315,), the LCU (G307D, G314, and G316), and DA (G314D) along the perimeter of AP1. Groundwater samples will be collected and analyzed for the laboratory and field parameters in **Table D** below.

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Table D. Part 845 Groundwater Monitoring Program Parameters

| Field Parameters ¹ | | | | | | |
|--------------------------------|----------|-----------|------------|--|--|--|
| Groundwater Elevation | рН | Turbidity | | | | |
| Metals (Total) | | | | | | |
| Antimony | Boron | Cobalt | Molybdenum | | | |
| Arsenic | Cadmium | Lead | Selenium | | | |
| Barium | Calcium | Lithium | Thallium | | | |
| Beryllium | Chromium | Mercury | | | | |
| Inorganics (Total, except TDS) | | | | | | |
| Fluoride | Sulfate | Chloride | TDS | | | |
| Other (Total) | | | | | | |
| Radium 226 and 228 combined | | | | | | |

¹ Dissolved oxygen, temperature, specific conductance, and oxidation/reduction potential will be recorded during sample collection.

All parameters listed above were sampled a minimum of eight times by October 18, 2021 to establish background groundwater quality in accordance with 35 I.A.C. § 845.650 (b)(1)(A). Discussion of background groundwater quality is included in **Section 3.2**.

4.2 Sampling Schedule

Groundwater sampling for the Part 845 monitoring well network will initially be performed quarterly according to the following schedule:

Table E. Part 845 Sampling Schedule

| Frequency | Duration |
|---|---|
| Monthly | Begins: the quarter following approval of this plan and issuance of the Operating Permit. |
| (groundwater elevations only) | Ends: Following the 30-year post closure care period and following IEPA approval of documentation that groundwater concentrations are below standards in 35 I.A.C. § 845.600 and concentrations exceeding background are not increasing and meet requirements in 35 I.A.C. § 845.780 (c)(2)(B)(i) and (ii). |
| Quarterly | Begins: the quarter following approval of this plan and issuance of the Operating Permit. |
| (groundwater quality) | Ends: Following the 30-year post closure care period and following IEPA approval of documentation that groundwater concentrations are below standards in 35 I.A.C. § 845.600 and concentrations exceeding background are not increasing and meet requirements in 35 I.A.C. § 845.780 (c)(2)(B)(i) and (ii), or upon IEPA approval of an alternate schedule as allowed by 35 I.A.C. § 845.650(b)(4). |
| Semi-annual (groundwater quality) | Begins: Following 5 years of quarterly groundwater monitoring and IEPA approval of a demonstration that groundwater concentrations are below standards in 35 I.A.C. § 845.600 and not exhibiting statistically-significant increasing trends, monitoring effectiveness is not compromised by a semi-annual schedule, and sufficient data has been collected to characterize groundwater. |
| | Ends: Following detection of a statistically-significant increasing trend in groundwater concentrations or an exceedance of the standards in 35 I.A.C. § 845.600 (quarterly monitoring shall be resumed in these circumstances), or following the 30-year post closure care period and following IEPA approval of documentation that groundwater concentrations |

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are below standards in 35 I.A.C. § 845.600 and concentrations exceeding background are not increasing and meet requirements in 35 I.A.C. § 845.780 (c)(2)(B)(i) and (ii).

4.3 Groundwater Sample Collection

Groundwater sampling procedures have been developed and the collection of groundwater samples is being implemented to meet the requirements of 35 I.A.C. § 845.640. In addition to groundwater well samples, quality assurance samples will be collected as described in **Section 4.5** (**Table 4-1**).

4.4 Laboratory Analysis

Laboratory analysis will be performed consistent with the requirements of 35 I.A.C. § 845.640(j) by a state-certified laboratory using methods approved by IEPA and USEPA. Laboratory methods may be modified based on laboratory equipment availability or procedures, but the Reporting Limit (RL) for all parameters analyzed, regardless of method, will be lower than the applicable groundwater quality standard. RLs for the applicable parameters are summarized in **Table 4-2**. Concentrations lower than the RL will be reported as less than the RL.

4.5 Quality Assurance Program

Consistent with the requirements of 35 I.A.C. § 845.640(a)(5), the sampling and analysis program includes procedures and techniques for quality assurance/quality control (QA/QC). Additional quality assurance samples to be collected will include the following:

- Field duplicates will be collected at a frequency of one per group of ten or fewer investigative water samples.
- One equipment blank sample will be collected and analyzed for each day of sampling. If dedicated sampling equipment is used, then equipment blank samples will not be collected.
- The duplicate and equipment blank quality assurance samples will be supplemented by the laboratory QA/QC program, which typically includes:
 - Regular generation of instrument calibration curves to assure instrument reliability
 - Laboratory control samples and/or quality control check standards that have been spiked,
 and analyses to monitor the performance of the analytical method
 - Matrix spike/matrix spike duplicate analyses to determine percent recoveries and relative percent differences for each of the parameters detected
 - Analysis of replicate samples to check the precision of the instrumentation and/or methodology employed for all analytical methods
 - Analysis of method blanks to assure that the system is free of contamination

Water quality meters used to measure pH and turbidity will be calibrated according to manufacturer's specifications. At a minimum, it is recommended that calibration of pH occur daily prior to sampling and checked for accuracy at the end of each day. Unusual or suspect pH measurements during sampling events will be flagged, evaluated, and additional calibration may be performed throughout the sampling events. Turbidity meters will be checked daily, prior to and following sampling. Unusual measurements or erratic meter performance will be flagged and evaluated for overall effects on the data prior to reporting.

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4.6 Groundwater Monitoring System Maintenance Plan

Consistent with the requirements of 35 I.A.C. § 845.630(e)(2), maintenance will be performed as needed to assure that the monitoring wells provide representative groundwater samples. Monitoring wells will be inspected during each groundwater sampling event; inspections will consist of the following:

- Visual inspection, clearing of vegetation, replacement of markers, and painting of protective casings as needed to assure that monitoring wells are clearly marked and accessible
- Visual inspection and repair or replacement of well aprons as needed to assure that they are intact, drain water away from the well, and have not heaved
- Visual inspection and repair or replacement of protective casings as needed to assure that they are undamaged, and that locks are present and functional
- Checks to assure that well caps are intact and vented, unless in flood-prone areas in which case caps will not be vented
- Annual measurement of monitoring well depths to determine the degree of siltation within the wells. Wells will be redeveloped as needed to remove siltation from the screened interval if it impedes flow of water into the well
- · Checks to assure that wells are clear of internal obstructions, and flow freely

If maintenance of a monitoring well cannot address an identified deficiency, a replacement well will be installed.

4.7 Statistical Analysis

Statistical analysis will be consistent with procedures listed in 35 I.A.C. § 845.640(f). A Statistical Analysis Plan, provided in **Appendix A**, has been developed to summarize the statistical procedures that will be used to evaluate the groundwater results.

4.8 Data Reporting

Data reporting for the 40 C.F.R. § 257 monitoring program will be consistent with recordkeeping, notification, and internet posting requirements described in 40 C.F.R. § 257.105 through 257.107.

Groundwater monitoring and analysis completed in accordance with the Part 845 monitoring under an approved monitoring program will be reported to IEPA within 60 days after completion of sampling and the data placed in the facility's operating record as required by 35 I.A.C. § 845.610(b)(3)(D). Within 14 days of posting to the operating record, information will be posted to the publicly accessible internet site "Illinois CCR Rule Compliance Data and Information" as required by 35 I.A.C. § 845.810(d). Information will also be submitted to IEPA annually by January 31 as required by 35 I.A.C. § 845.550, for data collected the preceding year. The report will include the status of the groundwater monitoring and any required corrective action plan for AP1 in addition to other requirements detailed in 35 I.A.C. § 845.610(e).

4.9 Compliance with Applicable On-site Groundwater Protection Standards

In accordance with 35 I.A.C. § 845.600(a)(1), the groundwater protection standard at the waste boundary will be the higher of either the 35 I.A.C. § 845.600 standard or the concentration determined by background groundwater monitoring.

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As provided in 35 I.A.C. § 845.780(c)(2), at the end of the 30-year post-closure care period, groundwater monitoring will continue to be conducted in post-closure care until the groundwater results show the concentrations are:

- Below the GWPS in 35 I.A.C. § 845.600; and
- Not increasing for those constituents over background, using the statistical procedures and performance standards in 35 I.A.C. § 845.640(f) and (q), provided that:
 - Concentrations have been reduced to the maximum extent feasible; and
 - Concentrations are protective of human health and the environment.

Following detection of an exceedance of the GWPS, an Alternate Source Demonstration (ASD) will be evaluated as described in **Section 4.10**.

4.10 Alternate Source Demonstrations

As allowed in 35 I.A.C. § 845.650(e), following detection of an exceedance of the GWPS, an ASD will be evaluated and, if completed, submitted to IEPA within 60 days. The ASD will provide lines of evidence that a source other than AP1 caused the contamination and AP1 did not contribute to the contamination, or that the exceedance of the GWPS resulted from error in sampling, analysis, statistical evaluation, natural variation in groundwater quality, or a change in the potentiometric surface and groundwater flow direction.

The ASD will include information and analysis that supports the conclusions and a certification of accuracy by a qualified professional engineer. Once the ASD is approved by IEPA, the Part 845 groundwater monitoring will continue as defined in **Section 4.1.2**.

If an ASD is not completed and submitted, or IEPA does not approve the ASD, a notification of the exceedance will be provided to IEPA and placed in the operating record. Additional actions will also be completed as required by 35 I.A.C § 845.650(d)(1) through (3), including initiation of an assessment of corrective measures under 35 I.A.C § 845.660. As allowed in 35 I.A.C § 845.650(e)(7) a petition for review of IEPA's non-concurrence under 35 I.A.C. § 105 may also be filed.

4.11 Assessment of Corrective Measures and Corrective Action

As described in 35 I.A.C. § 845.660, if the ASD summarized in **Section 4.10** has not been approved by IEPA, an assessment of corrective measures will be initiated within 90 days of the detection of a result exceeding 35 I.A.C. § 845.600 standards (*i.e.*, receipt of laboratory data). The assessment of corrective measures will include at least the following (35 I.A.C. § 845.660 (c)):

- The performance, reliability, ease of implementation, and potential impacts of appropriate
 potential remedies, including safety impacts, cross-media impacts, and control of exposure to
 any residual contamination;
- The time required to begin and complete the corrective action plan; and
- The institutional requirements, such as State or local permit requirements or other environmental or public health requirements that may substantially affect implementation of the corrective action plan.

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Within one year of completing the assessment of corrective measures, a corrective action plan will be developed to identify the selected remedy in accordance with 35 I.A.C. § 845.670. If closure of the CCR Unit is required, a closure alternatives analysis will be completed as specified in 35 I.A.C. § 845.710. The analysis and selected alternative will be submitted to IEPA in a Closure Plan as specified by 35 I.A.C. § 845.720. Groundwater monitoring proposed in this Addendum will continue as specified until the post closure care period has expired and IEPA has approved termination of post-closure care.

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5. REFERENCES

Illinois Environmental Protection Agency, 2021. Standards for the Disposal of Coal Combustion Residuals in Surface Impoundments: Title 35 of the Illinois Administrative Code § 845, April 15, 2021.

Natural Resource Technology, An OBG Company (NRT/OBG), 2017. Sampling and Analysis Plan, Coffeen Ash Pond No. 1, Coffeen Power Station, Coffeen, Illinois, Project No. 2285, Revision 0, October 17, 2017.

Ramboll Americas Engineering Solutions, Inc. (Ramboll), 2021. *Hydrogeologic Site Characterization Report. Coffeen Ash Pond No. 1, Coffeen Power Plant. Coffeen, Illinois.*

United States Environmental Protection Agency (USEPA), March 2009. *Statistical Analysis of Groundwater Monitoring Data at RCRA Facilities – Unified Guidance*. Office of Resource Conservation and Recovery, Program Implementation and Information Division, United States Environmental Protection Agency, Washington D.C. EPA/530/R-09/007.

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TABLES

TABLE 1-1. PART 845 REQUIREMENTS CHECKLIST

GROUNDWATER MONITORING PLAN
COFFEEN POWER PLANT
ASH POND NO. 1
COFFEEN, ILLINOIS

| Part 845 Reference | Part 845 Components | Location of Information in GMP | | | | |
|--|---|---|--|--|--|--|
| 845.630 | Groundwater Monitoring Systems | | | | | |
| 845.630(a)(2) | Potential contaminant pathways must be monitored. | Sections 2.2 & 4.1.2 | | | | |
| 845.630(a) 845.630(b) 845.630(c) | At least two upgradient wells and four downgradient wells (min. 1 and 3, but requires additional documentation) | Sections 2.2 & 4.1.2 Table 2-1 Figure 2-1 | | | | |
| 845.630(a) 845.630(b) 845.630(c) | Downgradient Well Density | Figure 2-1 | | | | |
| 845.630(a)(2) | Downgradient wells at waste boundary | Figure 2-1 | | | | |
| 845.640 | Groundwater Sampling and Analysis Requirements | | | | | |
| 845.640(a) | Consistent sampling and analysis procedures | Section 4 Tables 4-1 & 4-2 | | | | |
| 845.640(b) | Methods are appropriate | Section 4 Tables 4-1 & 4-2 | | | | |
| 845.640(c) | Groundwater elevations must be measured in each well prior to purging, each time groundwater is sampled. | Section 4.3 | | | | |
| 845.640 (d)(e)(f)(g)(h) | Establishment of background and application of statistical methods | Sections 3.2 & 4.7 Appendix A | | | | |
| 845.640(i) | Analyze total recoverable metals | Section 4.1.2 | | | | |
| 845.640(j) | Analyze groundwater samples using a certified laboratory | Section 4.4 | | | | |

TABLE 1-1. PART 845 REQUIREMENTS CHECKLIST

GROUNDWATER MONITORING PLAN COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Part 845 Reference | Part 845 Components | Location of Information in GMP | | | |
|-----------------------|---|--|--|--|--|
| 845.650 | Groundwater Monitoring Program | | | | |
| 845.650(a) | Must include monitoring for all constituents with a groundwater protection standard in Section 845.600(a), calcium, and turbidity | Section 4.1.2 | | | |
| 845.650(b)(c) | Groundwater Monitoring Frequency | Sections 4.1.2 & 4.2 | | | |
| 845.650(d)(e) | Exceedances of the groundwater protection standard | Sections 4.9, 4.10 & 4.11 | | | |
| 845.650(b)(2) and (3) | Staff gauge/ piezometer to monitor head in impoundment | Sections 2.2 & 4.1.2 Figure 2-1 (XSG-01) | | | |
| NA | Staff gauge/ piezometer to monitor head of neighboring surface water body | Sections 2.2 & 4.1.2 Figure 2-1 (SG-02 & SG-03) | | | |

[O: CJC 09/01/21; C: SSW 09/15/21]

Notes:

GMP = Groundwater Monitoring Plan NA = Not Applicable

TABLE 2-1. MONITORING WELL LOCATIONS AND CONSTRUCTION DETAILS

GROUNDWATER MONITORING PLAN COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Well Number | Туре | HSU | Date Constructed | Top of PVC Elevation (ft) | Measuring Point Elevation (ft) | Measuring Point Description | Ground Elevation (ft) | Screen Top Depth (ft BGS) | Screen Bottom Depth (ft BGS) | Screen Top Elevation (ft) | Screen Bottom Elevation (ft) | Well Depth (ft BGS) | Bottom of Boring Elevation (ft) | Screen Length (ft) | Screen Diameter (inches) | Latitude (Decimal Degrees) | Longitude (Decimal Degrees) |
|----------------|------|-----|---------------------|---------------------------------|---|-----------------------------------|-----------------------------|------------------------------------|---------------------------------------|---------------------------------|---------------------------------------|---------------------------|--|--------------------------|--------------------------------|----------------------------------|-----------------------------------|
| G281 | В | UA | 09/08/2015 | | 626.36 | Top of Disk | 623.82 | 15.51 | 20.16 | 608.31 | 603.66 | 20.30 | 603.50 | 4.7 | 2 | 39.065405 | -89.399322 |
| G301 | С | UA | 09/04/2015 | | 622.65 | Top of Disk | 620.88 | 11.31 | 15.96 | 608.96 | 604.31 | 16.21 | 604.10 | 4.7 | 2 | 39.05951 | -89.395415 |
| G302 | С | UA | 09/04/2015 | | 620.04 | Top of Disk | 618.52 | 13.21 | 17.86 | 604.74 | 600.09 | 18.39 | 599.60 | 4.7 | 2 | 39.059544 | -89.393192 |
| G303 | С | UA | 08/26/2010 | | 622.02 | Top of Disk | 619.33 | 10.00 | 20.00 | 609.07 | 599.07 | 20.40 | 598.70 | 10 | 2 | 39.057144 | -89.391721 |
| G305 | С | UA | 05/03/2016 | 625.67 | 625.67 | Top of PVC | 623.23 | 13.44 | 18.27 | 609.10 | 604.27 | 18.50 | 604.10 | 4.8 | 2 | 39.056558 | -89.396798 |
| G306 | В | UA | 05/03/2016 | 625.91 | 625.91 | Top of PVC | 623.57 | 13.07 | 17.68 | 609.77 | 605.16 | 17.90 | 604.80 | 4.6 | 2 | 39.056494 | -89.393556 |
| G307 | С | UA | 07/27/2016 | 624.60 | 624.60 | Top of PVC | 624.73 | 12.96 | 17.80 | 609.12 | 604.28 | 18.22 | 603.90 | 4.8 | 2 | 39.057214 | -89.395545 |
| G307D | С | LCU | 01/19/2021 | 624.88 | 624.88 | Top of PVC | 622.51 | 48.98 | 58.75 | 573.53 | 563.76 | 59.60 | 562.50 | 9.8 | 2 | 39.05721 | -89.39552 |
| G308 | С | UA | 01/18/2021 | 624.59 | 624.59 | Top of PVC | 621.59 | 10.10 | 14.89 | 611.49 | 606.70 | 15.24 | 605.80 | 4.8 | 2 | 39.057379 | -89.397134 |
| G310 | С | UA | 02/09/2021 | 622.87 | 622.87 | Top of PVC | 619.89 | 10.24 | 15.03 | 609.65 | 604.86 | 15.38 | 604.00 | 4.8 | 2 | 39.059532 | -89.396907 |
| G312 | С | UA | 01/15/2021 | 619.78 | 619.78 | Top of PVC | 616.92 | 9.79 | 14.58 | 607.13 | 602.34 | 14.93 | 601.70 | 4.8 | 2 | 39.059558 | -89.391983 |
| G313 | С | UA | 02/05/2021 | 614.30 | 614.30 | Top of PVC | 611.51 | 6.30 | 11.11 | 605.21 | 600.40 | 11.46 | 599.50 | 4.8 | 2 | 39.058773 | -89.391124 |
| G314 | С | LCU | 02/05/2021 | 613.88 | 613.88 | Top of PVC | 611.11 | 14.56 | 19.58 | 596.55 | 591.53 | 20.02 | 591.10 | 5 | 2 | 39.05782 | -89.390964 |
| G314D | С | DA | 02/04/2021 | 613.70 | 613.70 | Top of PVC | 610.87 | 39.34 | 49.11 | 571.53 | 561.76 | 49.47 | 510.60 | 9.8 | 2 | 39.057852 | -89.390958 |
| G315 | С | UA | 01/14/2021 | 623.52 | 623.52 | Top of PVC | 620.94 | 9.69 | 14.48 | 611.25 | 606.46 | 14.85 | 605.00 | 4.8 | 2 | 39.057165 | -89.393667 |
| G316 | С | LCU | 02/26/2021 | 602.59 | 602.59 | Top of PVC | 599.64 | 10.02 | 14.82 | 589.62 | 584.82 | 15.16 | 583.90 | 4.8 | 2 | 39.057847 | -89.389698 |
| XSG-01 | WLO | CCR | | 635.52 | 635.52 | staff gauge | 635.52 | | | | | | | | | 39.059128 | -89.396727 |
| SG-02 | WLO | SW | | | 605.87 | Top of Prot Casing | 605.87 | | | | | | | | | 39.059695 | -89.391429 |
| SG-03 | WLO | SW | | | 594.94 | Top of Prot Casing | 594.94 | | | | | | | | | 39.059092 | -89.390342 |



TABLE 2-1. MONITORING WELL LOCATIONS AND CONSTRUCTION DETAILS

GROUNDWATER MONITORING PLAN COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Number Type HSU Constructed (ft) (ft) Description (ft) (ft BGS) (ft BGS) (ft BGS) (ft) (ft BGS) (ft BGS) (ft BGS) (ft BGS) (ft BGS) | We | | - Turno | Hell | Date | Top of PVC Elevation | Measuring Point Elevation | Measuring Point | Ground Elevation | Screen Top Depth | Screen Bottom Depth | Screen Top Elevation | Screen Bottom Elevation | Well Depth | Bottom of Boring Elevation | Screen Length | Screen Diameter | Latitude (Decimal | Longitude (Decimal Degrees) |
|---|----|--|---------|------|------|-------------------------|---------------------------|--------------------|---------------------|------------------------|---------------------------|-------------------------|-------------------------------|---------------|----------------------------------|------------------|--------------------|----------------------|-----------------------------------|
|---|----|--|---------|------|------|-------------------------|---------------------------|--------------------|---------------------|------------------------|---------------------------|-------------------------|-------------------------------|---------------|----------------------------------|------------------|--------------------|----------------------|-----------------------------------|

Notes:

All elevation data are presented relative to the North American Vertical Datum 1988 (NAVD88), GEOID 12A Type refers to the role of the well in the monitoring network: background (B), compliance (C), or water level measurements only (WLO) WLO wells are temporary pending implementation of impoundment closure per an approved Construction Permit application

-- = data not available

BGS = below ground surface CCR = Coal Combustion Residual

DA = deep aquifer

ft = foot or feet

HSU = Hydrostratigraphic Unit LCU = lower confining unit PVC = polyvinyl chloride SW = surface water

UA = uppermost aquifer

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TABLE 3-1. BACKGROUND GROUNDWATER QUALITY AND STANDARDS

GROUNDWATER MONITORING PLAN COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Parameter | Background Concentration | 845 Limit | Groundwater Protection Standard | Unit |
|-----------------------------|-----------------------------|--------------|---------------------------------|-------|
| Antimony, total | 0.003 | 0.006 | 0.006 | mg/L |
| Arsenic, total | 0.0043 | 0.010 | 0.010 | mg/L |
| Barium, total | 0.12 | 2.0 | 2.0 | mg/L |
| Beryllium, total | 0.001 | 0.004 | 0.004 | mg/L |
| Boron, total | 3.2 | 2 | 3.2 | mg/L |
| Cadmium, total | 0.001 | 0.005 | 0.005 | mg/L |
| Chloride, total | 120 | 200 | 200 | mg/L |
| Chromium, total | 0.011 | 0.1 | 0.1 | mg/L |
| Cobalt, total | 0.0056 | 0.006 | 0.006 | mg/L |
| Fluoride, total | 0.411 | 4.0 | 4.0 | mg/L |
| Lead, total | 0.0063 | 0.0075 | 0.0075 | mg/L |
| Lithium, total | 0.013 | 0.04 | 0.04 | mg/L |
| Mercury, total | 0.0013 | 0.002 | 0.002 | mg/L |
| Molybdenum, total | 0.0015 | 0.1 | 0.1 | mg/L |
| pH (field) | 7.3 / 6.6 | 9.0 / 6.5 | 9.0 / 6.5 | SU |
| Radium 226 and 228 combined | 1.6 | 5 | 5 | pCi/L |
| Selenium, total | 0.0015 | 0.05 | 0.05 | mg/L |
| Sulfate, total | 367 | 400 | 400 | mg/L |
| Thallium, total | 0.001 | 0.002 | 0.002 | mg/L |
| Total Dissolved Solids | 1010 | 1200 | 1200 | mg/L |

Notes:

For pH, the values presented are the upper / lower limits

Groundwater protection standards for calcium and turbidity do not apply per 35 I.A.C. § 845.600(b)

mg/L = milligrams per liter

SU = standard units

pCi/L = picocuries per liter

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TABLE 4-1. SAMPLING AND ANALYSIS SUMMARY

GROUNDWATER MONITORING PLAN COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Parameter | Analytical Method ¹ | Number of Samples | | Field Blanks ³ | Equipment Blanks ³ | MS/MSD ⁴ | Total | Container Type | Minimum Volume ⁵ | Preservation (Cool to 4 °C for all samples) | Sample Hold Time from Collection Date |
|--|--------------------------------|-------------------|----|------------------------------|----------------------------------|---------------------|-------|--|--------------------------------|---|---|
| Metals | • | - | | | | | | | | • | |
| Metals ⁶ | 6020, Li - EPA 200.7 | 16 | 2 | 0 | 0 | 1 | 19 | plastic | 600 mL | HNO ₃ to pH<2 | 6 months |
| Mercury | 7470A or 6020 | 16 | 2 | 0 | 0 | 1 | 19 | plastic | 400 mL | HNO ₃ to pH<2 | 28 days |
| Inorganic Parameters | | | | | _ | | | | | | |
| Fluoride | 9214 or EPA 300 | 16 | 2 | 0 | 0 | 1 | 19 | plastic | 300 mL | Cool to 4 °C | 28 days |
| Chloride | 9251 or EPA 300 | 16 | 2 | 0 | 0 | 1 | 19 | plastic | 100 mL | Cool to 4 °C | 28 days |
| Sulfate | 9036 or EPA 300 | 16 | 2 | 0 | 0 | 1 | 19 | plastic | 50 mL | Cool to 4 °C | 28 days |
| Total Dissolved Solids | SM 2540 C | 16 | 2 | 0 | 0 | 1 | 19 | plastic | 200 mL | Cool to 4 °C | 7 days |
| Radium | | | | | | | | | | | |
| Radium 226 | 9315 or EPA 903 | 16 | 0 | 0 | 0 | 0 | 16 | plastic | 1000 mL | HNO ₃ to pH<2 | 6 months |
| Radium 228 | 9320 or EPA 904 | 16 | 0 | 0 | 0 | 0 | 16 | plastic | 1000 mL | HNO ₃ to pH<2 | 6 months |
| Field Parameters | | | | | | | | | | | |
| pH | SM 4500-H+ B | 16 | NA | NA | NA | NA | 16 | flow-through cell | NA | none | immediately |
| Dissolved Oxygen ⁸ | SM 4500-O/405.1 | 16 | NA | NA | NA | NA | 16 | flow-through cell | NA | none | immediately |
| Temperature ⁸ | SM 2550 | 16 | NA | NA | NA | NA | 16 | flow-through cell | NA | none | immediately |
| Oxidation/Reduction Potential ⁸ | SM 2580 B | 16 | NA | NA | NA | NA | 16 | flow-through cell | NA | none | immediately |
| Specific Conductance 8 | SM 2510 B | 16 | NA | NA | NA | NA | 16 | flow-through cell | NA | none | immediately |
| Turbidity ⁷ | SM 2130 B | 16 | NA | NA | NA | NA | 16 | flow-through cell or hand-held turbidity meter | NA | none | immediately |

[O: CJC 09/01/21; C: SSW 09/15/21]

Notes

- ¹ Analytical method numbers are from SW-846 unless otherwise indicated. Analytical methods may be updated with more recent versions as appropriate.
- ² Field duplicates will be collected at a frequency of one per group of 10 or fewer investigative water samples. Field duplicates will not be collected for radium analysis.
- ³ Field blanks will be collected at the discretion of the project manager; Equipment blanks will be collected at a rate of 1 per sampling event if non-dedicated equipment is used.
- ⁴ Matrix Spike/Matrix Spike Duplicate (MS/MSD) samples will be collected at a frequency of one per group of 20 or fewer investigative water samples per CCR unit/multi-unit. Additional volume to be determined by laboratory.
- ⁵ Sample volume is estimated and will be determined by the laboratory.
- ⁶ Metals = antimony, arsenic, barium, beryllium, boron, cadmium, calcium, chromium, cobalt, lead, lithium, molybdenum, selenium, thallium. Metals may be analyzed via ICP/ ICP-MS USEPA methods 6010 or 6020 depending on laboratory instrument availability
- ⁷ If turbidity exceeds 10 NTUs, a duplicate sample filtered through a .45 micron filter may be collected for metals analysis in addition to the unfiltered sample. Both samples would be submitted for analysis.
- ⁸ Parameter collected for quality assurance and quality control for field sampling purposes only; not required to be collected or reported under Part 845; collection of parameter may be discontinued without notification.
- < = less than

°C = degrees Celsius

 $HNO_3 = nitric acid$ mL = milliliter

NA = not applicable

NTU = nephelometric turbidity unit

TABLE 4-2. DETECTION AND REPORTING LIMITS FOR PART 845 PARAMETERS

GROUNDWATER MONITORING PLAN
COFFEEN POWER PLANT
ASH POND NO. 1
COFFEEN, ILLINOIS

| Constituent | CAS | Unit | Analytical Methods ¹ | USEPA MCL ² | 35 I.A.C. § 845.600 | RL ^{4, 5} | MDL ⁵ |
|-----------------------------|------------|-------|---------------------------------|---------------------------|------------------------|--------------------|------------------|
| Metals | | | | | | | |
| Antimony | 7440-36-0 | mg/L | 6020 | 0.006 | 0.006 | 0.003 | 0.00036 |
| Arsenic | 7440-38-2 | mg/L | 6020 | 0.01 | 0.01 | 0.001 | 0.00013 |
| Barium | 7440-39-3 | mg/L | 6020 | 2 | 2 | 0.001 | 0.00028 |
| Beryllium | 7440-41-7 | mg/L | 6020 | 0.004 | 0.004 | 0.001 | 0.000017 |
| Boron | 7440-42-8 | mg/L | 6020 | NS | 2 | 0.01 | 0.0023 |
| Cadmium | 7440-43-9 | mg/L | 6020 | 0.005 | 0.005 | 0.001 | 0.000042 |
| Calcium | 7440-70-2 | mg/L | 6020 | NS | NS | 0.15 | 0.15 |
| Chromium | 7440-47-3 | mg/L | 6020 | 0.1 | 0.1 | 0.004 | 0.00027 |
| Cobalt | 7440-48-4 | mg/L | 6020 | 0.006 | 0.006 | 0.002 | 0.000017 |
| Lead | 7439-92-1 | mg/L | 6020 | 0.015 | 0.0075 | 0.001 | 0.000025 |
| Lithium | 7439-93-2 | mg/L | 6020 or EPA 200.7 | 0.04 | 0.04 | 0.02 | 0.0001 |
| Mercury | 7439-97-6 | mg/L | 6020 or 7470A | 0.002 | 0.002 | 0.0002 | 0.000078 |
| Molybdenum | 7439-98-7 | mg/L | 6020 | 0.1 | 0.1 | 0.001 | 0.000063 |
| Selenium | 7782-49-2 | mg/L | 6020 | 0.05 | 0.05 | 0.001 | 0.00032 |
| Thallium | 7440-28-0 | mg/L | 6020 | 0.002 | 0.002 | 0.001 | 0.000062 |
| Inorganics | | | | | | | |
| Fluoride | 7681 | mg/L | 9214 or EPA 300 | 4 | 4 | 0.25 | 0.065 |
| Chloride | 16887-00-6 | mg/L | 9251 or EPA 300 | 250 ³ | 200 | 1 | 0.15 |
| Sulfate | 18785-72-3 | mg/L | 9036 or EPA 300 | 250 ³ | 400 | 1 | 0.24 |
| Total Dissolved Solids | 10052 | mg/L | SM 2540C | 500 ³ | 1200 | 17 | |
| Other | | | | | | | |
| Radium 226 and 228 combined | 7440-14-4 | pCi/L | 9315/9320 or EPA 903/904 | 5 | 5 | 6 | ⁷ |

TABLE 4-2. DETECTION AND REPORTING LIMITS FOR PART 845 PARAMETERS

GROUNDWATER MONITORING PLAN COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

| Constituent | CAS | Unit | Analytical Methods ¹ | USEPA MCL ² | 35 I.A.C. § 845.600 | RL ^{4, 5} | MDL ⁵ |
|-------------------------------|-----|-------|---------------------------------|---------------------------|------------------------|--------------------|------------------|
| Field | | | | | | | |
| рН | NA | SU | SM 4500-H+ B | NS | 6.5-9.0 | NA | NA |
| Oxidation/Reduction Potential | NA | mV | SM 2580 B | NS | NS | NA | NA |
| Dissolved Oxygen | NA | mg/L | SM 4500-O/405.1 | NS | NS | NA | NA |
| Temperature | NA | °C | SM 2550 | NS | NS | NA | NA |
| Specific Conductivity | NA | μS/cm | SM 2510 B | NS | NS | NA | NA |
| Turbidity | NA | NTU | SM 2130 B | NS | NS | NA | NA |

[O: CJC 09/01/21; C: SSW 09/15/21]

Notes:

 μ S/cm = microSiemens per centimeter

CAS = Chemical Abstract Number

MDL = Method detection limit as established by the laboratory

mg/L = milligrams per liter

mV = millivolts

NS = No standard

NTU = nephelometric turbidity unit

pCi/L = picoCuries per liter

RL = Reporting limit as established by the laboratory

SM = Standard Methods for the Examination of Water and Wastewater

SU = standard units



¹ Analytical method numbers are from SW-846 unless otherwise indicated. Metals will be analyzed via Method 6020 or 6010 depending on laboratory equipment availability. Selected method will ensure reporting limits (RL) are below Title 35 of the Illinois Administrative Code (35 I.A.C.) § 845.600 groundwater protection standards.

² USEPA MCL = United States Environmental Protection Agency Maximum Contaminant Level.

³ USEPA SMCL = United States Environmental Protection Agency Secondary Maximum Contaminant Level.

⁴ RLs will be less than the 35 I.A.C. § 845.600 groundwater protection standards.

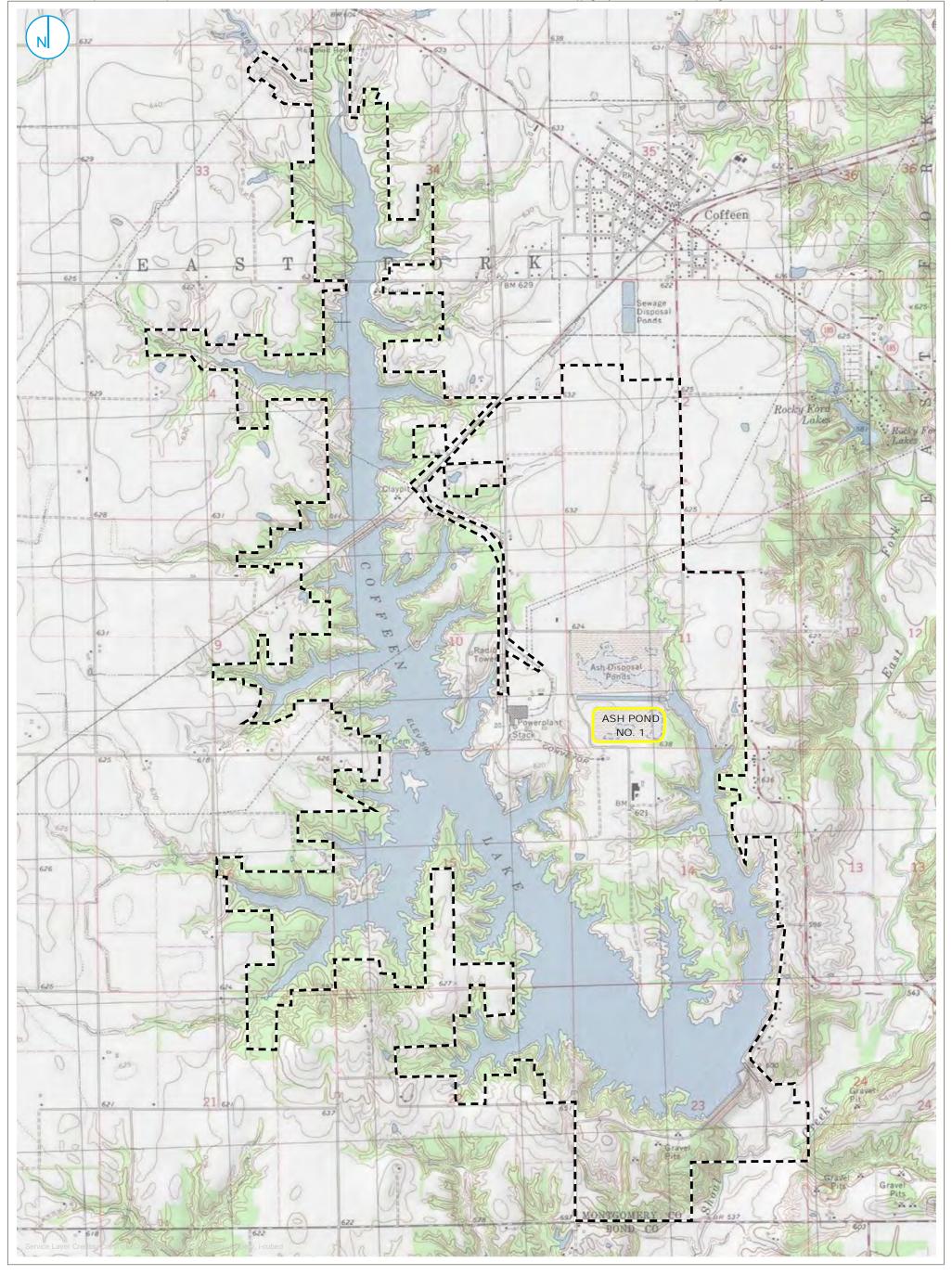
⁵ RLs and method detection limits (MDL) will vary depending on the laboratory performing the work.

⁶ All radium results will be reported (values may be positive or negative) and will include uncertainty and the calculated MDC.

⁷ Laboratories calculate a minimum detectable concentration (MDC) based on the sample.

[°]C = degrees Celsius

FIGURES



PART 845 REGULATED UNIT (SUBJECT UNIT)
PROPERTY BOUNDARY

SITE LOCATION MAP

FIGURE 1-1





■ COAL MINE SHAFT

PART 845 REGULATED UNIT (SUBJECT UNIT)

SITE FEATURE

275

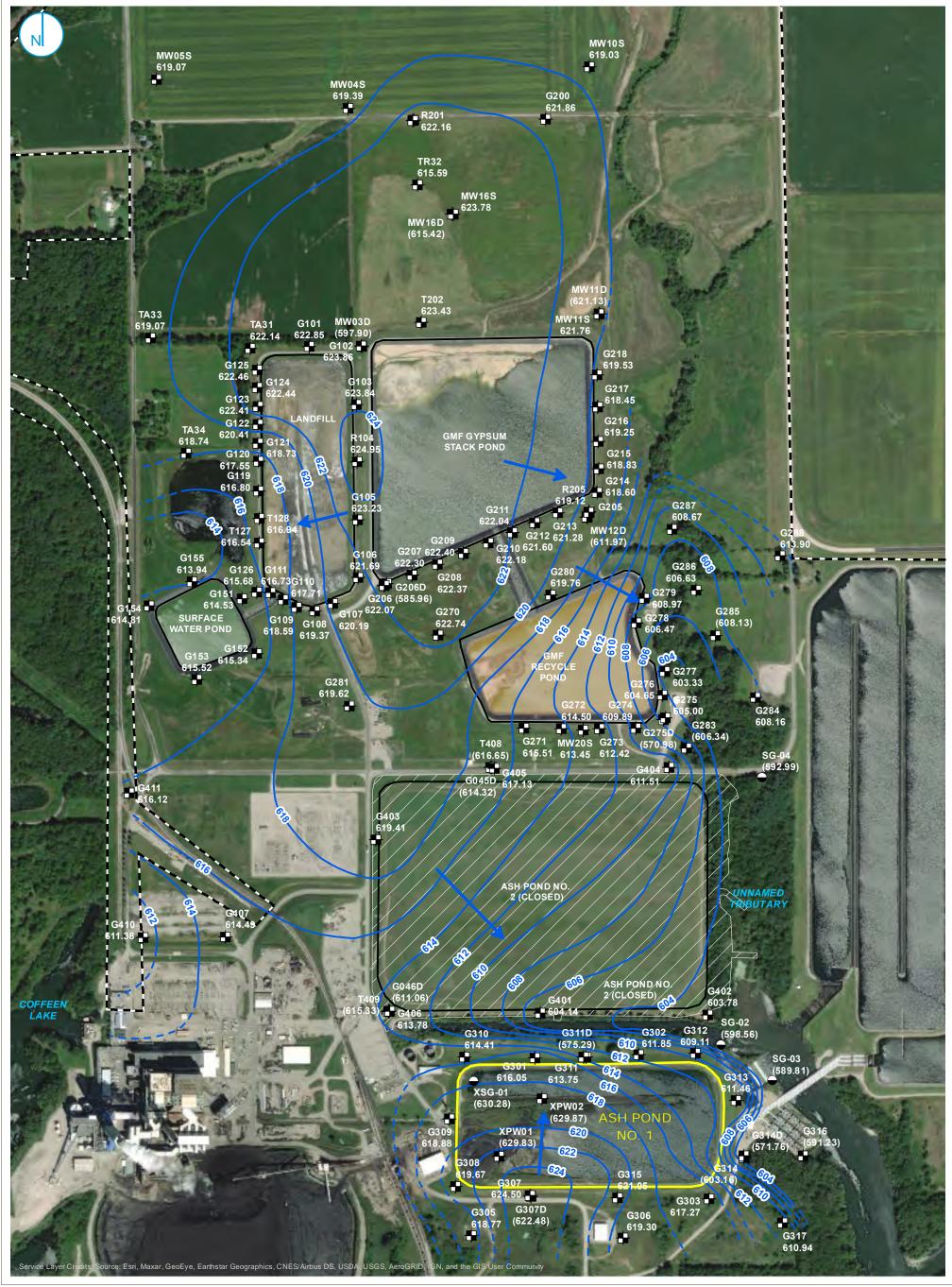
LIMITS OF FINAL COVER

PROPERTY BOUNDARY

550 ☐ Feet **SITE MAP**

FIGURE 1-2





MONITORING WELL

igoplus STAFF GAGE

PART 845 REGULATED UNIT (SUBJECT UNIT)

PROPERTY BOUNDARY

SITE FEATURE
LIMITS OF FINAL COVER

GROUNDWATER ELEVATION
CONTOUR (2-FT CONTOUR
INTERVAL, NAVD88)

INFERRED GROUNDWATER ELEVATION CONTOUR

GROUNDWATER FLOW DIRECTION

UPPERMOST AQUIFER GROUNDWATER ELEVATION CONTOURS APRIL 20, 2021

GROUNDWATER MONITORING PLAN
ASH POND NO.1
COFFEEN POWER PLANT
COFFEEN, ILLINOIS

FIGURE 1-3





COMPLIANCE WELL
PART 845 REGULATED UNIT (SUBJECT UNIT)
BACKGROUND WELL
SITE FEATURE
LIMITS OF FINAL COVER
PROPERTY BOUNDARY

PROPOSED 845 GROUNDWATER MONITORING WELL NETWORK

ETWORK FIGURE 2-1

GROUNDWATER MONITORING PLAN
ASH POND NO.1
COFFEEN POWER PLANT
COFFEEN, ILLINOIS



APPENDIX A STATISTICAL ANALYSIS PLAN

Prepared for

Illinois Power Generating Company

Date

October 25, 2021

Project No.

1940100806-002

STATISTICAL ANALYSIS PLAN

ASH POND NO. 1 COFFEEN POWER PLANT COFFEEN, ILLINOIS

STATISTICAL ANALYSIS PLAN COFFEEN POWER PLANT ASH POND NO. 1

Project Name Coffeen Power Plant Ash Pond No. 1

Project No. **1940100806-002**

Recipient Illinois Power Generating Company

Document Type Statistical Analysis Plan

Version FINAL

Date October 25, 2021

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Rachel A. Banoff, EIT Project Statistician

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LICENSED PROFESSIONAL CERTIFICATIONS

This certification is based on the description of the statistical methods selected to evaluate groundwater as presented in the following Statistical Analysis Plan; Coffeen Power Plant Ash Pond No. 1. The procedures described in the plan will be used to establish background conditions and implement compliance monitoring as necessary and required by 35 I.A.C. § 845.640 and 35 I.A.C. § 845.650. The Statistical Analysis Plan was prepared in accordance with the requirements of 35 I.A.C. § 845.640(f), with reference to the acceptable statistical procedures provided in the United States Environmental Protection Agency (USEPA)'s Statistical Analysis of Groundwater Monitoring Data at RCRA Facilities, Unified Guidance (Unified Guidance, March 2009), and is intended to provide a logical process and framework for conducting the statistical analysis of the data obtained during groundwater monitoring. In accordance with 35 I.A.C. § 845.640(f)(1), the statistical method chosen for analysis of background groundwater quality will be either the tolerance interval or the prediction interval procedure for each constituent listed in 35 I.A.C. § 845.600(a)(1) at this CCR unit per 35 I.A.C. § 845.640(f)(1)(C). Groundwater Protection Standards (GWPS) will be established in accordance with 35 I.A.C. § 845.600(a) (greater of the background concentration or numerical limit specified in 35 I.A.C. § 845.600(a)(1)). The GWPS will be compared to the lower confidence limit for the observed concentrations for each constituent in each compliance well. Consistent with the *Unified Guidance*, the same general statistical method of confidence interval testing against a fixed GWPS is recommended in compliance and corrective action programs. Confidence intervals provide a flexible and statistically accurate method to test how a parameter estimated from a single sample compares to a fixed numerical limit. Confidence intervals explicitly account for variation and uncertainty in the sample data used to construct them.

Description of the statistical methods chosen for analysis of groundwater monitoring data and application of these methods for determining exceedances of the GWPS identified in 35 I.A.C. § 845.600(a) is provided in this Statistical Analysis Plan.

35 I.A.C. § 845.640 Statistical Analysis (PE)

I, Eric J. Tlachac, a qualified professional engineer in good standing in the State of Illinois, certify that the statistical methods summarized above and described in this document (Statistical Analysis Plan; Coffeen Power Plant Ash Pond No. 1) are appropriate for evaluating the groundwater monitoring data collected as described in the attached document and are in substantial compliance with 35 I.A.C. § 845.640.

Eric J. Tlachac

Qualified Professional Engineer

062-063091

Illinois

Date: October 25, 2021

ERIC J. TLACHAC O62-063091

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35 I.A.C. § 845.640 Statistical Analysis (PG)

I, Brian G. Hennings, a qualified professional geologist in good standing in the State of Illinois, certify that the statistical methods described in this document (Statistical Analysis Plan; Coffeen Power Plant Ash Pond No. 1) are appropriate for evaluating the groundwater monitoring data collected as described in the attached document and are in substantial compliance with 35 I.A.C. § 845.640.

Brian G. Hennings

Professional Geologist

196.001482 Illinois

Date: October 25, 2021



35 I.A.C. § 845.640 Statistical Analysis

I, Rachel A. Banoff, a qualified professional, certify that the statistical methods described in this document (Statistical Analysis Plan; Coffeen Power Plant Ash Pond No. 1), are appropriate for evaluating the groundwater monitoring data collected as described in the attached document and are in substantial compliance with 35 I.A.C. § 845.640.

Rachel A. Banoff, EIT

Project Statistician
Date: October 25, 2021

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ACRONYMS AND ABBREVIATIONS

§ Section

35 I.A.C. Title 35 of the Illinois Administrative Code

ANOVA analysis of variance

CCR coal combustion residuals
COC constituents of concern

GWPS groundwater protection standard

IEPA Illinois Environmental Protection Agency

LCL lower confidence limit
LTL lower tolerance limit
MSE mean squared error

P probability

Part 845 Residuals in Surface Impoundments: Title 35 of the Illinois Administrative Code

§ 845

RCRA Resource Conservation and Recovery Act

RL reporting limit

ROS regression on order statistics

SI surface impoundment

SSI statistically significant increase
SWFPR site-wide false positive rate

Unified Guidance Statistical Analysis of Groundwater Monitoring Data at RCRA Facilities,

Unified Guidance (USEPA, 2009)

UPL upper prediction limit

USEPA United States Environmental Protection Agency

UTL upper tolerance limit

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1. INTRODUCTION

In April 2021, the Illinois Environmental Protection Agency (IEPA) issued a final rule for the regulation and management of Coal Combustion Residuals (CCR) in surface impoundments (SIs) under the Standards for the Disposal of CCR in Surface Impoundments: Title 35 of the Illinois Administrative Code (35 I.A.C.) § 845 (Part 845). Facilities regulated under Part 845 are required to develop and sample a groundwater monitoring well network to evaluate whether impounded CCR materials are impacting downgradient groundwater quality. The groundwater quality evaluation must include selection and certification by a qualified professional engineer of the statistical procedures to be used. The procedures described in the evaluation will be used to establish background conditions and implement compliance and corrective action monitoring as necessary and required by 35 I.A.C. § 845.640 and 35 I.A.C. § 845.650. This Statistical Analysis Plan was prepared in accordance with the requirements of 35 I.A.C. § 845.640(f), with reference to the acceptable statistical procedures provided in United States Environmental Protection Agency's (USEPA's) *Statistical Analysis of Groundwater Monitoring Data at RCRA Facilities, Unified Guidance* (*Unified Guidance*) (March 2009).

This Statistical Analysis Plan does not include procedures for groundwater sample collection and analysis, as these activities are conducted in accordance with the Sampling and Analysis Plan prepared for each CCR unit in accordance with 35 I.A.C. § 845.640. This Statistical Analysis Plan will be used as the primary reference for evaluating groundwater quality during operation and post-closure care.

1.1 Statistical Analysis Objectives

This Statistical Analysis Plan is intended to provide a logical process and framework for conducting the statistical analyses of data obtained during groundwater monitoring conducted in accordance with the Sampling and Analysis Plan for each CCR unit. The Statistical Analysis Plan will enable a qualified professional engineer to certify that the selected statistical methods are appropriate for evaluating the groundwater monitoring data for the applicable CCR unit(s).

1.2 Statistical Analysis Plan Approach

The main sections of this Statistical Analysis Plan should be viewed as a "generic" outline of statistical methods utilized for each CCR unit and constituent required to be monitored. The statistical analysis of the groundwater monitoring data, however, will be conducted on an individual-constituent or well basis, and may involve the use of appropriate statistical procedures depending on multiple factors such as detection frequency and normality distributions.

The CCR Rule outlines two phases of groundwater monitoring:

- Background Monitoring in accordance with 35 I.A.C. § 845.650(b)(1)
- Compliance Monitoring in accordance with 35 I.A.C. § 845.650

Each phase of the groundwater monitoring program requires specific statistical procedures to accomplish the intended purpose. During the background monitoring phase, background groundwater quality will be established utilizing upgradient and background wells and downgradient groundwater quality data will be collected to facilitate statistics in subsequent phases. Compliance Monitoring is then initiated through the evaluation of the downgradient

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groundwater monitoring data for exceedances of the groundwater protection standard (GWPS) established by Part 845 (concentration specified in 35 I.A.C. § 845.600 or an IEPA-approved background concentration). The developed statistical analysis plan will be implemented for each monitoring phase and in accordance with the statistical procedures.

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2. BACKGROUND MONITORING AND DATA PREPARATION

The background and compliance monitoring wells were sampled and analyzed for constituents, as listed in Part 845 (antimony, arsenic, barium, beryllium, boron, cadmium, calcium, chloride, chromium, cobalt, fluoride, lead, lithium, mercury, molybdenum, pH, radium 226 and 228 combined, selenium, sulfate, thallium, total dissolved solids, and turbidity), during the baseline phase of the groundwater monitoring program.

The background monitoring well(s) were placed upgradient of the CCR unit, or at an alternative background location, where they are not affected by potential leakage from the CCR unit. Compliance monitoring wells were placed at the waste boundary of the CCR unit, along the same groundwater flow path. As 35 I.A.C. § 845.630(a) specifies, the location of these wells ensures that background accurately represents the quality of unaffected groundwater, while compliance wells accurately represent groundwater quality at the waste boundary and monitor all potential contaminant pathways.

As required by 35 I.A.C. § 845.650(a)(1), eight sampling events were completed within 180 days of April 21, 2021. As outlined, groundwater sampling procedures included sampling of the background and compliance wells using low-flow sampling methods, collection of one field quality control sample per event, and groundwater samples were not field filtered before laboratory analysis of total recoverable metals.

Following completion of the eight sampling events, background groundwater quality was established for Part 845 constituents. Groundwater monitoring will be conducted quarterly for at least the first five years. In accordance with 35 I.A.C. § 845.650(b)(4), after the first five years, a request to reduce the monitoring frequency to semiannual may be submitted to IEPA if all of the following can be demonstrated:

- Groundwater monitoring effectiveness will not be compromised by the reduced frequency
- Sufficient data has been collected to characterize groundwater
- Monitoring to date does not show any statistically significant increasing trends
- The concentrations of monitored constituents at the compliance monitoring wells are below the applicable GWPSs established in 35 I.A.C. § 845.600

The following subsections outline the statistical tests and procedures (methods) that will be utilized to evaluate data collected for each constituent in both background and compliance wells for Background and Compliance Monitoring. When necessary and contingent upon equivalent statistical power, an alternative test not included in this Statistical Analysis Plan may be chosen due to site-specific data requirements.

2.1 Sample Independence

Independence of sample results is a major assumption for most statistical analyses. To ensure physical independence of groundwater sampling results, the minimum time between sampling events must be longer than the time required for groundwater to move through the monitoring well. The sampling schedules for both the baseline and compliance monitoring periods are specified in 35 I.A.C. § 845.650(b) and may conflict with the statistical assumption of independence of sample results.

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2.2 Non-Detect Data Processing

The reporting limit (RL) will be used as the lower level for the reporting of non-detected groundwater quality data. For all summary statistics (box plots, timeseries, etc.), the RL will be substituted for concentrations reported below the RL, including non-detects. With professional judgement, analytical results between the RL and the method detection limit, *i.e.*, estimated values, typically identified with a "J" flag, may be utilized if provided by the laboratory.

For all statistical test procedures:

- If the frequency of non-detect data are less than or equal to 15 percent, half of the RL will be substituted for these data
- If the non-detect frequency is between 15 percent and 50 percent, either the Kaplan-Meier or robust regression on order statistics (ROS) will be used to estimate the mean and standard deviation adjusted for the presence of left-censored values
- If the non-detect frequency is greater than 50 percent, a non-parametric test will be used
- If only one background result is detected that value will be used as the non-parametric upper prediction limit (UPL)

2.3 Testing for Normality

Many statistical analyses assume that sample data are normally distributed (parametric). However, environmental data are frequently not normally distributed (nonparametric). 35 I.A.C. § 845.640(g) requires the knowledge of the background data distribution for comparison to compliance results. The *Unified Guidance* document recommends the Shapiro-Wilk normality test for sample sizes of 50 or less, and the Shapiro-Francia normality test for sample sizes greater than 50.

When possible, transformation of datasets to achieve normal distributions is preferred.

2.4 Testing for Outliers

Part 845 constituents will be screened for the existence of outliers using a method described by the *Unified Guidance*. Outliers are extreme data points that may represent an anomaly or erroneous data point. To test for outliers, one or more of the following outlier tests will be utilized:

- Dixon's test, for well-constituent pairs with less than 25 samples, assumes normally distributed data.
- Rosner's test, for well-constituent pairs with more than 20 samples, assumes normally distributed data.
- Grubb's test for well-constituent pairs with seven or more samples, assumes normally distributed data.
- Time series, box-whisker plots, and probability plots provide visual tools to identify potential outliers, and evaluation of seasonal, spatial, or temporal variability for both normally and non-normally distributed data.

Data quality control, groundwater geochemistry, and sampling procedures will be evaluated as potential sources of error leading to an outlier result. The outlier tests cannot be used alone to determine whether a value is a true outlier that should be excluded from future statistical

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analysis. Corroborating evidence needed to exclude values includes a discrete data reporting or analytical error, or potential laboratory bias. Absent corroborating evidence, the flagged values are considered true, but extreme, values in the data set. Professional judgement will be used to exclude extreme outliers from further statistical analyses. Outliers will be retained in the database.

With professional judgement, a confirmatory sample may be collected to allow for the distinction between an outlier and a true representation of groundwater quality at the monitoring point. If re-sampling is conducted, this sample will be collected within 90 days following outlier identification. If the confirmatory sample indicates the original result as an outlier, it will be reported as such.

2.5 Trend Analysis

Statistical analyses supporting the lack of trend are a fundamental step to confirm the assumption that groundwater quality values are stationary or constant over time at a CCR unit. These analyses allow for evaluation of variation in the background and compliance data for each constituent over time. A statistically significant increasing trend in background data could indicate an existing release from the CCR unit or alternate source, requiring further investigation. In addition, statistically significant trending background data can result in increased standard deviation and, therefore, greater prediction or control limits. Consequently, the increased prediction or control limit will have less power or ability to identify a release from the CCR unit.

A linear regression, coupled with a t-test for slope significance at a 95 percent confidence level (0.05 significance level), may be used on datasets for each constituent with few non-detects and a normally distributed variance of the mean to evaluate time trends. The Theil-Sen trend line, coupled with the Mann-Kendall test for slope significance at a 95 percent confidence level (0.05 significance level), will be used for datasets with frequent non-detects or non-normal variance. Similarly, trend analyses could also be used on compliance data to evaluate a possible release from the CCR unit.

2.6 Spatial Variation

Spatial trends and/or variation between background wells could indicate an existing release from a CCR unit. If the spatial variability is not due to an existing release, intrawell comparisons in compliance wells may be used to account for spatial variability and monitor for a future release. However, the CCR unit being monitored was placed into service prior to the start of groundwater monitoring and it is unknown whether a previous release has occurred. Accordingly, intrawell comparisons in compliance wells cannot be used to determine the occurrence of a future release. Interwell comparisons between compliance wells and background wells will be used.

2.7 Temporal Variation

Time series plots can be used to identify temporal dependence. Potentially significant temporal components of variability can be identified by graphing single constituent data from multiple wells together on a time series plot. With temporal dependence, the time series plot as a pattern of parallel traces, in which the individual wells will tend to rise and fall together across the sequence of sampling dates. Time series plots can be helpful by plotting multiple constituents over time for the same well, or averaging values for each constituent across wells on each sampling event and then plotting the averages over time. In either case, the plots can signify whether the general concentration pattern over time is simultaneously observed for different

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constituents. If so, it may indicate that a group of constituents is highly correlated in groundwater or that the same artifacts of sampling and/or lab analysis impacted the results of several monitoring parameters.

Hydrologic factors such as drought, recharge patterns or regular (e.g., seasonal) water table fluctuations may be responsible for the temporal variation. In these cases, it may be useful to test for the presence of a significant temporal effect by first constructing a parallel time series plot and then running a formal one-way analysis of variance (ANOVA) ($\alpha=0.05$) for temporal effects. A one-way ANOVA for temporal effects considers multiple well data sets for individual sampling events or seasons as the relevant statistical factor. If event-specific analytical differences or seasonality appear to be an important temporal factor, the one-way ANOVA for temporal effects can be used to formally identify seasonality, parallel trends, or changes in lab performance that affect other temporal effects. The one-way ANOVA for temporal effects assumes that the data groups are normally distributed with constant variance. It is also assumed that for each of a series of background wells, measurements are collected at each well on sampling events or dates common to all the wells. Results of the ANOVA can also be used to create temporally stationary residuals, where the temporal effect has been 'subtracted from' the original measurements. These stationary residuals may be used to replace the original data in subsequent statistical testing.

If the data cannot be normalized, a similar test for a temporal or seasonal effect can be performed using the Kruskal-Wallis test ($\alpha=0.05$). Each sampling event should be treated as a separate 'well,' while each well is treated as a separate 'sampling event.' In this case, no residuals can be computed since the Kruskal-Wallis test employs ranks of the data rather than the measurements themselves.

Where both spatial and temporal variation occur, two-way ANOVA can be considered where both well location and sampling event/season are treated as statistical factors. This procedure is described in Davis (1994).

2.8 Updating Background

Updating the background dataset periodically by adding recent results to an existing background dataset can improve the statistical power and accuracy of the statistical analysis, especially for non-parametric prediction intervals. The Unified Guidance recommends updating statistical limits (background) when at least four to eight new measurements (every 1 to 2 years under a quarterly monitoring program), are available for comparison to historical data. Professional judgement will be used to evaluate whether any background data appear to be affected by a release and need to be excluded from a background update. A t-test for equal means (if normal data distribution) or appropriate non-parametric test (if non-normal data distribution) such as a Mann-Whitney (or Wilcoxon) rank-sum or box-whisker plots, will be conducted to evaluate whether the two groups of background sample populations are statistically different prior to updating any background datasets. A 0.05 significance level will be utilized when evaluating the two populations, with the null hypothesis that they are equivalent. In addition, time series graphs or other trend evaluation statistics will be conducted on the new background dataset to verify the absence of a release or changing groundwater quality. If the tests indicate that there are no statistical differences between the two background populations, the new data will be combined with the existing dataset. If the two populations are found to be different, the data will be reviewed to evaluate the cause of the difference. If the differences appear to be caused by a

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release (if the new data are significantly higher, or lower for pH), then the previous background dataset may continue to be used. Furthermore, verified outliers will not be added to an existing background dataset. In accordance with the *Unified Guidance*, continual background updates will not be conducted due to the lack of sufficient samples for a statistical comparison.

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3. COMPLIANCE MONITORING

Compliance monitoring is designed to monitor groundwater for evidence of a release by comparing Part 845 constituents in compliance wells to both background concentrations and the GWPS. Compliance Monitoring will begin the 1st quarter following approval of this Groundwater Monitoring Plan and issuance of the Operating Permit. The selected Compliance Monitoring statistical method used to compare compliance groundwater quality data for each constituent to the GWPS will provide for adequate statistical power, error levels and individual test false positive rates, and be appropriate for the distribution and detection frequency of the background dataset. Statistical power is the ability of a statistical test to detect a true exceedance.

In accordance with 35 I.A.C. § 845.610(b)(3)(D), compliance monitoring statistical analyses will be completed and submitted to IEPA within 60 days after completion of sampling.

3.1 GWPS Establishment and Exceedance Determination

In accordance with 35 I.A.C. § 845.600(a), the GWPS will be the constituent concentrations specified in 35 I.A.C. § 845.600(a)(1) except for when the background concentration is greater, or no concentration is specified (*i.e.*, for calcium and turbidity), in which case the GWPS will be the background concentration. The GWPS based on background concentration will be calculated using a parametric upper tolerance limit (UTL), a parametric UPL for a future mean, or a non-parametric UPL for a future median.

Statistical calculations that will be utilized in Compliance Monitoring procedures are summarized in **Table A** below and listed in **Sections 3.1.1** through **3.1.7**. Depending on the distribution of the data and the percentage of non-detects, it may be more appropriate to use a parametric model over a non-parametric model. As necessary, other techniques as mentioned in the *Unified Guidance* and/or new methods will be implemented.

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Table A. Statistical Calculations Used in Compliance Monitoring Procedures

| | | | Compliance M | lonitoring | | |
|-----------------------|----------------------------|--------------|---|------------------------|--|--|
| | | Background | Data | | Compliance | e Data |
| Significant Trend? | Percent Non- Detects | Distribution | GWPS Determination | Percent Non-Detects | Distribution | Method to Determine Exceedance |
| | | | 25 1 4 6 6 | ≤75 | Normal | Parametric Lower Confidence Limit around a Normal Mean |
| No | 0 ≤ 50 | Normal | 35 I.A.C § 845.600(a)(1) constituent concentration or The Upper | ≤75 | Log-Normal | Parametric Lower Confidence Limit around a Lognormal Geometric Mean |
| | | | Tolerance Limit | NA | Non-Normal | Non-Parametric Lower |
| | | | | >75 | Unknown/ Cannot be determined | Confidence Limit around a Median |
| | 50 ≤ 70 | Normal | The Upper Prediction Limit for a Future Mean | NA | NA | Future mean |
| | >70 | Non-Normal | Upper Prediction Limit for a Future Median | NA | NA | Future median |
| | 100 | Non-Normal | Double Quantification Rule | NA | NA | Individual Retesting Values |
| Yes | 0 ≤ 50 | Normal | UCL of Confidence Band around Linear Regression | ≤75 | Residuals after subtracting trend are normal, equal variance | Lower Limit from Confidence Band around Linear Regression |
| | 50 ≤ 100 | Non-Normal | UCL of Confidence Band around Thiel-Sen trend line | ≤75 | Residuals not normal | Lower Limit from Confidence Band around Thiel-Sen |

3.1.1 The Upper Tolerance Limit

The UTL will be used to calculate the GWPS when pooled background data are normally distributed, with a non-detect frequency of 50 percent or less. When non-detect frequency is 15 percent or less, half the RL will be substituted for non-detects. The *Unified Guidance* recommends 95 percent confidence level and 95 percent coverage (95/95 tolerance interval).

• When non-detect frequency is 15 percent or less, half the RL will be substituted for non-detects (simple substitution), and the normal mean and standard deviation will be calculated.

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- The Kaplan-Meier or the ROS method will be used when the detection frequency is between 15 percent and 50 percent. The Kaplan-Meier method assesses the linearity of a censored probability plot to determine whether the background sample can be approximately normalized. If so, then the Kaplan-Meier method will be used to compute estimates of the mean and standard deviation adjusted for the presence of left-censored values. The Kaplan-Meier or ROS estimate of the mean and standard deviation will be substituted for the sample mean and standard deviation.
- If background normality cannot be achieved, non-parametric UTLs will not be calculated until a minimum of 60 background samples have been collected (to achieve 95 percent coverage).

The parametric UTL on a future mean will be calculated from the background dataset as follows:

$$UTL = \overline{x} + \kappa (n, \gamma, \alpha - 1) \cdot s$$

 \overline{x} = background sample mean

s = background sample standard deviation

 κ $(n,\gamma,\alpha-1)$ = one-sided normal tolerance factor based on the chosen coverage (γ) and confidence level $(\alpha$ -1) and the size of the background dataset (n). Values are tabulated in Table 17-3 in Appendix D of the *Unified Guidance*. If exact values are not provided, then κ values can be estimated by linear interpolation.

If the UTL is constructed on the logarithms of original observations to achieve normality, where \overline{y} and s_y are the log-mean and log-standard deviation, the limit will be exponentiated for backtransformation to the concentration scale as follows:

$$UTL = \exp\left[\overline{y} + \kappa (n, \gamma, \alpha - 1) \cdot s_{\gamma}\right]$$

 \overline{y} = background sample log-mean

 s_v = background sample log-standard deviation

When the GWPS is based on the 35 I.A.C. § 845.600(a)(1) constituent concentrations or a UTL derived from the background dataset, an exceedance in compliance wells relative to the GWPS will be evaluated using confidence intervals. A confidence interval defines the upper and lower bound of the true mean of a constituent concentration in groundwater within a specified confidence range.

- Non-detects in compliance data will be handled similarly to upgradient analyses, with half the RL substituted for non-detects when the frequency is 15 percent or less.
- The Kaplan-Meier, or the ROS method, will be used when the detection frequency is between 15 percent and 50 percent to compute estimates of the mean and standard deviation adjusted for the presence of left-censored values. These estimates will then be substituted for the sample mean and standard deviation.

Once the GWPS is established for background data using the UTL, either parametric or non-parametric confidence intervals will be computed for each constituent in compliance wells to identify GWPS exceedances.

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3.1.2 Parametric Confidence Intervals around a Mean

If compliance data are approximately normal, one-sided parametric confidence intervals around a sample mean will be constructed for each constituent and well pair. The lower confidence limit (LCL) will be calculated as:

$$LCL_{1-\alpha} = \overline{x} - t_{1-\alpha,n-1} \cdot \frac{s}{\sqrt{n}}$$

 \overline{x} = compliance sample mean

s = compliance sample standard deviation

n =compliance sample size

 $t_{1-\alpha,n-1}$ = obtained from a Student's t-table with (n-1) degrees of freedom (Table 16-1 in Appendix D of the *Unified Guidance*)

The chosen t value will aim to achieve both a low false-positive rate, and high statistical power. Minimum a values are tabulated in Table 22-2 of Appendix D of the *Unified Guidance*. The selected minimum a value, from which the t value will be derived, will have at least 80 percent power $(1-\beta=0.8)$ when the underlying mean concentration is twice the GWPS.

If compliance data are distributed lognormally, the LCL will be computed around the lognormal geometric mean as:

$$LCL_{1-\alpha} = \exp\left(\overline{y} - t_{1-\alpha,n-1} \cdot \frac{s_y}{\sqrt{n}}\right)$$

 \overline{y} = compliance sample log-mean

 $s_v = compliance sample log-standard deviation$

3.1.3 Non-Parametric Confidence Intervals around a Median

Non-parametric confidence intervals around the median will be computed if the compliance data contain greater than 50 percent non-detects or are not normally distributed. The mathematical algorithm used to construct non-parametric confidence intervals is based on the probability (P) that any randomly selected measurement in a sample of n concentration measurements will be less than an unknown $P \times 100$ th percentile of interest (where P is between 0 and 1). Then the probability that the measurement will exceed the $P \times 100$ th percentile is (1-P). The number of sample values falling below the $P \times 100$ th percentile out of a set of n should follow a binomial distribution with parameters n and success probability P, where 'success' is defined as the event that a sample measurement is below the $P \times 100$ th percentile. The probability that the interval formed by a given pair of order statistics will contain the percentile of interest will then be determined by a cumulative binomial distribution Bin(x;n,p), representing the probability of x or fewer successes occurring in n trials with success probability p. P will be set to 0.50 for an interval around the median.

The sample size n will be ordered from least to greatest. Given P = 0.50, candidate interval endpoints will be chosen by ordered data values with ranks close to the product of $(n+1) \times 0.50$. If the result of $(n+1) \times 0.50$ is a fraction (for even-numbered sample sizes), the rank values immediately above and below will be selected as possible candidate endpoints. If the result of $(n+1) \times 0.50$ is an integer (for odd-numbered sample sizes), one will be added to and subtracted

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from the result to get the upper and lower candidate endpoints. The ranks of the endpoints will be denoted L* and U*. For a one-sided LCL, the confidence level associated with endpoint L* will be computed as:

$$1 - \alpha = Bin(L^* - 1; n, 0.50) = \sum_{x=L^*}^{n} {n \choose x} \left(\frac{1}{2}\right)^n$$

If the candidate endpoint(s) do not achieve the desired confidence level, new candidate endpoints (L^*-1) and (U^*+1) and achieved confidence levels will be calculated. If one candidate endpoint equals the data minimum or maximum, only the rank of the other endpoint will be changed. Achievable confidence levels are tabulated using these equations in Table 21-11 in Appendix D of the *Unified Guidance*.

Both parametric and non-parametric confidence limits will then be compared to the GWPS. The CCR unit is considered to be in compliance if the LCL is equal to or lower than the GWPS for all detected constituents at all compliance monitoring wells. A GWPS exceedance is determined if the LCL exceeds the GWPS.

3.1.4 The Upper Prediction Limit for a Future Mean

The parametric UPL for a future mean will be used to calculate the GWPS if the pooled background data contain 50 to 70 percent non-detects and normality can be achieved. The Kaplan-Meier or ROS methods will be used to estimate the mean and standard deviation. The non-parametric UPL for a future median will be calculated as the GWPS if background samples cannot be normalized or contain greater than 70 percent non-detects. The parametric UPL for a future mean will be calculated from the background dataset at follows:

$$UPL_{1-\alpha} = \overline{x} + \kappa s$$

 \overline{x} = background sample mean

s =background standard deviation

 κ = multiplier based on the order (p) of the future mean to be predicted, the number of compliance wells to be tested (w), the background sample size (n) the number (c) of constituents of concern (COCs), the "1-of-m" retesting scheme, and the evaluation schedule (annual, semi-annual, quarterly). Values are tabulated in 19-5 to 19-9 in Appendix D of the *Unified Guidance*.

The mean of order p will be computed for each well and compared against the UPL. For any compliance point mean that exceeds the limit, p additional resamples may be collected at that well for a 1-of-2 retesting scheme. Resample means will then be compared to the UPL. A GWPS exceedance has been deemed to occur at a compliance well when the initial mean and all resample means exceed the UPL.

3.1.5 The Non-Parametric Upper Prediction Limit for a Future Median

The non-parametric UPL for a future median will be used to calculate the GWPS if the pooled background data contain greater than 70 percent non-detects and normality cannot be achieved. Non-parametric methods assume that the data does not have an underlying distribution. To calculate the non-parametric UPL on a future value, the target per-constituent false positive rate (a_{const}) will be determined as follows:

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$$\alpha_{const} = 1 - (1 - \alpha)^{1/c}$$

 α = the site-wide false positive rate (SWFPR) of 0.10 recommended by the *Unified Guidance*

c = the number of monitoring constituents

The number of yearly statistical evaluation (nE) will be multiplied by the number of compliance wells (w) to determine the look-up table entry, w*. The background sample size (n) and w* will be used to select an achievable per-constituent false positive rate value in Table 19-24 of Appendix D in the *Unified Guidance*. The chosen achievable per-constituent false positive rate value will determine the type of non-parametric prediction limit (maximum or 2nd highest value in background) and a retesting scheme for a future median. The background data will be sorted in ascending order, and the upper prediction limit will be set to the appropriate order statistic previously determined by the achievable per-constituent false positive rate value in Table 19-24. If all constituent measurements in a background sample are non-detect, the Double Quantification rule will be used. The use of the Double Quantification rule in Compliance Monitoring will only be applicable if the RL is above the 35 I.A.C. § 845.600(a)(1) constituent concentration or a constituent concentration is not specified in § 845.600(a)(1). This scenario is highly unlikely. The constituent will also be removed from calculations identifying the target false positive rate.

Two initial measurements per compliance well will be collected. If both do not exceed the upper prediction limit, a third initial measurement will not be collected since the median of order 3 will also not exceed the limit. If both exceed the prediction limit, a third initial measurement will not be collected since the median will also exceed the limit. If one initial measurement is above and one below the limit, a third initial observation may be collected to determine the position of the median relative to the UPL. Up to three resamples will be collected in order to assess the resample median. In all cases, if two or more of the compliance point observations are non-detect, the median will be set equal to the RL. The median value for each compliance well will be compared to the UPL. For the 1-of-2 retesting scheme, if any compliance point median exceeds the limit, up to three additional resamples will may be collected from that well. The resample median will be computed and compared to the UPL. A GWPS exceedance has been deemed to occur at a compliance well when either the initial median, or both the initial median and resample median exceed the UPL.

If the concentrations of detected constituents are below the established GWPS, Compliance Monitoring will continue.

3.1.6 Parametric Linear Regression and Confidence Band

If the t-test detects a significant trend in the parametric linear regression line using either background or compliance data for a particular constituent, confidence bands accounting for trends will be constructed to account for the trend-induced variation. If this is not accounted for, a wider confidence interval will inevitably be calculated for a given confidence level and sample size (n). A wider confidence interval will result in less statistical power, or ability to demonstrate an exceedance or return to compliance. When a linear trend line has been estimated, a series of confidence intervals is estimated at each point along the trend. This creates a simultaneous confidence band that follows the trend line. As the underlying population mean increases or decreases, the confidence band does also to reflect this change at that point in time.

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Linear regression will be used when background or compliance data are approximately normally distributed, with a constant sample variance around the mean, and the frequency of non-detects is low. The linear regression of concentration against sampling date (time) will be computed as follows:

$$\hat{b} = \sum_{i=1}^{n} (t_i - \overline{t}) \cdot x_i / (n-1) \cdot s_t^2$$

 $x_i = i^{th}$ concentration value and

 $t_i = i^{th}$ sampling date

 \overline{t} = sampling mean date

 s_t^2 = variance of the sampling dates

This estimate leads to the following regression equation:

$$\hat{x} = \overline{x} + \hat{b} \cdot (t - \overline{t})$$

 \overline{x} = mean concentration level

 \hat{x} = estimated mean concentration at time t

The regression residuals will also be computed at each sampling event to ensure uniformity and lack of significant skewness. Regression residuals will be computed at each sampling event as follows:

$$r_i = x_i - \hat{x}_i$$

The estimated variance around the regression line, or mean squared error (MSE) will be computed as follows:

$$s_e^2 = \frac{1}{n-2} \sum_{i=1}^n r_i^2$$

The confidence intervals around a linear regression trend line given confidence level (1- α) and a point in time (t₀), will be computed as follows:

$$LCL_{1-\alpha} = \hat{x}_0 - \sqrt{2s_e^2 \cdot F_{1-2\alpha,2,n-1} \cdot \left[\frac{1}{n} + \frac{(t_0 - \overline{t})^2}{(n-1) \cdot s_t^2}\right]}$$

$$UCL_{1-\alpha} = \hat{x}_0 - \sqrt{2s_e^2 \cdot F_{1-2\alpha,2,n-2} \cdot \left[\frac{1}{n} + \frac{\left(t_0 - \overline{t}\right)^2}{(n-1) \cdot s_t^2} \right]}$$

 \hat{x}_0 = estimated mean concentration from the regression equation at time t_0

 $F_{1-2\alpha,2,n-2}$ = upper (1-2 α)th percentage point from an F-distribution with 2 and (n-2) degrees of freedom

For background data, the UCL around the linear regression line will be used as the GWPS for the trending constituent. For compliance data, confidence bands around the linear regression line will be compared to the GWPS. The CCR unit is considered to be in compliance if the LCL is equal to or lower than the GWPS for all detected constituents at all compliance wells. A GWPS exceedance is determined when the LCL based on the trend line first exceeds the GWPS.

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3.1.7 Non-Parametric Thiel-Sen Trend Line and Confidence Band

If the Mann-Kendall test detects a significant trend in the non-parametric Thiel-Sen line using either background or compliance data for a particular constituent, confidence bands accounting for trends will be constructed to account for the trend-induced variation. The Thiel-Sen trend line will be used as a non-parametric alternative to linear regression when trend residuals cannot be normalized or if there are a higher percentage of non-detects in either background or compliance data. The Thiel-Sen trend line estimates the median concentration over time by combining the median pairwise slope with the median concentration value and the median sample date. To compute the Thiel-Sen line, the data will first be ordered by sampling event x1, x2, xn. All possible distinct pairs of measurements (x_i, x_j) for j > i will be considered and the simple pairwise slope estimate will be computed for each pair as follows:

$$m_{ij} = (x_i - x_i)/(j - i)$$

With a sample size of n, there will be a total of N = n(n-1)/2 pairwise estimates (m_{ij}) . If a given observation is a non-detect, half the RL will be substituted. The N pairwise slope estimates (m_{ij}) will be ordered from least to greatest (renamed m(1), m(2),...m(N)). The Thiel-Sen estimate of slope (Q) will be calculated as the median value of the list depending on whether N is even or odd as follows:

$$Q = \begin{cases} m_{([N+1]/2)} \text{ if N is odd} \\ (m_{(N/2)} + m_{([N+2]/2)})/2 \text{ if N is even} \end{cases}$$

The sample concentration magnitude will be ordered from least to greatest, x(1), x(2), to x(n) and the median concentration will be calculated as follows:

$$\tilde{x} = \begin{cases} x_{([n+1]/2)} & \text{if n is odd} \\ (x_{(n/2)} + x_{([n+2]/2)})/2 & \text{if n is even} \end{cases}$$

The median sampling date (\tilde{t}) with ordered times (t(1), t(2), to t(n)) will also be determined in this way. The Thiel-Sen trend line will then be computed for an estimate at any time (t) of the expected median concentration (x) as follows:

$$x = \tilde{x} + O \cdot (t - \tilde{t}) = (\tilde{x} - O \cdot \tilde{t}) + O \cdot t$$

To construct a confidence band around the Thiel-Sen line, sample pairs (ti, xi) will be formed with a sample date (ti) and the concentration measurement from that date (xi). Bootstrap samples (B) will be formed by repeatedly sampling n pairs at random with replacement from the original sample pairs. This will be repeated 500 times. For each bootstrap sample, a Thiel-Sen trend line will be constructed using the equation above. A series of equally spaced time points (tj) will be identified along the range of sampling dates represented in the original sample, j =1 to m. The Thiel-Sen trend line associated with each bootstrap replicate will be used to compute an estimated concentration (\hat{x}_j^B). An LCL will be constructed for the lower α^{th} percentile $\hat{x}_j^{[\alpha]}$ from the distribution of estimated concentrations at each time point (tj). For a UCL, compute the upper (1- α)th percentile, $\hat{x}_j^{[1-\alpha]}$ at each time point (tj).

For background data, the UCL around the Thiel-Sen trend line will be used as the GWPS for the trending constituent. For compliance data, confidence bands around the Thiel-Sen trend line will be compared to the GWPS. The CCR unit is considered to be in compliance if the LCL is equal to or lower than the GWPS for all detected constituents at all compliance wells. A GWPS exceedance is confirmed when the LCL based on the trend line first exceeds the GWPS.

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3.2 Determination of Statistically Significant Increases over Background

In accordance with 35 I.A.C. §§ 845.610(b)(3)(B) and 845.640(h), individual monitoring event concentrations for each constituent detected in the compliance monitoring wells during compliance monitoring sampling events will be compared to the background concentration as determined by the methods described above. An exceedance of the background concentration for any constituent measured at any compliance monitoring well, or constituent detection if not detected in the background samples, constitutes a Statistically Significant Increase (SSI). An exception to this method is pH, where two-sided (upper and lower) tolerance limits are established from the distribution of the background groundwater quality data. An exceedance of either the UTL or lower tolerance limit (LTL) would constitute an SSI for pH.

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4. REFERENCES

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United States Environmental Protection Agency (USEPA), 2009. *Statistical Analysis of Groundwater Monitoring Data at RCRA Facilities: Unified Guidance*. EPA 530-R-09-007. March 2009.

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ATTACHMENT J

Memorandum



Date: 25 October 2021

Subject: 35 I.A.C. Section 845.430 – Slope Maintenance Documentation for Ash Pond No. 1

at Coffeen Power Plant

Illinois Power Generating Company operates the coal fired Coffeen Power Plant (Plant) located in Montgomery County, Illinois. The Ash Pond No. 1 is an inactive surface impoundment storing coal combustion residuals (CCR). The requirements for the Coffeen Ash Pond No. 1 are found in 35 Ill. Admin. Code 845, Standards for the Disposal of Coal Combustion Residuals in Surface Impoundments (Part 845).

Pursuant to Part 845, Section 845.230(d)(2)(F), the initial operating permit application for existing or inactive CCR surface impoundments that have not completed an Agency approved closure before prior to July 30, 2021, must contain documentation that the CCR surface impoundment, if not incised, will be operated, and maintained with one of the forms of slope protection specified in Section 845.430. This statement addresses the requirements of Part 845, Section 845.430 Slope Maintenance, which states:

<u>Section 845.430:</u> The slopes and pertinent surrounding areas of the CCR surface impoundment must be designed, constructed, operated, and maintained with one of the forms of slope protection specified in subsection (a) that meets all the performance standards of subsection (b).

<u>Section 845.430(a):</u> Slope protection must consist of one of the following: 1) A vegetative cover consisting of grassy vegetation; 2) An engineered cover consisting of a single form or combination of forms of engineered slope protection measures; or 3) A combination of the forms of cover specified in subsections (a)(1) or (a)(2).

Section 845.430(b): Any form of cover for slope protection must meet the following performance standards: 1) The cover must be installed and maintained on the slopes and pertinent surrounding areas of the CCR surface impoundment; 2) The cover must provide protection against surface erosion, wave action, and adverse effects of rapid drawdown; 3) The cover must be maintained to allow for the observation of, and access to, the slopes and pertinent surrounding areas during routine and emergency events; 4) Woody vegetation must be removed from the slopes or pertinent surrounding areas. Any removal of woody vegetation with a diameter greater than 1/2 inch must be directed by a person familiar with the design and operation of the CCR surface impoundment and in consideration of the complexities of removal of a tree or a shrubbery, who must ensure the removal does not create a risk of destabilizing the CCR surface impoundment or otherwise adversely affect the stability and safety of the CCR surface impoundment or

Memorandum (cont'd)



35 I.A.C. Part 845 – Slope Maintenance Documentation for Ash Pond No. 1 at Coffeen Power Plant 25 October 2021 Page 2

personnel undertaking the removal; and 5) The height of vegetation must not exceed 12 inches.

Slope protection, consisting of vegetative cover, was installed on the slopes and pertinent surrounding areas of the Coffeen Ash Pond 1, and is inspected, maintained and repaired as needed. Based on observations from weekly inspections conducted in accordance with Section 845.540(a), and the 2020 annual inspections conducted by Hanson Professional Services Inc., the vegetative cover is described to be in good working condition with a maximum vegetation height of 12 inches. The owner's Operations and Maintenance Plan (O&M Plan) provides details for maintaining grass and removing woody vegetation and addressing erosion features on the slopes. Based on a review of the documentation described above, the owner is implementing the O&M Plan, including the completion of repairs and maintenance as needed and when issues are identified during weekly and/or annual inspections. The slope maintenance portion of the O&M Plan and the Annual Inspection performed by Hanson in 2020 are included in Attachment J. The surface impoundment slope protection (vegetative cover) installed and maintained on the slopes and pertinent areas around the slopes is depicted in the aerial photograph provided below.

Memorandum (cont'd)



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Excerpt from the Coffeen AP1 Operations and Maintenance Manual

1.0 Dam Safety Requirements

- 1.1 Dam Safety Inspections The plant's impoundment and flood prevention structures shall be inspected and maintained in a manner to ensure safe and environmentally responsible operations. A regular maintenance program shall be performed and shall consist of the following inspection items:
 - 1. Earth embankments: Walk the crest, side slopes, and downstream toe of the dam concentrating on surface erosion, seepage, cracks, settlement, slumps, slides, and animal burrows. Frequency of inspection: Weekly.
 - 2. Vegetation: Grass should be a thick vigorous growth to stabilize the earth embankment soils and prevent erosion form occurring. There should be NO trees on the earth embankment and none within a minimum of 20 feet of the embankment toe or other structures. Mowing frequency: Semiannually.
 - 3. Well Readings: Record level of wells on the crest and toe of the berm. Frequency: Quarterly.
 - 4. Special Inspections Special inspections of the levees and ash pond berms shall be performed after earthquakes, floods, water level exceedance in the ponds, or heavy rainfall events. Inspection and report shall be equal to an annual inspection level of detail. Water level in the pond should be noted after a heavy rainfall. Dam Safety staff shall accompany plant personnel on special inspections. Frequency: As required.

Dam Inspection Report

| Name of I | Dam | | Coffeen A | sh Pond #1 | Dam | Dam ID No. | None | | |
|---|----------------------------------|--|-------------------|------------|------------------|------------|------------------|--|--|
| Permit Nu | ımber | N | one | _ | Class of Dam | NA | | | |
| Location | SW 1/4 | Section | 11 | Township | 7N | _Range | 3W | | |
| Owner | Dyne | gy Midwe | st Generat | ion, LLC | | | -534-7668 | | |
| | | Name | | | | Telephon | e Number (Day) | | |
| | 13 | 34 CIPS L | .ane | | | 217 | -534-7668 | | |
| | 1200 | Street | | | <u>.</u> : | Telephone | Number (Night) | | |
| | en, IL ity | - | 52017 Zip Code | _ | N | lontgomery | | | |
| Type of D |)am | | | Е | arth Embankn | nent | | | |
| Type of S | | | | Cor | ncrete Inlet Str | ucture | | | |
| Date(s) Ir | nspected | | | | 16-Nov-20 | | | | |
| Weather ' | When Insլ | pected | | | Clea | ar | | | |
| Temperat | ture When | Inspecte | d | | 50° F | | | | |
| Pool Elev | ation Whe | en Inspect | ted | Unknown | | | | | |
| Tailwater | Elevation | When Ins | spected | None | | | | | |
| annunu PE | OFESSION | innin. | | Inspection | Personnel: | | | | |
| S S S | | CZGIIIII | | James Kn | utelski, PE | Geotech | nnical Engineer | | |
| E ST JAM | ES P. KNUTEL | SKI | | | Name | | Title | | |
| | 002-034200 | | | Jason Car | mpbell, PE | Dvnegv Da | m Safety Manager | | |
| SNIJIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII | OF ILLINOIS | HIRITINE TO THE PARTY OF THE PA | | | Vame | | Title | | |
| 1/1/ | 1 | 17,17,7 | LÖ | Gina Kran | ner | ID | NR-OWR | | |
| V Km | 1 14 | 121 | | 1 | Name | | Title | | |
| と ソド Professio | A 12/ 0 (1/34) 0 nal Engin | eer's Sea | ĺ | John Rom | nang | Cot | ffeen Plant | | |

The Department of Nautural Resources is requesting information that is necessary to accomplish the statutory purpose as outlined under the River, Lakes and Streams Act, 615 ILCS 5. Submittal of this information is REQUIRED. Failure to provide the required information could result in the initiation of non-compliance procedures as outlined in Section 3702.160 of the "Rules for Construction and Maintenance of Dams".

CONDITION CODES

- NE No evidence of a problem
- GC Good condition
- MM Item needing minor maintenance and/or repairs within the year, the safety or integrity of the item is not yet imperiled
- Item needing immediate maintenance to restore or ensure its safety or integrity
- EC Emergency condition which if not immediately repaired or other appropriate measures taken could lead to failure of the dam
- OB Condition requires regular observation to ensure that the condition does not become worse
- NA Not applicable to this dam
- NI Not inspected list the reason for non-inspection under deficiencies

EARTH EMBANKMENT

| ITEM | CONDITION CODE | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES AND IMPLEMENTATION SCHEDULE |
|--|-------------------|--|---|
| Surface Cracks | NE | DEFICIENCIES | AND IMPLEMENTATION SCHEDULE |
| Vertical and Horizontal Alignment of Crest | GC | | |
| Unusual Movement or Cracking At or Beyond Toe | NE | | |
| Sloughing or Erosion of Embankment and Abutment Slopes | NE | | |
| Upstream Face Slope Protection | GC | | |
| Seepage | ОВ | Seepage/wet area on east side lower portion of embankment. | Continue to observe this area for increased seepage volume and transportation of soil in water. |
| Filter and Filter Drains | NA | | |

EARTH EMBANKMENT

(Continued)

| | CONDITION | | RECOMMENDED REMEDIAL MEASURES |
|-----------------------------|-----------|--------------|-------------------------------|
| ITEM | CODE | DEFICIENCIES | AND IMPLEMENTATION SCHEDULE |
| Animal Damage | NE | | |
| Embankment Drainage Ditches | NE | | |
| Vegetative Cover | GC | | |
| Other (Name) | NA | | |
| Other | NA | | |
| Other | NA | | |
| Other | NA | | |

PRINCIPAL SPILLWAY APPROACH CHANNEL

| ITEM | CONDITION CODE | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES AND IMPLEMENTATION SCHEDULE |
|----------------------|-------------------|--------------|---|
| Debris | NE | BEHOLEIVOIEO | AND INIT ELIMENTATION CONEDUCE |
| Side Slope Stability | GC | | |
| Slope Protection | NE | | |
| Other (Name) | NA | | |
| Other | NA | | |
| Other | NA | | |
| Other | NA | | |
| | | | |

PRINCIPAL SPILLWAY

| Drop Inlet Spillway | | X Overflow Spillway S | Structure Gated | |
|-------------------------------------|-------------------|-----------------------|---|--|
| ITEM | CONDITION CODE | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES AND IMPLEMENTATION SCHEDULE | |
| Erosion, Spalling, Cavitation | NE | | | |
| Structure to Embankment Junction | GC | | | |
| Drains | NA | | | |
| Seepage Around or Into Structure | NE | | | |
| Surface Cracks | NE | | | |
| Structural Cracks | NE | | | |

IF THE SPILLWAY IS GATED FILL OUT THE GATES SECTION

PRINCIPAL SPILLWAY

| Drop Inlet Spillway | | X Overflow Spillway S | Structure Gated | |
|-----------------------------|-------------------|-----------------------|---|--|
| ITEM | CONDITION CODE | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES AND IMPLEMENTATION SCHEDULE | |
| Alignment of Abutment Walls | NA | | | |
| Construction Joints | NE | | | |
| Filter and Filter Drains | NA | | | |
| Trash Racks | GC | | | |
| Bridge and Piers | NA | | | |
| Differential Settlement | NE | | | |
| Other (Name) | NA | | | |

ENERGY DISSIPATOR

| ∐ Pr | incipal Spillway 「ype: | None | Outlet Works | |
|-------------------------------------|---------------------------|--------------|---|--|
| | | 140110 | | |
| ITEM | CONDITION CODE | DEFICIENCIES | RECOMMENDED REMEDIAL MEASURES AND IMPLEMENTATION SCHEDULE | |
| Erosion, Spalling, Cavitation | NA | | | |
| Structure to Embankment Junction | NA | | | |
| Construction Joints | NA | | | |
| Surface Cracks | NA | | | |
| Structural Cracks | NA | | | |
| Differential Alignment | NA | | | |
| Expansion and Contraction Joints | NA | | | |

EMERGENCY SPILLWAY

| Earth | | | Other: Name | None |
|------------------------------------|-------------------|--------------|--|------|
| ITEM | CONDITION CODE | DEFICIENCIES | RECOMMENDED REMEDIA AND IMPLEMENTATION SC | |
| Erosion | NA | | | |
| Weeds, Logs, Other Obstructions | NA | | | |
| Side Slope Sloughing | NA | | | |
| Vegetation | NA | | | |
| Sedimentation | NA | | | |
| Riprap | NA | | | |
| Settlement of Crest | NA | | | |
| Downstream Channel | NA | | | |
| Other (Name) | NA | | | |

SUMMARY OF MAINTENANCE DONE AND/OR REPAIRS MADE SINCE THE LAST INSPECTION

| DA | TE OF PRESENT INSPECTION | 16-Nov-20 |
|----|---|-----------------|
| DA | TE OF LAST INSPECTION | 22-Oct-19 |
| 1. | EARTH EMBANKMENT DAMS Periodic Mowing of upstream and dow | nstream slopes. |
| 2. | CONCRETE MASONRY DAMS | |
| | NA | |
| 3. | PRINCIPAL SPILLWAY | |
| | None Noted | |
| 4. | OUTLET WORKS | |
| | None Noted | |
| 5. | EMERGENCY SPILLWAY | |

NA

Owner's Maintenance Statement

| I, | | , o | wner of | een Ash Pond #1 Dam , |
|---------------------------------|------------------|-----------------|--------------------|---------------------------------------|
| Dam Identification Number | None | , in | Montgomery | County, |
| am maintaining the dam in acco | rdance with the | accepted m | aintenance plan | which is part of |
| Permit Number No | ne . | | | |
| | | | | |
| | | | Signature | |
| | | | Oignature | |
| | | | Date | |
| | | | Date | |
| | | | | |
| Owner's Opera | ition and Ma | intenance | Plan Staten | nent |
| | | | | |
| I, | | | | een Ash Pond #1 Dam , |
| <u> </u> | | · | | · · · · · · · · · · · · · · · · · · · |
| Dam Identification Number | None | , in | Montgomery | County, |
| have reviewed the operation and | d maintenance | plan includin | g the Emergenc | y Action Plan (EAF |
| which is part of, Permit Number | | None | | |
| l h | nave enclosed th | ne appropria | te revisions or | |
| | | | | n are necessary. |
| ' | iave determined | i illai lio lev | isions to the plai | rare necessary. |
| | | | | |
| | | | Signature | |
| | | | | |
| | | | Date | |

The Department of Nautural Resources is requesting information that is necessary to accomplish the statutory purpose as outlined under the River, Lakes and Streams Act, 615 ILCS 5. Submittal of this information is REQUIRED. Failure to provide the required information could result in the initiation of non-compliance procedures as outlined in Section 3702.160 of the "Rules for Construction and Maintenance of Dams".



South side



South side



East side



East side



East side seepage at toe – observe this area



North side



North side



West side



West side



Outlet structure

ATTACHMENT K

POST-CLOSURE PLAN FOR EXISTING CCR SURFACE IMPOUNDMENT 40 C.F.R. § 257.104 and 35 I.A.C. 845.780 REV 0 – 10/30/2021

| SITE INFORMATION | | | | | | | | |
|----------------------|---------------------------|--|---|--|--|--|--|--|
| Site Name / Address | Coffeen Power Plant / 2 | ffeen Power Plant / 134 Cips Lane, Coffeen, IL 61207 | | | | | | |
| Owner Name / Address | Illinois Power Generation | ng Company / 6555 Sierra Driv | e Irving, Texas 75039 | | | | | |
| CCR Unit | Ash Pond No. 1 | Closure Method and Final Cover Type | Close In-Place Clayey Soil Cover with Vegetation | | | | | |

POST-CLOSURE PLAN DESCRIPTION

40 C.F.R. § 257.104(c)(1) and 35 I.A.C. 845.780(c)(1) – Length of post-closure care period.

40 C.F.R. § 257.104(c)(2) and 35 I.A.C. 845.780(c)(2) – Circumstances extending the post closure care period.

Post-closure care will be conducted for a period of 30 years as required by 40 C.F.R. § 257.104(c)(1) and 35 I.A.C. 845.780(c)(1), except as provided by 40 C.F.R. § 257.104(c)(2) and 35 I.A.C. 845.780(c)(2).

If at the end of the post-closure care period the CCR unit is operating under assessment monitoring in accordance with §257.95, the post-closure care as described in this plan will continue until returning to detection monitoring in accordance with §257.95.

Under 35 I.A.C. 845.780(c)(2), the post-closure care period will be extended until groundwater monitoring data demonstrate that concentrations are below the groundwater protection standards in Section 845.600 and are not increasing for those constituents over background, using the statistical procedures and performance standards in Section 845.640(f) and (g), provided that concentrations have been reduced to the maximum extent feasible and concentrations are protective of human health and the environment.

40 C.F.R. § 257.104(d)(1)(i) and 35 I.A.C. 845.780(d)(1)(A) – A description of the monitoring and maintenance activities required in 40 C.F.R. § 257.104(b) and 35 I.A.C. 845.780(b), and the frequency at which these activities will be performed, to maintain the integrity and effectiveness of the final cover system, maintain the groundwater monitoring system and monitor the groundwater.

Pursuant to § 257.104(b)(1) and 35 I.A.C. 845.780(b)(1), throughout the post-closure care period, periodic visual observations of the final cover system and stormwater management system will be performed at least annually for evidence of settlement, subsidence, erosion, or other damage that may adversely affect the integrity and effectiveness of the final cover system. When practical, visual observations of the final cover will be made concurrent with groundwater monitoring activities.

Noted evidence of damage, such as rills, surface cracks and settlement, will be repaired to maintain the integrity and effectiveness of the final cover system. Vegetation will be established and maintained on the final cover system, including storm drainage areas, where appropriate, to provide long-term erosion control. Established vegetation and the slope design of the final cover system will prevent potential erosion and damage that may be caused by run-on and run-off.

Repair activities may include, but are not limited to, replacing and compacting soil cover, repairing drainage channels that have been eroded, filling in depressions with soil, regrading, and reseeding areas of failed vegetation, as necessary.

Pursuant to § 257.104(b)(3) and 35 I.A.C. 845.780(b)(3), the groundwater monitoring system will be maintained, and groundwater will be monitored as required by 40 C.F.R. § 257.90 through 40 C.F.R. § 257.98 and 35 I.A.C. 845.600 through 35 I.A.C. 845.680. Monitoring wells will be inspected during each groundwater sampling event. Monitoring wells and associated instrumentation will be maintained so that they perform to the design specifications throughout the life of the monitoring program. Groundwater monitoring frequency will be at least quarterly, except as provided in 40 C.F.R. § 257.94(d), 257.94(c), and 35 I.A.C. 845.650(b)(4).

40 C.F.R. § 257.104(d)(1)(ii) and 35 I.A.C. 845.780(d)(1)(B) – The name, address,

telephone number and email address of the person or office to contact about the facility during the post-closure care period.

Illinois Power Generating Company 6555 Sierra Drive Irving, Texas 75039 800.633.4704 ccr@dynegy.com

40 C.F.R. § 257.104(d)(1)(iii) and 35 I.A.C. 845.780(d)(1)(C) – A description of the planned uses of the property during the post-closure period.

The CCR unit is located at a closed electric generation facility. Planned uses of the property during the post-closure period are currently unknown, except for post-closure care of the CCR unit.

Post-closure use of the property will not disturb the integrity of the final cover system or other components of the containment system, or the function of the monitoring systems unless necessary to comply with the requirements of 40 C.F.R. Part § 257, Subpart D and 35 I.A.C. Part 845. Any other disturbance will be conducted following a demonstration that it will not increase the potential threat to human health or the environment, as required by 40 C.F.R. § 257.104(d)(1)(iii) and 35 I.A.C. 845.780 (d)(1)(C). The demonstration will be certified by a qualified professional engineer and submitted to the Illinois Environmental Protection Agency (IEPA). Per 40 C.F.R. § 257.104(d)(1)(iii) notification shall be provided to the State Director that the demonstration has been placed in the operating record and on the owners or operator's publicly accessible internet site.

Following closure of the CCR unit, a notation on the deed to the property, or some other instrument that is normally examined during title search, will be recorded in accordance with 40 C.F.R. § 257.102(i) and 35 I.A.C. 845.760(h). The notation will notify potential purchasers of the property that the land has been used as a CCR unit and its use is restricted under the post-closure care requirements in 40 C.F.R. § 257.104(d)(1)(iii) and 35 I.A.C. 845.780(d)(1)(C) or groundwater monitoring requirements per 35 I.A.C. 845.740(b). Within 30 days of recording the deed notation, a notification stating that the notation has been recorded will be submitted to the IEPA and placed in the facility's operating record per 35 I.A.C. 845.760(h)(3). The notification will be placed on the owner or operator's publicly accessible CCR Web site in accordance with 40 C.F.R. § 257.107 (i)(9) and 35 I.A.C. 845.810(e) and placed in the facility's operating record as required by 35 I.A.C. 845.800(d)(26) and §257.105(i)(9).

40 C.F.R. § 257.104(d)(3) and 35 I.A.C. 845.780(d)(3) -Pursuant to 40 C.F.R. § 257.104(d), the initial post closure care plan for Amendments to the initial or subsequent written postthe Coffeen Ash Pond No. 1 was prepared on October 17, 2016. That closure plan. plan is being amended pursuant to 40 C.F.R. § 257.104(d)(3)(i). This plan also serves as the initial post-closure care plan, prepared in accordance with 35 I.A.C. 845.780(d). Pursuant to § 257.104(d)(3) and 35 I.A.C. 845.780(d)(3), an operating permit modification application to amend the initial or any subsequent written post-closure care plan developed under 35 I.A.C. 845.780 (d)(1) and § 257.104(d)(1) will be submitted to IEPA. The written post-closure care plan will be amended whenever there is a change in the operation of the CCR surface impoundment that would substantially affect the written post-closure care plan in effect; or unanticipated events necessitate a revision of the written post-closure care plan, after postclosure activities have started. The written post-closure care plan will be amended at least 60 days before a planned change in the operation of the facility or CCR surface impoundment, or within 60 days after an unanticipated event requires the need to revise the existing plan. If the plan is revised after postclosure activities have started, a request to modify the operating permit, including an amended written post-closure care plan, will be submitted to the IEPA within 30 days following the triggering event. Certification by a qualified professional engineer will be appended to 40 C.F.R. § 257.104(d)(4) and 35 I.A.C. 845.780(d)(4) -Qualified professional engineering certification. this plan and any amendment of this plan. 35 I.A.C. 845.780(e) – Termination of post-closure care. Upon completion of the post-closure period, a request to terminate post-closure care will be submitted to the IEPA. The request will include a certification by a qualified professional engineer verifying that postclosure care has been completed in accordance with the post-closure care plan specified in 35 I.A.C. 845.780(d) and the requirements of 35 I.A.C. 845.780. 40 C.F.R. § 257.104(e) and 35 I.A.C. 845.780(f) -A notification of completion of post-closure care will be prepared and Notification of completion of the post-closure care period placed in the facility's operating record within 30 days after IEPA approval of the request to terminate post-closure care. The notification will be placed in the facility's operating record in accordance with 35 I.A.C. 845.800(d)(31) and § 257.105(i)(13). The notification will be placed on the owner or operator's publicly accessible CCR Internet site in accordance with the requirements of § 257.107(i)(13) and 35 I.A.C. 845.810(e). The IEPA will be notified when the notification has been placed in the operating record and on the owner or operator's publicly accessible Internet site in accordance with the requirements of § 257.106(i)(13).

Certification Statement 40 C.F.R. § 257.104 (d)(4) and 35 I.A.C. 845.780(d)(4) – Amended/Initial Written Post Closure Plan for a CCR Surface Impoundment

CCR Unit: Illinois Power Generating Company; Coffeen Power Plant; Ash Pond No.1

I, John R. Hesemann, being a Registered Professional Engineer in good standing in the State of Illinois, do hereby certify, to the best of my knowledge, information, and belief, that the information contained in this certification has been prepared in accordance with the accepted practice of engineering. I certify, for the above referenced CCR Unit, that the information contained in the amended/initial written post closure plan, dated October 30, 2021, meets the requirements of 40 C.F.R. § 257.104 and 35 I.A.C. 845.780.

John R. Hesemann

Printed Name

9/27/2021

Date

DERT HESELLING BERT H

ATTACHMENT M

HISTORY OF POTENTIAL EXCEEDANCES

This presentation of the History of Potential Exceedances, and any corrective action taken to remediate groundwater, is provided to meet the requirements of Title 35 of the Illinois Administrative Code (35 I.A.C.) § 845.230(d)(2)(M) for the Coffeen Power Plant Ash Pond No. 1, Illinois Environmental Protection Agency (IEPA) ID No. W1350150004-01.

Note

Groundwater concentrations from 2015 to 2021 presented in the Hydrogeologic Site Characterization Report (HCR) Table 4-1, and evaluated and summarized in the following tables, are considered potential exceedances because the methodology used to determine them is proposed in the Statistical Analysis Plan (Appendix A to Groundwater Monitoring Plan [GMP]), which has not been reviewed or approved by the IEPA at the time of submittal of the 35 I.A.C. § 845 Operating Permit application.

Alternate sources for potential exceedances as allowed by 35 I.A.C. § 845.650(e) have not yet been evaluated. These will be evaluated and presented in future submittals to IEPA as appropriate.

Table 1 summarizes how the potential exceedances were determined. Table 2 is a summary of all potential exceedances.

Background Concentrations

Background monitoring wells identified in the GMP include G281 and G306.

For monitoring wells that have been historically monitored in accordance with Title 40, Code of Federal Regulations, Part 257, Subpart D (Standards for the Disposal of Coal Combustion Residuals in Landfills and Surface Impoundments), background concentrations calculated from sampling events in 2015-2017 were compared to the standards identified in 35 I.A.C. § 845.600(a)(1). For constituents with calculated background concentrations in 2015-2017 greater than the standards in 35 I.A.C. § 845.600(a)(1), those calculated background concentrations were used as Groundwater Protection Standards (GWPSs) for comparing to statistical calculation results for each compliance well to determine potential exceedances. Compliance well statistical calculations consider concentrations from all sampling events in 2015-2021.

For all other monitoring wells, either newly constructed in 2021 or existing wells not monitored under Title 40, Code of Federal Regulations, Part 257, Subpart D, background concentrations calculated from the eight sampling events required by 35 I.A.C. § 845.650(b)(1)(A), to be collected within 180 days from April 21, 2021, were compared to the standards identified in 35 I.A.C. § 845.600(a)(1). For constituents with calculated background concentrations greater than the standards in 35 I.A.C. § 845.600(a)(1), those calculated background concentrations were used as GWPSs. Compliance well statistical calculations from that same time period were compared to the GWPSs to determine potential exceedances.

Corrective Action

No corrective actions have been taken to remediate the groundwater.

COF AP1 HPE FINAL 10.17.2021 1/1

| Sample Location | | Program | Constituent | Result Unit | Sample Date Range | Statistical Calculation | Statistical Result | GWPS | Background | Part 845 Standard | GWPS Source |
|-----------------|----|---------|------------------------------|-------------|-------------------------|-------------------------|--------------------|---------|------------|-------------------|-------------------|
| G301 | UA | 257 | Antimony, total | mg/L | 11/20/2015 - 01/27/2021 | All ND - Last | 0.003 | 0.006 | 0.003 | 0.006 | Standard |
| G301 | UA | 257 | Arsenic, total | mg/L | 11/20/2015 - 01/27/2021 | CI around median | 0.001 | 0.010 | 0.0043 | 0.01 | Standard |
| G301 | UA | 257 | Barium, total | mg/L | 11/20/2015 - 01/27/2021 | CI around mean | 0.029 | 2.0 | 0.13 | 2 | Standard |
| G301 | UA | 257 | Beryllium, total | mg/L | 11/20/2015 - 01/27/2021 | All ND - Last | 0.001 | 0.004 | 0.001 | 0.004 | Standard |
| G301 | UA | 257 | Boron, total | mg/L | 11/20/2015 - 01/27/2021 | CB around linear reg | 1.7 | 2.9 | 2.9 | 2 | Background |
| G301 | UA | 257 | Cadmium,total | mg/L | 11/20/2015 - 01/27/2021 | CI around median | 0.001 | 0.005 | 0.001 | 0.005 | Standard |
| G301 | UA | 257 | Chloride, total | mg/L | 11/20/2015 - 01/27/2021 | CB around linear reg | 9.3 | 200 | 75 | 200 | Standard |
| G301 | UA | 257 | Chromium, total | mg/L | 11/20/2015 - 01/27/2021 | CI around median | 0.004 | 0.10 | 0.012 | 0.1 | Standard |
| G301 | UA | 257 | Cobalt, total | mg/L | 11/20/2015 - 01/27/2021 | Future median | 0.002 | 0.0064 | 0.0064 | 0.006 | Background |
| G301 | UA | 257 | Fluoride, total | mg/L | 11/20/2015 - 01/27/2021 | CI around geomean | 0.26 | 4.0 | 0.47 | 4 | Standard |
| G301 | UA | 257 | Lead, total | mg/L | 11/20/2015 - 01/27/2021 | CI around geomean | 0.0012 | 0.0075 | 0.0063 | 0.0075 | Standard |
| G301 | UA | 257 | Lithium, total | mg/L | 11/20/2015 - 01/27/2021 | CB around linear reg | 0.014 | 0.040 | 0.013 | 0.04 | Standard |
| G301 | UA | 257 | Mercury, total | mg/L | 11/20/2015 - 01/27/2021 | CI around median | 0.0002 | 0.002 | 0.0002 | 0.002 | Standard |
| G301 | UA | 257 | Molybdenum, total | mg/L | 11/20/2015 - 01/27/2021 | All ND - Last | 0.001 | 0.10 | 0.0019 | 0.1 | Standard |
| G301 | UA | 257 | pH (field) | SU | 11/20/2015 - 01/27/2021 | CI around mean | 6.7 | 6.5/9.0 | 6.5/7.1 | 6.5/9 | Standard/Standard |
| G301 | UA | 257 | Radium-226 + Radium 228, tot | pCi/L | 11/20/2015 - 01/27/2021 | CI around mean | 0.63 | 5.0 | 1.9 | 5 | Standard |
| G301 | UA | 257 | Selenium, total | mg/L | 11/20/2015 - 01/27/2021 | All ND - Last | 0.001 | 0.050 | 0.0011 | 0.05 | Standard |
| G301 | UA | 257 | Sulfate, total | mg/L | 11/20/2015 - 01/27/2021 | Future median | 750 | 700 | 700 | 400 | Background |
| G301 | UA | 257 | Thallium, total | mg/L | 11/20/2015 - 01/27/2021 | All ND - Last | 0.001 | 0.002 | 0.001 | 0.002 | Standard |
| G301 | UA | 257 | Total Dissolved Solids | mg/L | 11/20/2015 - 01/27/2021 | CI around mean | 1100 | 1200 | 893 | 1200 | Standard |
| G302 | UA | 257 | Antimony, total | mg/L | 11/20/2015 - 01/27/2021 | All ND - Last | 0.003 | 0.006 | 0.003 | 0.006 | Standard |
| G302 | UA | 257 | Arsenic, total | mg/L | 11/20/2015 - 01/27/2021 | CI around geomean | 0.00152 | 0.010 | 0.0043 | 0.01 | Standard |
| G302 | UA | 257 | Barium, total | mg/L | 11/20/2015 - 01/27/2021 | CI around mean | 0.026 | 2.0 | 0.13 | 2 | Standard |
| G302 | UA | 257 | Beryllium, total | mg/L | 11/20/2015 - 01/27/2021 | All ND - Last | 0.001 | 0.004 | 0.001 | 0.004 | Standard |
| G302 | UA | 257 | Boron, total | mg/L | 11/20/2015 - 01/27/2021 | Future median | 1.2 | 2.9 | 2.9 | 2 | Background |
| G302 | UA | 257 | Cadmium,total | mg/L | 11/20/2015 - 01/27/2021 | All ND - Last | 0.001 | 0.005 | 0.001 | 0.005 | Standard |



| Sample Location | | Program | Constituent | Result Unit | Sample Date Range | Statistical Calculation | Statistical Result | GWPS | Background | Part 845 Standard | GWPS Source |
|-----------------|----|---------|------------------------------|-------------|-------------------------|-------------------------|--------------------|---------|------------|-------------------|-------------------|
| G302 | UA | 257 | Chloride, total | mg/L | 11/20/2015 - 01/27/2021 | CI around mean | 10 | 200 | 75 | 200 | Standard |
| G302 | UA | 257 | Chromium, total | mg/L | 11/20/2015 - 01/27/2021 | CI around median | 0.004 | 0.10 | 0.012 | 0.1 | Standard |
| G302 | UA | 257 | Cobalt, total | mg/L | 11/20/2015 - 01/27/2021 | Future median | 0.002 | 0.0064 | 0.0064 | 0.006 | Background |
| G302 | UA | 257 | Fluoride, total | mg/L | 11/20/2015 - 01/27/2021 | CI around mean | 0.27 | 4.0 | 0.47 | 4 | Standard |
| G302 | UA | 257 | Lead, total | mg/L | 11/20/2015 - 01/27/2021 | CI around median | 0.001 | 0.0075 | 0.0063 | 0.0075 | Standard |
| G302 | UA | 257 | Lithium, total | mg/L | 11/20/2015 - 01/27/2021 | CI around mean | 0.016 | 0.040 | 0.013 | 0.04 | Standard |
| G302 | UA | 257 | Mercury, total | mg/L | 11/20/2015 - 01/27/2021 | CI around median | 0.0002 | 0.002 | 0.0002 | 0.002 | Standard |
| G302 | UA | 257 | Molybdenum, total | mg/L | 11/20/2015 - 01/27/2021 | CI around geomean | 0.00108 | 0.10 | 0.0019 | 0.1 | Standard |
| G302 | UA | 257 | pH (field) | SU | 11/20/2015 - 01/27/2021 | CI around mean | 6.9 | 6.5/9.0 | 6.5/7.1 | 6.5/9 | Standard/Standard |
| G302 | UA | 257 | Radium-226 + Radium 228, tot | pCi/L | 11/20/2015 - 01/27/2021 | CI around geomean | 0.35 | 5.0 | 1.9 | 5 | Standard |
| G302 | UA | 257 | Selenium, total | mg/L | 11/20/2015 - 01/27/2021 | CI around median | 0.001 | 0.050 | 0.0011 | 0.05 | Standard |
| G302 | UA | 257 | Sulfate, total | mg/L | 11/20/2015 - 01/27/2021 | Future median | 350 | 700 | 700 | 400 | Background |
| G302 | UA | 257 | Thallium, total | mg/L | 11/20/2015 - 01/27/2021 | All ND - Last | 0.001 | 0.002 | 0.001 | 0.002 | Standard |
| G302 | UA | 257 | Total Dissolved Solids | mg/L | 11/20/2015 - 01/27/2021 | CI around mean | 909 | 1200 | 893 | 1200 | Standard |
| G303 | UA | 257 | Antimony, total | mg/L | 11/20/2015 - 01/26/2021 | All ND - Last | 0.003 | 0.006 | 0.003 | 0.006 | Standard |
| G303 | UA | 257 | Arsenic, total | mg/L | 11/20/2015 - 01/26/2021 | CI around mean | 0.00296 | 0.010 | 0.0043 | 0.01 | Standard |
| G303 | UA | 257 | Barium, total | mg/L | 11/20/2015 - 01/26/2021 | CI around median | 0.015 | 2.0 | 0.13 | 2 | Standard |
| G303 | UA | 257 | Beryllium, total | mg/L | 11/20/2015 - 01/26/2021 | All ND - Last | 0.001 | 0.004 | 0.001 | 0.004 | Standard |
| G303 | UA | 257 | Boron, total | mg/L | 11/20/2015 - 01/26/2021 | Future median | 2.0 | 2.9 | 2.9 | 2 | Background |
| G303 | UA | 257 | Cadmium,total | mg/L | 11/20/2015 - 01/26/2021 | All ND - Last | 0.001 | 0.005 | 0.001 | 0.005 | Standard |
| G303 | UA | 257 | Chloride, total | mg/L | 11/20/2015 - 01/26/2021 | CI around mean | 28 | 200 | 75 | 200 | Standard |
| G303 | UA | 257 | Chromium, total | mg/L | 11/20/2015 - 01/26/2021 | CI around median | 0.004 | 0.10 | 0.012 | 0.1 | Standard |
| G303 | UA | 257 | Cobalt, total | mg/L | 11/20/2015 - 01/26/2021 | Future median | 0.002 | 0.0064 | 0.0064 | 0.006 | Background |
| G303 | UA | 257 | Fluoride, total | mg/L | 11/20/2015 - 01/26/2021 | CI around mean | 0.27 | 4.0 | 0.47 | 4 | Standard |
| G303 | UA | 257 | Lead, total | mg/L | 11/20/2015 - 01/26/2021 | CI around median | 0.001 | 0.0075 | 0.0063 | 0.0075 | Standard |
| G303 | UA | 257 | Lithium, total | mg/L | 11/20/2015 - 01/26/2021 | CI around mean | 0.037 | 0.040 | 0.013 | 0.04 | Standard |



| Sample Location | HSU | Program | Constituent | Result Unit | Sample Date Range | Statistical Calculation | Statistical Result | GWPS | Background | Part 845 Standard | GWPS Source |
|-----------------|-----|---------|------------------------------|-------------|-------------------------|-------------------------|--------------------|---------|------------|-------------------|-------------------|
| G303 | UA | 257 | Mercury, total | mg/L | 11/20/2015 - 01/26/2021 | CI around median | 0.0002 | 0.002 | 0.0002 | 0.002 | Standard |
| G303 | UA | 257 | Molybdenum, total | mg/L | 11/20/2015 - 01/26/2021 | CI around mean | 0.00184 | 0.10 | 0.0019 | 0.1 | Standard |
| G303 | UA | 257 | pH (field) | SU | 11/20/2015 - 01/26/2021 | CI around mean | 6.9 | 6.5/9.0 | 6.5/7.1 | 6.5/9 | Standard/Standard |
| G303 | UA | 257 | Radium-226 + Radium 228, tot | pCi/L | 11/20/2015 - 01/26/2021 | CI around mean | 0.49 | 5.0 | 1.9 | 5 | Standard |
| G303 | UA | 257 | Selenium, total | mg/L | 11/20/2015 - 01/26/2021 | All ND - Last | 0.001 | 0.050 | 0.0011 | 0.05 | Standard |
| G303 | UA | 257 | Sulfate, total | mg/L | 11/20/2015 - 01/26/2021 | Future median | 730 | 700 | 700 | 400 | Background |
| G303 | UA | 257 | Thallium, total | mg/L | 11/20/2015 - 01/26/2021 | All ND - Last | 0.001 | 0.002 | 0.001 | 0.002 | Standard |
| G303 | UA | 257 | Total Dissolved Solids | mg/L | 11/20/2015 - 01/26/2021 | CI around mean | 1460 | 1200 | 893 | 1200 | Standard |
| G304 | UA | 257 | Antimony, total | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 0.003 | 0.006 | 0.003 | 0.006 | Standard |
| G304 | UA | 257 | Arsenic, total | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 0.0023 | 0.010 | 0.0043 | 0.01 | Standard |
| G304 | UA | 257 | Barium, total | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 0.032 | 2.0 | 0.13 | 2 | Standard |
| G304 | UA | 257 | Beryllium, total | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 0.001 | 0.004 | 0.001 | 0.004 | Standard |
| G304 | UA | 257 | Boron, total | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 2.6 | 2.9 | 2.9 | 2 | Background |
| G304 | UA | 257 | Cadmium,total | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 0.001 | 0.005 | 0.001 | 0.005 | Standard |
| G304 | UA | 257 | Chloride, total | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 27 | 200 | 75 | 200 | Standard |
| G304 | UA | 257 | Chromium, total | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 0.0049 | 0.10 | 0.012 | 0.1 | Standard |
| G304 | UA | 257 | Cobalt, total | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 0.0047 | 0.0064 | 0.0064 | 0.006 | Background |
| G304 | UA | 257 | Fluoride, total | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 0.48 | 4.0 | 0.47 | 4 | Standard |
| G304 | UA | 257 | Lead, total | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 0.0017 | 0.0075 | 0.0063 | 0.0075 | Standard |
| G304 | UA | 257 | Lithium, total | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 0.010 | 0.040 | 0.013 | 0.04 | Standard |
| G304 | UA | 257 | Mercury, total | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 0.0002 | 0.002 | 0.0002 | 0.002 | Standard |
| G304 | UA | 257 | Molybdenum, total | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 0.0017 | 0.10 | 0.0019 | 0.1 | Standard |
| G304 | UA | 257 | pH (field) | SU | 11/20/2015 - 05/20/2016 | Most recent sample | 7.1 | 6.5/9.0 | 6.5/7.1 | 6.5/9 | Standard/Standard |
| G304 | UA | 257 | Radium-226 + Radium 228, tot | pCi/L | 11/20/2015 - 05/20/2016 | Most recent sample | 0.22 | 5.0 | 1.9 | 5 | Standard |
| G304 | UA | 257 | Selenium, total | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 0.001 | 0.050 | 0.0011 | 0.05 | Standard |
| G304 | UA | 257 | Sulfate, total | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 1000 | 700 | 700 | 400 | Background |



| Sample Location | HSU | Program | Constituent | Result Unit | Sample Date Range | Statistical Calculation | Statistical Result | GWPS | Background | Part 845 Standard | GWPS Source |
|-----------------|-----|---------|------------------------------|-------------|-------------------------|-------------------------|--------------------|---------|------------|-------------------|-------------------|
| G304 | UA | 257 | Thallium, total | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 0.001 | 0.002 | 0.001 | 0.002 | Standard |
| G304 | UA | 257 | Total Dissolved Solids | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 1300 | 1200 | 893 | 1200 | Standard |
| G305 | UA | 257 | Antimony, total | mg/L | 05/19/2016 - 11/17/2016 | All ND - Last | 0.003 | 0.006 | 0.003 | 0.006 | Standard |
| G305 | UA | 257 | Arsenic, total | mg/L | 05/19/2016 - 11/17/2016 | CI around median | 0 | 0.010 | 0.0043 | 0.01 | Standard |
| G305 | UA | 257 | Barium, total | mg/L | 05/19/2016 - 11/17/2016 | CI around geomean | 0.023 | 2.0 | 0.13 | 2 | Standard |
| G305 | UA | 257 | Beryllium, total | mg/L | 05/19/2016 - 11/17/2016 | All ND - Last | 0.001 | 0.004 | 0.001 | 0.004 | Standard |
| G305 | UA | 257 | Boron, total | mg/L | 05/19/2016 - 11/17/2016 | Future median | 2.4 | 2.9 | 2.9 | 2 | Background |
| G305 | UA | 257 | Cadmium,total | mg/L | 05/19/2016 - 11/17/2016 | All ND - Last | 0.001 | 0.005 | 0.001 | 0.005 | Standard |
| G305 | UA | 257 | Chloride, total | mg/L | 05/19/2016 - 11/17/2016 | CI around median | 0 | 200 | 75 | 200 | Standard |
| G305 | UA | 257 | Chromium, total | mg/L | 05/19/2016 - 11/17/2016 | CI around median | 0 | 0.10 | 0.012 | 0.1 | Standard |
| G305 | UA | 257 | Cobalt, total | mg/L | 05/19/2016 - 11/17/2016 | Future median | 0.002 | 0.0064 | 0.0064 | 0.006 | Background |
| G305 | UA | 257 | Fluoride, total | mg/L | 05/19/2016 - 11/17/2016 | CI around mean | 0.39 | 4.0 | 0.47 | 4 | Standard |
| G305 | UA | 257 | Lead, total | mg/L | 05/19/2016 - 11/17/2016 | CI around geomean | 0.000447 | 0.0075 | 0.0063 | 0.0075 | Standard |
| G305 | UA | 257 | Lithium, total | mg/L | 05/19/2016 - 11/17/2016 | CI around mean | 0.00673 | 0.040 | 0.013 | 0.04 | Standard |
| G305 | UA | 257 | Mercury, total | mg/L | 05/19/2016 - 11/17/2016 | All ND - Last | 0.0002 | 0.002 | 0.0002 | 0.002 | Standard |
| G305 | UA | 257 | Molybdenum, total | mg/L | 05/19/2016 - 11/17/2016 | CI around mean | 0.00000974 | 0.10 | 0.0019 | 0.1 | Standard |
| G305 | UA | 257 | pH (field) | SU | 05/19/2016 - 11/17/2016 | CI around mean | 6.9 | 6.5/9.0 | 6.5/7.1 | 6.5/9 | Standard/Standard |
| G305 | UA | 257 | Radium-226 + Radium 228, tot | pCi/L | 05/19/2016 - 11/17/2016 | CI around mean | 0.21 | 5.0 | 1.9 | 5 | Standard |
| G305 | UA | 257 | Selenium, total | mg/L | 05/19/2016 - 11/17/2016 | All ND - Last | 0.001 | 0.050 | 0.0011 | 0.05 | Standard |
| G305 | UA | 257 | Sulfate, total | mg/L | 05/19/2016 - 11/17/2016 | Future median | 890 | 700 | 700 | 400 | Background |
| G305 | UA | 257 | Thallium, total | mg/L | 05/19/2016 - 11/17/2016 | All ND - Last | 0.001 | 0.002 | 0.001 | 0.002 | Standard |
| G305 | UA | 257 | Total Dissolved Solids | mg/L | 05/19/2016 - 11/17/2016 | CI around mean | 1280 | 1200 | 893 | 1200 | Standard |
| G307 | UA | 257 | Antimony, total | mg/L | 08/16/2016 - 01/27/2021 | All ND - Last | 0.003 | 0.006 | 0.003 | 0.006 | Standard |
| G307 | UA | 257 | Arsenic, total | mg/L | 08/16/2016 - 01/27/2021 | CI around median | 0.001 | 0.010 | 0.0043 | 0.01 | Standard |
| G307 | UA | 257 | Barium, total | mg/L | 08/16/2016 - 01/27/2021 | CI around geomean | 0.026 | 2.0 | 0.13 | 2 | Standard |
| G307 | UA | 257 | Beryllium, total | mg/L | 08/16/2016 - 01/27/2021 | CI around median | 0.001 | 0.004 | 0.001 | 0.004 | Standard |



| Sample Location | HSU | Program | Constituent | Result Unit | Sample Date Range | Statistical Calculation | Statistical Result | GWPS | Background | Part 845 Standard | GWPS Source |
|-----------------|-----|---------|------------------------------|-------------|-------------------------|-------------------------|--------------------|---------|------------|-------------------|-------------------|
| G307 | UA | 257 | Boron, total | mg/L | 08/16/2016 - 01/27/2021 | Future median | 2.1 | 2.9 | 2.9 | 2 | Background |
| G307 | UA | 257 | Cadmium,total | mg/L | 08/16/2016 - 01/27/2021 | CI around median | 0.001 | 0.005 | 0.001 | 0.005 | Standard |
| G307 | UA | 257 | Chloride, total | mg/L | 08/16/2016 - 01/27/2021 | CB around linear reg | 9.9 | 200 | 75 | 200 | Standard |
| G307 | UA | 257 | Chromium, total | mg/L | 08/16/2016 - 01/27/2021 | CI around median | 0.004 | 0.10 | 0.012 | 0.1 | Standard |
| G307 | UA | 257 | Cobalt, total | mg/L | 08/16/2016 - 01/27/2021 | Future median | 0.0024 | 0.0064 | 0.0064 | 0.006 | Background |
| G307 | UA | 257 | Fluoride, total | mg/L | 08/16/2016 - 01/27/2021 | CI around geomean | 0.25 | 4.0 | 0.47 | 4 | Standard |
| G307 | UA | 257 | Lead, total | mg/L | 08/16/2016 - 01/27/2021 | CI around median | 0.001 | 0.0075 | 0.0063 | 0.0075 | Standard |
| G307 | UA | 257 | Lithium, total | mg/L | 08/16/2016 - 01/27/2021 | CI around geomean | 0.012 | 0.040 | 0.013 | 0.04 | Standard |
| G307 | UA | 257 | Mercury, total | mg/L | 08/16/2016 - 01/27/2021 | CI around median | 0.0002 | 0.002 | 0.0002 | 0.002 | Standard |
| G307 | UA | 257 | Molybdenum, total | mg/L | 08/16/2016 - 01/27/2021 | CI around geomean | 0.00125 | 0.10 | 0.0019 | 0.1 | Standard |
| G307 | UA | 257 | pH (field) | SU | 08/16/2016 - 01/27/2021 | CB around linear reg | 7.1 | 6.5/9.0 | 6.5/7.1 | 6.5/9 | Standard/Standard |
| G307 | UA | 257 | Radium-226 + Radium 228, tot | pCi/L | 08/16/2016 - 01/27/2021 | CI around mean | 0.45 | 5.0 | 1.9 | 5 | Standard |
| G307 | UA | 257 | Selenium, total | mg/L | 08/16/2016 - 01/27/2021 | CI around median | 0.001 | 0.050 | 0.0011 | 0.05 | Standard |
| G307 | UA | 257 | Sulfate, total | mg/L | 08/16/2016 - 01/27/2021 | Future median | 910 | 700 | 700 | 400 | Background |
| G307 | UA | 257 | Thallium, total | mg/L | 08/16/2016 - 01/27/2021 | All ND - Last | 0.001 | 0.002 | 0.001 | 0.002 | Standard |
| G307 | UA | 257 | Total Dissolved Solids | mg/L | 08/16/2016 - 01/27/2021 | CI around mean | 1350 | 1200 | 893 | 1200 | Standard |
| G307D | LCU | 845 | Antimony, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.003 | 0.006 | 0.003 | 0.006 | Standard |
| G307D | LCU | 845 | Arsenic, total | mg/L | 03/29/2021 - 07/27/2021 | CI around geomean | 0.00072 | 0.010 | 0.0043 | 0.01 | Standard |
| G307D | LCU | 845 | Barium, total | mg/L | 03/29/2021 - 07/27/2021 | CI around mean | 0.030 | 2.0 | 0.12 | 2 | Standard |
| G307D | LCU | 845 | Beryllium, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.004 | 0.001 | 0.004 | Standard |
| G307D | LCU | 845 | Boron, total | mg/L | 03/29/2021 - 07/27/2021 | Future median | 1.4 | 3.2 | 3.2 | 2 | Background |
| G307D | LCU | 845 | Cadmium,total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.005 | 0.001 | 0.005 | Standard |
| G307D | LCU | 845 | Chloride, total | mg/L | 03/29/2021 - 07/27/2021 | CI around mean | 17 | 200 | 120 | 200 | Standard |
| G307D | LCU | 845 | Chromium, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.004 | 0.10 | 0.011 | 0.1 | Standard |
| G307D | LCU | 845 | Cobalt, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.002 | 0.006 | 0.0056 | 0.006 | Standard |
| G307D | LCU | 845 | Fluoride, total | mg/L | 03/29/2021 - 07/27/2021 | CI around mean | 0.33 | 4.0 | 0.41 | 4 | Standard |



| Sample Location | HSU | Program | Constituent | Result Unit | Sample Date Range | Statistical Calculation | Statistical Result | GWPS | Background | Part 845 Standard | GWPS Source |
|-----------------|-----|---------|------------------------------|-------------|-------------------------|-------------------------|--------------------|---------|------------|-------------------|-------------------|
| G307D | LCU | 845 | Lead, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.0075 | 0.0063 | 0.0075 | Standard |
| G307D | LCU | 845 | Lithium, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.020 | 0.040 | 0.013 | 0.04 | Standard |
| G307D | LCU | 845 | Mercury, total | mg/L | 03/29/2021 - 07/27/2021 | CI around median | 0 | 0.002 | 0.0013 | 0.002 | Standard |
| G307D | LCU | 845 | Molybdenum, total | mg/L | 03/29/2021 - 07/27/2021 | CI around mean | 0.00823 | 0.10 | 0.0015 | 0.1 | Standard |
| G307D | LCU | 845 | pH (field) | SU | 03/29/2021 - 07/27/2021 | CI around mean | 7.2 | 6.5/9.0 | 6.6/7.3 | 6.5/9 | Standard/Standard |
| G307D | LCU | 845 | Radium-226 + Radium 228, tot | pCi/L | 03/29/2021 - 06/28/2021 | CI around mean | 0.032 | 5.0 | 1.6 | 5 | Standard |
| G307D | LCU | 845 | Selenium, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.050 | 0.0015 | 0.05 | Standard |
| G307D | LCU | 845 | Sulfate, total | mg/L | 03/29/2021 - 07/27/2021 | CI around mean | 765 | 400 | 367 | 400 | Standard |
| G307D | LCU | 845 | Thallium, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.002 | 0.001 | 0.002 | Standard |
| G307D | LCU | 845 | Total Dissolved Solids | mg/L | 03/29/2021 - 07/27/2021 | CI around mean | 1210 | 1200 | 1010 | 1200 | Standard |
| G308 | UA | 845 | Antimony, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.003 | 0.006 | 0.003 | 0.006 | Standard |
| G308 | UA | 845 | Arsenic, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.010 | 0.0043 | 0.01 | Standard |
| G308 | UA | 845 | Barium, total | mg/L | 03/29/2021 - 07/27/2021 | CI around mean | 0.021 | 2.0 | 0.12 | 2 | Standard |
| G308 | UA | 845 | Beryllium, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.004 | 0.001 | 0.004 | Standard |
| G308 | UA | 845 | Boron, total | mg/L | 03/29/2021 - 07/27/2021 | Future median | 2.6 | 3.2 | 3.2 | 2 | Background |
| G308 | UA | 845 | Cadmium,total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.005 | 0.001 | 0.005 | Standard |
| G308 | UA | 845 | Chloride, total | mg/L | 03/29/2021 - 07/27/2021 | CI around mean | 17 | 200 | 120 | 200 | Standard |
| G308 | UA | 845 | Chromium, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.004 | 0.10 | 0.011 | 0.1 | Standard |
| G308 | UA | 845 | Cobalt, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.002 | 0.006 | 0.0056 | 0.006 | Standard |
| G308 | UA | 845 | Fluoride, total | mg/L | 03/29/2021 - 07/27/2021 | CI around geomean | 0.48 | 4.0 | 0.41 | 4 | Standard |
| G308 | UA | 845 | Lead, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.0075 | 0.0063 | 0.0075 | Standard |
| G308 | UA | 845 | Lithium, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.020 | 0.040 | 0.013 | 0.04 | Standard |
| G308 | UA | 845 | Mercury, total | mg/L | 03/29/2021 - 07/27/2021 | CI around median | 0.0002 | 0.002 | 0.0013 | 0.002 | Standard |
| G308 | UA | 845 | Molybdenum, total | mg/L | 03/29/2021 - 07/27/2021 | CI around median | 0.0005 | 0.10 | 0.0015 | 0.1 | Standard |
| G308 | UA | 845 | pH (field) | SU | 03/29/2021 - 07/27/2021 | CI around mean | 7.2 | 6.5/9.0 | 6.6/7.3 | 6.5/9 | Standard/Standard |
| G308 | UA | 845 | Radium-226 + Radium 228, tot | pCi/L | 03/29/2021 - 07/14/2021 | CI around mean | -0.0615 | 5.0 | 1.6 | 5 | Standard |



| Sample Location | | Program | Constituent | Result Unit | Sample Date Range | Statistical Calculation | Statistical Result | GWPS | Background | Part 845 Standard | GWPS Source |
|-----------------|----|---------|------------------------------|-------------|-------------------------|-------------------------|--------------------|---------|------------|-------------------|-------------------|
| G308 | UA | 845 | Selenium, total | mg/L | 03/29/2021 - 07/27/2021 | CI around median | 0.001 | 0.050 | 0.0015 | 0.05 | Standard |
| G308 | UA | 845 | Sulfate, total | mg/L | 03/29/2021 - 07/27/2021 | CI around median | 1100 | 400 | 367 | 400 | Standard |
| G308 | UA | 845 | Thallium, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.002 | 0.001 | 0.002 | Standard |
| G308 | UA | 845 | Total Dissolved Solids | mg/L | 03/29/2021 - 07/27/2021 | CI around mean | 1820 | 1200 | 1010 | 1200 | Standard |
| G309 | UA | 845 | Antimony, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.003 | 0.006 | 0.003 | 0.006 | Standard |
| G309 | UA | 845 | Arsenic, total | mg/L | 03/29/2021 - 07/27/2021 | CI around median | 0.001 | 0.010 | 0.0043 | 0.01 | Standard |
| G309 | UA | 845 | Barium, total | mg/L | 03/29/2021 - 07/27/2021 | CI around median | 0.021 | 2.0 | 0.12 | 2 | Standard |
| G309 | UA | 845 | Beryllium, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.004 | 0.001 | 0.004 | Standard |
| G309 | UA | 845 | Boron, total | mg/L | 03/29/2021 - 07/27/2021 | Future median | 2.0 | 3.2 | 3.2 | 2 | Background |
| G309 | UA | 845 | Cadmium,total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.005 | 0.001 | 0.005 | Standard |
| G309 | UA | 845 | Chloride, total | mg/L | 03/29/2021 - 07/27/2021 | CI around mean | 18 | 200 | 120 | 200 | Standard |
| G309 | UA | 845 | Chromium, total | mg/L | 03/29/2021 - 07/27/2021 | CI around median | 0.004 | 0.10 | 0.011 | 0.1 | Standard |
| G309 | UA | 845 | Cobalt, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.002 | 0.006 | 0.0056 | 0.006 | Standard |
| G309 | UA | 845 | Fluoride, total | mg/L | 03/29/2021 - 07/27/2021 | CI around mean | 0.27 | 4.0 | 0.41 | 4 | Standard |
| G309 | UA | 845 | Lead, total | mg/L | 03/29/2021 - 07/27/2021 | CI around median | 0.001 | 0.0075 | 0.0063 | 0.0075 | Standard |
| G309 | UA | 845 | Lithium, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.020 | 0.040 | 0.013 | 0.04 | Standard |
| G309 | UA | 845 | Mercury, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.0002 | 0.002 | 0.0013 | 0.002 | Standard |
| G309 | UA | 845 | Molybdenum, total | mg/L | 03/29/2021 - 07/27/2021 | CB around linear reg | 0.000796 | 0.10 | 0.0015 | 0.1 | Standard |
| G309 | UA | 845 | pH (field) | SU | 03/29/2021 - 07/27/2021 | CB around linear reg | 7.3 | 6.5/9.0 | 6.6/7.3 | 6.5/9 | Standard/Standard |
| G309 | UA | 845 | Radium-226 + Radium 228, tot | pCi/L | 03/29/2021 - 07/13/2021 | CI around mean | -0.142 | 5.0 | 1.6 | 5 | Standard |
| G309 | UA | 845 | Selenium, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.050 | 0.0015 | 0.05 | Standard |
| G309 | UA | 845 | Sulfate, total | mg/L | 03/29/2021 - 07/27/2021 | CI around mean | 746 | 400 | 367 | 400 | Standard |
| G309 | UA | 845 | Thallium, total | mg/L | 03/29/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.002 | 0.001 | 0.002 | Standard |
| G309 | UA | 845 | Total Dissolved Solids | mg/L | 03/29/2021 - 07/27/2021 | CI around median | 1300 | 1200 | 1010 | 1200 | Standard |
| G310 | UA | 845 | Antimony, total | mg/L | 03/29/2021 - 07/28/2021 | All ND - Last | 0.003 | 0.006 | 0.003 | 0.006 | Standard |
| G310 | UA | 845 | Arsenic, total | mg/L | 03/29/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.010 | 0.0043 | 0.01 | Standard |



| Sample Location | HSU | Program | Constituent | Result Unit | Sample Date Range | Statistical Calculation | Statistical Result | GWPS | Background | Part 845 Standard | GWPS Source |
|-----------------|-----|---------|------------------------------|-------------|-------------------------|-------------------------|--------------------|---------|------------|-------------------|-------------------|
| G310 | UA | 845 | Barium, total | mg/L | 03/29/2021 - 07/28/2021 | CI around mean | 0.016 | 2.0 | 0.12 | 2 | Standard |
| G310 | UA | 845 | Beryllium, total | mg/L | 03/29/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.004 | 0.001 | 0.004 | Standard |
| G310 | UA | 845 | Boron, total | mg/L | 03/29/2021 - 07/28/2021 | Future median | 1.8 | 3.2 | 3.2 | 2 | Background |
| G310 | UA | 845 | Cadmium,total | mg/L | 03/29/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.005 | 0.001 | 0.005 | Standard |
| G310 | UA | 845 | Chloride, total | mg/L | 03/29/2021 - 07/28/2021 | CI around mean | 20 | 200 | 120 | 200 | Standard |
| G310 | UA | 845 | Chromium, total | mg/L | 03/29/2021 - 07/28/2021 | All ND - Last | 0.004 | 0.10 | 0.011 | 0.1 | Standard |
| G310 | UA | 845 | Cobalt, total | mg/L | 03/29/2021 - 07/28/2021 | All ND - Last | 0.002 | 0.006 | 0.0056 | 0.006 | Standard |
| G310 | UA | 845 | Fluoride, total | mg/L | 03/29/2021 - 07/28/2021 | CI around mean | 0.20 | 4.0 | 0.41 | 4 | Standard |
| G310 | UA | 845 | Lead, total | mg/L | 03/29/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.0075 | 0.0063 | 0.0075 | Standard |
| G310 | UA | 845 | Lithium, total | mg/L | 03/29/2021 - 07/28/2021 | All ND - Last | 0.020 | 0.040 | 0.013 | 0.04 | Standard |
| G310 | UA | 845 | Mercury, total | mg/L | 03/29/2021 - 07/28/2021 | All ND - Last | 0.0002 | 0.002 | 0.0013 | 0.002 | Standard |
| G310 | UA | 845 | Molybdenum, total | mg/L | 03/29/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.10 | 0.0015 | 0.1 | Standard |
| G310 | UA | 845 | pH (field) | SU | 03/29/2021 - 07/28/2021 | CI around mean | 7.1 | 6.5/9.0 | 6.6/7.3 | 6.5/9 | Standard/Standard |
| G310 | UA | 845 | Radium-226 + Radium 228, tot | pCi/L | 03/29/2021 - 07/13/2021 | CI around mean | -0.375 | 5.0 | 1.6 | 5 | Standard |
| G310 | UA | 845 | Selenium, total | mg/L | 03/29/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.050 | 0.0015 | 0.05 | Standard |
| G310 | UA | 845 | Sulfate, total | mg/L | 03/29/2021 - 07/28/2021 | CI around geomean | 550 | 400 | 367 | 400 | Standard |
| G310 | UA | 845 | Thallium, total | mg/L | 03/29/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.002 | 0.001 | 0.002 | Standard |
| G310 | UA | 845 | Total Dissolved Solids | mg/L | 03/29/2021 - 07/28/2021 | CI around mean | 1450 | 1200 | 1010 | 1200 | Standard |
| G311 | UA | 845 | Antimony, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.003 | 0.006 | 0.003 | 0.006 | Standard |
| G311 | UA | 845 | Arsenic, total | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 0.001 | 0.010 | 0.0043 | 0.01 | Standard |
| G311 | UA | 845 | Barium, total | mg/L | 03/30/2021 - 07/27/2021 | CI around mean | 0.026 | 2.0 | 0.12 | 2 | Standard |
| G311 | UA | 845 | Beryllium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.004 | 0.001 | 0.004 | Standard |
| G311 | UA | 845 | Boron, total | mg/L | 03/30/2021 - 07/27/2021 | Future median | 2.5 | 3.2 | 3.2 | 2 | Background |
| G311 | UA | 845 | Cadmium,total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.005 | 0.001 | 0.005 | Standard |
| G311 | UA | 845 | Chloride, total | mg/L | 03/30/2021 - 07/27/2021 | CI around geomean | 21 | 200 | 120 | 200 | Standard |
| G311 | UA | 845 | Chromium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.004 | 0.10 | 0.011 | 0.1 | Standard |



| Sample Location | HSU | Program | Constituent | Result Unit | Sample Date Range | Statistical Calculation | Statistical Result | GWPS | Background | Part 845 Standard | GWPS Source |
|-----------------|-----|---------|------------------------------|-------------|-------------------------|-------------------------|--------------------|---------|------------|-------------------|-------------------|
| G311 | UA | 845 | Cobalt, total | mg/L | 03/30/2021 - 07/27/2021 | CI around mean | 0.00269 | 0.006 | 0.0056 | 0.006 | Standard |
| G311 | UA | 845 | Fluoride, total | mg/L | 03/30/2021 - 07/27/2021 | CI around mean | 0.23 | 4.0 | 0.41 | 4 | Standard |
| G311 | UA | 845 | Lead, total | mg/L | 03/30/2021 - 07/27/2021 | Most recent sample | 0.001 | 0.0075 | 0.0063 | 0.0075 | Standard |
| G311 | UA | 845 | Lithium, total | mg/L | 03/30/2021 - 07/27/2021 | Most recent sample | 0.020 | 0.040 | 0.013 | 0.04 | Standard |
| G311 | UA | 845 | Mercury, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.0002 | 0.002 | 0.0013 | 0.002 | Standard |
| G311 | UA | 845 | Molybdenum, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.10 | 0.0015 | 0.1 | Standard |
| G311 | UA | 845 | pH (field) | SU | 03/30/2021 - 07/27/2021 | CI around mean | 6.8 | 6.5/9.0 | 6.6/7.3 | 6.5/9 | Standard/Standard |
| G311 | UA | 845 | Radium-226 + Radium 228, tot | pCi/L | 03/30/2021 - 07/14/2021 | CI around mean | -0.101 | 5.0 | 1.6 | 5 | Standard |
| G311 | UA | 845 | Selenium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.050 | 0.0015 | 0.05 | Standard |
| G311 | UA | 845 | Sulfate, total | mg/L | 03/30/2021 - 07/27/2021 | CI around mean | 773 | 400 | 367 | 400 | Standard |
| G311 | UA | 845 | Thallium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.002 | 0.001 | 0.002 | Standard |
| G311 | UA | 845 | Total Dissolved Solids | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 1500 | 1200 | 1010 | 1200 | Standard |
| G311D | LCU | 845 | Antimony, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.003 | 0.006 | 0.003 | 0.006 | Standard |
| G311D | LCU | 845 | Arsenic, total | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 0.000746 | 0.010 | 0.0043 | 0.01 | Standard |
| G311D | LCU | 845 | Barium, total | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 0.21 | 2.0 | 0.12 | 2 | Standard |
| G311D | LCU | 845 | Beryllium, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.004 | 0.001 | 0.004 | Standard |
| G311D | LCU | 845 | Boron, total | mg/L | 03/30/2021 - 07/28/2021 | Future median | 0.29 | 3.2 | 3.2 | 2 | Background |
| G311D | LCU | 845 | Cadmium,total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.005 | 0.001 | 0.005 | Standard |
| G311D | LCU | 845 | Chloride, total | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 0.37 | 200 | 120 | 200 | Standard |
| G311D | LCU | 845 | Chromium, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.004 | 0.10 | 0.011 | 0.1 | Standard |
| G311D | LCU | 845 | Cobalt, total | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 0.00191 | 0.006 | 0.0056 | 0.006 | Standard |
| G311D | LCU | 845 | Fluoride, total | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 0.35 | 4.0 | 0.41 | 4 | Standard |
| G311D | LCU | 845 | Lead, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.0075 | 0.0063 | 0.0075 | Standard |
| G311D | LCU | 845 | Lithium, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.020 | 0.040 | 0.013 | 0.04 | Standard |
| G311D | LCU | 845 | Mercury, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.0002 | 0.002 | 0.0013 | 0.002 | Standard |
| G311D | LCU | 845 | Molybdenum, total | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 0.00895 | 0.10 | 0.0015 | 0.1 | Standard |



| Sample Location | HSU | Program | Constituent | Result Unit | Sample Date Range | Statistical Calculation | Statistical Result | GWPS | Background | Part 845 Standard | GWPS Source |
|-----------------|-----|---------|------------------------------|-------------|-------------------------|--------------------------------|--------------------|---------|------------|-------------------|-------------------|
| G311D | LCU | 845 | pH (field) | SU | 03/30/2021 - 07/28/2021 | CI around mean | 7.0 | 6.5/9.0 | 6.6/7.3 | 6.5/9 | Standard/Standard |
| G311D | LCU | 845 | Radium-226 + Radium 228, tot | pCi/L | 03/30/2021 - 06/29/2021 | CI around mean | -0.153 | 5.0 | 1.6 | 5 | Standard |
| G311D | LCU | 845 | Selenium, total | mg/L | 03/30/2021 - 07/28/2021 | CI around median | 0 | 0.050 | 0.0015 | 0.05 | Standard |
| G311D | LCU | 845 | Sulfate, total | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 77 | 400 | 367 | 400 | Standard |
| G311D | LCU | 845 | Thallium, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.002 | 0.001 | 0.002 | Standard |
| G311D | LCU | 845 | Total Dissolved Solids | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 490 | 1200 | 1010 | 1200 | Standard |
| G312 | UA | 845 | Antimony, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.003 | 0.006 | 0.003 | 0.006 | Standard |
| G312 | UA | 845 | Arsenic, total | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 0.001 | 0.010 | 0.0043 | 0.01 | Standard |
| G312 | UA | 845 | Barium, total | mg/L | 03/30/2021 - 07/27/2021 | CI around mean | 0.023 | 2.0 | 0.12 | 2 | Standard |
| G312 | UA | 845 | Beryllium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.004 | 0.001 | 0.004 | Standard |
| G312 | UA | 845 | Boron, total | mg/L | 03/30/2021 - 07/27/2021 | Future median | 2.2 | 3.2 | 3.2 | 2 | Background |
| G312 | UA | 845 | Cadmium,total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.005 | 0.001 | 0.005 | Standard |
| G312 | UA | 845 | Chloride, total | mg/L | 03/30/2021 - 07/27/2021 | CI around mean | 21 | 200 | 120 | 200 | Standard |
| G312 | UA | 845 | Chromium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.004 | 0.10 | 0.011 | 0.1 | Standard |
| G312 | UA | 845 | Cobalt, total | mg/L | 03/30/2021 - 07/27/2021 | CI around mean | 0.00215 | 0.006 | 0.0056 | 0.006 | Standard |
| G312 | UA | 845 | Fluoride, total | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 0.25 | 4.0 | 0.41 | 4 | Standard |
| G312 | UA | 845 | Lead, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.0075 | 0.0063 | 0.0075 | Standard |
| G312 | UA | 845 | Lithium, total | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 0.020 | 0.040 | 0.013 | 0.04 | Standard |
| G312 | UA | 845 | Mercury, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.0002 | 0.002 | 0.0013 | 0.002 | Standard |
| G312 | UA | 845 | Molybdenum, total | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 0.001 | 0.10 | 0.0015 | 0.1 | Standard |
| G312 | UA | 845 | pH (field) | SU | 03/30/2021 - 07/27/2021 | CI around mean | 6.4 | 6.5/9.0 | 6.6/7.3 | 6.5/9 | Standard/Standard |
| G312 | UA | 845 | Radium-226 + Radium 228, tot | pCi/L | 03/30/2021 - 07/13/2021 | CI around mean | 0.062 | 5.0 | 1.6 | 5 | Standard |
| G312 | UA | 845 | Selenium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.050 | 0.0015 | 0.05 | Standard |
| G312 | UA | 845 | Sulfate, total | mg/L | 03/30/2021 - 07/27/2021 | CI around mean | 687 | 400 | 367 | 400 | Standard |
| G312 | UA | 845 | Thallium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.002 | 0.001 | 0.002 | Standard |
| G312 | UA | 845 | Total Dissolved Solids | mg/L | 03/30/2021 - 07/27/2021 | CB around linear reg | 1620 | 1200 | 1010 | 1200 | Standard |



| Sample Location | HSU | Program | Constituent | Result Unit | Sample Date Range | Statistical Calculation | Statistical Result | GWPS | Background | Part 845 Standard | GWPS Source |
|-----------------|-----|---------|------------------------------|-------------|-------------------------|-------------------------|--------------------|---------|------------|-------------------|-------------------|
| G313 | UA | 845 | Antimony, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.003 | 0.006 | 0.003 | 0.006 | Standard |
| G313 | UA | 845 | Arsenic, total | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 0.001 | 0.010 | 0.0043 | 0.01 | Standard |
| G313 | UA | 845 | Barium, total | mg/L | 03/30/2021 - 07/27/2021 | CB around linear reg | 0.017 | 2.0 | 0.12 | 2 | Standard |
| G313 | UA | 845 | Beryllium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.004 | 0.001 | 0.004 | Standard |
| G313 | UA | 845 | Boron, total | mg/L | 03/30/2021 - 07/27/2021 | Future median | 3.5 | 3.2 | 3.2 | 2 | Background |
| G313 | UA | 845 | Cadmium,total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.005 | 0.001 | 0.005 | Standard |
| G313 | UA | 845 | Chloride, total | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 23 | 200 | 120 | 200 | Standard |
| G313 | UA | 845 | Chromium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.004 | 0.10 | 0.011 | 0.1 | Standard |
| G313 | UA | 845 | Cobalt, total | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 0.002 | 0.006 | 0.0056 | 0.006 | Standard |
| G313 | UA | 845 | Fluoride, total | mg/L | 03/30/2021 - 07/27/2021 | CI around mean | 0.26 | 4.0 | 0.41 | 4 | Standard |
| G313 | UA | 845 | Lead, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.0075 | 0.0063 | 0.0075 | Standard |
| G313 | UA | 845 | Lithium, total | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 0.020 | 0.040 | 0.013 | 0.04 | Standard |
| G313 | UA | 845 | Mercury, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.0002 | 0.002 | 0.0013 | 0.002 | Standard |
| G313 | UA | 845 | Molybdenum, total | mg/L | 03/30/2021 - 07/27/2021 | CI around mean | 0.00113 | 0.10 | 0.0015 | 0.1 | Standard |
| G313 | UA | 845 | pH (field) | SU | 03/30/2021 - 07/27/2021 | CI around mean | 6.9 | 6.5/9.0 | 6.6/7.3 | 6.5/9 | Standard/Standard |
| G313 | UA | 845 | Radium-226 + Radium 228, tot | pCi/L | 03/30/2021 - 07/13/2021 | CI around mean | 0.16 | 5.0 | 1.6 | 5 | Standard |
| G313 | UA | 845 | Selenium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.050 | 0.0015 | 0.05 | Standard |
| G313 | UA | 845 | Sulfate, total | mg/L | 03/30/2021 - 07/27/2021 | CI around mean | 686 | 400 | 367 | 400 | Standard |
| G313 | UA | 845 | Thallium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.002 | 0.001 | 0.002 | Standard |
| G313 | UA | 845 | Total Dissolved Solids | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 1600 | 1200 | 1010 | 1200 | Standard |
| G314 | LCU | 845 | Antimony, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.003 | 0.006 | 0.003 | 0.006 | Standard |
| G314 | LCU | 845 | Arsenic, total | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 0.001 | 0.010 | 0.0043 | 0.01 | Standard |
| G314 | LCU | 845 | Barium, total | mg/L | 03/30/2021 - 07/27/2021 | CI around mean | 0.019 | 2.0 | 0.12 | 2 | Standard |
| G314 | LCU | 845 | Beryllium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.004 | 0.001 | 0.004 | Standard |
| G314 | LCU | 845 | Boron, total | mg/L | 03/30/2021 - 07/27/2021 | Future median | 0.14 | 3.2 | 3.2 | 2 | Background |
| G314 | LCU | 845 | Cadmium,total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.005 | 0.001 | 0.005 | Standard |



| Sample Location | | Program | Constituent | Result Unit | Sample Date Range | Statistical Calculation | Statistical Result | GWPS | Background | Part 845 Standard | GWPS Source |
|-----------------|-----|---------|------------------------------|-------------|-------------------------|-------------------------|--------------------|---------|------------|-------------------|-------------------|
| G314 | LCU | 845 | Chloride, total | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 30 | 200 | 120 | 200 | Standard |
| G314 | LCU | 845 | Chromium, total | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 0.004 | 0.10 | 0.011 | 0.1 | Standard |
| G314 | LCU | 845 | Cobalt, total | mg/L | 03/30/2021 - 07/27/2021 | CB around linear reg | 0.00959 | 0.006 | 0.0056 | 0.006 | Standard |
| G314 | LCU | 845 | Fluoride, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.25 | 4.0 | 0.41 | 4 | Standard |
| G314 | LCU | 845 | Lead, total | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 0.001 | 0.0075 | 0.0063 | 0.0075 | Standard |
| G314 | LCU | 845 | Lithium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.020 | 0.040 | 0.013 | 0.04 | Standard |
| G314 | LCU | 845 | Mercury, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.0002 | 0.002 | 0.0013 | 0.002 | Standard |
| G314 | LCU | 845 | Molybdenum, total | mg/L | 03/30/2021 - 07/27/2021 | CB around linear reg | 0.000545 | 0.10 | 0.0015 | 0.1 | Standard |
| G314 | LCU | 845 | pH (field) | SU | 03/30/2021 - 07/27/2021 | CI around median | 6.6 | 6.5/9.0 | 6.6/7.3 | 6.5/9 | Standard/Standard |
| G314 | LCU | 845 | Radium-226 + Radium 228, tot | pCi/L | 03/30/2021 - 07/13/2021 | CI around mean | 0.29 | 5.0 | 1.6 | 5 | Standard |
| G314 | LCU | 845 | Selenium, total | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 0.001 | 0.050 | 0.0015 | 0.05 | Standard |
| G314 | LCU | 845 | Sulfate, total | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 830 | 400 | 367 | 400 | Standard |
| G314 | LCU | 845 | Thallium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.002 | 0.001 | 0.002 | Standard |
| G314 | LCU | 845 | Total Dissolved Solids | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 1900 | 1200 | 1010 | 1200 | Standard |
| G314D | DA | 845 | Antimony, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.003 | 0.006 | 0.003 | 0.006 | Standard |
| G314D | DA | 845 | Arsenic, total | mg/L | 03/30/2021 - 07/28/2021 | CI around median | 0 | 0.010 | 0.0043 | 0.01 | Standard |
| G314D | DA | 845 | Barium, total | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 0.043 | 2.0 | 0.12 | 2 | Standard |
| G314D | DA | 845 | Beryllium, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.004 | 0.001 | 0.004 | Standard |
| G314D | DA | 845 | Boron, total | mg/L | 03/30/2021 - 07/28/2021 | Future median | 0.16 | 3.2 | 3.2 | 2 | Background |
| G314D | DA | 845 | Cadmium,total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.005 | 0.001 | 0.005 | Standard |
| G314D | DA | 845 | Chloride, total | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 53 | 200 | 120 | 200 | Standard |
| G314D | DA | 845 | Chromium, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.004 | 0.10 | 0.011 | 0.1 | Standard |
| G314D | DA | 845 | Cobalt, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.002 | 0.006 | 0.0056 | 0.006 | Standard |
| G314D | DA | 845 | Fluoride, total | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 0.48 | 4.0 | 0.41 | 4 | Standard |
| G314D | DA | 845 | Lead, total | mg/L | 03/30/2021 - 07/28/2021 | CI around median | 0 | 0.0075 | 0.0063 | 0.0075 | Standard |
| G314D | DA | 845 | Lithium, total | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 0.018 | 0.040 | 0.013 | 0.04 | Standard |



| Sample Location | HSU | Program | Constituent | Result Unit | Sample Date Range | Statistical Calculation | Statistical Result | GWPS | Background | Part 845 Standard | GWPS Source |
|-----------------|-----|---------|------------------------------|-------------|-------------------------|-------------------------|--------------------|---------|------------|-------------------|-------------------|
| G314D | DA | 845 | Mercury, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.0002 | 0.002 | 0.0013 | 0.002 | Standard |
| G314D | DA | 845 | Molybdenum, total | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 0.0073 | 0.10 | 0.0015 | 0.1 | Standard |
| G314D | DA | 845 | pH (field) | SU | 03/30/2021 - 07/28/2021 | CI around mean | 7.2 | 6.5/9.0 | 6.6/7.3 | 6.5/9 | Standard/Standard |
| G314D | DA | 845 | Radium-226 + Radium 228, tot | pCi/L | 03/30/2021 - 06/28/2021 | CI around mean | 1.1 | 5.0 | 1.6 | 5 | Standard |
| G314D | DA | 845 | Selenium, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.050 | 0.0015 | 0.05 | Standard |
| G314D | DA | 845 | Sulfate, total | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 464 | 400 | 367 | 400 | Standard |
| G314D | DA | 845 | Thallium, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.002 | 0.001 | 0.002 | Standard |
| G314D | DA | 845 | Total Dissolved Solids | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 1110 | 1200 | 1010 | 1200 | Standard |
| G315 | UA | 845 | Antimony, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.003 | 0.006 | 0.003 | 0.006 | Standard |
| G315 | UA | 845 | Arsenic, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.010 | 0.0043 | 0.01 | Standard |
| G315 | UA | 845 | Barium, total | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 0.023 | 2.0 | 0.12 | 2 | Standard |
| G315 | UA | 845 | Beryllium, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.004 | 0.001 | 0.004 | Standard |
| G315 | UA | 845 | Boron, total | mg/L | 03/30/2021 - 07/28/2021 | Future median | 1.3 | 3.2 | 3.2 | 2 | Background |
| G315 | UA | 845 | Cadmium,total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.005 | 0.001 | 0.005 | Standard |
| G315 | UA | 845 | Chloride, total | mg/L | 03/30/2021 - 07/28/2021 | CI around median | 1.9 | 200 | 120 | 200 | Standard |
| G315 | UA | 845 | Chromium, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.004 | 0.10 | 0.011 | 0.1 | Standard |
| G315 | UA | 845 | Cobalt, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.002 | 0.006 | 0.0056 | 0.006 | Standard |
| G315 | UA | 845 | Fluoride, total | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 0.25 | 4.0 | 0.41 | 4 | Standard |
| G315 | UA | 845 | Lead, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.0075 | 0.0063 | 0.0075 | Standard |
| G315 | UA | 845 | Lithium, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.020 | 0.040 | 0.013 | 0.04 | Standard |
| G315 | UA | 845 | Mercury, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.0002 | 0.002 | 0.0013 | 0.002 | Standard |
| G315 | UA | 845 | Molybdenum, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.10 | 0.0015 | 0.1 | Standard |
| G315 | UA | 845 | pH (field) | SU | 03/30/2021 - 07/28/2021 | CI around mean | 6.8 | 6.5/9.0 | 6.6/7.3 | 6.5/9 | Standard/Standard |
| G315 | UA | 845 | Radium-226 + Radium 228, tot | pCi/L | 03/30/2021 - 07/14/2021 | CI around mean | 0.00773 | 5.0 | 1.6 | 5 | Standard |
| G315 | UA | 845 | Selenium, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.050 | 0.0015 | 0.05 | Standard |
| G315 | UA | 845 | Sulfate, total | mg/L | 03/30/2021 - 07/28/2021 | CI around median | 850 | 400 | 367 | 400 | Standard |



| Sample Location | HSU | Program | Constituent | Result Unit | Sample Date Range | Statistical Calculation | Statistical Result | GWPS | Background | Part 845 Standard | GWPS Source |
|-----------------|-----|---------|------------------------------|-------------|-------------------------|-------------------------|--------------------|---------|------------|-------------------|-------------------|
| G315 | UA | 845 | Thallium, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.002 | 0.001 | 0.002 | Standard |
| G315 | UA | 845 | Total Dissolved Solids | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 1440 | 1200 | 1010 | 1200 | Standard |
| G316 | LCU | 845 | Antimony, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.003 | 0.006 | 0.003 | 0.006 | Standard |
| G316 | LCU | 845 | Arsenic, total | mg/L | 03/30/2021 - 07/27/2021 | CI around mean | 0.00669 | 0.010 | 0.0043 | 0.01 | Standard |
| G316 | LCU | 845 | Barium, total | mg/L | 03/30/2021 - 07/27/2021 | CI around mean | 0.060 | 2.0 | 0.12 | 2 | Standard |
| G316 | LCU | 845 | Beryllium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.004 | 0.001 | 0.004 | Standard |
| G316 | LCU | 845 | Boron, total | mg/L | 03/30/2021 - 07/27/2021 | Future median | 0.49 | 3.2 | 3.2 | 2 | Background |
| G316 | LCU | 845 | Cadmium,total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.005 | 0.001 | 0.005 | Standard |
| G316 | LCU | 845 | Chloride, total | mg/L | 03/30/2021 - 07/27/2021 | CI around geomean | 21 | 200 | 120 | 200 | Standard |
| G316 | LCU | 845 | Chromium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.004 | 0.10 | 0.011 | 0.1 | Standard |
| G316 | LCU | 845 | Cobalt, total | mg/L | 03/30/2021 - 07/27/2021 | CI around mean | 0.00298 | 0.006 | 0.0056 | 0.006 | Standard |
| G316 | LCU | 845 | Fluoride, total | mg/L | 03/30/2021 - 07/27/2021 | CI around mean | 0.24 | 4.0 | 0.41 | 4 | Standard |
| G316 | LCU | 845 | Lead, total | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 0.001 | 0.0075 | 0.0063 | 0.0075 | Standard |
| G316 | LCU | 845 | Lithium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.020 | 0.040 | 0.013 | 0.04 | Standard |
| G316 | LCU | 845 | Mercury, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.0002 | 0.002 | 0.0013 | 0.002 | Standard |
| G316 | LCU | 845 | Molybdenum, total | mg/L | 03/30/2021 - 07/27/2021 | CB around linear reg | 0.00407 | 0.10 | 0.0015 | 0.1 | Standard |
| G316 | LCU | 845 | pH (field) | SU | 03/30/2021 - 07/27/2021 | CI around mean | 7.0 | 6.5/9.0 | 6.6/7.3 | 6.5/9 | Standard/Standard |
| G316 | LCU | 845 | Radium-226 + Radium 228, tot | pCi/L | 03/30/2021 - 07/13/2021 | CI around geomean | 0.17 | 5.0 | 1.6 | 5 | Standard |
| G316 | LCU | 845 | Selenium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.050 | 0.0015 | 0.05 | Standard |
| G316 | LCU | 845 | Sulfate, total | mg/L | 03/30/2021 - 07/27/2021 | CB around T-S line | 237 | 400 | 367 | 400 | Standard |
| G316 | LCU | 845 | Thallium, total | mg/L | 03/30/2021 - 07/27/2021 | All ND - Last | 0.001 | 0.002 | 0.001 | 0.002 | Standard |
| G316 | LCU | 845 | Total Dissolved Solids | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 1100 | 1200 | 1010 | 1200 | Standard |
| G317 | UA | 845 | Antimony, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.003 | 0.006 | 0.003 | 0.006 | Standard |
| G317 | UA | 845 | Arsenic, total | mg/L | 03/30/2021 - 07/28/2021 | CI around median | 0.001 | 0.010 | 0.0043 | 0.01 | Standard |
| G317 | UA | 845 | Barium, total | mg/L | 03/30/2021 - 07/28/2021 | CB around linear reg | 0.00867 | 2.0 | 0.12 | 2 | Standard |
| G317 | UA | 845 | Beryllium, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.004 | 0.001 | 0.004 | Standard |



| Sample Location | HSU | Program | Constituent | Result Unit | Sample Date Range | Statistical Calculation | Statistical Result | GWPS | Background | Part 845 Standard | GWPS Source |
|-----------------|-----|---------|------------------------------|-------------|-------------------------|-------------------------|--------------------|---------|------------|-------------------|-------------------|
| G317 | UA | 845 | Boron, total | mg/L | 03/30/2021 - 07/28/2021 | Future median | 0.024 | 3.2 | 3.2 | 2 | Background |
| G317 | UA | 845 | Cadmium,total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.005 | 0.001 | 0.005 | Standard |
| G317 | UA | 845 | Chloride, total | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 8.4 | 200 | 120 | 200 | Standard |
| G317 | UA | 845 | Chromium, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.004 | 0.10 | 0.011 | 0.1 | Standard |
| G317 | UA | 845 | Cobalt, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.002 | 0.006 | 0.0056 | 0.006 | Standard |
| G317 | UA | 845 | Fluoride, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.25 | 4.0 | 0.41 | 4 | Standard |
| G317 | UA | 845 | Lead, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.0075 | 0.0063 | 0.0075 | Standard |
| G317 | UA | 845 | Lithium, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.020 | 0.040 | 0.013 | 0.04 | Standard |
| G317 | UA | 845 | Mercury, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.0002 | 0.002 | 0.0013 | 0.002 | Standard |
| G317 | UA | 845 | Molybdenum, total | mg/L | 03/30/2021 - 07/28/2021 | CB around linear reg | 0.00107 | 0.10 | 0.0015 | 0.1 | Standard |
| G317 | UA | 845 | pH (field) | SU | 03/30/2021 - 07/28/2021 | CI around mean | 6.5 | 6.5/9.0 | 6.6/7.3 | 6.5/9 | Standard/Standard |
| G317 | UA | 845 | Radium-226 + Radium 228, tot | pCi/L | 03/30/2021 - 07/13/2021 | CI around geomean | 0.79 | 5.0 | 1.6 | 5 | Standard |
| G317 | UA | 845 | Selenium, total | mg/L | 03/30/2021 - 07/28/2021 | CI around median | 0.001 | 0.050 | 0.0015 | 0.05 | Standard |
| G317 | UA | 845 | Sulfate, total | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 853 | 400 | 367 | 400 | Standard |
| G317 | UA | 845 | Thallium, total | mg/L | 03/30/2021 - 07/28/2021 | All ND - Last | 0.001 | 0.002 | 0.001 | 0.002 | Standard |
| G317 | UA | 845 | Total Dissolved Solids | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 1570 | 1200 | 1010 | 1200 | Standard |



HISTORY OF POTENTIAL EXCEEDANCES COFFEEN POWER PLANT ASH POND NO. 1 COFFEEN, ILLINOIS

Notes:

Potential exceedance of GWPS

HSU = hydrostratigraphic unit:

DA = deep aquifer

LCU = lower confining unit

UA = uppermost aquifer

Program = regulatory program data were collected under:

257 = 40 C.F.R. Part 257 Subpart D (Standards for the Disposal of Coal Combustion Residuals in Landfills and Surface Impoundments)

845 = 35 I.A.C. Part 845 (Sampling events completed to assess well locations for inclusion in the Part 845 monitoring well network)

mg/L = milligrams per liter

pCi/L = picocuries per liter

SU = standard units

Statistical Calculation = method used to calculate the statistical result:

All ND - Last = All results were below the reporting limit, and the last determined reporting limit is shown

CB around linear reg = Confidence band around linear regression

CB around T-S line = Confidence band around Thiel-Sen line

CI around geomean = Confidence interval around the geometric mean

CI around mean = Confidence interval around the mean

CI around median = Confidence interval around the median

Future median = Median of the three most recent samples

Most recent sample = Result for the most recently collected sample used due to insufficient data

Statistical Result = calculated in accordance with Statistical Analysis Plan using constituent concentrations observed at monitoring well during all sampling events within the specified date range

For pH, the values presented are the lower / upper limits

GWPS = Groundwater Protection Standard

GWPS Source:

Standard = standard specified in 35 I.A.C. § 845.600(a)(1)

Background = background concentration (see cover page for additional information)



TABLE 2. SUMMARY OF POTENTIAL EXCEEDANCES

| Sample Location | | Program | Constituent | Result Unit | Sample Date Range | Statistical Calculation | Statistical Result | GWPS | Background | Part 845 Standard | GWPS Source |
|-----------------|-----|---------|------------------------|-------------|-------------------------|-------------------------|--------------------|---------|------------|-------------------|-------------------|
| G301 | UA | 257 | Sulfate, total | mg/L | 11/20/2015 - 01/27/2021 | Future median | 750 | 700 | 700 | 400 | Background |
| G303 | UA | 257 | Sulfate, total | mg/L | 11/20/2015 - 01/26/2021 | Future median | 730 | 700 | 700 | 400 | Background |
| G303 | UA | 257 | Total Dissolved Solids | mg/L | 11/20/2015 - 01/26/2021 | CI around mean | 1460 | 1200 | 893 | 1200 | Standard |
| G304 | UA | 257 | Sulfate, total | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 1000 | 700 | 700 | 400 | Background |
| G304 | UA | 257 | Total Dissolved Solids | mg/L | 11/20/2015 - 05/20/2016 | Most recent sample | 1300 | 1200 | 893 | 1200 | Standard |
| G305 | UA | 257 | Sulfate, total | mg/L | 05/19/2016 - 11/17/2016 | Future median | 890 | 700 | 700 | 400 | Background |
| G305 | UA | 257 | Total Dissolved Solids | mg/L | 05/19/2016 - 11/17/2016 | CI around mean | 1280 | 1200 | 893 | 1200 | Standard |
| G307 | UA | 257 | Sulfate, total | mg/L | 08/16/2016 - 01/27/2021 | Future median | 910 | 700 | 700 | 400 | Background |
| G307 | UA | 257 | Total Dissolved Solids | mg/L | 08/16/2016 - 01/27/2021 | CI around mean | 1350 | 1200 | 893 | 1200 | Standard |
| G307D | LCU | 845 | Sulfate, total | mg/L | 03/29/2021 - 07/27/2021 | CI around mean | 765 | 400 | 367 | 400 | Standard |
| G307D | LCU | 845 | Total Dissolved Solids | mg/L | 03/29/2021 - 07/27/2021 | CI around mean | 1210 | 1200 | 1010 | 1200 | Standard |
| G308 | UA | 845 | Sulfate, total | mg/L | 03/29/2021 - 07/27/2021 | CI around median | 1100 | 400 | 367 | 400 | Standard |
| G308 | UA | 845 | Total Dissolved Solids | mg/L | 03/29/2021 - 07/27/2021 | CI around mean | 1820 | 1200 | 1010 | 1200 | Standard |
| G309 | UA | 845 | Sulfate, total | mg/L | 03/29/2021 - 07/27/2021 | CI around mean | 746 | 400 | 367 | 400 | Standard |
| G309 | UA | 845 | Total Dissolved Solids | mg/L | 03/29/2021 - 07/27/2021 | CI around median | 1300 | 1200 | 1010 | 1200 | Standard |
| G310 | UA | 845 | Sulfate, total | mg/L | 03/29/2021 - 07/28/2021 | CI around geomean | 550 | 400 | 367 | 400 | Standard |
| G310 | UA | 845 | Total Dissolved Solids | mg/L | 03/29/2021 - 07/28/2021 | CI around mean | 1450 | 1200 | 1010 | 1200 | Standard |
| G311 | UA | 845 | Sulfate, total | mg/L | 03/30/2021 - 07/27/2021 | CI around mean | 773 | 400 | 367 | 400 | Standard |
| G311 | UA | 845 | Total Dissolved Solids | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 1500 | 1200 | 1010 | 1200 | Standard |
| G312 | UA | 845 | pH (field) | SU | 03/30/2021 - 07/27/2021 | CI around mean | 6.4 | 6.5/9.0 | 6.6/7.3 | 6.5/9 | Standard/Standard |
| G312 | UA | 845 | Sulfate, total | mg/L | 03/30/2021 - 07/27/2021 | CI around mean | 687 | 400 | 367 | 400 | Standard |
| G312 | UA | 845 | Total Dissolved Solids | mg/L | 03/30/2021 - 07/27/2021 | CB around linear reg | 1620 | 1200 | 1010 | 1200 | Standard |
| G313 | UA | 845 | Boron, total | mg/L | 03/30/2021 - 07/27/2021 | Future median | 3.5 | 3.2 | 3.2 | 2 | Background |
| G313 | UA | 845 | Sulfate, total | mg/L | 03/30/2021 - 07/27/2021 | CI around mean | 686 | 400 | 367 | 400 | Standard |
| G313 | UA | 845 | Total Dissolved Solids | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 1600 | 1200 | 1010 | 1200 | Standard |
| G314 | LCU | 845 | Cobalt, total | mg/L | 03/30/2021 - 07/27/2021 | CB around linear reg | 0.00959 | 0.006 | 0.0056 | 0.006 | Standard |



TABLE 2. SUMMARY OF POTENTIAL EXCEEDANCES

HISTORY OF POTENTIAL EXCEEDANCES COFFEEN POWER PLANT ASH POND NO. 1

COFFEEN, ILLINOIS

| Sample Location | HSU | Program | Constituent | Result Unit | Sample Date Range | Statistical Calculation | Statistical Result | GWPS | Background | Part 845 Standard | GWPS Source |
|-----------------|-----|---------|------------------------|-------------|-------------------------|-------------------------|--------------------|------|------------|-------------------|-------------|
| G314 | LCU | 845 | Sulfate, total | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 830 | 400 | 367 | 400 | Standard |
| G314 | LCU | 845 | Total Dissolved Solids | mg/L | 03/30/2021 - 07/27/2021 | CI around median | 1900 | 1200 | 1010 | 1200 | Standard |
| G314D | DA | 845 | Sulfate, total | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 464 | 400 | 367 | 400 | Standard |
| G315 | UA | 845 | Sulfate, total | mg/L | 03/30/2021 - 07/28/2021 | CI around median | 850 | 400 | 367 | 400 | Standard |
| G315 | UA | 845 | Total Dissolved Solids | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 1440 | 1200 | 1010 | 1200 | Standard |
| G317 | UA | 845 | Sulfate, total | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 853 | 400 | 367 | 400 | Standard |
| G317 | UA | 845 | Total Dissolved Solids | mg/L | 03/30/2021 - 07/28/2021 | CI around mean | 1570 | 1200 | 1010 | 1200 | Standard |

Notes:

HSU = hydrostratigraphic unit:

DA = deep aquifer

LCU = lower confining unit

UA = uppermost aquifer

Program = regulatory program data were collected under:

257 = 40 C.F.R. Part 257 Subpart D (Standards for the Disposal of Coal Combustion Residuals in Landfills and Surface Impoundments)

845 = 35 I.A.C. Part 845 (Sampling events completed to assess well locations for inclusion in the Part 845 monitoring well network)

mg/L = milligrams per liter

pCi/L = picocuries per liter

SU = standard units

Statistical Calculation = method used to calculate the statistical result:

CB around linear reg = Confidence band around linear regression

CI around geomean = Confidence interval around the geometric mean

CI around mean = Confidence interval around the mean

CI around median = Confidence interval around the median

Future median = Median of the three most recent samples

Most recent sample = Result for the most recently collected sample used due to insufficient data

Statistical Result = calculated in accordance with Statistical Analysis Plan using constituent concentrations observed at monitoring well during all sampling events within the specified date range

For pH, the values presented are the lower / upper limits GWPS = Groundwater Protection Standard

GWPS Source:

Standard = standard specified in 35 I.A.C. § 845.600(a)(1)

Background = background concentration (see cover page for additional information)



ATTACHMENT N

Certification of Financial Assurance Requirements

On June 17, 2021, Illinois Power Generating Company provided financial assurance in the form of performance bonds to the Illinois Environmental Protection Agency in the amount of \$27,884,983 for Ash Pond 1, Ash Pond 2, and the GMF Pond System at the Coffeen Power Plant.¹

I, Matthew A. Goering, Senior Vice President of Illinois Power Generating Company, do hereby certify to the best of my knowledge for the above referenced CCR Units that the financial assurance instruments satisfy the requirements of 35 I.A.C. Part 845, Subpart I.

Matthew A. Goering

Senior Vice President

Illinois Power Generating Company

¹In the operating permit applications, the GMF Pond System is referred to as the GMF Gypsum Stack Pond and GMF Recycle Pond.

ATTACHMENT O



Stantec Consulting Services Inc. 1859 Bowles Avenue Suite 250, Fenton MO 63026-1944

October 12, 2016

File: let_020_175666013_certification

Revision 0

Initial Hazard Potential Classification Assessment EPA Final CCR Rule Ash Pond No. 1 Coffeen Power Station Montgomery County, Illinois

1.0 PURPOSE

This report documents Stantec's certification of the initial hazard potential classification assessment for the Coffeen Power Station Ash Pond No. 1.

40 CFR 257.73(a)(2) requires the owner or operator of an existing CCR surface impoundment to conduct an initial hazard potential classification assessment and document the hazard potential classification, and the basis for the classification, of the CCR unit as either a high hazard potential CCR surface impoundment, a significant hazard potential CCR surface impoundment, or a low hazard potential CCR surface impoundment.

2.0 FINDINGS

A breach analysis was performed to evaluate potential hazards associated with a failure of Ash Pond No. 1's perimeter containment dike. Breach failure scenarios were modeled near the northwest and northeast corners of the containment dike. The breach from the northwest corner was modeled to discharge west towards the Coffeen Power Station facilities (parking lot, buildings, stacks, etc.) and the northeast corner breach was modeled to discharge eastward into the eastern cove of Coffeen Lake. Breach scenarios were simulated using water volumes corresponding to the maximum water surface elevation calculated within Ash Pond No. 1 during the Probable Maximum Precipitation (PMP) storm event.

Model results from the breach analyses indicate that the northeast breach will be contained within the eastern cove of Coffeen Lake, while a westward breach from the northwest corner will inundate portions of the Coffeen Power Station property and may cause damages to onsite equipment and infrastructure. However, the resultant maximum flood depths and velocities at locations of regularly occupied structures/areas do not indicate concern for loss of human life. Per these findings, it was concluded that a breach failure of the Ash Pond No. 1 containment dike will result in no probable loss of human life. However, it is anticipated that a breach failure of the containment dike will result in the release of the stored CCR materials into Coffeen Lake and cause environmental damage.

40 CFR 257.53 defines a "significant hazard potential CCR surface impoundment" as a diked surface impoundment where failure or mis-operation results in no probable loss of human life, but



Page 2 of 2

can cause economic loss, environmental damage, disruption of lifeline facilities, or impact other concerns.

Based on the results of the analysis summarized above, Ash Pond No. 1 was assigned a Significant hazard potential classification per 40 CFR 257.53.

3.0 QUALIFIED PROFESSIONAL ENGINEER CERTIFICATION

- I, Matthew Hoy, being a Professional Engineer in good standing in the State of Illinois, do hereby certify, to the best of my knowledge, information, and belief that;
 - the information contained in this report and the underlying data in the operating record
 was prepared in accordance with the accepted practice of engineering and is accurate
 as of the date of my signature below; and
 - 2. the initial hazard potential classification assessment for Coffeen Power Station Ash Pond No. 1 was conducted in accordance with the requirements specified in 40 CFR 257.73.

SIGNATURE

ADDRESS:

Stantec Consulting Services Inc.

1859 Bowles Avenue Suite 250

Fenton MO 63026-1944

TELEPHONE:

(636) 343-3880



DATE 10/12/2016

Design with community in mind

ATTACHMENT P



Submitted to Illinois Power Generating Company 134 Cips Lane Coffeen, IL 62017 Submitted by AECOM 1001 Highlands Plaza Drive West Suite 300 St. Louis, MO 63110

October 2016

CCR Rule Report: Initial Structural Stability Assessment

For

Ash Pond No. 1

At Coffeen Power Station

1 Introduction

This Coal Combustion Residual (CCR) Rule Report documents that Ash Pond No. 1 at the Illinois Power Generating Company Coffeen Power Station meets the structural stability assessment requirements specified in 40 Code of Federal Regulations (CFR) §257.73(d), except as noted herein. Ash Pond No. 1 is located near Coffeen, Illinois in Montgomery County, approximately 0.3 miles east of the Coffeen Power Station. Ash Pond No. 1 serves as the primary wet impoundment basin for bottom ash produced by the Coffeen Power Station.

Ash Pond No. 1 is an existing CCR surface impoundment as defined by 40 CFR §257.53. The CCR Rule requires that an initial structural stability assessment for an existing CCR surface impoundment be completed by October 17, 2016. In general, the initial structural stability assessment must document that the design, construction, operation, and maintenance of the CCR unit is consistent with recognized and generally accepted good engineering practices.

The owner or operator of the CCR unit must obtain a certification from a qualified professional engineer stating that the initial structural stability assessment was conducted in accordance with the requirements of 40 CFR §257.73(d). The owner or operator must prepare a periodic structural stability assessment every five years.

2 Initial Structural Stability Assessment

40 CFR §257.73(d)(1)

The owner or operator of the CCR unit must conduct initial and periodic structural stability assessments and document whether the design, construction, operation, and maintenance of the CCR unit is consistent with recognized and generally accepted good engineering practices for the maximum volume of CCR and CCR wastewater which can be impounded therein. The assessment must, at a minimum, document whether the CCR unit has been designed, constructed, operated, and maintained with [the standards in (d)(1)(i)-(vii)].

An initial structural stability assessment has been performed to document that the design, construction, operation and maintenance of Ash Pond No. 1 is consistent with recognized and generally accepted good engineering practices. The results of the structural stability assessment are discussed in the following sections. Based on the assessment and its results, the design, construction, operation, and maintenance of Ash Pond No. 1 were found to be consistent with recognized and generally accepted good engineering practices, and meets the standards in 257.73(d)(1)(i)-(vii), except as noted herein.

2.1 Foundations and Abutments (§257.73(d)(1)(i))

CCR unit designed, constructed, operated, and maintained with stable foundations and abutments.

The stability of the foundations was evaluated using soil data from field investigations and reviewing design drawings, operational and maintenance procedures, and conditions observed in the field by AECOM. Additionally, slope stability analyses were performed to evaluate slip surfaces passing through the foundations. Ash Pond No. 1 is a ring dike structure and does not have abutments.

The foundation consists of medium stiff to stiff soil, overlying very soft soil, which in turn overlies very stiff to hard glacial till. Slope stability analyses exceed the criteria listed in §257.73(e)(1)(i) through (iii) for slip surfaces passing through the foundation. The slope stability analyses are discussed in the *CCR Rule Report: Initial Safety Factor Assessment for Ash Pond No. 1 at Coffeen Power Station* (October 2016). Additional slope stability analyses were performed to evaluate the effects of cyclic softening in the foundation, and were found to satisfy the criteria listed in §257.73(e)(1)(iv) applicable to dikes. A review of operational and maintenance procedures as well as current and past performance of the dikes has determined appropriate processes are in place for continued operational performance.

Based on the conditions observed by AECOM, Ash Pond No. 1 was designed and constructed with stable foundations. Operational and maintenance procedures are in place to address any issues related to the stability of foundations. Therefore, Ash Pond No. 1 meets the requirements in §257.73(d)(1)(i).

2.2 Slope Protection (§257.73(d)(1)(ii))

CCR unit designed, constructed, operated, and maintained with adequate slope protection to protect against surface erosion, wave action and adverse effects of sudden drawdown.

The adequacy of slope protection was evaluated by reviewing design drawings, operational and maintenance procedures, and conditions observed in the field by AECOM.

Based on this evaluation, adequate slope protection was designed and constructed at Ash Pond No. 1. No evidence of significant areas of erosion or wave action was observed. The interior slopes are protected with vegetation and stacked bottom ash, and the exterior slopes are protected with vegetation. Operational and

maintenance procedures to repair the vegetation and stacked bottom ash as needed are appropriate to protect against surface erosion or wave action. Sudden drawdown of the pool in Ash Pond No. 1 is not expected to occur due to operational controls associated with lowering the pool level. Therefore, slope protection to protect against the adverse effects of sudden drawdown is not required as sudden drawdown conditions are not expected to occur. Therefore, Ash Pond No. 1 meets the requirements in §257.73(d)(1)(ii).

2.3 Dike Compaction (§257.73(d)(1)(iii))

CCR unit designed, constructed, operated, and maintained with dikes mechanically compacted to a density sufficient to withstand the range of loading conditions in the CCR unit.

The density of the dike materials was evaluated using soil data from field investigations and reviewing design drawings, operational and maintenance procedures, and conditions observed in the field by AECOM. Additionally, slope stability analyses were performed to evaluate slip surfaces passing through the dike over the range of expected loading conditions as defined within §257.73(e)(1).

Based on this evaluation, the dike consists of medium stiff to stiff material, which is indicative of mechanically compacted dikes. As discussed in the *CCR Rule Report: Initial Safety Factor Assessment for Ash Pond No. 1 at Coffeen Power Station* (October 2016), slope stability analyses exceed the criteria listed in §257.73(e)(1) for slip surfaces passing through the dike. Therefore, the original design and construction of Ash Pond No. 1 included sufficient dike compaction. Operational and maintenance procedures are in place to identify and mitigate deficiencies in order to maintain sufficient compaction of the dikes to withstand the range of loading conditions. Therefore, Ash Pond No. 1 meets the requirements in §257.73(d)(1)(iii).

2.4 Vegetated Slopes (§257.73(d)(1)(iv))¹

CCR unit designed, constructed, operated, and maintained with vegetated slopes of dikes and surrounding areas, except for slopes which have an alternate form or forms of slope protection.

The adequacy of slope vegetation was evaluated by reviewing design drawings, operational and maintenance procedures, and conditions observed in the field by AECOM.

Based on this evaluation, the vegetation on the exterior and interior slopes is adequate as no substantial bare or overgrown areas were observed. Stacked bottom ash is present on some portions of the interior slopes and is used as an alternate form of slope protection, which is adequate as significant areas of erosion were not observed. Therefore, the original design and construction of Ash Pond No. 1 included adequate vegetation of the dikes and surrounding areas. Adequate operational and maintenance procedures are in place to regularly manage vegetation growth, including mowing and seeding any bare areas, as evidenced by the conditions observed by AECOM. Therefore, Ash Pond No. 1 meets the requirements in §257.73(d)(1)(iv).

As modified by court order issued June 14, 2016, Utility Solid Waste Activities Group v. EPA, D.C. Cir. No. 15-1219 (order granting remand and vacatur of specific regulatory provisions).

2.5 Spillways (§257.73(d)(1)(v))

CCR unit designed, constructed, operated, and maintained with a single spillway or a combination of spillways configured as specified in [paragraph (A) and (B)]:

- (A) All spillways must be either:
 - (1) of non-erodible construction and designed to carry sustained flows; or
 - (2) earth- or grass-lined and designed to carry short-term, infrequent flows at non-erosive velocities where sustained flows are not expected.
- (B) The combined capacity of all spillways must adequately manage flow during and following the peak discharge from a:
 - (1) Probable maximum flood (PMF) for a high hazard potential CCR surface impoundment; or
 - (2) 1000-year flood for a significant hazard potential CCR surface impoundment; or
 - (3) 100-year flood for a low hazard potential CCR surface impoundment.

The spillway was evaluated using design drawings, operational and maintenance procedures, and conditions observed in the field by AECOM. Additionally, hydrologic and hydraulic analyses were completed to evaluate the capacity of the spillway relative to inflow estimated for the 1,000-year flood event for the significant hazard potential Ash Pond No. 1. The hazard potential classification assessment was performed by Stantec in 2016 in accordance with §257.73(a)(2).

The spillway is comprised of a concrete riser structure, a steel primary outflow pipe, and corrugated metal and steel overflow pipe, which are non-erodible materials designed to carry sustained flows. The capacity of the spillway was evaluated using hydrologic and hydraulic analysis performed per §257.82(a). The analysis found that the spillway can adequately manage flow during peak discharge resulting from the 1,000-year storm event without overtopping of the embankments. The hydrologic and hydraulic analyses are discussed in the *CCR Rule Report: Initial Inflow Design Flood Control System Plan for Ash Pond No. 1 at Coffeen Power Station* (October 2016). Operational and maintenance procedures are in place to repair any issues with the spillway and remove debris or other obstructions from the spillway, as evidenced by the conditions observed by AECOM. As a result, these procedures are appropriate for maintaining the spillway. Therefore, Ash Pond No. 1 meets the requirements in §257.73(d)(1)(v).

2.6 Stability and Structural Integrity of Hydraulic Structures (§257.73(d)(1)(vi))

CCR unit designed, constructed, operated, and maintained with hydraulic structures underlying the base of the CCR unit or passing through the dike of the CCR unit that maintain structural integrity and are free of significant deterioration, deformation, distortion, bedding deficiencies, sedimentation, and debris which may negatively affect the operation of the hydraulic structure.

Two hydraulic structures pass through the dike at Ash Pond No. 1: the steel recycle intake pipe, which acts as the primary outflow pipe for Ash Pond No. 1, and a corrugated metal and steel secondary overflow pipe. The stability and structural integrity of the pipes was evaluated using design drawings, operational and maintenance procedures, inspections, and conditions observed in the field by AECOM. No other hydraulic structures are known to pass through the dike or underlie the base of Ash Pond 1.

The evaluation of design drawings, operational and maintenance procedures, and conditions observed in the field did not identify any issues with the steel recycle intake pipe. However, the evaluation of the stability and structural integrity of the steel recycle intake pipe has not been fully completed because high pipe flows, required for operation of the Coffeen Power Station, precluded closed circuit television (CCTV) inspection.

The CCTV pipe inspection of the corrugated metal and steel secondary overflow pipe covered the complete length of the pipe and found the pipe to be free of significant deterioration, deformation, distortion, bedding deficiencies, sedimentation, and debris that may negatively affect the operation of the hydraulic structure. Evaluation of design drawings and operational and maintenance procedures for this pipe also did not identify any issues.

Based on this evaluation, all Ash Pond No. 1 hydraulic structures cannot be certified to meet the requirements of §257.73(d)(1)(iv) because a CCTV inspection of the steel recycle intake pipe has not yet been performed, thus, precluding completion of the evaluation of the stability and structural integrity of that pipe. In accordance with §257.73(d)(2), AECOM recommends that a CCTV pipe inspection of the steel recycle intake pipe be completed as soon as feasible and that this assessment be updated once the inspection is completed.

2.7 Downstream Slope Inundation/Stability (§257.73(d)(1)(vii))

CCR unit designed, constructed, operated, and maintained with, for CCR units with downstream slopes which can be inundated by the pool of an adjacent water body, such as a river, stream or lake, downstream slopes that maintain structural stability during low pool of the adjacent water body or sudden drawdown of the adjacent water body.

The structural stability of the downstream slopes of Ash Pond No. 1 was evaluated by comparing the location of Ash Pond No. 1 relative to adjacent water bodies using published Federal Emergency Management Agency (FEMA) Flood Insurance Rate Maps (FIRM), aerial imagery, and conditions observed in the field by AECOM.

The nearest downstream water bodies are Coffeen Lake and the Coffeen Station's process water flume. However, as shown on the FEMA FIRM for the area, the 100-year flood zone for Coffeen Lake is beyond the downstream slopes of Ash Pond No. 1. The process water flume only has water to a depth of approximately 3 ft, and a drawdown of this magnitude is not expected to affect the structural stability of the Ash Pond No. 1 downstream slopes. Additionally, a steel sheet pile wall separates the pool in the process water flume from the Ash Pond No. 1 downstream slopes.

Based on this evaluation, the requirements in §257.73(d)(1)(vii) are not applicable to Ash Pond No. 1, as inundation of the downstream slopes by a water body such as a river, stream, or lake is not expected to occur, and the depth of water in the process flume is shallow enough that drawdown would not be expected to affect the structural stability of the downstream slopes.

3 Certification Statement

CCR Unit: Illinois Power Generating Company; Coffeen Power Station; Ash Pond No. 1

A MODER JR.

I, Victor A. Modeer, being a Registered Professional Engineer in good standing in the State of Illinois, do hereby certify, to the best of my knowledge, information, and belief that the information contained in this CCR Rule Report, and the underlying data in the operating record, has been prepared in accordance with the accepted practice of engineering. I certify, for the above-referenced CCR Unit, that the initial structural stability assessment dated October 2, 2016 was conducted in accordance with the requirements of 40 CFR § 257.73(d).

Printed Name

Date

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AECOM (NYSE: ACM) is a global provider of professional technical and management support services to a broad range of markets, including transportation, facilities, environmental, energy, water and government. With nearly 100,000 employees around the world, AECOM is a leader in all of the key markets that it serves. AECOM provides a blend of global reach, local knowledge, innovation, and collaborative technical excellence in delivering solutions that enhance and sustain the world's built, natural, and social environments. A Fortune 500 company, AECOM serves clients in more than 100 countries and has annual revenue in excess of \$19 billion.

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ATTACHMENT Q



Submitted to Illinois Power Generating Company 134 Cips Lane Coffeen, IL 62017 Submitted by AECOM 1001 Highlands Plaza Drive West Suite 300 St. Louis, MO 63110

October 2016

CCR Rule Report: Initial Safety Factor Assessment

For

Ash Pond No. 1

At Coffeen Power Station

1 Introduction

This Coal Combustion Residual (CCR) Rule Report documents that Ash Pond No. 1 at the Illinois Power Generating Company Coffeen Power Station meets the safety factor assessment requirements specified in 40 Code of Federal Regulations (CFR) §257.73(e). Ash Pond No. 1 is located near Coffeen, Illinois in Montgomery County, approximately 0.3 miles east of the Coffeen Power Station. Ash Pond No. 1 serves as the primary wet impoundment basin for bottom ash produced by the Coffeen Power Station.

Ash Pond No. 1 is an existing CCR surface impoundment as defined by 40 CFR §257.53. The CCR Rule requires that the initial safety factor assessment for an existing CCR surface impoundment be completed by October 17, 2016.

The owner or operator of the CCR unit must obtain a certification from a qualified professional engineer stating that the initial safety factor assessment meets the requirements of 40 CFR § 257.73(e). The owner or operator must prepare a safety factor assessment every five years.

2 Initial Safety Factor Assessment

40 CFR §257.73(e)(1)

The owner or operator must conduct initial and periodic safety factor assessments for each CCR unit and document whether the calculated factors of safety for each CCR unit achieve the minimum safety factors specified in (e)(1)(i) through (iv) of this section for the critical cross section of the embankment. The critical cross section is the cross section anticipated to be the most susceptible of all cross sections to structural failure based on appropriate engineering considerations, including loading conditions. The safety factor assessments must be supported by appropriate engineering calculations.

- (i) The calculated static factor of safety under the long-term, maximum storage pool loading condition must equal or exceed 1.50.
- (ii) The calculated static factor of safety under the maximum surcharge pool loading condition must equal or exceed 1.40.
- (iii) The calculated seismic factor of safety must equal or exceed 1.00.
- (iv) For dikes constructed of soils that have susceptibility to liquefaction, the calculated liquefaction factor of safety must equal or exceed 1.20.

A geotechnical investigation program and stability analyses were performed to evaluate the design, performance, and condition of the earthen dikes of Ash Pond No. 1. The exploration consisted of hollow-stem auger borings, cone penetration tests, piezometers, and laboratory program including strength, hydraulic conductivity, consolidation, and index testing. Data collected from the geotechnical investigation, available design drawings, construction records, inspection reports, previous engineering investigations, and other pertinent historic documents were utilized to perform the safety factor assessment and geotechnical analyses.

In general, the subsurface conditions at Ash Pond No. 1 consist of medium stiff to stiff lean clay embankment fill, overlying medium stiff to stiff weathered loess clay, overlying a thin zone of very soft clay, which in turn overlies very stiff to hard glacial till. The phreatic surface within the subsurface is typically at the ground surface at the toe of the embankment and near the embankment/foundation interface beneath the crest.

Five (5) representative cross sections were analyzed using limit equilibrium slope stability analysis software to evaluate stability of the perimeter dike system and foundations. The cross sections were located to represent critical surface geometry, subsurface stratigraphy, and phreatic conditions across the site. Each cross section was evaluated for each of the loading conditions stipulated in §257.73(e)(1).

The Soils Susceptible to Liquefaction loading condition, §257.73(e)(1)(iv), was not evaluated because a liquefaction susceptibly evaluation did not find soils susceptible to liquefaction within the Ash Pond No. 1 dikes. As a result, this loading condition is not applicable to Ash Pond No. 1.

Results of the Initial Safety Factor Assessments, for the critical cross-section for each loading condition, are listed in **Table 1** (i.e., the table identifies the lowest calculated factor of safety for any one of the five analyzed cross sections for each loading condition).

§257.73(e)(1) Minimum Factor of Calculated Factor of **Loading Conditions** Subsection Safety Safety Maximum Storage Pool Loading (i) 1.50 1.50 (ii) Maximum Surcharge Pool Loading 1.40 1.49 1.00 1.03 Seismic (iii) 1.20 Soils Susceptible to Liquefaction (iv) Not Applicable

Table 1 – Summary of Initial Safety Factor Assessments

Based on this evaluation, Ash Pond No. 1 meets the requirements in §257.73(e)(1).

3 Certification Statement

CCR Unit: Illinois Power Generating Company; Coffeen Power Station; Ash Pond No. 1

A MODER JR.

I, Victor A. Modeer, being a Registered Professional Engineer in good standing in the State of Illinois, do hereby certify, to the best of my knowledge, information, and belief that the information contained in this CCR Rule Report, and the underlying data in the operating record, has been prepared in accordance with the accepted practice of engineering. I certify, for the above-referenced CCR Unit, that the initial safety factor assessment dated October 2, 2016 meets the requirements of 40 CFR §257.73(e).

Printed Name

Date

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AECOM (NYSE: ACM) is a global provider of professional technical and management support services to a broad range of markets, including transportation, facilities, environmental, energy, water and government. With nearly 100,000 employees around the world, AECOM is a leader in all of the key markets that it serves. AECOM provides a blend of global reach, local knowledge, innovation, and collaborative technical excellence in delivering solutions that enhance and sustain the world's built, natural, and social environments. A Fortune 500 company, AECOM serves clients in more than 100 countries and has annual revenue in excess of \$19 billion.

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ATTACHMENT R



Submitted to Illinois Power Generating Company 134 Cips Lane Coffeen, IL 62017 Submitted by AECOM 1001 Highlands Plaza Drive West Suite 300 St. Louis, MO 63110

October 2016

CCR Rule Report: Initial Inflow Design Flood Control System Plan

For

Ash Pond No. 1

At Coffeen Power Station

1 Introduction

This Coal Combustion Residual (CCR) Rule Report documents that the initial inflow design flood control system plan for Ash Pond No. 1 at the Illinois Power Generating Company Coffeen Power Station meets the requirements specified in 40 Code of Federal Regulations (CFR) §257.82. Ash Pond No. 1 is located near Coffeen, Illinois in Montgomery County, approximately 0.3 miles east of the Coffeen Power Station. Ash Pond No. 1 serves as the primary wet impoundment basin for bottom ash produced by the Coffeen Power Station.

Ash Pond No. 1 is an existing CCR surface impoundment as defined by 40 CFR §257.53. The CCR Rule requires that the initial inflow design flood control system plan for an existing CCR surface impoundment be prepared by October 17, 2016. The plan must document how the inflow design flood control system has been designed and constructed to meet the requirements of 40 CFR §257.82 and be supported by appropriate engineering calculations.

The owner or operator of the CCR unit must obtain a certification from a qualified professional engineer stating that the inflow design flood control system meets the requirements of 40 CFR §257.82. The owner or operator must prepare an inflow design flood control system plan every five years.

2 Initial Inflow Design Flood Control System Plan

40 CFR §257.82

- (a) The owner or operator of an existing ... CCR surface impoundment ... must design, construct, operate, and maintain an inflow design flood control system as specified in paragraphs (a)(1) and (2) of this section.
 - (1) The inflow design flood control system must adequately manage flow into the CCR unit during and following the peak discharge of the inflow design flood specified in paragraph (a)(3) of this section.
 - (2) The inflow design flood control system must adequately manage flow from the CCR unit to collect and control the peak discharge resulting from the inflow design flood specified in paragraph (a)(3) of this section.
 - (3) The inflow design flood is:
 - (i) For a high hazard potential CCR surface impoundment, ..., the probable maximum flood;
 - (ii) For a significant hazard potential CCR surface impoundment, ..., the 1,000-year flood;
 - (iii) For a low hazard potential CCR surface impoundment, ..., the 100-year flood; or
 - (iv) For an incised CCR surface impoundment, the 25-year flood.
- (b) Discharge from the CCR unit must be handled in accordance with the surface water requirements under §257.3-3.

Analyses completed for the initial inflow design flood control system plan of Ash Pond No. 1 are described in the following subsections. Data and analysis results in the following subsection are based on spillway design information shown on design drawings, construction information, topographic surveys, information about operational and maintenance procedures provided by Illinois Power Generating Company, and field measurements collected by AECOM. The analysis approach and results of the hydrologic and hydraulic analyses are presented in the following subsections.

Ash Pond No. 1 has a significant hazard potential, based on the initial hazard potential classification assessment performed by Stantec in 2016 in accordance with §257.73(a)(2).

2.1 Initial Inflow Design Flood Control Systems (§257.82(a))

An initial inflow design flood control system plan, supported by a hydraulic and hydrologic analysis, was developed for Ash Pond No. 1 by evaluating the effects of a 24-hour duration design storm for the 1,000-year Inflow Design Flood (IDF) using a hydrologic HydroCAD (Version 10) computer model and a starting water surface elevation of 631.0 feet (NAVD88 datum). The computer model evaluated Ash Pond No. 1's ability to collect and control the 1,000-year IDF under existing operational and maintenance procedures. Rainfall data for the 1,000-year IDF was obtained from the National Oceanic and Atmospheric Administration (NOAA) Atlas 14. The NOAA Atlas 14 rainfall depth is 9.13 inches.

The HydroCAD model results for Ash Pond No. 1 indicate that the CCR unit has sufficient storage capacity and spillway structures to adequately manage (1) flow into the CCR unit during and following the peak discharge of the 1,000-year IDF and (2) flow from the CCR unit to collect and control the peak discharge resulting from the 1,000-year IDF. The peak water surcharge elevation is 632.0 feet (NAVD88 datum) during the IDF, and the minimum crest elevation of the Ash Pond No. 1 dike is 635.0 feet (NAVD88 datum). Therefore, overtopping is not expected.

Based on this evaluation, Ash Pond No. 1 meets the requirements in §257.82(a).

2.2 Discharge from the CCR Unit (§257.82(b))

40 CFR §257.82(b) provides that the discharge from the CCR unit must be handled in accordance with the surface water requirements under 40 CFR §257.3-3, which states the following:

- (a) For purposes of section 4004(a) of the Act, a facility shall not cause a discharge of pollutants into waters of the United States that is in violation of the requirements of the National Pollutant Discharge Elimination System (NPDES) under section 402 of the Clean Water Act, as amended.
- (b) For purposes of section 4004(a) of the Act, a facility shall not cause a discharge of dredged material or fill material to waters of the United States that is in violation of the requirements under section 404 of the Clean Water Act, as amended. (c) A facility or practice shall not cause non-point source pollution of waters of the United States that violates applicable legal requirements implementing an areawide or Statewide water quality management plan that has been approved by the Administrator under section 208 of the Clean Water Act, as amended.
- (d) Definitions of the terms Discharge of dredged material, Point source, Pollutant, Waters of the United States, and Wetlands can be found in the Clean Water Act, as amended, 33 U.S.C. 1251 et seq., and implementing regulations, specifically 33 CFR part 323 (42 FR 37122, July 19, 1977).

The handling of discharge was evaluated by reviewing design drawings, operational and maintenance procedures, conditions observed in the field by AECOM, and the inflow design flood control system plan developed per §257.82(a).

Based on this evaluation, Ash Pond No. 1 does not discharge into waters of the United States. Clear water from Ash Pond No. 1 is recycled to the Coffeen Power Station for use as process water. Hydraulic and hydrologic analyses performed as part of the initial inflow design flood control system plan found that Ash Pond No. 1 adequately manages outflow during the 1,000-year IDF, as overtopping of Ash Pond No. 1 embankments is not expected.

Therefore, discharge into waters of the United States is not expected during normal or 1,000-year IDF conditions, and Ash Pond No. 1 meets the requirements in §257.82(b).

3 Certification Statement

CCR Unit: Illinois Power Generating Company; Coffeen Power Station; Ash Pond No. 1

A MODELE SR.

I, Victor A. Modeer, being a Registered Professional Engineer in good standing in the State of Illinois, do hereby certify, to the best of my knowledge, information, and belief that the information contained in this CCR Rule Report, and the underlying data in the operating record, has been prepared in accordance with the accepted practice of engineering. I certify, for the above-referenced CCR Unit, that the initial inflow design flood control system plan dated October 13, 2016 meets the requirements of 40 CFR §257.82.

Printed Name

Date

REGISTERED LOS PROFESSIONAL FOR CHISTOPHER COFFICIENT CONTROL OF C

About AFCOM

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ATTACHMENT S

PART 845 SAFETY AND HEALTH PLAN

COFFEEN POWER PLANT GMF GYPSUM STACK POND, GMF RECYCLE POND, AND ASH POND NO. 1

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PART 845 SAFETY AND HEALTH PLAN Coffeen Power Plant GMF Gypsum Stack Pond, GMF Recycle Pond, and Ash Pond No. 1

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ACRONYMS & ABBREVIATIONS

% Percent Section

35 I.A.C. Title 35 of the Illinois Administrative Code 29 C.F.R. Title 29 of the Code of Federal Regulations

ACGIH American Conference of Governmental Industrial Hygienists

AP1 Ash Pond No. 1

CCR Coal Combustion Residual
CPP Coffeen Power Plant

GMF Gypsum Management Facility GMF GSP GMF Gypsum Stack Pond

GMF RP GMF Recycle Pond

HAZWOPER Hazardous Waste Operations and Emergency Response

ID identification

IDLH Immediately Dangerous to Life and Health
IEPA Illinois Environmental Protection Agency
IPGC Illinois Power Generating Company

kV kilovolt

NID National Inventory of Dams

NIOSH National Institute for Occupational Safety and Health

No. number

IDLH Immediately Dangerous to Life and Health

kV kilovolt

NIOSH National Institute for Occupational Safety and Health OSHA Occupational Safety and Health Administration

Part 845 35 I.A.C. Part 845: Residuals in Surface Impoundments

PEL Permissible Exposure Level

PFAS Per- and polyfluoroalkyl substances

PFD Personal Flotation Device

PNOR particulates not otherwise recognized

POC Point of Contact

PPE personal protective equipment

ppm parts per million SDS Safety Data Sheet

Site GMF GSP, GMF RP, and AP1
STEL Short Term Exposure Limit
TLV Threshold Limit Value
TWA time-weighted averages
USCG United States Coast Guard

REVISION SUMMARY

| Revision Date | Description of Changes (Section title or number – description) | Responsible Party (individual name or title, company / agency name, document reference and date) |
|---------------|---|--|
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PREFACE

Illinois Power Generating Company (IPGC) has prepared this Safety and Health Plan in accordance with requirements set forth in Title 35 of the Illinois Administrative Code (35 I.A.C.) Part 845: Residuals in Surface Impoundments (Part 845), Section (§) 845.530. IPGC assessed health and safety hazards of its coal combustion residual (CCR) surface impoundments to develop and update this Safety and Health Plan.

This document describes the minimum anticipated protective measures necessary for worker health and safety at the Coffeen Power Plant (CPP) Gypsum Management Facility (GMF) Gypsum Stack Pond (GMF GSP; Vistra identification [ID] number [No.] 103, Illinois Environmental Protection Agency [IEPA] ID No. W1350150004-03, National Inventory of Dams [NID] No. IL50579), GMF Recycle Pond (GMF RP; Vistra ID No. 104, IEPA ID No. W1350150004-04, NID No. IL50578), and Ash Pond No. 1 (AP1; Vistra ID No. 101, IEPA ID No. W13501050004-01, NID No. IL50722), collectively referred to as the Site. Employees of IPGC, contract workers, and third-party contractors must read and comply with the contents of this document. The contents of this document are not intended to cover all situations that may arise nor to waive any provisions specified in Federal, State, and local regulations or site owner / contractor health and safety requirements.

Third-party contractors are accountable for the health and safety of their employees. Third-party contractors are required to prepare a Safety and Health Plan that meets the minimum requirements herein. However, no requirements or provisions within this plan shall be construed as an assumption of IPGC of their legal responsibilities as an employer.

This Safety and Health Plan will be reviewed and updated annually, at a minimum. The Safety and Health Plan will also be updated if facility operations change, or a new hazard is identified.

1. INTRODUCTION

This Safety and Health Plan has been developed to outline the requirements to be met by employees of IPGC, contract workers, and third-party contractors while performing any activity to construct, operate, or close the CCR Units at the Site. This Safety and Health Plan has been developed to meet the requirements of 35 I.A.C. § 845.530 and describes the responsibilities, training requirements, protective equipment, and safety procedures necessary to minimize the risk of injury, fires, explosion, chemical spills, material damage incidents, and near misses related to CCR activities. This Safety and Health Plan incorporates by reference the Occupational Safety and Health Administration (OSHA) regulations contained in Title 29 of the Code of Federal Regulations (29 C.F.R.) § 1910 and 29 C.F.R. § 1926.

The requirements and guidelines in this Safety and Health Plan are based on a review of available information and data, and an evaluation of identified on-site hazards. This Safety and Health Plan will be reviewed with persons assigned to work at the Site and will be available on-site.

1.1 Site Description/History

The CPP is a retired coal-fired power plant located in Montgomery County, in central Illinois, within Section 11 Township 7 North and Range 7 East. The CPP is approximately 2 miles south of the city of Coffeen and about 8 miles southeast of the city of Hillsboro, Illinois. The Site is located between the two lobes of Coffeen Lake to the west, east, and south, and is bordered by agricultural land to the north. The approximately 1,100-acre Coffeen Lake was built by damming the McDavid Branch of the East Fork of Shoal Creek in 1963 for use as an artificial cooling lake for the CPP. Appendix A is a site map showing the location of the CCR Units at the Site.

1.2 Facility Personnel

The following table outlines key personnel with respect to facility operations and health and safety.

| Name | Position | Phone Number |
|------------------|--|----------------------------|
| Scott Bell | Primary Point-of-Contact / Plant Manager | 217-248-7720 |
| John Romang | Secondary Point-of-Contact / Environmental Manager | 217-341-7319 |
| Gate House | Security Guard | 217-534-2363 |
| Matt Ballance | Engineering Manager | 618-343-7739 (office) |
| | | 618-792-7274 (mobile) |
| Jason Campbell | Dam Safety Manager | 271-753-8904 (Springfield) |
| | | 217-622-3491 (mobile) |
| Stu Cravens | Senior Technical Expert | 217-390-1503 (mobile) |
| Vic Modeer | Engineering Manager | 618-541-0878 |
| Charles Koudelka | Plant Closure Director | 903-235-8633 |

1.3 Responsibilities

The following persons have responsibilities associated with communicating and implementing the Safety and Health Plan for the CCR Units at the Site.

1.3.1 IPGC Point of Contact

The IPGC Point of Contact (POC) is a management-level person who is requiring employees, contract workers, or third-party contractors to enter the Site. The IPGC POC is responsible to communicate Safety and Health Plan information and requirements to employees, contract workers, and third-party contractors, and oversee work performed in the Site to the extent necessary to confirm implementation of Safety and Health Plan requirements.

1.3.2 IPGC Employees

IPGC employees are directly hired by IPGC. They are required to implement and/or follow Safety and Health Plan requirements as applicable to their work and exercise their "stop work authority" if safety requirements are unclear or unanticipated site conditions or hazards are observed.

1.3.3 Contract Workers

Contract workers are those hired by IPGC through an agency firm. Similar to IPGC employees, contract workers are required to implement and/or follow Safety and Health Plan requirements as applicable to their work and exercise their "stop work authority" if safety requirements are unclear or unanticipated site conditions or hazards are observed.

1.3.4 Third-Party Contractor Employees

Third-party contractor employees work for firms under contract to IPGC. Third-party contractors include prime contractors and all of their lower tier subcontractors. Similar to IPGC employees, third-party contractors are required to implement Safety and Health Plan requirements as applicable to their work and exercise their "stop work authority" if safety requirements are unclear or unanticipated site conditions or hazards are observed.

1.3.5 Third-Party Contractor Safety Competent Person

Third-party contractors will be required to designate a Safety Competent Person. The Safety Competent Person must be in a management position (*e.g.*, superintendent, foreman, etc.) with OSHA 30-hour construction safety certification who may perform other duties, unless IPGC requires a dedicated Safety Competent Person. A Safety Competent Person must be on site at all times when the subcontractor has employees performing work for IPGC and must possess a sound working knowledge of pertinent OSHA regulations, this Safety and Health Plan, and other applicable safety requirements related to the scope of work. Third-party contractors must also designate a backup Safety Competent Person that possesses the same authority and training. The competent person will ensure timely correction of safety deficiencies identified by IPGC. The Safety Competent Person is responsible to ensure Safety and Health Plan requirements have been communicated to lower-tier subcontractors and enforce Safety and Health Plan requirements.

2. SITE ACCESS & CONTROL

This section outlines requirements for ensuring that only authorized personnel and visitors are permitted at the Site.

2.1 Facility Security

Elements of site control include restricting access to the Site to persons until they have met the training requirements outlined in this Safety and Health Plan and have been authorized to do so by the CPP POC or their representative.

Upon arrival to the facility all IPGC employees, contract workers, and third-party contractors must sign in at the gate house. The security guard will call the POC to confirm the individual(s) is authorized to enter the facility.

Upon arrival to the Site, all IPGC employees, contract workers, and third-party contractors must check in/out at Security. A COVID-19 screening must also be completed per Section 3.8.

2.2 Third-Party Contractor Management

Prior to working at the Site, all third-party prime contractors must maintain an active registration with ISNetworld and maintain a grade of A or B. Lower tier subcontractors are currently not required to be registered in ISNetworld, but this requirement may change at the discretion of IPGC.

2.3 Third-Party Contractor Safety and Health Plan

Prior to being authorized to conduct work at the Site, third-party contractors must develop and submit a Safety and Health Plan. The third-party contractor's Safety and Health Plan must be specific to the scope of work that they will be performing at the Site. The third-party contractor's Safety and Health Plan must meet or exceed all the requirements in this Safety and Health Plan, other IPGC requirements, and applicable regulations. All lower tier subcontractors of third-party contractors must meet the requirements in this Safety and Health Plan as well as the requirements outlined in the Safety and Health Plan of the third-party with whom they are contracted.

2.4 Authorized Personnel

At a minimum, authorized personnel who will be granted unescorted access to the project include IPGC employees, contract workers, and third-party contractors that meet the following:

- Reviewed this Safety and Health Plan and other applicable safety planning documentation
- Have completed all the training, medical surveillance, and drug screen and background investigation requirements as outlined in Section 3 of this Safety and Health Plan.
- Have received the Site Orientation Training

2.5 Visitors

Visitors must be escorted by Authorized Personnel through the Site if they have not reviewed this Safety and Health Plan or completed the training requirements outlined in Section 3 of this Safety and Health Plan. Visitors may not undertake any activity to construct, operate, or close a CCR surface impoundment.

2.6 Communication

Communication between workers and emergency services must be maintained at all times. Cellular service is consistently available and can be relied upon to summon emergency services.

3. TRAINING & MEDICAL REQUIREMENTS

Project personnel must be properly trained for the type of work being performed and in accordance with 35 I.A.C. § 845.530, 29 C.F.R. § 1926 and 29 C.F.R. § 1910, and IPGC policies. Additionally, personnel working in areas regulated by the OSHA Hazardous Waste Operations and Emergency Response (HAZWOPER) standards (29 C.F.R. § 1910.120 and 29 C.F.R. § 1926.65) must have current medical surveillance. All employees, contractors, and third-party contractors must complete the following prior to beginning any activity to construct, operate, or close the CCR Units at the Site.

3.1 HAZWOPER Training

35 I.A.C. § 845.530(c)(2)(E) requires that all employees, contract workers, and third-party contractors be trained in accordance with 29 C.F.R. § 1910.120 and 29 C.F.R. § 1926.65. The following training will be completed as required by job function:

- **OSHA 40-Hour Training** per 29 C.F.R. § 1910.120 and 29 C.F.R. § 1926.65, for those personnel who are expected to have extensive contact with contaminated materials and/or may be required to wear a respirator.
- **OSHA 24-Hour Training** per 29 C.F.R. § 1910.120 and 29 C.F.R. § 1926.65, for those personnel who are expected to have minimal contact with contaminated materials and will NOT be required to wear a respirator.
- **OSHA 8-hour Supervisor Training** per 29 C.F.R. § 1910.120 and 29 C.F.R. § 1926.65, for Site Supervisors, Foremen, Superintendents, and others who will be directing and managing site activities.
- **OSHA 8-hour Refresher** per 29 C.F.R. § 1910.120 and 29 C.F.R. § 1926.65, completed within 12 months of initial 40-hour or 24-hour training and annually thereafter.

The following matrix outlines HAZWOPER training requirements based on typical job functions at the Site. It is not intended to be all inclusive, new job functions must be evaluated per 29 C.F.R. § 1910.120 and 29 C.F.R. § 1926.65.

| Training | Job Function |
|---------------------------------|---|
| OSHA 40-hour | Ash handlers |
| OSHA 24-hour | Personnel not required to handle CCR materials |
| OSHA 8-hour Supervisor Training | Third-Party Contractor Safety Competent Persons |
| OSHA 8-hour refresher | All personnel |

3.2 OSHA Construction Outreach Training

35 I.A.C. § 845.530(c)(2)(E) requires that all employees, contract workers, and third-party contractors complete an OSHA 10-hour or 30-hour construction safety training. These trainings will be completed as follows:

- All employees, contract workers, and third-party contract employees: OSHA 10-hour or 30-hour construction outreach training.
- Supervisors, superintendents, foreman and safety professionals: OSHA 30-hour construction outreach training.

3.3 Site Safety and Health Plan Review

Pursuant to 35 I.A.C. § 845.530(d)(e), before beginning any activity at the Site, and annually thereafter, all IPGC employees, contract workers, and third-party contractors must review the content of this HASP. After reviewing this Safety and Health Plan all personnel will understand the following:

- Procedures for using, inspecting, repairing, and replacing facility emergency and monitoring equipment
- Communications or alarm systems outlined in Section 6
- Response to fires and explosions outlined in Section 6
- · Response to a spill or release of CCR
- Information about chemical hazards and hazardous materials outlined in Section 5
- The use of engineering controls, administrative controls, and personal protective equipment (PPE) outlined in Section 4

All personnel will acknowledge this HASP by signing the *Safety and Health Plan Acknowledgment Form (Appendix B)*.

3.4 Emergency and Monitoring Equipment Training

All IPGC employees, contract workers, and third-party contractors must be aware of how to respond to alarms and other emergencies as outlined in Section 6 of this plan. Individuals may only use facility emergency and monitoring equipment if they have been trained in their use and authorized to do so by the designated POC. Additionally, a written release may need to be completed as required by Vistra Corporate Procedure FFA-POL-0006.

Individual IPGC employees and contract workers may be responsible for using, inspecting, repairing and replacing facility emergency monitoring equipment. These individuals will be trained in accordance with procedures identified by IPGC. These individuals will review and adhere to the manufacturer's instructions, where applicable.

Third-party contractors are responsible for inspecting, repairing, and replacing any owned emergency (*i.e.*, fire extinguishers) and monitoring equipment (*i.e.*, air monitoring equipment). Third-party contractors will maintain procedures for using, inspecting, repairing, and replacing owned emergency and monitoring equipment that is consistent with the manufacturer's requirements. Third-party contractor employees who are responsible for this equipment will be trained in procedures for using, inspecting, and repairing owned equipment by their employer.

3.5 Hazard Communication

All employees, contract workers, and third-party contractors must be trained in chemical hazards (if any) associated with their work in accordance with 29 C.F.R. § 1910.1200. Work tasks performed on the Site may include exposure to compounds identified in the Hazard Communication section of this Safety and Health Plan and is included as part of the Safety and Health Plan Review outlined previously in Section 3.3.

3.6 Medical Surveillance

All employees, contract workers, and third-party contractors engaged in operations specified in 29 C.F.R. § 1910.120 and 29 C.F.R. § 1926.65 and meet one of the criteria outlined in 29 C.F.R. § 1910.120(f)(2) and 29 C.F.R. § 1926.65(f)(2) must participate in a medical surveillance program that is administered by their employer. The criteria for participating in a medical surveillance program are:

- All employees who are or may be exposed to hazardous substances at or above the
 established permissible exposure limit, without regard to the use of respirators, for 30 days or
 more a year;
- All employees who wear a respirator for 30 days or more a year; or
- All employees who are injured, become ill or develop signs or symptoms due to possible overexposure involving hazardous substances or health hazards from an emergency response or hazardous waste operation.

The medical surveillance program must result in documentation that an individual is cleared to work on sites covered by 29 C.F.R. § 1910.120 and 20 C.F.R. § 1926.65 and is medically fit to wear a respirator when applicable.

3.7 Drug Screen and Background Investigations

IPGC requires that contract worker agencies and third-party contractors are responsible for ensuring that all personnel have completed and passed a drug and alcohol test and background investigation prior to on-site work as described in Appendix C.

3.8 COVID-19 Site Entry Guidelines

All personnel entering Vistra work sites shall review and adhere to the site entry guidelines provided in Appendix D.

3.9 Document Management

IPGC will maintain employee and contract employee training and medical surveillance records in the main office. Third-party contractors are responsible for maintaining training and medical surveillance documentation for their employees. Third-party contractors will produce documentation upon IPGC request.

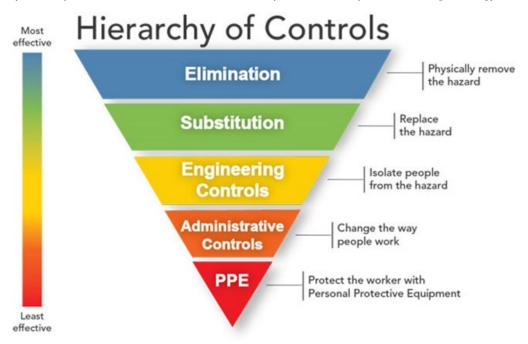
3.10 Industrial Hygiene Sampling Records

Upon receipt of exposure sampling results IPGC and third-party contractors must distribute exposure sampling results to employees within 15 business days unless otherwise required by applicable regulation. All personnel exposure sampling results and records must be maintained by the employee's company for at least 30 years following termination of employment.

4. HAZARD & CONTROLS

The following section outlines general controls for the hazards and controls. Third-party contractors are still responsible for developing a Safety and Health Plan that incorporates requirements of this Safety and Health Plan, other safety requirements for the CPP, as well as the third-party contractor's safety policies and procedures. Safety and Health Plans developed by third-party contractors must be specific to the site and the anticipated work means and methods. Safety and Health Plans that consist of only standard operating procedures or are not otherwise specific to the work performed at the Site will not be accepted by the IPGC.

IPGC requires that a hierarchy of controls be considered when performing work at the Site. Implement controls that favor elimination, substitution, and engineering over the use of administrative controls and PPE when feasible. See the figure below for additional guidance (courtesy of the National Institute for Occupational Safety and Health [NIOSH]).



4.1 Ash/Unstable Surfaces

At least 24 hours prior to working in or on an ash pond, third-party contractors must notify the facility POC. Work in or on an ash pond may not begin until the facility POC has approved the work. Upon completion of the work, third-party contractors must notify the POC that they have left the ash pond.

When working on ash ponds or unstable surfaces the following requirements must be implemented where applicable and feasible. The following table summarizes safety controls for work performed in ash ponds and on unstable surfaces and are aligned to the hierarchy of controls:

| Elimination | Substitution | Engineering | Administrative | PPE |
|---|--|--|--|---|
| Change the work task or work methods so that work on ash ponds is no longer required | Use the lightest available tracked equipment to reduce ground pressure | Use crane mats or other cribbing to support heavy equipment on ash ponds | Traverse compacted paths that have previously been used by heavy equipment | Use a restraint (tethering) system to prevent falls or slips into unstable ash pond surfaces or surface water that represents a drowning hazard |

| Elimination | Substitution | Engineering | Administrative | PPE |
|-------------|--------------|-------------|---|-----|
| | | | If an unstable condition exists, complete a Next Level Up Pre-Job Brief prior to accessing the ash pond. | |
| | | | Approach the ash pond from the most stable direction | |
| | | | Inspect travel paths for recent terrain shifts, particularly following heavy rains or rapid dewatering | |
| | | | Working alone on ash ponds is prohibited without pre-approval from the POC. | |
| | | | When a drowning hazard exists, implement requirements for working on/near water as outlined in Section 4.4. | |
| | | | Implement an emergency response plan with trained responders for falls into (or engulfment by) ash | |

4.2 Ash Inhalation/Airborne Exposure

Ash that becomes airborne due to site activities or environmental conditions may result in an exposure to its components as outlined in Section 5.1. IPGC and third-party contractors are responsible for ensuring their respective employees' and contract workers' exposures are below occupational exposure limits. Upon request, third-party contractors must demonstrate to IPGC that exposure control methods are adequate. The following table summarizes airborne exposure controls and is aligned to the hierarchy of controls:

| Elimination | Substitution | Engineering | Administrative | PPE |
|---|---|--|--|---|
| Change the work task or work methods so that work on ash ponds is no longer required | Substitute manual work methods for those that can be completed from the cab of a vehicle | Continually wet work areas to reduce the amount of ash that becomes airborne Equip vehicles and heavy equipment cabs with filters. Clean and change filters as required | Conduct air monitoring or exposure sampling to confirm that airborne exposure is below regulatory limits | If exposure levels are above the PEL, equip employees with respirators appropriate to the level of exposure |

4.3 Stuck Vehicles/Equipment

If a vehicle or piece of equipment becomes stuck, a third-party towing or wrecking company who is trained in vehicle extraction must be retained and the POC will be notified. The POC will make recommendations on extraction companies depending on the type of vehicle/equipment that is stuck. Third-party contractors may extract their own vehicle if they have an approved extraction plan, and a competent person is on site to implement the extraction. The extraction plan shall be included as part of the third-party contractor's reviewed and approved Safety and Health Plan. The above notifications are still required.

The hazards presented by stuck vehicles/equipment must not be underestimated. While the weight of the stuck equipment can be calculated, it's impossible to precisely calculate the other forces that are pulling against the towing vehicle which requires special training and experience to properly size towing equipment and select towing techniques. This is especially true for "complex" or high-hazard extractions involving equipment stuck at axle depth (or beyond) or sloped surfaces or any area where extraction activities could trigger shifts in the ground surface. No chains shall be used to remove stuck vehicles/equipment.

The following table summarizes safety controls related to stuck vehicles and equipment and are aligned to the hierarchy of controls:

| Elimination | Substitution | Engineering | Administrative | PPE |
|--|--|--|---|--|
| Change the work task or work methods so that work on ash ponds is no longer required | Use the lightest available tracked equipment to reduce ground pressure Substitute tracked equipment for wheeled equipment | Use crane mats or other cribbing to support heavy equipment on ash ponds Lighten the load – Remove materials from stuck vehicles or equipment prior to extraction if possible | Only persons trained in vehicle extraction are permitted to remove stuck vehicles/equipment A professional towing/wrecking service is required Prepare for spills (damage to fuel or hydraulic systems) | All persons involved in removing stuck equipment must wear PPE that includes hard hat, safety boots, safety glasses, high visibility vests, and cut resistant gloves |

4.4 Working Near/Over Water

All employees, contract workers, and third-party contractors must wear a United States Coast Guard (USCG) approved personal floatation device (PFD), when within 6 feet of water, over water, and/or wading in water where the danger of drowning exists. The PFD must be properly

secured to the wearer, free of all defects including rips, tears, stress, and fading, and be kept clean and free of excessive dirt and oil.

If the possibility of falling into water has been eliminated through the use of guardrails, fall restraint, or other method, the use of a PFD is no longer required.

When performing work on water from a vessel, at least one lifesaving rescue vessel (e.g., a skiff) shall be immediately available at locations where employees are working over, in, on, or adjacent to water where the danger of drowning exists. However, if the water is so shallow that rescuers could simply walk/run into the water body without endangering themselves and/or others or the work was being conducted very close to shore (e.g., the length of the skiff from shore would be greater than the working distance from shore and/or the skiff would foul on the bottom), a skiff would not be required.

The following table summarizes the requirements for working over/near water where a drowning hazard exists and are aligned to the hierarchy of controls:

| Elimination | Substitution | Engineering | Administrative | PPE |
|---|--------------|--|--|--|
| Change the work task or work methods so that work near a drowning hazard is no longer required | | Install guardrails that separate work areas from the drowning hazard | All work to be performed by at least two people where each is equipped with proper safety gear and capable of summoning emergency rescue | All personnel are required to wear suitable PFDs |
| | | Utilize equipment (crowd-control barricades, safety fence, etc.) that will keep personnel at least 6 feet from a drowning hazard | When working on water use of a rescue skiff as outlined above | |
| | | | Use of a ring buoy with 90 feet of braided polycarbonate (or equivalent) line | |
| | | | Ring buoys must be positioned within 100 feet of work (maximum of 200 feet spacing) | |

4.5 Heavy Equipment

All heavy equipment operators must be competent and authorized to operate each piece of heavy equipment. Forklift and telehandler (e.g., Lull, JLG) operators must have a license or certificate that indicates they have passed a written test and "road" test for the equipment they will be operating within the last 3 years. Third-party contractors will provide proof of qualification upon request of IPGC.

Persons working around heavy equipment must implement the "25 Foot Rule." The 25 Foot Rule requires that persons get the operator's attention and permission prior to approaching closer than 25 feet to heavy equipment. Persons must walk quickly through blind spots. Loitering in heavy equipment blind spots (especially to the rear) must be avoided.

Temporary fuel storage tanks will be labelled as to their content and be protected from collision by Site vehicles using solid barricades including balusters, chain link fence, or equivalent. Spill kit (55-gallon sorbent capacity contained in an overpack) and one 20-pound Type ABC fire extinguisher will be located within 45 feet of fueling areas. Tanks will be rated for above ground use and will be double walled or have secondary containment in case of a leak. Tanks and dispensing hose will be bonded and grounded. On-site filling of fuel storage tanks will be completed with trucks that have automatic over-flow shutoffs. These trucks will be properly bonded to the storage tank and meet all of the other storage tank requirements. Temporary secondary containment must be provided in the refueling area that includes the storage tank and dispensing hoses.

| Elimination | Substitution | Engineering | Administrative | PPE |
|-------------|--------------|--|---|---|
| | | Heavy equipment (and vehicles) must be equipped with backup alarms, horns, roll- over protection (when feasible) | Operators must be competent and authorized | Operators must use seatbelts when equipped |
| | | Vehicles and heavy equipment operated at night must have headlights, tail lamps, and reflectors | Forklift operators must have a current license or certificate (within 3 years) | High visibility vests are required when working around heavy equipment |
| | | | All vehicles and equipment must be turned off when not in use | |
| | | | Operators must inspect equipment daily prior to use | |
| | | | Persons working near heavy equipment must follow the "25 Foot Rule" and avoid lingering in blind spots as outlined above | |
| | | | Always obey site speed limits – 15 mph unless otherwise posted | |

4.6 Overhead Powerlines

All overhead powerlines must be assumed to be energized until confirmed otherwise. The minimum clearance distance for equipment working near energized power lines must be in accordance with table found in 29 C.F.R. § 1926.1408(h).

The following table summarizes safety controls for work near energized power lines:

| Elimination | Substitution | Engineering | Administrative | PPE |
|-----------------------------------|---|---|--|-----|
| Plan to work away from powerlines | Use heavy equipment with shorter booms/attachments to avoid coming close to power lines | Contact the utility owner to deenergize the line | Install signs to warn personnel of overhead powerlines | |
| | | Contact the utility owner to install insulated sleeves over energized lines | Install a non- conductive distance marker to delineate minimum clearance | |
| | | | Use a dedicated spotter to ensure equipment does not enter minimum clearance distances | |

4.7 Severe Weather

Severe weather conditions include but are not limited to high winds, electrical storms, heavy rain, and tornados can cause hazardous conditions at CCR surface impoundments. The primary control for severe weather is monitoring weather reports prior to beginning work and as work occurs throughout the day.

Monitor lightning using a commercially available mobile application if cellular service is available. When lightning is observed within 10 miles of the CCR surface impoundment, or a storm is imminent, take shelter in the nearest solid structure or fully enclosed vehicle. If possible secure all tools, materials, and equipment prior to the storm arriving. Work may resume 30 minutes after the last lightning strike is observed within 10 miles. The severe weather shelter location is the storm shelter located next to the security office.

Do not conduct work on a CCR surface impoundment when there is a risk for tornados in the area. If on a CCR surface impoundment and a tornado forms, seek the nearest substantial shelter. The closest tornado shelter is the storm shelter located next to the security office; shelter locations will be reviewed during the Site Orientation Training. If no shelter is available, attempt to evacuate to a shelter using a vehicle. If a tornado forms and you are not in a shelter, take one of the following actions:

- Stay in a vehicle with the seat belt on, keep your head below the windows and cover it with your hands
- If there is an area which is noticeably lower than the work area, lie in that area and cover your head with your hands.

The following table summarizes safety controls related to severe weather:

| Elimination | Substitution | Engineering | Administrative | PPE |
|--------------------|--------------|-------------|--------------------|-----|
| Plan outdoor tasks | | | Prior to beginning | |
| on days with low | | | outdoor work | |
| potential for | | | monitor the day's | |
| severe weather. | | | weather. | |

| Elimination | Substitution | Engineering | Administrative | PPE |
|-------------|--------------|-------------|---|-----|
| | | | Periodically monitor weather throughout the day. Use a weather app which issues alerts for severe weather and lightning, assuming cell service is available | |
| | | | Utilize a weather radio if cellular service is inconsistent | |
| | | | Stop all outdoor work and seek shelter when lightning is observed | |

4.8 Heat Stress

Heat stress can be a significant hazard, especially for workers wearing protective clothing. Depending on the ambient conditions and the work being performed, heat stress can occur very rapidly, within as little as 15 minutes. Employees, contract workers, and third-party contractors will be instructed in the identification of a heat stress victim, the first-aid treatment procedures for the victim, and in the prevention of heat stress incidents.

Workers will be encouraged to immediately report any heat-related problems that they experience or observe in fellow workers. Any worker exhibiting signs of heat stress and exhaustion should be made to rest in a cool location and drink plenty of water. Emergency help by a medical professional is required immediately for anyone exhibiting symptoms of heat stroke, such as red, dry skin, confusion, delirium, or unconsciousness. Heat stroke is a life-threatening condition that must be treated immediately by competent medical authority.

4.8.1 Heat Stress Prevention

To prevent heat stress, IPGC employees, contract workers, and third-party contractors will implement heat stress prevention measures as outlined in OSHA's Heat Index (below). A summary of these precautions is described below.

| Heat Index | Risk Level | Protective Measures |
|--------------------------|-------------------------|--|
| Less than 91°F | Lower (Caution) | Basic heat safety and planning |
| 91°F to 103°F | Moderate | Implement precautions and heighten awareness |
| 103°F to 115°F | High | Additional precautions to protect workers |
| Greater than 115°F | Very High to Extreme | Triggers even more aggressive protective measures |

Know the Symptoms: Some symptoms associated with heat stress are: Employees should be aware of these symptoms with themselves and with their co-workers:

- Elevated heart rate, lack of concentration, difficulty focusing on a task, fatigue
- Irritability and/or sickness
- · Cramps, rash, headache
- · Loss of desire to drink water
- Fainting
- Skin clammy, moist, and pale (severe heat exhaustion)
- Skin extremely dry and red (heat stroke)

Acclimatize: When high heat stress conditions arise, employees should be exposed to the heat for short work periods followed by longer periods of work. Acclimatization usually takes five (5) days and should be provided for all new employees and employees returning from an absence of two (2) weeks or more. Contact Corporate Health and Safety for proper procedures.

Hydration & Pace of Work: Make sure all employees intake plenty of water throughout the work day (sometimes as much as a quart per worker per hour) and let employees know where the drinking water is located. Adjust your work pace and expectations on how much work can be done during periods of high heat stress. Workers cannot do as much during periods of high heat stress compared with similar periods of low heat stress. After acclimatization, workers may be able to resume a more "normal" work pace as long as fluid intake is adequate.

Work/Rest Periods: If possible, heavy work should be scheduled during the cooler parts of the day (*i.e.*, early morning) and rest periods should be taken in cool areas for longer periods.

Personal Protective Equipment (PPE): Employees using PPE (*i.e.*, Tyvek® suits or other equipment which may retain heat) can be more susceptible to heat stress due to the fact that heat/sweat often cannot escape the suits and/or the equipment. Persons wearing PPE that contributes to heat stress require more hydration, longer rest periods, or a reduced pace of work. Also, more careful monitoring of each person's health status is required by co-workers and management.

The following table summarizes safety controls for heat related illnesses:

| Elimination | Substitution | Engineering | Administrative | PPE |
|--|---|---|---|---|
| Perform outdoor, strenuous, tasks at cooler times of day/year | Use mechanized equipment in place of manual labor | Install fans or air conditioning units in the work area | Train all personnel to know the signs of heat stress/stroke and how to prevent it | Implement the use of cooling vests or other similar PPE |
| | | Install a canopy to provide shade to work areas | Allow workers to acclimatize to the work environment | |
| | | Provide cool, shaded break areas | Adjust work pace to allow for the effects of heat | |
| | | | Implement work/rest periods | |

4.9 Cold Stress

The four environmental conditions that cause cold-related stress are low temperatures, high/cool winds (wind chill), dampness, and cold water. One, or any combination of these factors, can cause cold-related hazards. Cold stress, including frostbite and hypothermia, can result in severe health effects. Employees, contract employees, and third-party contractors will be instructed in the identification of a cold stress victim, the first-aid treatment procedures for the victim and in the prevention of heat stress incidents.

A dangerous situation of rapid heat loss may arise for any individual exposed to high winds and cold temperatures. Major risk factors for cold-related stresses include:

- Wearing inadequate or wet clothing thus increasing the effects of cold on the body.
- Taking certain drugs or medications such as alcohol, nicotine, caffeine, and medication thus inhibiting the body's response to the cold and/or impairing judgment.
- Having a cold or certain disease, such as diabetes, heart, vascular and thyroid problems, and thereby increasing susceptibility to the winter elements.
- Lower body-fat composition or other physiological differences. Statistics show that men experience far greater death rates due to cold exposure than women, potentially attributable to participation in risk-taking activities, lower body-fat composition and/or other physiological differences.
- Becoming exhausted or immobilized, especially due to injury or entrapment, thus speeding up the effects of cold weather.

The following table provides the resulting equivalent chill temperature to exposed skin because of increasing wind speeds at decreasing actual temperatures. Personnel shall be aware of predicted weather conditions before beginning site work and stay apprised of changes.

| | Actual | Tempe | erature | Readi | ng (°F) | | | | | | | |
|---|--|-------|---|--------|---------|----------|---------|-----------|------------|------------|------|------|
| Estimated Wind Speed (in mph) | 50 | 40 | 30 | 20 | 10 | 0 | -10 | -20 | -30 | -40 | -50 | -60 |
| | | | | | Equiva | lent Chi | ll Temp | erature (| °F) | | 100 | |
| çalm | 50 | 40 | 30 | 20 | 10 | 0 | -10 | -20 | -30 | -40 | -50 | -60 |
| 5 | 48 | 37 | 27 | 16 | 6 | -5 | -15 | -26 | -36 | -47 | -57 | -68 |
| 10 | 40 | 28 | 16 | 4 | -9 | -24 | -33 | -46 | -58 | -70 | -83 | -95 |
| 15 | 36 | 22 | 9 | -5 | -18 | -32 | -45 | -58 | -72 | -85 | -99 | -112 |
| 20 | 32 | 18 | 4 | -10 | -25 | -39 | -53 | -67 | -82 | -96 | -110 | -121 |
| 25 | 30 | 16 | 0 | -15 | -29 | -44 | -59 | -74 | -88 | -104 | -118 | -133 |
| 30 | 28 | 13 | -2 | -18 | -33 | -48 | -63 | -79 | -94 | -109 | -125 | -140 |
| 35 | 27 | 11 | -4 | -20 | -35 | -51 | -67 | -82 | -98 | -113 | -129 | -145 |
| 40 | 26 | 10 | -6 | -21 | -37 | -53 | -69 | -85 | -100 | -116 | -132 | -148 |
| (Wind speeds greater than 40 mph have little additional effect.) | LITTLE DANGER In < hr with dry skin. Maximum danger of false sense of security | | INCREASING DANGER Danger from freezing of exposed flesh within one minute. GREAT DANGER Flesh may freeze within 3 seconds. | | | | | 1 30 | | | | |
| | | Tı | renchfo | ot and | immersi | on foot | may occ | ur at an | y point or | n this cha | ırt. | |

The following table summarizes safety controls for preventing cold stress:

| Elimination | Substitution | Engineering | Administrative | PPE |
|---|--------------|--|--|---|
| Perform work during warm parts of the day or warmer parts of the year | | Install heaters in enclosed work areas | Train all personnel on the symptoms of cold stress and how to prevent it | All personnel must wear multiple layers of clothing |
| | | Provide a warm break area | Implement work/rest schedule | Utilize hand/foot warmers when required |

An additional hazard in cold weather conditions is the increased risk for slips from the accumulation of ice and snow in general work areas, ruts where water is accumulated, and heavy equipment. The following table outlines controls that may be used for preventing slips:

| Elimination | Substitution | Engineering | Administrative | PPE |
|---|--------------|------------------------------------|----------------|--|
| Perform work during warm parts of the day or in areas free of accumulated areas | | Clear snow in work areas | | Use traction control devices (i.e., YakTrax) on work boots to provide additional traction. |
| | | Apply salt/sand to icy areas | | |
| | | Use equipment to access work areas | | |

4.10 Biological Hazards

The following are biological hazards that may be present at the Site.

4.10.1 Ticks (Lyme Disease) & Mites

Although Lyme disease has been detected throughout the continental United States, it is prevalent primarily in certain areas in New England, the Mid-Atlantic and the northern Midwest states.

per cold stress TLV

Although Lyme disease is the most common tickborne illness, other tickborne illnesses include southern tick-associated rash illness, Rocky Mountain spotted fever, ehrlichiosis, and tularemia. More information on Lyme disease and other tickborne illnesses can be found from the CDC.

Prevention

- Standard field gear (work boots, socks, and light-colored coveralls) provides good protection
 against tick bites, particularly if the joints are taped. However, even when wearing field gear,
 the following precautions shall be taken when working in areas that might be infested with
 ticks:
 - Wear long pants and long-sleeved shirts that fit tightly at the ankles and wrists, tape cuffs
 if necessary
 - Wear light colored clothing so ticks can be easily spotted
 - o Per- and polyfluoroalkyl substances (PFAS)-free tick repellents (DEET and Permethrin) must be used when walking in all overgrown areas. DEET (≥25 percent [%]) must be applied to skin while permethrin must be applied to clothes and allowed to dry. Spray outer clothing, particularly your pant legs and socks, BUT NOT YOUR SKIN, with an insect repellent that contains permethrin. For heavily infested tick areas, wear spun polypropylene coveralls that have been sprayed with permethrin.
 - Inspect clothing frequently
 - Inspect head and body thoroughly when you return from the field, particularly on your lower legs and areas covered with hair
 - When walking in wooded areas, wear a hard hat, and avoid contact with bushes, tall grass, or brush as much as possible

Removal

- Remove any ticks by tugging with tweezers or special tick removal tools
- Do not squeeze or crush the tick
- DO NOT use matches, a lit cigarette, nail polish, or any other type of chemical to "coax" the tick out

Treatment

- Disinfect the area with alcohol or a similar antiseptic after removal
- Notify the Safety Competent Person of the embedded tick
- For several days to several weeks after removal of the tick, look for the signs of the onset of Lyme disease, such as a rash.
- No further treatment is necessary for ticks embedded <48 hours.
- If other signs or symptoms of Lyme are observed (fever/chills, aches, and pains), then notify the Safety Competent Person and seek medical attention

The following table summarizes safety controls to reduce the hazards associated with ticks and mites.

| Elimination | Substitution | Engineering | Administrative | PPE |
|---|--------------|---|--|--|
| Use mechanical equipment to remove overgrown vegetation | | Remove overgrowth and excessive vegetation from walkways and work areas (provide safe access) | Train personnel on tick and mite prevention. Areas of vegetation overgrowth and/or debris piles should be considered "high risk" areas | Wear light-colored long sleeved shirt tucked into pants. Tuck pant legs into socks |

| Elimination | Substitution | Engineering | Administrative | PPE |
|-------------|--------------|-------------|---|---|
| | | | Perform frequent tick checks in the field and a thorough tick check after completing work activities | Apply Permethrin to clothes and DEET (20% or more) to exposed skin |
| | | | Call licensed pesticide contractors to remove infestations of bees, wasps, fire ants, etc. | |

4.10.2 Insect Bites/Stings

Stinging/biting insects at the Site include spiders, wasps, and bees. Contact with these insects may result in project personnel experiencing adverse health effects that range from being mildly uncomfortable to being life-threatening. Therefore, insects present a serious hazard to project personnel, and extreme caution must be exercised whenever Site and weather conditions increase the risk of encountering stinging insects. Some of the factors related to stinging insects that increase the degree of risk associated with accidental contact are as follows:

- The nests for these insects are frequently found in remote wooded or grassy areas or equipment staging areas where equipment has not been moved recently.
- Some people are hypersensitive to the toxins injected by a sting, and when stung, experience a violent and immediate allergic reaction resulting in a life-threatening condition known as anaphylactic shock. Anaphylactic shock manifests itself very rapidly and is characterized by extreme swelling of the body, eyes, face, mouth, and respiratory passages.
- The hypersensitivity needed to cause anaphylactic shock, can in some people accumulate over time and exposure, therefore even if someone has been stung previously and not experienced an allergic reaction, there is no guarantee that they will not have an allergic reaction if they are stung again
- Spider bites generally only cause localized reactions such as swelling, pain, and redness. However, bites from a Black Widow or Brown Recluse, or if you are allergic to spiders, can cause symptoms that are more serious.
- If a worker knows that they are hypersensitive to bee, wasp, or hornet stings, or other insects, they must inform the Safety Competent Person prior to site work. Persons who have been prescribed epi-pens by their physician must have an epi-pen on the Site.
- Inspect any clothing or PPE that has been left for a period of time prior to putting it on. Shake out the clothing and inspect the inside of safety shoes/boots prior to putting them on
- Nests in active work areas must be eradicated. Small nests may be handled by Site personnel
 using consumer-type insecticide. A pest control contractor should be hired to handle large or
 difficult to reach nests.

The following table outlines safety controls to reduce the risk of hazards associated with stinging/biting insects.

| Elimination | Substitution | Engineering | Administrative | PPE |
|---|--------------|---|---|--|
| Use mechanical equipment to remove overgrown vegetation | | Remove overgrowth and excessive vegetation from walkways and work areas (provide safe access) | Train personnel on stinging/biting insect prevention. Areas of vegetation overgrowth and/or debris piles should be considered "high risk" areas | Wear light-colored long sleeved shirt tucked into pants. Tuck pant legs into socks |
| | | Eradicate nests in the work area as outlined above. | Instruct personnel to inspect/shake out clothing and work boots that have been left for a period of time. | Apply Permethrin to clothes and DEET (20% or more) to exposed skin – NOTE this will not repel bees/wasps |
| | | | Instruct employees who are hypersensitive to insect bites/stings to carry their epipen while on site | |

4.10.3 Venomous Snakes

There are four species of venomous snakes in Illinois, they are:

- Copperhead
- Cottonmouth Water Moccasin
- Timber rattlesnake
- Eastern Massasauga

Generally, these snakes are found in the southern one-third of the state, with the Cottonmouth Water Moccasin found mostly in the southernmost portions of Illinois. Snakes are generally found in tall grass, wood piles, or other covered areas. Snakes are generally not aggressive towards humans, but if they are encountered avoid the snake and do not provoke it. If bitten by a snake that may be venomous seek medical treatment.

The following table outlines safety controls to reduce the hazard associated with venomous snakes.

| Elimination | Substitution | Engineering | Administrative | PPE |
|---|--------------|---|--|---|
| Use mechanical equipment to remove overgrown vegetation | | Remove debris piles, overgrowth and excessive vegetation from walkways and work areas (provide safe access) | Train personnel on the identification of venomous snakes. Areas of vegetation overgrowth and/or debris piles should be considered "high risk" areas | If working in area with snakes cannot be avoided, wear snake chaps |
| | | | Instruct personnel to not disturb snakes if they identify one in their work area | |

| Elimination | Substitution | Engineering | Administrative | PPE |
|-------------|--------------|-------------|--------------------|-----|
| | | | Use caution when | |
| | | | moving staged | |
| | | | tools or materials | |
| | | | into which snakes | |
| | | | may have moved | |

4.10.4 Poisonous Plants and Plant Hazards

Poison ivy and poison oak may be present at the Site. Poison ivy thrives in all types of light and usually grows in the form of a trailing vine; however, it can also grow as a bush and can attain heights of 10 feet or more. Poison ivy has pointed leaves that grow in clusters of three. Poison oak resembles poison ivy except that the poison oak leaves are more rounded rather than jagged like poison ivy, and the underside of poison oak leaves are covered with hair.

The skin reaction associated with contacting these plants is caused by the body's allergic reaction to toxins contained in oils produced by the plant. Becoming contaminated with the oils does not require contact with just the leaves. Contamination can be achieved through contact with other parts of the plant such as the branches, stems or berries, or contact with contaminated items such as tools and clothing. The allergic reaction associated with exposure to these plants will generally cause the following signs and symptoms:

Symptoms

- Blistering at the site of contact, usually occurring within 12 to 48 hours after contact and in many cases, persons experience almost immediate irritation.
- Reddening, swelling, itching, and burning at the site of contact.
- Pain, if the reaction is severe.
- Conjunctivitis, asthma, and other allergic reactions if the person is extremely sensitive to the poisonous plant toxin.

Prevention

- The best treatment appears to be removal of the irritating oil before it has had time to cause inflammation by wiping exposed skin with rubbing alcohol followed by washing with soap and water.
- A visual Site inspection and identification of the plants should be completed prior to starting work so that all individuals are aware of the potential exposure. Avoid contact with any poisonous plants on the Site, and keep a steady watch to identify, report, and mark poisonous plants found on the Site.
- · Avoid contact with, and wash daily, contaminated tools, equipment, and clothing.
- Barrier creams (Ivy Block®) and orally administered desensitization may prove effective and should be tried to find the best preventive solution.
- Keeping the skin covered as much as possible (i.e., long pants and long-sleeved shirts) in areas where these plants are known to exist will limit much of the potential exposure.
 PFAS-free spun polypropylene coveralls or Tyvek® may be worn to prevent contact of skin and clothes with poison ivy.

The following table outlines safety controls to mitigate the hazards associated with poisonous plants.

| Elimination | Substitution | Engineering | Administrative | PPE |
|---|--------------|---|---|---|
| Use mechanical equipment to remove overgrown vegetation | | Remove overgrowth and excessive vegetation from walkways and work areas (provide safe access) | Train personnel on the identification of poisonous plants | Wear pants and long sleeves when working in overgrown areas |
| | | | Instruct personnel to avoid areas where poisonous plants have been identified | Consider the use of a coverall when working in areas where these plants are present, especially for hypersensitive employees. |
| | | | Provide isopropyl alcohol along with soap and water to remove oils from skin, tools, and equipment. | |

4.11 Working Alone

As outlined in Section 4.1, working alone while on an ash pond must be pre-approved by the POC. Working alone is prohibited for tasks deemed to be high risk by IPGC including, but not limited to, handling highly hazardous chemicals (sulfuric acid), work over/near water, excavation and trenching, hot work (grinding, welding and torch cutting), and elevated work that requires personal fall arrest. Third-party contractors are responsible for identifying potential high-risk tasks in their Safety and Health Plan and requiring that a buddy system be implemented while high risk work is performed. The buddy must be located in a safe area but may perform other tasks that do not prevent observing the person performing high risk work. Working alone may occur on and around other parts of the Site when there is no drowning hazard or risk of severe injury due to high-risk work.

| Elimination | Substitution | Engineering | Administrative | PPE |
|-------------|--|--|---|-----|
| | Modify work methods by substituting lower hazard methods for high hazard methods | Varies depending on the hazard, but for example, could include installing guardrails (temporary or permanent) which mitigates a fall hazard reducing the risk to levels where working alone may be permitted | Prohibit working alone on ash ponds and for other high hazard tasks without prior approval from the POC | |
| | | | Implement a buddy system whenever feasible (required for high hazard work) | |

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| Elimination | Substitution | Engineering | Administrative | PPE |
|-------------|--------------|-------------|--|-----|
| | | | Implement a worker check-in, emergency alerting, and monitoring system | |

5. HAZARD COMMUNICATION

As required by 35 I.A.C. § 845.530, the OSHA HAZWOPER standards (29 C.F.R. § 1910.120 and 29 C.F.R. § 1926.65) and OSHA Hazard Communication Standard, site personnel, subcontractors, and visitors must be informed of chemical hazards associated with their work area. The information in this section is based on:

- Recommendations in the most recent "NIOSH Pocket Guide to Chemical Hazards" by the Department of Health and Human Services, Centers for Disease Control and Prevention, and the NIOSH Pocket Guide.
- Requirements set forth in the OSHA regulations from as defined in Chapter 17 of 29 C.F.R. § 1910.1200(c) for all hazards not otherwise classified.

5.1 Coal Combustion Residuals

Primary exposure to CCR is through inhalation and skin contact. CCR is typically a fine, black, grey, or tan particulate. CCR is comprised of several components. The following table outlines the components of the CCR. The exact percentage of each component will vary based on the type of ash and location at the surface impoundment.

| Chemical | Percentage | PEL | IDLH | ACGIH TLV | Symptoms of Exposure & Health Effects |
|-----------------------|-------------------|--|--------------------------|---|--|
| Crystalline Silica | 20-60% (total) | 0.05 mg/m ³ (respirable) | 25 mg/m³ (respirable) | 0.025 mg/m ³ (respirable) | Cough, dyspnoea (breathing difficulty), wheezing; decreased pulmonary function, progressive respiratory symptoms (silicosis); irritation eyes; [potential occupational carcinogen] |
| Iron oxide | 1-10% | 5 mg/m ³ | 2500 mg/m ³ | 5 mg/m ³ | Benign pneumoconiosis with X-ray shadows indistinguishable from fibrotic pneumoconiosis (siderosis) |
| Calcium oxide | 10-30% | 5 mg/m ³ | 25 mg/m ³ | 2 mg/m ³ | irritation eyes, skin, upper respiratory tract; ulcer, perforation nasal septum; pneumonitis; dermatitis |
| Titanium dioxide | <3% | 15 mg/m³ | ND | 10 mg/m ³ | Lung fibrosis; [potential occupational carcinogen] |
| Aluminosilicates | 10-60% | irrit | | irritation eyes, skin, throat, upper | |
| Magnesium oxide | 2-10% | 15 mg/m³ (PNOR) | ND | 10 mg/m³ | respiratory system |
| Magnesium dioxide | <2% | - (FNOK) | | (PNOR) | |
| Phosphorous pentoxide | ≤2% | | | | |
| Sodium oxide | 1-10% | | | | |
| Potassium oxide | ≤1% | | | | |
| Bromide salt | <0.1% | | | | |

Footnotes:

All values are 8-hour time-weighted averages (TWAs) unless otherwise indicated.

- PEL: Permissible Exposure Limit, the concentration an employee may be exposed to for an 8-hour work day for a 40-hour work week for which nearly all employees may be repeatedly exposed without adverse health effects.
- IDLH: IMMEDIATELY Dangerous to Life and Health, contaminant concentration which present the possibility for severe health consequences if exposed to the IDLH concentration without the appropriate personal protective equipment (PPE).
- ACGIH TLV: American Conference of Governmental Industrial Hygienists Threshold Limit Value
- mg/m³ = milligrams per cubic meter of air
- PNOR: Particulates Not Otherwise Regulated
- ND: Not Determined

5.2 Safety Data Sheets

Pursuant to 35 I.A.C. § 845.530(b)(3), IPGC will provide Safety Data Sheets (SDSs) to all employees, contract workers, and third-party contractors for the CCR located at the Site. Third-party contractors will incorporate SDSs in their Safety and Health Plan and provide SDSs to IPGC prior to bringing a material on site. SDSs are provided in Appendix E.

5.3 Signage

The absence of any of the following signage does not mean that a potential hazard does not exist. Signage will be posted by IPGC, but employees, contract workers, and third-party contractors must remain vigilant for changing site conditions.

To aid in hazard communication and pursuant to 35 I.A.C. § 845.530(f), IPGC will post the following signs at the Site:

- Signs identifying the hazards of CCR, including dust inhalation when handling CCR.
- Signs identifying unstable CCR areas that make the operation of heavy equipment hazardous.
- Signs identifying the necessary safety measures and necessary precautions, including the proper use of PPE.

The following signs may also be posted at the CCR units to aid in hazard communication:

• Overhead electrical lines that may be struck by heavy equipment of vehicles will have signs warning drivers of their presence.

6. EMERGENCY RESPONSE PLAN

This emergency response section details actions to be taken in the event of site emergencies. This section is consistent with the CPP Emergency Action Plan. All personnel on site must be familiar with emergency signals and the content of this section.

6.1 Emergency Phone Numbers & Notifications

| Emergency Number | | | |
|-------------------------------------|------------------------------|--|--|
| Site Address Emergency Phone Number | | | |
| 134 Cips Lane | 911 | | |
| Coffeen, IL | | | |
| | Security Guard: 217-534-2363 | | |

| Medica | I Treatment |
|--------------------------|--------------|
| Local Hospital | Phone Number |
| Hillsboro Area Hospital | 217-532-6111 |
| 1200 East Tremont Street | |
| Hillsboro, IL 62049 | |

| Incident Notifications | | | | |
|---------------------------------------|-------------|----------------|--|--|
| Title | Name | Contact Number | | |
| Primary POC / Plant Manager | Scott Bell | 217-248-7720 | | |
| Secondary POC / Environmental Manager | John Romang | 217-341-7319 | | |

6.2 Evacuation Signal

Upon hearing verbal notification (cell phones and radios) to evacuate all personnel will leave the work area and proceed to the muster point.

6.3 Muster Point

The muster point for the Site is located at the Plant Closure/Environmental Office. The severe weather shelter location is the storm shelter located next to the Security Office. The muster point and severe weather locations will be reviewed during the Site Orientation Training.

6.4 Calls for Emergency Support

In the case of an emergency site personnel will call the facility emergency phone number. Security will coordinate the arrival of on-site emergency personnel. The individual calling for emergency support will briefly explain the nature of the emergency and site conditions as follows:

- Indicate his/her name
- · Location of emergency
- Description of emergency conditions that may require special rescue equipment, such as confined spaces, excavations, and elevated work platforms
- · Potential chemical hazards and recommended PPE

6.5 Fire & Explosion Response Plan

Trained site personnel may respond to incipient stage fires using a 20-pound Type ABC dry chemical fire extinguisher or hose. An incipient stage fire is a fire which is in the initial or beginning stage and which can be controlled or extinguished by portable fire extinguishers, Class II standpipe or small hose systems without the need for protective clothing or breathing apparatus. Personnel shall only attempt to extinguish the fire if it is safe to do so.

A fire that CANNOT be readily extinguished with a fire extinguisher will require evacuation of the work area personnel to Muster Point areas per this Safety and Health Plan. If personal injuries result from any fire or explosion, the procedures outlined in the Personal Injury Response Plan will also be followed.

All fires or explosions must be reported to the contacts outlined in Section 6.1 of this Safety and Health Plan.

6.6 Injury Response Plan

Treatment for minor injuries will be provided on site using available first aid supplies and personnel trained in first aid. All third-party contractors must have at least one individual on site who is trained in first aid, CPR, and AED use. Third-party contractors must provide their own first aid kits and AED. For minor injuries that are not life-threatening but require further medical attention, employees should be treated by occupational physicians at occupational clinics whenever possible. Treatment of minor injuries by emergency room or personal physicians should be avoided. When injured workers are released back to work with restrictions, all subcontractors are expected to accommodate those restrictions.

Emergency medical incidents include puncture wounds to the head, chest, and abdomen, serious head and spinal cord injuries, and loss of consciousness must be treated at the hospital emergency room listed in Section 6.1 of this Safety and Health Plan.

All injuries must be reported to the contacts outlined in Section 6.1 of this Safety and Health Plan.

6.7 Spill Response Plan

In general, IPGC employees, contract workers, and third-party contractors are trained and equipped to handle small spills associated with their work. Third-party contractors must include an approved spill response plan in their Safety and Health Plan. Site personnel will generally respond to spills as follows:

- Stop the leak immediately if it can be done without directly contacting the leaking material.
- Remove or stop all ignition sources (hot work, generators, etc.) that are within 25 feet of any part of the spill.
- On-site personnel should immediately secure the area to prevent unauthorized entry into the spill area.
- Although not likely given the anticipated types of spills, site personnel must immediately initiate evacuation if a spill may cause an explosion, death, or serious injury.
- Site personnel may only respond to incipient stage fires regardless if such fires are associated with a spill.
- PPE for spills to open areas generally requires Modified Level D PPE (poly-coat Tyvek®, nitrile gloves, and boot covers or boot decontamination). Over-boots or boot covers may also be used if persons cleaning the spill would have to walk on spilled materials. Latex gloves are not acceptable and will degrade with exposure to petroleum products.

6.8 CCR Spill or Release Response Plan

Response to minor or incidental spills of CCR will be managed as outlined in the General Spill Response Plan. An incidental release is a release of a hazardous substance which does not pose a significant safety or health hazard to employees in the immediate vicinity or to the employee cleaning it up, nor does it have the potential to become an emergency within a short time frame. Incidental releases are limited in quantity, exposure potential, or toxicity and present minor safety or health hazards to employees in the immediate work area or those assigned to clean them up. An incidental spill may be safely cleaned up by employees who are familiar with CCR. Response to major releases of CCR will be in accordance with the Site Emergency Response Plan.

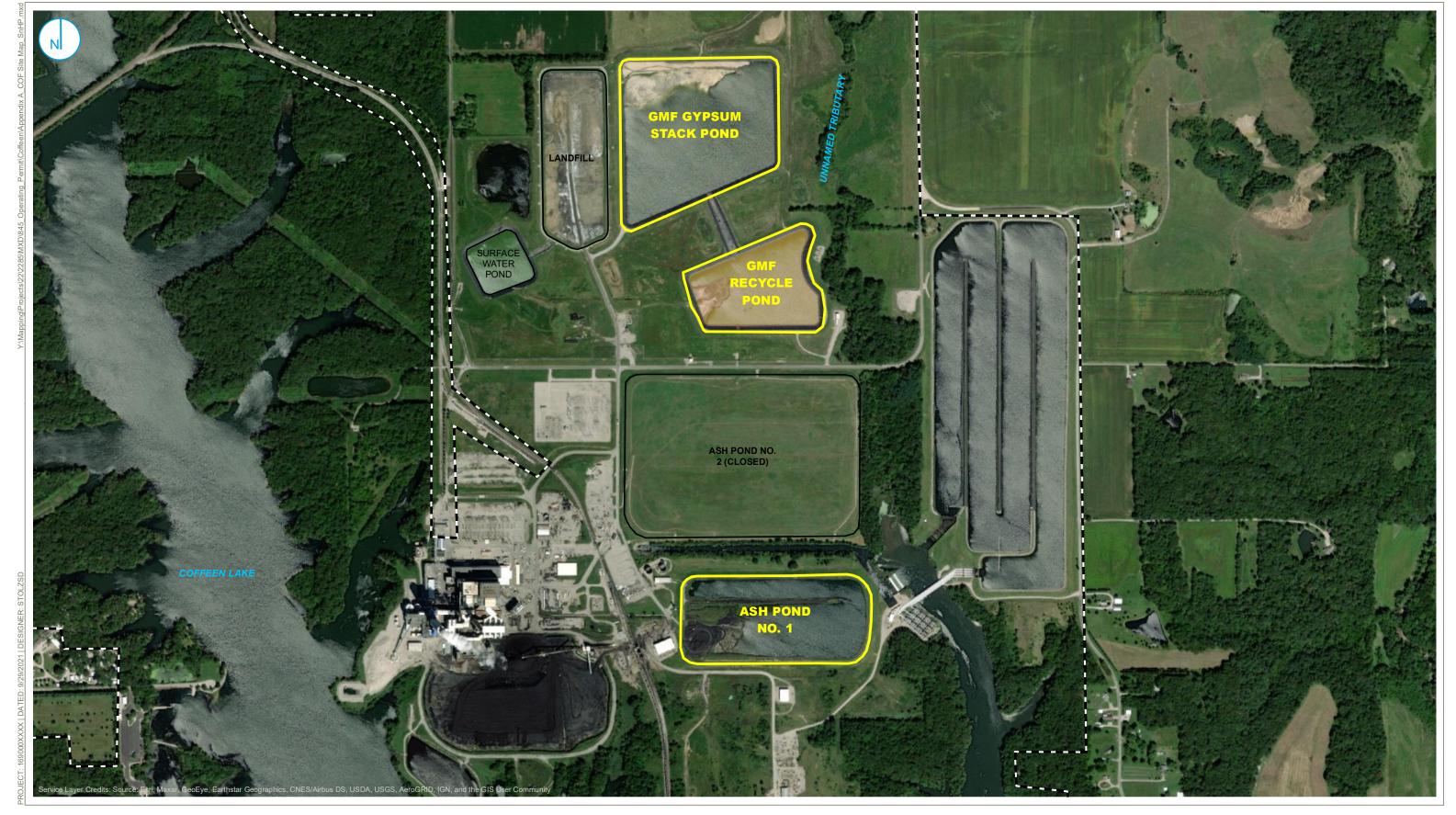
6.9 Ash Pond Rescue

Ash ponds may be unstable and represent an engulfment hazard if persons and equipment traverse the surface, berms, or other unstable areas. Special training is required on behalf of emergency responders to retrieve persons and equipment who become trapped in unstable ash. **Untrained persons must not enter unstable areas** in an attempt to conduct rescue because of the significant potential that they will also become victims. Call the CPP emergency number and state that an "ash pond rescue" is required. The CPP emergency contact will notify the designated service to perform the ash pond rescue. On-site personnel should remain on stand-by to support the ash pond rescue team as necessary.

6.10 Incident Reporting

All incidents must be reported to the contacts outlined in Section 6.1 of this Safety and Health Plan. An Incident Report must be completed for all injuries, illnesses, spills, fire, explosion, or property damage. The absence of an injury does not preclude the need to complete an Incident Report as such incidents will be classified as "near miss" or "other." It will include, but is not limited to, the nature of the problem, time, location, and corrective actions taken to prevent recurrence.

APPENDIX A SITE MAP



PART 845 REGULATED UNIT (SUBJECT UNIT)

SITE FEATURE PROPERTY BOUNDARY **SITE MAP**

APPENDIX A

RAMBOLL AMERICAS ENGINEERING SOLUTIONS, INC.

APPENDIX B SAFETY AND HEALTH PLAN ACKNOWLEDGMENT FORM

SAFETY AND HEALTH PLAN ACKNOWLEDGEMENT FORM

I HEREBY CERTIFY THAT I HAVE READ AND UNDERSTOOD ALL HEALTH AND SAFETY PROCEDURES AS STATED HEREIN:

| Name and Affiliation (printed) | | Signature | Date |
|--------------------------------|----------|-----------|------|
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APPENDIX C DRUG SCREEN POLICIES AND SUPPLEMENTAL TERMS



Drug and Background Investigations

Contractor is solely responsible for ensuring that all members of Contractor Project Team have completed and passed all drug and alcohol tests and background investigations required under this Attachment and under Contractor's own programs before assigning such personnel to perform Work. Contractor is also solely responsible for ensuring that such testing and investigations are performed in accordance with all applicable laws.

- **1. Required Investigations.** Except as otherwise required by applicable law, Required Investigations shall consist of all of the following:
 - 1.1 a 7-panel drug screening;
 - **1.2** a background investigation that includes a criminal records check in all counties where the applicable person has resided for at least the last seven (7) years;
 - **1.3** a third-party verification of previous employment and the highest education level completed by the applicable person;
 - 1.4 a check of the National Sex Offender Registry and Terrorist Watch List (Denied Parties); and
 - **1.5** a check of Motor Vehicles Record (if work to be performed by the applicable person requires driving as part of the defined duties).
- 2. Notices to Tested Persons Regarding Background Checks. All background checks will be conducted in compliance with applicable provisions of the Fair Credit Reporting Act.
- 3. Forms and Testing Organization for Drug Tests. Except for those positions subject to Department of Transportation ("DOT") drug and alcohol testing regulations, all drug testing shall be performed using the Universal Toxicology four part "Non-DOT" Chain of Custody and Request Form with white and blue top page, and shall be conducted by an independent third-party organization.
- **4.** Pass/Fail Standards Background Checks. A person shall be deemed to have failed the applicable background check if:
 - **4.1** information is reported through the background check process indicating that such person has failed to disclose or misrepresented information requested at any time about such a person's criminal background history; or
 - **4.2** such person has ever committed any felony constituting a violent crime, crime against a person, sexual offense or fraud; or
 - **4.3** such person has committed any other felony, or has been incarcerated for a felony, within ten (10) years prior to the date of such background check (i.e., for these felonies there must be a ten (10) year lapse in time from the later of the commission and the end of any period of incarceration); or
 - **4.4** such person has committed any misdemeanor that:
 - **4.4.1** involves violence that is sexually related; or

- **4.4.2** consists of a DUI that is the second (or more) DUI in the last two (2) years prior to the date of the background check; or
- **4.4.3** consists of a theft-related offense; <u>provided</u> that there can be no more than one theft by check and it must have been for an amount less that \$100; or
- **4.4.4** consists of any drug-related misdemeanor committed at any time within forty-eight (48) months prior to the date of the background check.
- **4.4** For purposes of both felonies and misdemeanors, a person is deemed to have committed the applicable offense if he/she is convicted or enters a plea of guilty or nolo contendere for such offense (to include, without limitation, sentences of probation and deferred adjudication).
- 5. Pass/Fail Standards Drug Tests. A person shall be deemed to have failed the applicable drug test if any of the following maximum cut-off levels are exceeded, unless there is a legitimate medical explanation for the presence of a tested substance at or above the applicable cut-off level:

5.1 Amphetamines 500ng/mL

5.2 Barbiturates 150ng/mL

5.3 Benzodiazepines 150ng/mL

5.4 Cocaine 150ng/mL

5.5 Marijuana 150ng/mL

5.6 Opiates 2000ng/mL

5.7 Phencyclidine 25ng/mL

For any positions subject to DOT drug and alcohol testing requirements, testing shall be conducted according to the applicable DOT panel and cutoff levels.

6. Other Requirements.

- **6.1** Background checks and drug tests will be paid for by Contractor without reimbursement by Company.
- **6.2** Contractor will keep background checks and drug test records while the applicable persons are working pursuant to this Agreement and for three (3) years thereafter.
- **6.3** Upon request, Contractor will provide a certification to Company that no person required hereunder to pass a background check or drug test has failed such investigation or test. Contractor will not provide the specific results of the background check or drug test of any individual to Company.
- **6.4** If any person required under this Agreement to pass a background check or drug test fails such check or test, Contractor will not report the specific results of such check or test to Company and will not allow such individual to perform any Work for Company. Although such person may not be assigned to perform any Work for Company, nothing in this Attachment requires Contractor to take any other action with respect to such person's employment with Contractor.



Supplemental Terms for Onsite Services

1. SAFETY

- 1.1 Contractor agrees that any safety-related assistance or initiatives undertaken by Company will not relieve Contractor while on Company Property from responsibility for the implementation of, and compliance with, safe working practices, as developed from their own experience, or as imposed by law or regulation, and will not in any way, affect the responsibilities resting with Contractor under the provisions of any agreement to which these policies are attached and to meet all safety requirements as specified by the Occupational Safety & Health Administration (OSHA), the Mine Safety Health Administration (MSHA), including the "Mining Contractor Safety Reference Handbook" located at http://www.vistraenergy.com/wp-content/uploads/2016/12/Contractors-Safety-Handbook Final-MC-08262016.pdf, the Department of Transportation (DOT) and any other applicable state or federal safety and health laws or regulations.
- 1.2 In the event that a material safety data sheet, warning label, or other documentation concerning the use of hazardous chemicals at any property owned or controlled by Company or any of its affiliates (collectively, "Company Properties"), applies to any materials or equipment provided by Contractor as an aspect of the Work, such documentation will be provided by Contractor to Company prior to the commencement of any such Work.
- 1.3 Contractor will report to Company all accidents involving personal injuries (including death) and damage to property occurring directly or indirectly as a result of the Work performed by Contractor hereunder immediately, but in no event, no later than 24 hours after the occurrence of any such accident. Any accident or incident occurring directly or indirectly as a result of the Work which Contractor must report to a regulatory agency (e.g. OSHA, MSHA, TCEQ) must also be reported to Company immediately following notification to the regulatory agency.

2. SECURITY

- 2.1 It will be the affirmative duty of Contractor to ensure that Contractor Group assists in carrying out all security measures, to include reporting all information or knowledge of matters adversely affecting security to Company's designated security personnel.
- 2.2 Company reserves the right to exclude any of Contractor's employees from any Company Property by denial of access, suspension or revocation of access authorization, preemptory expulsion, or by any other means, without notice or cause. Former Company employees, and any of Contractor's employees who previously have been excluded from any Company Property, may be brought onto Company property or facilities only if prior approval from Company is obtained. If Contractor terminates a member of Contractor Group performing Work on Company's premises, Contractor shall inform Company immediately, but in no event, no later than twenty-four (24) hours after such employee is terminated in order for Company to remove access to Company Property for such employee.
- 2.3 Company measures may also include investigations, whether by Company or law enforcement officials. Contractor agrees to cooperate in such investigations and understands that Company

reserves the right to require anyone in Contractor Group to authorize appropriate agencies to release his or her criminal records to Contractor as a condition of either initial or continued permission for access to any Company Property. Investigations may include searches of Contractor Group. Such searches may include searches of facilities assigned to Contractor Group, search of all Company Property areas and property at such Company Property areas, searches of including, but not limited to, offices, lockers, desks, lunch boxes, packages and motor vehicles (regardless of ownership). Without limiting the foregoing, Contractor acknowledges and agrees that all members of Contractor Group, to the extent that Company reasonably determines that such members require security badge access prior to entering onto any Company Property, shall be required to comply with Company's standard security badge requirements, including without limitation a background check to be performed by Company.

3. ISNETWORLD

- 3.1 Contractor agrees to maintain at Contractor's expense a subscription with ISNetworld (www.ISNetworld.com), Company's safety compliance program or any replacement program therefor, as directed by Company, for the Term of the Agreement. Contractor shall also furnish ISNetworld with any information requested by ISNetworld relating to ISNetworld's evaluation of the Contractor's safety program and practices. As a minimum, requested documents will be related to safety, health, and insurance (i.e., regulatory required training, certifications, safety plans, safe and secure workplace practices, insurance certificates, etc.), OSHA and MSHA injury rates and Experience Modification Rate (EMR).
- 3.2 Contractor has and during the performance of this Agreement shall continue to report full, complete and accurate information to ISNetworld concerning Contractor's employees.
- 4. MATERIALS, EQUIPMENT AND LABOR. Contractor will be solely responsible for the proper storage, transportation and disposal of any product or waste, other than sandblasting waste, used or generated in connection with the Work in accordance with all applicable Environmental Laws. Contractor will dispose of all waste materials, other than sandblasting waste, at an off-site disposal facility approved for such waste materials pursuant to applicable Environmental Laws and will complete and sign all waste manifests as the generator of such waste. Company will be responsible for the storage, transportation and disposal of any sandblasting waste generated during the performance of the Work.

5. CONDITIONS AFFECTING WORK

- 5.1 Contractor will investigate and acquaint itself with the conditions affecting the Work, including but not limited to those related to the transportation, disposal, handling and storage of materials and waste; availability of labor, water, electric power and roads; the uncertainties of weather, river stages or similar physical conditions at the site; the conformation and condition of the ground; and the character of equipment and facilities needed preliminary to and during prosecution of the Work. Contractor has satisfied itself as to the character, quality and quantity of surface and subsurface materials or obstacles to be encountered. Contractor's failure to acquaint itself with any conditions affecting the Work or any available related information will not relieve it from responsibility for properly estimating the difficulty or cost of successfully performing the Work.
- 5.2 Contractor assumes full responsibility for investigating conditions and determining the existence and magnitude of any hazards to the physical well-being of property of Contractor, the employees, agents, and servants of Contractor, or any other person or entity who is or may become involved in

the performance of Work, and any and all other persons in the vicinity of the Work. Contractor will advise all of the above-specified persons or entities of any hazards relating to Work, and will ensure that those persons or entities are advised of and fully understand the nature of the hazards and safety precautions that can be taken to eliminate or minimize dangers relating to the hazards.

- 5.3 Contractor will provide information to Company regarding hazardous chemicals and/or consumable products that contain constituents listed in 40 CFR 372.65 used at any Company Property. Contractor will report the amount of such material carried on and off the site, the amount actually used and the manner of use. Contractor will provide the maximum quantity of the material stored on site at any one time and if a waste material was collected, where it was disposed of (location name and address). Contractor will provide information on the amount of material used for the previous calendar year by the first of February.
- 5.4 Contractor will use its best efforts to ensure that the Work is performed so as to minimize any adverse impact upon natural resources and the environment and will use best industry practices in this regard at all times.
- 5.5 Contractor acknowledges and agrees that all members of Contractor Group performing Work at any Company Generation or Mining Property are required to view Company's "Contractor/Visitor Safety Orientation" video (in the case of Company Generation property), when applicable, and to read and adhere to Company's "Contractor/Visitor Safety Booklet" (in the case of Company Mining property) prior to performing any Work at any Company Generation or Mining Property.
- 5.6 Contractor will immediately notify Company as soon as Contractor has reason to believe that Contactor, or any employee or other person performing the Work, is not or may not be performing the Work in compliance with applicable Environmental Laws. Contractor will provide Company with written notice to Company of such actual or potential non-compliance within three (3) days following the discovery thereof. Contractor will take immediate steps to ensure compliance with all applicable Environmental Laws and will, if directed by Company, cease all Work until authorized by Company to resume the Work.
- 5.7 Contractor will report to Company all accidents involving personal injuries (including death) and damage to property occurring directly or indirectly as a result of the Work performed by Contractor hereunder immediately, but in no event, no later than 24 hours after the occurrence of any such accident. Any accident or incident occurring directly or indirectly as a result of the Work which Contractor must report to a regulatory agency (e.g. OSHA, MSHA, TCEQ) must also be reported to Company immediately following notification to the regulatory agency.

6. WORK SITE PERMITS AND LICENSES

- 6.1 Subject to the following two paragraphs, Contractor will obtain, prior to the commencement of the Work, and provide to Company upon request, all permits, licenses and governmental authorizations, at its sole expense, required for the performance of the Work. Contractor will be solely responsible for maintaining compliance with such permits, licenses and governmental authorizations.
- 6.2 In the event that a storm water discharge permit is required for the performance of the Work, (i)

 Contractor will be responsible for filing a Notice of Intent with respect to the Work, in addition to any

 Notice of Intent that Company may be required to file, and (ii) Contractor will coordinate with

Company in the preparation and execution of a Storm Water Pollution Prevention Plan for the Work Site.

- 6.3 In the event that the performance of the Work involves the handling or abatement of asbestos-containing materials, Contractor will coordinate with Company in the preparation and filing of all required notification forms.
- 7. ACCESS. Should Contractor desire access to the Work Site over any land not controlled by Company, it will, at its sole expense, obtain all proper permits or written permission necessary for that access.
- 8. COMPANY FACILITIES. Contractor will not use Company's sanitary facilities, changehouses, shops, parks, storage buildings, tools, equipment or other facilities unless so directed by Company. Contractor will not discharge, without Company's prior written authorization, any product or waste used or generated in connection with the Work through any (i) Company-permitted outfall, (ii) Company-owned or operated pollution control equipment, or (iii) storm or sanitary sewer located at or in the vicinity of the Work Site. Any request for authorization to discharge will include, at a minimum, either a copy of the Material Safety Data Sheet for the product or a written description of the waste, including a list of the constituents of the waste and the relative concentrations thereof.

9. ENVIRONMENTAL

- 9.1 In the event that Contractor discovers during the performance of the Work any substance at the Work Site that is not the subject of the Work or has not otherwise been identified by Company for Contractor, which substance Contractor has reason to believe is or may be a Hazardous Substance that (i) has been or may be released or spilled into the soil, surface water, or groundwater or in a building or structure, or (ii) consists of asbestos-containing materials, lead-based paint, batteries, thermostats, lighting equipment, or equipment containing polychlorinated biphenyls, Contractor will immediately stop Work and notify Company of the discovery. Contractor will not resume the Work until receiving authorization from Company to do so.
- 9.2 The term "Hazardous Substance" means any product, waste, emission or substance defined, listed or designated as a hazardous or toxic substance, hazardous waste, hazardous material or pollutant by or pursuant to any Environmental Law and includes, but is not limited to, any petroleum-based product, substance or waste, including any additives associated therewith, pesticides, fertilizers, solvents, polychlorinated biphenyls, mercury, lead, lead-based paint, asbestos-containing material or explosives.
- 9.3 Contractor will immediately notify Company in the event of a spill or release of any material which Contractor knows or has reason to believe is a Hazardous Substance, whether onto the ground, into any body of water, a storm or sanitary sewer, or the air, or anywhere on property owned or controlled by Company, including within any building or structure. Contractor will be solely responsible, as may be required by applicable Environmental Laws, for, in consultation with Company, (i) notifying the appropriate governmental agencies of such spill or release caused or permitted by the acts or omissions of Contractor and (ii) for the cleanup and remediation of such spill or release.
- 10. PROTECTION OF HIGHWAYS AND RAILROADS. Contractor will make suitable arrangements with governmental authorities and railroads for the construction of all structures, whether underneath or over roads, railroads or rights-of-way to protect the public from accident or delay. Contractor will repair, at its

own expense, to the satisfaction of the governmental authorities or other owners, all roads, railroads and bridges that may be damaged by, or given undue wear due to the Work.

11. CLEANING UP

- 11.1 Contractor will at all times keep the Work Site free of waste materials or rubbish caused by the Work. After completing the Work, Contractor will remove all its waste materials, rubbish, tools, supplies, equipment and surplus materials from and about the Work Site.
- 11.2 If Contractor fails to keep the Work Site clean or to clean up after completing the Work, Company may do so and charge all costs of cleaning up to Contractor. Those costs may be deducted from the final payment to Contractor.
- 12. COLLATERAL WORK. Company and other contractors may be working at the Work Site. Company reserves the right to coordinate the performance of Contractor's Work with the work of others. Contractor will cooperate with and will not delay, impede or otherwise impair the work of others. Company does not guarantee Contractor continuous uninterrupted access to the Work Site, but will provide such access as good construction practices will allow, considering the other activities in the area.
- 13. ALCOHOLIC BEVERAGES, DRUGS AND WEAPONS. Contractor will inform all members of Contractor Group who may be involved in the performance of any Work of the following Company rules relating to alcoholic beverages, drugs and weapons, with which all personnel are expected to comply:
- Bringing, attempting to bring, possessing, using or being under the influence of intoxicants, drugs, or narcotics while on any Company Property, including but not limited to parking areas, is prohibited. Possessing alcoholic beverages in sealed containers is permitted, however, in designated parking areas.
- 13.2 Prescription or over-the-counter medications that could affect the performance of safety-sensitive work are allowed on Company Property only if they have been previously cleared by Contractor. Contractor must confirm that the medication and dosage do not impair an individual's ability to perform safety-sensitive work before clearing the individual to perform such work while under the influence of the medication.
- 13.3 Bringing, attempting to bring, possessing or using firearms, whether classified as legal or illegal, while on any Company Property, including but not limited to buildings, parking areas, recreation facilities, equipment and vehicles, is prohibited, unless otherwise required by applicable law. Use or possession of firearms for specific situations is permitted if approved by function or higher level management of Company.
- 13.4 Off-the-job involvement with intoxicants, illegal drugs, or illegal narcotics that adversely affects Company's business, to include impairing the individual's ability to perform his job or the public trust in the safe operation of Company, is prohibited.
- 13.5 Any conduct on any Company Property which is in violation of any state or federal law or regulation is considered a violation of these rules and a breach of any agreement to which these policies are attached.

- 13.6 In order to enforce these rules, all individuals with access to any Company Property as well as the vehicles, offices, lockers and any personal belongings of such individuals on any Company Property are subject to search by Company and its agents, to include security representatives appointed or employed by Company. Individuals may be required to take a blood, urinalysis or Breathalyzer test, or submit to other recognized investigatory tests or procedures as are deemed appropriate or necessary by Company in the investigation of a violation of these rules.
- 14. TITLE AND RIGHT. Nothing in the Agreement will vest Contractor with any right of property in materials used after they have been attached to or incorporated into the Work, nor materials for which Contractor has received full or partial payment. All those materials, upon being so attached, incorporated or paid for, will become the property of Company. Any gravel, sand, stone, minerals, timber or other materials excavated, uncovered, developed or obtained in the Work, or on any land belonging to Company may be used, in the performance of the Work, provided such materials meet the requirements of this Agreement. Any objects or natural materials or animals excavated or exposed that may have historical significance or constitute a threatened or endangered species must be brought to the attention of Company.

15. PROTECTION AGAINST LIENS AND ENCUMBRANCES

- 15.1 Contractor will not at any time permit any lien, attachment or other encumbrance ("Encumbrance") by any person or persons whosoever or by reason of any claim or demand against Contractor to be placed or remain on the property of Company, including, but not limited to, the Work Site upon which Work is being performed or equipment and materials that are being furnished. To prevent an Encumbrance from being placed on the property of Company, Contractor will furnish during the progress of any Work, as requested from time to time, verified statements showing Contractor's total outstanding indebtedness in connection with the Work.
- 15.2 If Contractor allows any indebtedness to accrue to subcontractors or others and fails to pay or discharge that indebtedness within five (5) days after demand, then Company may withhold any money due Contractor until that indebtedness is paid or pay the indebtedness and apply that amount against the money due Contractor.
- 15.3 If Contractor allows any Encumbrances, whether valid or invalid to be placed on the property of Company, any and all claims or demands for payment to Contractor will be denied by Company until the Encumbrance is removed. If the Encumbrance is not removed immediately, Company may pay that claim or demand and deduct the amount paid, together with all related expenses, including attorneys' fees, from any further payment due Contractor, or at Company's election, Contractor will, upon demand, reimburse Company for the amount paid and all related expenses. Any payment made in good faith by Company will be binding on Contractor.

16. TERMINATION FOR DEFAULT

assignment for the benefit of creditors, or if a receiver should be appointed due to the insolvency of Contractor, or if Contractor should refuse or fail to supply enough properly skilled workmen or proper equipment, materials or services or should fail to make prompt payment to subcontractors, or to pay promptly for materials or labor, or disregard laws, ordinances or the instruction of Company's Contract Coordinator, or if Contractor should refuse or fail to abide by the SOW Construction Schedule or otherwise violate any provisions of the Agreement or SOW, then Company, upon a

determination by Company's Contract Coordinator that sufficient cause exists to justify such action, may, without prejudice to any other right or remedy available to it after giving Contractor seven (7) days' written notice, terminate the Agreement or the SOW and take possession of the Work Site. In the event of such a termination, Company may use all or part of Contractor's equipment and materials and may finish the Work by whatever method Company may deem expedient. In such event, Contractor will not be entitled to receive any further payment hereunder until the Work is finished. If the unpaid balance of the SOW fees will exceed the expense of finishing the Work, including compensation of Company's Contract Coordinator, other Company personnel, third party engineering companies, or other contractors for additional services, such excess will be paid to Contractor. If the expense of finishing the Work will exceed such unpaid balance, Contractor will pay the difference to Company within fifteen (15) days of receiving an invoice for same. The expenses incurred by Company herein, and the damage incurred through Contractor's default, will be determined by Company's Contract Coordinator, in its sole discretion, and such determination will be binding as between the parties.

- 16.2 In the event of a termination under the provisions of this Section 3, Contractor will transfer and assign to Company, in accordance with Company's instructions, all Work, all construction records, reports, permits, data and information, other materials (including all Company-supplied materials), supplies, Work in progress and other goods for which Contractor is entitled to receive reimbursement hereunder, and any and all plans, drawings, sketches, specifications, and information in connection with the Work, and will take such action as may be necessary to secure Company, at Company's sole election, the rights of Contractor under any or all orders and subcontracts made in connection with the Work.
- 16.3 In the event that Company so directs or authorizes, Contractor will sell at a price approved by Company, or retain at a mutually agreeable price, any such materials, supplies, Work in progress, or other goods as referred to in the preceding paragraph. In any event, Company will receive any and all records, plans, drawings, data, permits, specifications, sketches, reports, or other information relating to the Work. The proceeds of any such sale or the agreed price will be paid or credited to Company in such manner as Company may direct so as to reduce the amount payable by Company under this Section 3.

APPENDIX D COVID-19 SITE ENTRY GUIDELINES



COVID-19 Vistra Site Entry Guidelines – *Effective: June 17, 2021* These guidelines are applicable to ALL PERSONNEL entering Vistra work sites.

To enter a Vistra work site, each person must answer the following three questions with a "no" answer and pass the required temperature testing unless they display their Vistra vaccination sticker on their employee badge or hardhat:

Site Entry Questions:

- 1. In the past 10 days, have you tested positive for COVID-19 or are you currently waiting on test results?
- 2. In the past 10 days, have you been within six feet of someone, where masks were not worn, who:
 - a. has tested positive for COVID-19,
 - b. is known to be waiting on test results for COVID-19, or
 - c. is under a quarantine order?
- 3. In the past 10 days, have you or someone who has been within six feet of you where masks were not worn had:
 - a. flu-like symptoms,
 - b. a deep, dry cough,
 - c. recent shortness of breath or difficulty breathing,
 - d. new loss of taste or smell, and/or
 - e. fever of 100 degrees or above?

Temperature Testing:

You must register a temperature between 96- and 100-degrees Fahrenheit as described in the temperature procedures. (see next page for testing procedures)

- If your temperature is below 96 degrees, retest with a different device.
- If your temperature is 100-degrees Fahrenheit or above, retest on another device preferably an ear thermometer, if your temperature still registers 100-degrees Fahrenheit or above you may not enter the site.

Clearance to enter the site:

- If you have answered "no" to all three questions and passed the temperature test, you may enter the site.
- If you have an approved Vistra vaccination sticker, you are cleared to enter the site without the temperature test or answering COVID screening questions.
- If you passed the temperature test **and** answered "Yes" to any of the questions, but have been cleared through VistraTravelerSafety (HR clearance) to enter the Vistra work site for that instance of exposure, testing, or symptoms, you may enter the site.

Anyone *not* cleared to enter the work site must immediately leave the work site and notify their supervisor who will notify HR at VistraTravelerSafety@vistracorp.com for next steps.

Required Temperature Testing Procedures:

All persons entering the site without a Vistra vaccination sticker, who have cleared all questions above, will also submit to temperature testing or self-administer a temperature test as required by the facility management. If a self-administered test is required, then a member of the management team or their designee will witness the testing; however, where that is not practicable, each person must attest that they are only entering the site premises because they have passed the screening questions and temperature test required for entry. Also:

- a. Hats may cause false high temperatures and should not be worn for five minutes immediately preceding a forehead temperature test.
- b. Each person is responsible for ensuring all self-testing materials and areas touched during testing are sanitized.
- c. All personnel should maintain a **distance of at least six feet** from other people during this process or wear required masks.

Temperature Testing Requirements:

- 1. All persons entering the site without a Vistra vaccination sticker must register a temperature between 96- and 100-degrees Fahrenheit. Any such person who has a temperature not within that range or who triggers an alarm on a thermal camera must retest with a different device, preferably an ear thermometer, if available. If the second test registers a temperature of 100 degrees or above:
 - a. That person **may not enter** the Vistra work site and must notify their supervisor, who will notify HR at <u>VistraTravelerSafety@vistracorp.com</u> for next steps.
 - b. If there is significant inconsistency between the two tests, repeat another temperature test and use the two closest readings.
- 2. Anyone who registers a temperature between 96- and 100-degrees Fahrenheit may proceed to their work site.
 - If temperature is below 96 degrees, wait a few minutes and retest with a different device.

Control rooms and communal areas:

All persons entering the site without a Vistra vaccination sticker should maintain at least six-feet distance from other people as much as possible and should wear face coverings when six-feet distance is not feasible. No one should gather in communal areas (including the temperature-testing area) without a Vistra vaccination sticker. Only operators are allowed in control rooms without plant manager approval.

Vistra Vaccination Sticker protocols:

All persons with a valid Vistra vaccination sticker do not have to socially distance or wear masks while at the site. They will also not be required to quarantine as a part of COVID-19 exposures unless exhibiting COVID-19 symptoms. To be eligible for these protocols, each person must have their approved Vistra vaccination sticker easily visible at all times while at work. If someone who has applied for a Vistra vaccination sticker believes they have specific health conditions that may affect the ability to have a full immune response to the vaccination, please consult your health provider prior to working without a mask.

APPENDIX E SAFETY DATA SHEETS



afoty Data Shoot

Bottom Ash SDS Number: 0.0 Revision Date: 03/2018

Safety Data Sheet Section 1

1.1 Product Identifier

| Product Name/Identification: | ASTM Bottom Ash |
|------------------------------|---|
| Synonyms: | Ash; Ashes; Ash residues; Ashes, residues, bottom; Bottom ash; Bottom ash residues; Coal Fly Ash; Pozzolan; Waste solids. |
| Formula: | UVCB Substance |

Identification of the Substance and of the Supplier

1.2 Relevant Identified Uses of the Substance or Mixture and Uses Advices Against

| Relevant Identified Uses: | Component of wallboard, concrete, roofing material, bricks, cement kiln feed. |
|---------------------------|---|
| Uses Advised Against: | None known. |

1.3 Details of the Supplier of the SDS

| Manufacturer/Supplier: | Dynegy, Inc. |
|-----------------------------|-------------------------------|
| Street Address: | 601 Travis Street, Suite 1400 |
| City, State and Zip Code: | Houston, TX 77002 |
| Customer Service Telephone: | 800-633-4704 |

Preparation Date: 02/23/2018



Bottom Ash SDS Number: 1.0

Revision Date: 03/2018

Section 2 Hazards Identification

2.1 Classification of the Substance

GHS Classification(s) according to OSHA Hazard Communication Standard (29 CFR 1910.1200):

- Eye Irritant, Category 2A
- STOT-SE, Category 3 (Respiratory Irritation)
- Carcinogen, Category 1A
- STOT-RE, Category 1 (Lungs)
- Toxic to Reproduction, Category 2

2.2 Label Elements

| Labelling according to 29 CFR 1910.1200 Appendices A, B and C* | | |
|--|--|--|
| Hazard Pictogram(s): | | |
| Signal word: | DANGER | |
| Hazard Statement(s): | Causes serious eye irritation. May cause respiratory irritation. May cause damage to lungs after repeated/prolonged exposure via inhalation. May cause cancer of the lung. Suspected of damaging fertility or the unborn child. | |
| Precautionary Statement(s): | Obtain special instructions before use. Do not handle until all safety precautions have been read and understood. Avoid breathing dust. Wash thoroughly after handling. Do not eat drink or smoke when using this product. Wear protective gloves/protective clothing/eye protection/face protection. Use outdoors or in a well-ventilated area. If exposed or concerned: Get medical advice/attention. Store in a secure area. Dispose of product in accordance with local/national regulations. | |

^{*} Fly ash and other coal combustion products (CCPs) are UVCB substances (unknown or variable composition or biological). Various CCPs, noted as ashes/ash residuals; Ashes, residues, bottom; Bottom ash; Bottom ash residues; Waste solids, ashes under TSCA are defined as: "The residuum from the burning of a combination of carbonaceous materials. The following elements may be present as oxides: aluminum, calcium, iron, magnesium, nickel, phosphorus, potassium, silicon, sulfur, titanium, and vanadium." Ashes including fly ash and fluidized bed combustion ash are identified by CAS number 68131-74-8. The exact composition of the ash is dependent on the fuel source and flue additives composed of many constituents. The classification of the final substance is dependent on the presence of specific identified oxides as well as other trace elements.



2.3 Other Hazards

Listed Carcinogens:

-Respirable Crystalline Silica

IARC: [Yes] NTP: [Yes] OSHA: [Yes] Other: (ACGIH) [Yes]

Section 3 Composition/Information on Ingredients

| Substance | CAS No. | Percentage (%) | GHS Classification |
|---------------------------------------|-------------------------|----------------|---|
| Crystalline Silica | 14808-60-7 | 20 - 40% | Repeat Dose STOT, Category 1 Carcinogen, Category 1A |
| Silica, crystalline respirable (RCS) | 14808-60-7 | See Footnote 1 | Repeat Dose STOT, Category 1 Carcinogen. Category 1A |
| Aluminosilicates ² | Various, see Footnote 2 | 10 - 60% | Single Exposure STOT, Category 3 |
| Calcium oxide (CaO) | 1305-78-8 | 10 - 30% | Skin Irritant, Category 2 Eye Irritant, Category 1 Single Exposure STOT, Category 3 |
| Iron oxide | 1309-37-1 | 1 - 10% | Not Classified |
| Manganese dioxide (MnO ₂) | 1313-13-9 | <2% | Skin Irritant, Category 2 Eye Irritant, Category 2B |
| Magnesium oxide | 1309-48-4 | 2 - 10% | Not Classified |
| Phosphorus pentoxide (P_2O_5) | 1314-56-3 | ≤2% | Skin Irritant, Category 2 Eye Irritant, Category 2B |
| Sodium oxide | 1313-59-3 | 1 - 10% | Not Classified |
| Potassium oxide (K₂O) | 12136-45-7 | ≤1% | Skin Irritant Category 2 Eye Irritant Category 2B |
| Titanium dioxide (TiO ₂) | 13463-67-7 | <3% | Not Classified |
| Bromide salt (calcium) | 7789-41-5 | See Footnote 3 | Toxic to Reproduction Category 2 |

¹The percentage of respirable crystalline silica has not been determined. Therefore, a GHS classification of Carcinogen 1A has been assigned.

²Aluminosilicates (CAS# 1327-36-2) may be in the form of mullite (CAS# 1302-93-8); aluminosilicate glass; pozzolans (CAS# 71243-67-9); or calcium aluminosilicates such as tricalcium aluminate (C3A), or calcium sulfoaluminate (C4A3S). The form is dependent on the source of the coal and or the process used to create the CCP. Pulverized coal combustion would be more likely to create high levels of pozzolans. Aluminosilicates may have inclusions of calcium, titanium, iron, potassium, phosphorus, magnesium and other metal oxides.

³ Analytical data are not available to demonstrate that the concentration of bromide salt is <0.1%; therefore, a GHS classification of Toxic to Reproduction Category 2 has been assigned.



Section 4
First Aid Measures

4.1 Description of First Aid Measures

| Inhalation: | If product is inhaled and irritation of the nose or coughing occurs, remove person to fresh air. Get medical advice/attention if respiratory symptoms persist. |
|---------------|---|
| Skin Contact: | If skin exposure occurs, wash with soap and water. |
| Eye Contact: | If product gets into the eye, rinse copiously with water for several minutes. Remove contact lenses, if present and easy to do. Seek medical attention/advice if irritation occurs or persists. |
| Ingestion: | No specific first aid measures are required. |

4.2 Most Important Health Effects, Both Acute and Delayed

Acute Effects: Direct exposure may cause respiratory irritation, eye irritation and skin irritation. The product dust can dry and irritate the skin and cause dermatitis and can irritate eyes and skin through mechanical abrasion.

Chronic Effects: Chronic exposure may cause lung damage from repeated exposure. Prolonged inhalation of respirable crystalline silica above certain concentrations may cause lung diseases, including silicosis and lung cancer. Repeated exposure to dusts containing inorganic bromide salts may affect fertility and/or result in effects to the unborn child.

4.3 Indication of Any Immediate Medical Attention and Special Treatment Needed

Seek first aid or call a doctor or Poison Control Center if contact with eyes occurs and irritation remains after rinsing. Get medical advice if inhalation occurs and respiratory symptoms persist.



Section 5
Firefighting Measures

5.1 Extinguishing Media

| Suitable Extinguishing Media: | Product is not flammable. Use extinguishing media appropriate for surrounding fire. | |
|---------------------------------|---|--|
| Unsuitable Extinguishing Media: | Not applicable, the product is not flammable. | |

5.2 Special Hazards Arising from the Substance or Mixture

| Hazardous Combustion Products: | None known. |
|--------------------------------|-------------|
|--------------------------------|-------------|

5.3 Advice for Firefighters

Section 6 Accidental Release Measures

6.1 Personal Precautions, Protective Equipment and Emergency Procedures

| Personal precautions/Protective Equipment: | See Section 8.2.2 Individual Protective Measures. For concentrations exceeding Occupational Exposure Levels (OELs), use a self-contained breathing apparatus (SCBA). |
|--|--|
| Emergency procedures: | Use scooping, water spraying/flushing/misting or ventilated vacuum cleaning systems to clean up spills. Do not use pressurized air. |

6.2 Environmental Precautions

| Environmental precautions: | Prevent contamination of drains or waterways and dispose according to local and national regulations. |
|----------------------------|---|
|----------------------------|---|



6.3 Methods and Material for Containment and Cleaning Up

Methods and materials for containment and cleaning up:

Do not use brooms or compressed air to clean surfaces. Use dust collection vacuum and extraction systems.

Large spills of dry product should be removed by a vacuum system. Dampened material should be removed by mechanical means and recycled or disposed of according to local and national regulations.

See Sections 8 and 13 for additional information on exposure controls and disposal.

Section 7 Handling and Storage

7.1 Precautions for Safe Handling

Practice good housekeeping. Use adequate exhaust ventilation, dust collection and/or water mist to maintain airborne dust concentrations below permissible exposure limits (note: respirable crystalline silica dust may be in the air without a visible dust cloud).

Do not permit dust to collect on walls, floors, sills, ledges, machinery, or equipment. Maintain and test ventilation and dust collection equipment. In cases of insufficient ventilation, wear a NIOSH approved respirator for silica dust when handling or disposing dust from this product. Avoid contact with skin and eyes. Wash or vacuum clothing that has become dusty. Avoid eating, smoking, or drinking while handling the material.

7.2 Conditions for Safe Storage, Including any Incompatibilities

Minimize dust produced during loading and unloading.



Section 8 Exposure Controls/Personal Protection

8.1 Control Parameters

| OCCUPATIONAL EXPOSURE LIMITS | | | | | | | |
|----------------------------------|------------|----------------------|-----------------------|-----------------------|--------------------------|--|--|
| SUBSTANCE | | OSHA PEL TWA (mg/m³) | NIOSH REL TWA (mg/m³) | ACGIH TLV TWA (mg/m³) | CA - OSHA PEL (mg/m³) | | |
| Calcium oxide | | 5 | 2 | 2 | 2 | | |
| Particulates Not Otherwise | Total | 15 | 15 | 10 | 10 | | |
| Regulated | Respirable | 5 | 5 | 3 | 5 | | |
| Respirable Crystalline Silica | Respirable | 0.05 | 0.05 | 0.025 | 0.05 | | |
| Manganese dioxide (as manganese | Total | 5 (Ceiling) | 1 3 (STEL) | 0.1 | 0.2 | | |
| compounds) | Respirable | - | - | 0.02 | - | | |

8.2 Exposure Controls

8.2.1 Engineering Controls

Provide ventilation to maintain the ambient workplace atmosphere below the occupational exposure limit(s). Use general and local exhaust ventilation and dust collection systems as necessary to minimize exposure.

8.2.2 Personal Protective Equipment (PPE)

| Respiratory protection: | Wear a NIOSH approved particulate respirator if exposure to airborne particulates is unavoidable and where occupational exposure limits may be exceeded. If airborne exposures are anticipated to exceed applicable PELs or TLVs, a self-contained breathing apparatus or airline respirator is recommended. | | | | |
|---------------------------|--|--|--|--|--|
| Eye and face protection: | If eye contact is possible, wear protective glasses with side shields. Avoid contact lenses. | | | | |
| Hand and skin protection: | Wear gloves and protective clothing. Wash hands with soap and water after contact with material. | | | | |



Section 9
Physical and Chemical Properties

9.1 Information on Basic Physical and Chemical Properties

| Property: Value | Property: Value | | |
|--|--|--|--|
| Appearance (physical state, color, etc.): Fine tan/ gray particulate | Upper/lower flammability or explosive limits: Not applicable | | |
| Odor: Odorless ¹ | Vapor Pressure (Pa): Not applicable | | |
| Odor threshold: Not applicable | Vapor Density: Not applicable | | |
| pH (25 °C) (in water): 8 - 11 | Specific gravity or relative density: 2.2 – 2.9 | | |
| Melting point/freezing point (°C): Not applicable | Water Solubility: Slight | | |
| Initial boiling point and boiling range (°C): Not applicable | Partition coefficient: n-octane/water: Not determined | | |
| Flash point (°C): Not determined | Auto ignition temperature (°C): Not applicable | | |
| Evaporation rate: Not applicable | Decomposition temperature (°C): Not determined | | |
| Flammability (solid, gas): Not combustible | Viscosity: Not applicable | | |

The use of urea or aqueous ammonia injected into the flue gas to reduce nitrogen oxides (NOx) emissions may result in the presence of ammonium sulfate or ammonium bisulfate in the ash at less than 0.1%. When ash containing these substances becomes wet under high pH (>9), free ammonia gas may be released resulting in objectionable/nuisance ammonia odor and potential exposure to ammonia gas especially in confined spaces.



Section 10 Stability and Reactivity

| 10.1 Reactivity: | The material is an inert, inorganic material primarily composed of elemental oxides. | | |
|--|--|--|--|
| 10.2 Chemical stability: | The material is stable under normal use conditions. | | |
| 10.3 Possibility of hazardous reactions: | The material is a relatively stable, inert material; however, when ash containing ammonia becomes wet under high pH (>9), free ammonia gas may be released resulting in an objectionable/nuisance ammonia odor and potential exposure to ammonia gas especially in confined spaces. Polymerization will not occur. | | |
| 10.4 Conditions to avoid: | Product can become airborne in moderate winds. Dry material should be stored in silos. Materials stored out of doors should be covered or maintained in a damp condition. | | |
| 10.5 Incompatible materials: | None known. | | |
| 10. 6 Hazardous decomposition products: | None known. | | |



Section 11 Toxicological Information

11.1 Information on Toxicological Effects

| Endpoint | Data |
|--------------------------------|--|
| Acute oral toxicity | LD50 > 2000 mg/kg |
| Acute dermal toxicity | LD50 > 2000 mg/kg |
| Acute inhalation toxicity | LD50 > 5.0 mg/L |
| Skin corrosion/irritation | Does not meet the classification criteria but may cause slight skin irritation. Product dust can dry the skin which can result in irritation. |
| Eye damage/irritation | Causes serious eye irritation. Positive scores for conjunctiva irritation and chemosis in 2/3 animals based on average of 24, 48 and 72-hour scores with irritation clearing within 21 days; no corneal or iritis effects observed. |
| Respiratory/skin sensitization | Not a respiratory or dermal sensitizer. |
| Germ cell mutagenicity | Not mutagenic in in-vitro and in-vivo assays with or without metabolic activation. |
| Carcinogenicity | Not available. Respirable crystalline silica has been identified as a carcinogen by OSHA, NTP, ACGIH and IARC. |
| Reproductive toxicity | No developmental toxicity was observed in available animal studies. Reproductive studies on CCPs showed either no reproductive effects, or some effects on male and female reproductive organs and parameters but without a clear dose response. |
| | Inorganic bromide salts have been shown to have adverse effects on |
| | reproductive parameters in some animal studies. |
| STOT-SE | CCPs when present as a nuisance dust may result in respiratory irritation. |
| STOT-RE | In a 180-day inhalation study with fly ash dust, no effects were observed at the highest dose tested. NOEC = 4.2 mg/m³; it is not possible to assess the level at which toxicologically significant effects may occur. Repeated inhalation exposures to high levels of respirable crystalline silica may result in lung damage (i.e., silicosis). |
| Aspiration Hazard | Not applicable based product form. |

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Bottom Ash SDS Number: 1.0

Revision Date: 03/2018

Section 12 **Ecological Information**

Toxicity 12.1

| Fly Ash (CAS# 68131-74-8) | | | | |
|--------------------------------------|--|--|--|--|
| Toxicity to Fish | LC50 > 100 mg/L | | | |
| Toxicity to Aquatic Invertebrates | Data indicates that the test substance is not toxic to <i>Daphnia magna</i> (EC50 undetermined) | | | |
| Toxicity to Aquatic Algae and Plants | EC50 = 10 mg/L | | | |
| Calcium oxide CAS# 1305-78-8 | | | | |
| Toxicity to Fish | LC50 = 50.6 mg/L The findings were closely related to the pH of the test solutions; therefore, pH is considered to be the main reason for the effects. | | | |
| Toxicity to Aquatic Invertebrates | EC50 = 49.1 mg/L The findings were closely related to the pH of the test solutions; therefore, pH is considered to be the main reason for the effects. | | | |
| Toxicity to Aquatic Algae and Plants | NOEC =48 mg/L @ 72 hours based on Ca(OH) ₂ The initial pH of the test medium was not directly related to the biologically relevant effects. The formation of precipitates is likely the result of the reaction between CO ₂ dissolved in the medium. | | | |

12.2 Persistence and Degradability

Not relevant for inorganic materials.

12.3 Bioaccumulative Potential

This material does not contain any compounds that would bioaccumulate up the food chain.

12.4 Mobility in Soil

No data available.

12.5 Results of PBT and vPvB Assessment

This material does not contain any compounds classified as "persistent, bioaccumulative or toxic" nor as "very persistent/very bioaccumulative".

12.6 Other Adverse Effects

None known.



Section 13
Disposal Considerations

See Sections 7 and 8 above for safe handling and use, including appropriate industrial hygiene practices.

Dispose of all waste product and containers in accordance with federal, state and local regulations.

Section 14 Transport Information

| | Shipping Name: | Not Regulated |
|--------------------|----------------|---------------|
| Regulatory entity: | Hazard Class: | Not Regulated |
| U.S. DOT | ID Number: | Not Regulated |
| | Packing Group: | Not Regulated |

Section 15 **Regulatory Information**

15.1 Safety, Health and Environmental Regulations/Legislation Specific for the Mixture

TSCA Inventory Status

All components are listed on the TSCA Inventory.

California Proposition 65

The following substances are known to the State of California to be carcinogens and/or reproductive toxicants:

- Respirable crystalline silica
- Titanium dioxide
- State Right-to-Know (RTK)

| Component | CAS | MA ^{1,2} | NJ ^{3,4} | PA ⁵ | RI⁵ |
|--|------------|-------------------|-------------------|-----------------|-----|
| Ammonium bisulfate | 7803-63-6 | No | Yes | No | No |
| Ammonium sulfate | 7783-20-2 | Yes | No | Yes | No |
| Calcium oxide | 1305-78-8 | Yes | Yes | Yes | No |
| Iron oxide | 1309-37-1 | Yes | Yes | Yes | No |
| Magnesium oxide | 1309-48-4 | No | Yes | No | No |
| Phosphorus pentoxide (or | 1314-56-3 | Yes | Yes | Yes | No |
| phosphorus oxide) | | | | | |
| Potassium oxide | 12136-45-7 | No | Yes | No | No |
| Silica-crystalline (SiO ₂), quartz | 14808-60-7 | Yes | Yes | Yes | No |
| Sodium oxide | 1313-59-3 | No | Yes | No | No |
| Titanium dioxide | 13463-67-7 | Yes | Yes | Yes | Yes |

¹ Massachusetts Department of Public Health, no date ² 189th General Court of The Commonwealth of Massachusetts, no date

New Jersey Department of Health and Senior Services, 2010a

⁴ New Jersey Department of Health, 2010b

⁵ Pennsylvania Code, 1986

⁶ Rhode Island Department of Labor and Training, no date



Section 16

Other Information, Including Date of Preparation or Last Revision

16.1 Indication of Changes

Date of preparation or last revision: February 23, 2018

16.2 Abbreviations and Acronyms

ACGIH: American Conference of Industrial Hygienists

CA: California

CAS: Chemical Abstract Services
 CCP: Coal Combustion Product
 CFR: Code of Federal Regulations
 EPA: Environmental Protection Agency

GHS: Globally Harmonized System of Classification and Labelling

IARC: International Agency for Research on Cancer

LC50: Concentration resulting in the mortality of 50 % of an animal population

LD50: Dose resulting in the mortality of 50 % of an animal population

MA: Massachusetts
NA: Not Applicable
NJ: New Jersey

NOEC: No observed effect concentration

NIOSH: National Institute of Occupational Safety and Health

NOx: Nitrogen oxides

NTP: US National Toxicology Program
 OEL: Occupational Exposure Limit

OSHA: Occupational Safety and Health Administration

PA: Pennsylvania

PBT: Persistent, Toxic and Bioaccumulative

PEL: Permissible exposure limit
 PPE: Personal Protective Equipment
 REL: Recommended exposure limit

RI: Rhode Island

RCS: Respirable Crystalline Silica

RTK: Right-to-Know

SCBA: Self-contained breathing apparatus

SDS: Safety Data SheetSTEL: Short-term exposure limit

STOT-RE: Specific target organ toxicity-repeated exposureSTOT-SE: Specific target organ toxicity-single exposure

TLV: Threshold limit value

TSCA: Toxic Substances Control Act
 TWA: Time-weighted average
 UEL: Upper explosive limit

UVCB: Unknown or Variable Composition/Biological

U.S.: United States

Preparation Date: February 23, 2018

U.S. DOT: United States of Department of Transportation



16.3 Other Hazards

| Hazardous Mate | Hazardous Materials Identification System (HMIS) | | | | | | |
|--|--|---------------|---|----------------------|---|------------------------|--|
| Degree of hazard (0= low, 4 = extreme) | | | | | | | |
| Health: | 2* | Flammability: | 0 | Physical Hazards: | 0 | Personal protection:** | |

DISCLAIMER:

This SDS has been prepared in accordance with the Hazard Communication Rule 29 CFR 1910.1200. Information herein is based on data considered to be accurate as of date prepared. No warranty or representation, express or implied, is made as to the accuracy or completeness of this data and safety information. No responsibility can be assumed for any damage or injury resulting from abnormal use, failure to adhere to recommended practices, or from any hazards inherent in the nature of the product.

^{*} Chronic Health Effects

^{**} Appropriate personal protection is defined by the activity to be performed. See Section 8 for additional information.



Class C Fly Ash SDS Number: 1.0 Revision Date: 03/2018



Section 1 Identification of the Substance and of the Supplier

1.1 Product Identifier

| Product Name/Identification: | ASTM Class C Fly Ash |
|------------------------------|------------------------|
| Synonyms: | Coal Fly Ash, Pozzolan |
| Formula: | UVCB Substance |

1.2 Relevant Identified Uses of the Substance or Mixture and Uses Advices Against

| Relevant Identified Uses: | Component of wallboard, concrete, roofing material, bricks, cement kiln feed. |
|---------------------------|---|
| Uses Advised Against: | None known. |

1.3 Details of the Supplier of the SDS

| Manufacturer/Supplier: | Dynegy, Inc. |
|-----------------------------|-------------------------------|
| Street Address: | 601 Travis Street, Suite 1400 |
| City, State and Zip Code: | Houston, TX 77002 |
| Customer Service Telephone: | 800-633-4704 |



Class C Fly Ash SDS Number: 1.0 Revision Date: 03/2018

Section 2
Hazards Identification

2.1 Classification of the Substance

GHS Classification(s) according to OSHA Hazard Communication Standard (29 CFR 1910.1200):

- Eye Irritant, Category 2A
- STOT-SE, Category 3 (Respiratory Irritation)
- Carcinogen, Category 1A
- STOT-RE, Category 1 (Lungs)
- Toxic to Reproduction, Category 2

2.2 Label Elements

| Labelling according to 29 CFR 1910.1200 Appendices A, B and C* | | | |
|--|--|--|--|
| Hazard Pictogram(s): | | | |
| Signal word: | DANGER | | |
| Hazard Statement(s): | Causes serious eye irritation. May cause damage to lungs after repeated/prolonged exposure via inhalation. May cause respiratory irritation. May cause cancer of the lung. Suspected of damaging fertility or the unborn child. | | |
| Precautionary Statement(s): | Obtain special instructions before use. Do not handle until all safety precautions have been read and understood. Avoid breathing dust. Wear protective gloves/protective clothing/eye protection/face protection. Wash thoroughly after handling. Do not eat drink or smoke when using this product. Use outdoors or in a well-ventilated area. If exposed or concerned: Get medical advice/attention. Store in a secure area. Dispose of product in accordance with local/national regulations. | | |

^{*} Fly ash and other coal combustion products (CCPs) are UVCB substances (unknown or variable composition or biological). Various CCPs, noted as ashes/ash residuals; Ashes, residues, bottom; Bottom ash; Bottom ash residues; Waste solids, ashes under TSCA are defined as: "The residuum from the burning of a combination of carbonaceous materials. The following elements may be present as oxides: aluminum, calcium, iron, magnesium, nickel, phosphorus, potassium, silicon, sulfur, titanium, and vanadium." Ashes including fly ash and fluidized bed combustion ash are identified by CAS number 68131-74-8. The exact composition of the ash is dependent on the fuel source and flue additives composed of many constituents. The

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Class C Fly Ash SDS Number: 1.0 Revision Date: 03/2018

classification of the final substance is dependent on the presence of specific identified oxides as well as other trace elements.

2.3 Other Hazards

Listed Carcinogens:

-Respirable Crystalline Silica

IARC: [Yes] NTP: [Yes] OSHA: [Yes] Other: (ACGIH) [Yes]

Section 3 Composition/Information on Ingredients

| Substance | CAS No. | Percentage (%) | GHS Classification |
|---|-------------------------|----------------|---|
| Crystalline Silica | 14808-60-7 | 30 - 60% | Repeat Dose STOT, Category 1 Carcinogen, Category 1A |
| Silica, crystalline respirable (RCS) | 14808-60-7 | See Footnote 1 | Repeat Dose STOT, Category 1 Carcinogen, Category 1A |
| Aluminosilicates | 71243-67-9 1327-36-2 | 30 - 60% | Single Exposure STOT, Category 3 |
| Iron oxide | 1309-37-1 | 1 - 10% | Not Classified |
| Calcium oxide (CaO) | 1305-78-8 | 20 - 30% | Skin Irritant, Category 2 Eye Irritant, Category 1 Single Exposure STOT, Category 3 |
| Magnesium oxide | 1309-48-4 | 2 - 10% | Not Classified |
| Phosphorus pentoxide (P ₂ O ₅) | 1314-56-3 | ≤2% | Skin Irritant, Category 2 Eye Irritant, Category 2B |
| Sodium oxide | 1313-59-3 | 1-8% | Not Classified |
| Potassium oxide (K ₂ O) | 12136-45-7 | ≤1% | Skin Irritant, Category 2 Eye Irritant, Category 2B |
| Titanium dioxide (TiO ₂) | 13463-67-7 | <3% | Not Classified |
| Bromide salt (calcium) | <mark>7789-41-5</mark> | See Footnote 2 | Toxic to Reproduction, Category 2 |

Footnote 1: The percentage of respirable crystalline silica has not been determined. Therefore, a GHS classification of Carcinogen, Category 1A has been assigned.

Footnote 2: Analytical data are not available to demonstrate that the concentration of bromide salt is <0.1%; therefore, a GHS classification of Toxic to Reproduction, Category 2 has been assigned.



Section 4 First Aid Measures

4.1 Description of First Aid Measures

| Inhalation: | If product is inhaled and irritation of the nose or coughing occurs, remove person to fresh air. Get medical advice/attention if respiratory symptoms persist. |
|---------------|---|
| Skin Contact: | If skin exposure occurs, wash with soap and water. |
| Eye Contact: | If product gets into the eye, rinse copiously with water for several minutes. Remove contact lenses, if present and easy to do. Seek medical attention/advice if irritation occurs or persists. |
| Ingestion: | No specific first aid measures are required. |

4.2 Most Important Health Effects, Both Acute and Delayed

Acute Effects: Direct exposure may cause respiratory irritation, eye irritation and skin irritation. The product dust can dry and irritate the skin and cause dermatitis and can irritate eyes and skin through mechanical abrasion.

Chronic Effects: Chronic exposure may cause lung damage from repeated exposure. Prolonged inhalation of respirable crystalline silica above certain concentrations may cause lung diseases, including silicosis and lung cancer. Repeated exposure to dusts containing inorganic bromide salts may affect fertility and/or result in effects to the unborn child.

4.3 Indication of Any Immediate Medical Attention and Special Treatment Needed

Seek first aid or call a doctor or Poison Control Center if contact with eyes occurs and irritation remains after rinsing. Get medical advice if inhalation occurs and respiratory symptoms persist.



Section 5 Firefighting Measures

5.1 Extinguishing Media

| Suitable Extinguishing Media: | Product is not flammable. Use extinguishing media appropriate for surrounding fire. |
|---------------------------------|---|
| Unsuitable Extinguishing Media: | Not applicable, the product is not flammable. |

5.2 Special Hazards Arising from the Substance or Mixture

| Hazardous Combustion Products: | None known. |
|--------------------------------|-------------|
|--------------------------------|-------------|

5.3 Advice for Firefighters

| Special Protective Equipment and Precautions for Firefighters: As with any fire, wear self-contained breathing apparatus (NIOSH approved or equivalent) and full protective gear. | |
|--|--|
|--|--|



Section 6
Accidental Release Measures

6.1 Personal Precautions, Protective Equipment and Emergency Procedures

| Personal precautions/Protective Equipment: | See Section 8.2.2 Individual Protective Measures. For concentrations exceeding Occupational Exposure Levels (OELs), use a self-contained breathing apparatus (SCBA). |
|--|--|
| Emergency procedures: | Use scooping, water spraying/flushing/misting or ventilated vacuum cleaning systems to clean up spills. Do not use pressurized air. |

6.2 Environmental Precautions

| Environmental precautions: | Prevent contamination of drains or waterways and dispose according to local and national regulations. |
|----------------------------|---|
|----------------------------|---|

6.3 Methods and Material for Containment and Cleaning Up

| Methods and materials for containment and cleaning up: | Do not use brooms or compressed air to clean surfaces. Use dust collection vacuum and extraction systems. Large spills of dry product should be removed by a vacuum system. Dampened material should be removed by mechanical means and recycled or disposed of according to local and national regulations. |
|--|--|
|--|--|

See Sections 8 and 13 for additional information on exposure controls and disposal.



Section 7 Handling and Storage

7.1 Precautions for Safe Handling

Practice good housekeeping. Use adequate exhaust ventilation, dust collection and/or water mist to maintain airborne dust concentrations below permissible exposure limits (note: respirable crystalline silica dust may be in the air without a visible dust cloud).

Do not permit dust to collect on walls, floors, sills, ledges, machinery, or equipment. Maintain and test ventilation and dust collection equipment. In cases of insufficient ventilation, wear a NIOSH approved respirator for silica dust when handling or disposing dust from this product. Avoid contact with skin and eyes. Wash or vacuum clothing that has become dusty. Avoid eating, smoking, or drinking while handling the material.

7.2 Conditions for Safe Storage, Including any Incompatibilities

Minimize dust produced during loading and unloading.

Section 8 Exposure Controls/Personal Protection

8.1 Control Parameters

| OCCUPATIONAL EXPOSURE LIMITS | | | | | |
|---|-------------------------------------|-------------------------|-------------------------------|--------------------------|--------------------------|
| SUBSTANCE | | OSHA PEL TWA (mg/m³) | NIOSH REL TWA (mg/m³) | ACGIH TLV TWA (mg/m³) | CA - OSHA PEL (mg/m³) |
| Calcium oxide | Calcium oxide | | 2 | 2 | 2 |
| Particulates Not Otherwise Regulated | Total | 15 | 15 | 10 | 10 |
| | Respirable | 5 | 5 | 3 | 5 |
| Respirable Crystalline Silica | Respirable Crystalline Silica | 0.05 | 0.05 | 0.025 | 0.05 |
| Titanium dioxide | Total | 15 | 2.4 (fine) 0.3 (ultrafine) | 10 | 10 |
| Manganese dioxide (as manganese compounds) | Total | 5 (Ceiling) | 1 3 (STEL) | 0.1 | 0.2 |
| | Respirable | - | - | 0.02 | - |

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8.2 Exposure Controls

8.2.1 Engineering Controls

Provide ventilation to maintain the ambient workplace atmosphere below the occupational exposure limit(s). Use general and local exhaust ventilation and dust collection systems as necessary to minimize exposure.

8.2.2 Personal Protective Equipment (PPE)

| Respiratory protection: | Wear a NIOSH approved particulate respirator if exposure to airborne particulates is unavoidable and where occupational exposure limits may be exceeded. If airborne exposures are anticipated to exceed applicable PELs or TLVs, a self-contained breathing apparatus or airline respirator is recommended. |
|---------------------------|--|
| Eye and face protection: | If eye contact is possible, wear protective glasses with side shields. Avoid contact lenses. |
| Hand and skin protection: | Wear gloves and protective clothing. Wash hands with soap and water after contact with material. |



Section 9 Physical and Chemical Properties

9.1 Information on Basic Physical and Chemical Properties

| Property: Value | Property: Value |
|--|--|
| Appearance (physical state, color, etc.): Fine tan/ gray particulate | Upper/lower flammability or explosive limits: Not applicable |
| Odor: Odorless ¹ | Vapor Pressure (Pa): Not applicable |
| Odor threshold: Not applicable | Vapor Density: Not applicable |
| pH (25 °C) (in water): Not Determined | Specific gravity or relative density: 2.2 – 2.9 |
| Melting point/freezing point (°C): Not applicable | Water Solubility: Slight |
| Initial boiling point/boiling range (°C): NA | Partition coefficient: n-octane/water: NA |
| Flash point (°C): Not determined | Auto ignition temperature (°C): Not applicable |
| Evaporation rate: Not applicable | Decomposition temperature (°C): Not determined |
| Flammability (solid, gas): Not combustible | Viscosity: Not applicable |

The use of urea or aqueous ammonia injected into the flue gas to reduce nitrogen oxides (NOx) emissions may result in the presence of ammonium sulfate or ammonium bisulfate in the ash at less than 0.1%. When ash containing these substances becomes wet under high pH (>9), free ammonia gas may be released resulting in objectionable/nuisance ammonia odor and potential exposure to ammonia gas especially in confined spaces.



Section 10 Stability and Reactivity

| 10.1 Reactivity: | The material is an inert, inorganic material primarily composed of elemental oxides. |
|--|--|
| 10.2 Chemical stability: | The material is stable under normal use conditions. |
| 10.3 Possibility of hazardous reactions: | The material is a relatively stable, inert material; however, when ash containing ammonia becomes wet under high pH (>9), free ammonia gas may be released resulting in an objectionable/nuisance ammonia odor and potential exposure to ammonia gas especially in confined spaces. Polymerization will not occur. |
| 10.4 Conditions to avoid: | Product can become airborne in moderate winds. Dry material should be stored in silos. Materials stored out of doors should be covered or maintained in a damp condition. |
| 10.5 Incompatible materials: | None known. |
| 10. 6 Hazardous decomposition products: | None known. |



Section 11 Toxicological Information

11.1 Information on Toxicological Effects

| Endpoint | Data |
|--------------------------------|--|
| Acute oral toxicity | LD50 > 2000 mg/kg |
| Acute dermal toxicity | LD50 > 2000 mg/kg |
| Acute inhalation toxicity | LD50 > 5.0 mg/L |
| Skin corrosion/irritation | Does not meet the classification criteria but may cause slight skin irritation. Product dust can dry the skin which can result in irritation. |
| Eye damage/irritation | Causes serious eye irritation. Positive scores for conjunctiva irritation and chemosis in 2/3 animals based on average of 24, 48 and 72-hour scores with irritation clearing within 21 days; No corneal or iritis effects observed. |
| Respiratory/skin sensitization | Not a respiratory or dermal sensitizer. |
| Germ cell mutagenicity | Not mutagenic in in-vitro and in-vivo assays with or without metabolic activation. |
| Carcinogenicity | Not available. Respirable crystalline silica has been identified as a carcinogen by OSHA, NTP, ACGIH and IARC. |
| Reproductive toxicity | No developmental toxicity was observed in available animal studies. Reproductive studies on CCPs showed either no reproductive effects, or some effects on male and female reproductive organs and parameters but without a clear dose response. |
| | Inorganic bromide salts have been shown to have adverse effects on reproductive parameters in some animal studies. |
| STOT-SE | CCPs when present as a nuisance dust may result in respiratory irritation. |
| STOT-RE | In a 180-day inhalation study with fly ash dust, no effects were observed at the highest dose tested. NOEC = 4.2 mg/m³; it is not possible to assess the level at which toxicologically significant effects may occur. Repeated inhalation exposures to high levels of respirable crystalline silica may result in lung damage (i.e., silicosis). |
| Aspiration Hazard | Not applicable based product form. |



Section 12 Ecological Information

12.1 Toxicity

| Fly Ash C (CAS# 68131-74-8) | | | | | |
|--------------------------------------|--|--|--|--|--|
| Toxicity to Fish | LC50 > 100 mg/L | | | | |
| Toxicity to Aquatic Invertebrates | Data indicates that the test substance is not toxic to <i>Daphnia magna</i> (EC50 undetermined). | | | | |
| Toxicity to Aquatic Algae and Plants | EC50 = 10 mg/L | | | | |

| Calcium oxide CAS# 1305-78-8 | | | | |
|--------------------------------------|--|--|--|--|
| Toxicity to Fish | LC50 = 50.6 mg/L The findings were closely related to the pH of the test solutions; therefore, pH is considered to be the main reason for the effects. | | | |
| Toxicity to Aquatic Invertebrates | EC50 = 49.1 mg/L The findings were closely related to the pH of the test solutions; therefore, pH is considered to be the main reason for the effects. | | | |
| Toxicity to Aquatic Algae and Plants | NOEC =48 mg/L @ 72 hours based on Ca(OH) ₂ The initial pH of the test medium was not directly related to the biologically relevant effects. The formation of precipitates is likely the result of the reaction between CO ₂ dissolved in the medium. | | | |

12.2 Persistence and Degradability

Not relevant for inorganic materials.

12.3 Bioaccumulative Potential

This material does not contain any compounds that would bioaccumulate up the food chain.

12.4 Mobility in Soil

No data available.

12.5 Results of PBT and vPvB Assessment

This material does not contain any compounds classified as "persistent, bioaccumulative or toxic" nor as "very persistent/very bioaccumulative".

12.6 Other Adverse Effects

None known.

Section 13



Disposal Considerations

See Sections 7 and 8 above for safe handling and use, including appropriate industrial hygiene practices.

Dispose of all waste product and containers in accordance with federal, state and local regulations.

Section 14 Transport Information

| | Shipping Name: | Not Regulated |
|--------------------|----------------|---------------|
| Regulatory entity: | Hazard Class: | Not Regulated |
| U.S. DOT | ID Number: | Not Regulated |
| | Packing Group: | Not Regulated |

Section 15
Regulatory Information

15.1 Safety, Health and Environmental Regulations/Legislation Specific for the Mixture

TSCA Inventory Status

All components are listed on the TSCA Inventory.

California Proposition 65.

The following substances are known to the State of California to be carcinogens and/or reproductive toxicants:

- Respirable crystalline silica
- State Right-to-Know (RTK)

| Component | CAS | MA ^{1,2} | NJ ^{3,4} | PA⁵ | RI ⁶ |
|-----------------------------------|------------|-------------------|-------------------|-----|-----------------|
| Ammonium bisulfate | 7803-63-6 | No | Yes | No | No |
| Ammonium sulfate | 7783-20-2 | Yes | No | Yes | No |
| Calcium oxide | 1305-78-8 | Yes | Yes | Yes | No |
| Iron oxide | 1309-37-1 | Yes | Yes | Yes | No |
| Magnesium oxide | 1309-48-4 | No | Yes | No | No |
| Manganese oxide-as | 1313-13-9; | No | No | Yes | Yes |
| manganese compounds | Various | | | | |
| Phosphorus pentoxide (or | 1314-56-3 | Yes | Yes | Yes | No |
| phosphorus oxide) | | | | | |
| Potassium oxide | 12136-45-7 | No | Yes | No | No |
| Silica-crystalline (SiO2), quartz | 14808-60-7 | Yes | Yes | Yes | No |
| Sodium oxide | 1313-59-3 | No | Yes | No | No |
| Titanium dioxide | 13463-67-7 | Yes | Yes | Yes | Yes |

¹ Massachusetts Department of Public Health, no date

Section 16

Other Information, Including Date of Preparation or Last Revision

16.1 Indication of Changes

Date of preparation or last revision: February 23, 2018

16.2 Abbreviations and Acronyms

ACGIH: American Conference of Industrial Hygienists

CA: California

CAS: Chemical Abstract Services
 CCP: Coal Combustion Product
 CFR: Code of Federal Regulations
 EPA: Environmental Protection Agency

² 189th General Court of The Commonwealth of Massachusetts, no date

³ New Jersey Department of Health and Senior Services, 2010a

⁴ New Jersey Department of Health, 2010b

⁵ Pennsylvania Code, 1986

⁶ Rhode Island Department of Labor and Training, no date



Globally Harmonized System of Classification and Labelling

IARC: International Agency for Research on Cancer

• LC50: Concentration resulting in the mortality of 50 % of an animal population

• LD50: Dose resulting in the mortality of 50 % of an animal population

MA: Massachusetts
NA: Not Applicable
NJ: New Jersey

NOEC: No observed effect concentration

NIOSH: National Institute of Occupational Safety and Health

NOx: Nitrogen oxides

NTP: US National Toxicology ProgramOEL: Occupational Exposure Limit

OSHA: Occupational Safety and Health Administration

PA: Pennsylvania

PBT: Persistent, Toxic and Bioaccumulative

PEL: Permissible exposure limit
 PPE: Personal Protective Equipment
 REL: Recommended exposure limit

RI: Rhode Island

RCS: Respirable Crystalline Silica

• RTK: Right-to-Know

SCBA: Self-contained breathing apparatus

• SDS: Safety Data Sheet

• STEL: Short-term exposure limit

STOT-RE: Specific target organ toxicity-repeated exposure
 STOT-SE: Specific target organ toxicity-single exposure

TLV: Threshold limit value

TSCA: Toxic Substances Control Act
 TWA: Time-weighted average
 UEL: Upper explosive limit

UVCB: Unknown or Variable Composition/Biological

U.S.: United States

• U.S. DOT: United States of Department of Transportation

16.3 Other Hazards

| Hazardous Mate | Hazardous Materials Identification System (HMIS) | | | | | | | | | | |
|------------------|--|---------------|---|----------------------|---|------------------------|--|--|--|--|--|
| Degree of hazard | Degree of hazard (0= low, 4 = extreme) | | | | | | | | | | |
| Health: | 2* | Flammability: | 0 | Physical Hazards: | 0 | Personal protection:** | | | | | |

^{*} Chronic Health Effects

^{**} Appropriate personal protection is defined by the activity to be performed. See Section 8 for additional information.



DISCLAIMER:

This SDS has been prepared in accordance with the Hazard Communication Rule 29 CFR 1910.1200. Information herein is based on data considered to be accurate as of date prepared. No warranty or representation, express or implied, is made as to the accuracy or completeness of this data and safety information. No responsibility can be assumed for any damage or injury resulting from abnormal use, failure to adhere to recommended practices, or from any hazards inherent in the nature of the product.

ATTACHMENT T



Phil Morris
Illinois Power Generating Company
Luminant
1500 Eastport Plaza Drive
Collinsville, IL 62234

May 19, 2021

Mr. Darin LeCrone, P.E.
Manager, Industrial Unit
Bureau of Water, Division of Water Pollution Control, Permits Section
Illinois Environmental Protection Agency
1021 North Grand Avenue, East
Springfield, IL 62794-9276

Re: CCR Surface Impoundment Category Designation and Justification for Illinois Power Generating Company

Dear Mr. LeCrone:

Pursuant to 35 I.A.C. 845.700(c), Illinois Power Generating Company submits the information necessary to categorize the CCR surface impoundments located at the Newton Power Plant and the now retired Coffeen Power Plant. The following parameters were used in assessing and justifying each assigned category.

- Category 1 Impacts to existing potable water supply well or impacts to groundwater quality within the setback of an existing potable water supply well.
 - This review includes an assessment of potable water wells within 2,500 feet of CCR surface impoundments to determine whether any potential impacts are occurring within the setback zone of any community water supply well established under the Illinois Groundwater Protection Act.
 - This information was developed during the Part 845 rulemaking and is summarized in Attachment 1, Table 2: Impacts to Potable Water Supply.
- Category 2 Imminent threat to human health or the environment or have been designated by IEPA under (g)(5)
 - o The surface impoundments at Newton and Coffeen Power Plants do not pose an imminent threat to human health or the environment. There are no known conditions at or around the facility where someone or something may be exposed to contaminant concentrations reasonably expected to cause harm
- Category 3 Located in areas of environmental justice ("EJ") concern
 - EJ areas were evaluated using the EJ mapping link from IEPA's webpage located at https://www2.illinois.gov/epa/topics/environmental-justice. Per the IEPA mapping tool, the EJ Status thresholds were determined as twice the state averages for Minority and Low Income consistent with 35 IAC 845.700(g)(6).
 - o An EJ map denoting the facilities with impoundments is located in Attachment 2.

Category 4-7

- o Category 4 Inactive CCR surface impoundments that have an exceedance of the groundwater protection standards in Section 845.600
- o Category 5 Existing CCR surface impoundments that have exceedances of the groundwater protection standards in Section 845.600
- o Category 6 Inactive CCR surface impoundments that are in compliance with the groundwater protection standards in Section 845.600.
- o Category 7 Existing CCR surface impoundments that are in compliance with the groundwater protection standards in Section 845.600

Based on the information above, category designations have been assigned. The category designations for each CCR impoundment are shown in Attachment 1, Table 1: Category Designations.

If you have any questions regarding this submittal, please contact Phil Morris at 618-343-7794 or phil.morris@vistracorp.com.

Sincerely,

Senior Environmental Director

Attachments

Table 1: Category Designation

| Facility | Pond Description | Classifications | Potable Water Supply Impacts (Category 1) | Human Health or Environment Threat (Category 2) | Located within Environmental Justice Areas ¹ (Category 3) | Standards Exceedances ² (Categories 4,5,6,7) | Impoundment Category 845.700(g) |
|----------|------------------|-----------------|---|---|---|--|---------------------------------------|
| | Ash Pond 1 | Inactive | No | No | No | Yes | 5 |
| Coffeen | GMF Pond | Inactive | No | No | No | Yes | 5 |
| | GMF Recycle Pond | Inactive | No | No | No | Yes | 5 |
| Newton | Primary Ash Pond | Existing | No | No | No | Yes | 5 |

¹See Attachment 2 Environmental Justice Area Map

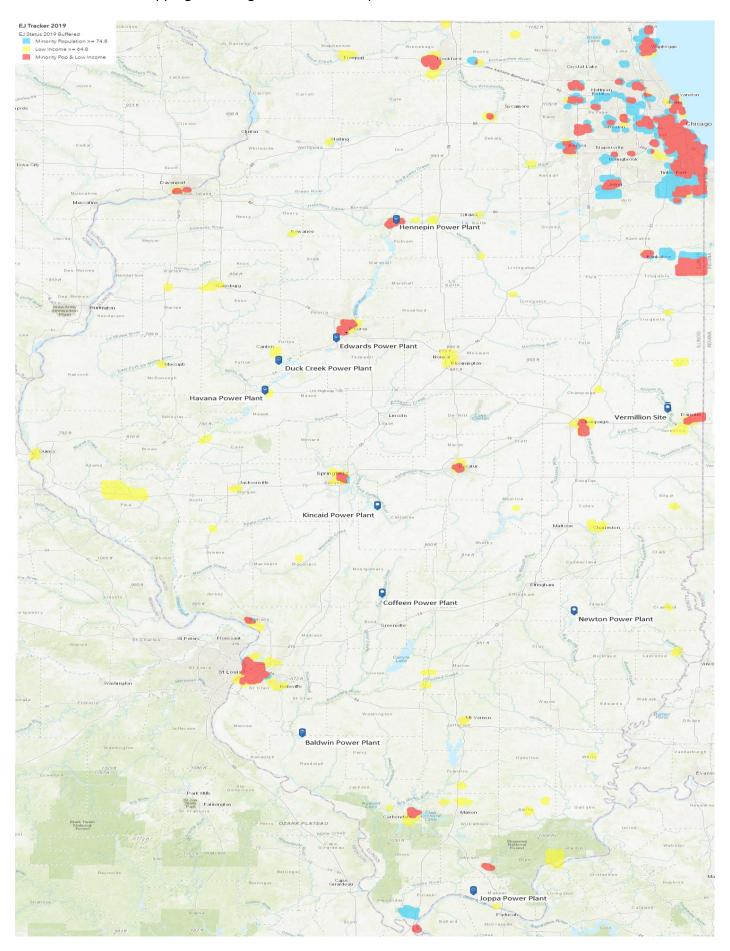
Table 2: Impacts to Potable Water Supply¹

| Site Name | Private and Semi-Private Wells | Non-Community Water Supply (CWS) Wells | Non-CWS Surface Water Intakes | Community Water Supply Wells | CWS Surface Water Intakes |
|-----------|--|---|-------------------------------------|------------------------------------|---------------------------------|
| Coffeen | Present, but not at risk Thirty-four (34) water wells were identified; however, they are unlikely to be at risk because of their hydrogeologic location relative to the power plant, they are abandoned, or they do not appear to be used for potable purposes. None of the off-site wells are located in a downgradient direction. | Present, but not at risk Three (3) non-CWS wells were identified; however, they are unlikely to be at risk because of their hydrogeologic location relative to the power plant and/or their inactive status. | Absent | Absent | Absent |
| Newton | Present, but not at risk Twenty-four (24) water wells were identified; however, they are unlikely to be at risk because of their hydrogeologic location relative to the power plant, they are abandoned, and/or they are unlikely to be present based on the mapped location. None of the offsite wells are located in a downgradient direction. | Absent | Absent | Absent | Absent |

¹ Ramboll, WELL/WATER SUPPLY SURVEY AND EVALUATION COAL-FIRED POWER PLANTS IN ILLINOIS (September 24, 2020), filed with the Illinois Pollution Control Board in R2020-019.

² Ground water analyses for purposes of categories 4-7, assumptions have been made based on current groundwater data. However, since sampling and analysis is ongoing and subject to IEPA review and approval, IPGC reserves the right to update its category designations for Categories 4-7.

Attachment 2: EJ Mapping Denoting Facilities with Impoundments



ATTACHMENT U



October 11, 2021

Illinois Power Generating Company 134 Cips Lane Coffeen, Illinois 62017

Subject: USEPA CCR Rule and IEPA Part 845 Rule Applicability Cross-Reference

2021 USEPA CCR Rule Periodic Certification Report Ash Pond No. 1, Coffeen Power Plant, Coffeen, Illinois

At the request of Illinois Power Generating Company (IPGC), Geosyntec Consultants (Geosyntec) has prepared this letter to document how the attached 2021 United States Environmental Protection Agency (USEPA) CCR Rule Periodic Certification Report (Report) was prepared in accordance with both the Federal USEPA CCR Rule¹ and the state-specific Illinois Environmental Protection Agency (IEPA) Part 845 Rule². Specific sections of the report and the applicable sections of the USEPA CCR Rule and Illinois Part 845 Rule are cross-referenced in **Table 1**. A certification from a Qualified Professional Engineer for each of the CCR Rule sections listed in **Table 1** is provided in Section 9 of the attached Report. This certification statement is also applicable to each section of the Part 845 Rule listed in **Table 1**.

Table 1 – USEPA CCR Rule and Illinois Part 845 Rule Cross-Reference

| Report Section | U | SEPA CCR Rule | | Illinois Part 845 Rule |
|-------------------|---|----------------------------|----------------------------------|--|
| 3 | §257.73 Hazard Potential (a)(2) Classification | | 845.440 | Hazard Potential Classification Assessment ³ |
| 4 | \begin{cases} \{\}8257.73 \\ (c)(1) \end{cases} \text{ History of Construction} | | 845.220(a) | Design and Construction Plans (Construction History) |
| 5 | §257.73 Structural Stability (d)(1) Assessment | | 845.450 (a) and (c) | Structural Stability Assessment |
| 6 | \$257.73 Safety Factor (e)(1) Assessment | | 845.460 (a-b) | Safety Factor Assessment |
| 7 | \$257.82 Adequacy of (a)(1-3) Design Control | | 845.510(a), (c)(1), (c)(3) | Hydrologic and Hydraulic Capacity Requirements / Inflow Design Flood Control System Plan |
| | §257.82 (b) | Discharge from CCR Unit | 845.510(b) | Discharge from CCR Surface Impoundment |

¹ United Stated Environmental Protection Agency, 2015. 40 CFR Parts 257 and 261, Hazardous and Solid Waste Management System, Disposal of Coal Combustion Residuals from Electric Utilities, Final Rule.

² State of Illinois, Joint Committee on Administrative Rule, Administrative Code (2021). *Title 35: Environmental Protection, Subtitle G: Waste Disposal, Chapter I: Pollution Control Board, Subchapter j: Coal Combustion Waste Surface Impoundment, Part 845 Standards for the Disposal of Coal Combustion Residuals in Surface Impoundments.*

³ "Significant" and "High" hazard, per the CCR Rule¹, are equivalent to Class II and Class I hazard potential, respectively, per Part 845².

Illinois Power Resources Generating Company October 11, 2021 Page 2

CLOSING

This letter has been prepared to demonstrate that the content and Qualified Professional Engineer Certification of the 2021 Periodic USEPA CCR Rule Certification Report fulfills the corresponding requirements of Part 845 of Illinois Administrative Code listed in **Table 1**.

Sincerely,

Lucas P. Carr, P.E.

Senior Engineer

John Seymour, P.E.

Senior Principal

2021 USEPA CCR RULE PERODIC CERTIFICATION REPORT

§257.73(a)(2), (c), (d¹), (e) and §257.82 ASH POND NO. 1 Coffeen Power Plant Coffeen, Illinois

Submitted to

Illinois Power Generating Company

134 Cips Lane Coffeen, Illinois 62017

Submitted by



engineers | scientists | innovators

1 McBride and Son Center Drive, Suite 202 Chesterfield, Missouri 63005

October 11, 2021

¹ Except for §257.73(d)(1)(vi).

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| | | |

EXECUTIVE SUMMARY

This Periodic United States Environmental Protection Agency (USEPA) Coal Combustion Residuals (CCR) Rule [1] certification report (Periodic Certification Report) for Ash Pond No. 1 (AP1)² at the Coffeen Power Plant, also known as the Coffeen Power Station (COF), has been prepared in accordance with Rule 40, Code of Federal Regulations (CFR) §257. herein referred to as the "CCR Rule" [1]. The CCR Rule requires that initial certifications for existing CCR surface impoundment, completed in 2016 and subsequently posted on the Illinois Power Generating Company (IPGC) CCR Website ([2], [3], [4], [5], [6], [7]) be updated on a five-year basis.

The initial certification reports developed in 2016 and 2017 were independently reviewed by Geosyntec ([2], [8], [3], [4], [9], [5], [6], [7]). Additionally, field observations, interviews with plant staff, and evaluations were performed to compare conditions in 2021 at AP1 relative to the 2016 and 2017 initial certifications. These tasks determined that updates are not required for the Initial Hazard Potential Classification and Initial Safety Factor Assessment. However, due to changes at the site and technical review comments, updates were required and were performed for the:

- History of Construction Report,
- Initial Structural Stability Assessment,
- Initial Inflow Design Flood Control System Plan.

Geosyntec's evaluations of the initial certification reports and updated analyses identified that the AP1 meets all requirements for hazard potential classification, history of construction reporting, structural stability, safety factor assessment, and hydrologic and hydraulic control, with the exception of the structural integrity of hydraulic structures (§257.73(d)(1)(vi)), which was certified by others. **Table 1** provides a summary of the initial 2016 certifications and the updated 2021 periodic certifications.

² AP1 is also referred to as ID Number W1350150004-01, Ash Pond 1 by the Illinois Environmental Protection Agency (IEPA); CCR unit ID 101 by IPGC; and IL50722 by the National Inventory of Dams (NID) maintained by the Illinois Department of Natural Resources (IDNR). Within this document it is referred to as API.

Table 1 – Periodic Certification Summary

| | | | | 016 Initial Certification | 2021 Periodic Certification | | |
|----------|-----------------------------|---|-------------------|---|-----------------------------|---|--|
| | CCR Rule | | Requirement | | Requirement | | |
| Section | Reference | Requirement Summary | Met? | Comments | Met? | Comments | |
| Hazard | Potential Classification | | | | | | |
| 3 | §257.73(a)(2) | Document hazard potential classification | Yes | Impoundment was determined to have a Significant hazard potential classification [2]. | Yes | Updates were not determined to be necessary. Geosyntec recommends retaining the Significant hazard potential classification. | |
| History | of Construction | | | | | | |
| 4 | \$257.73(c)(1) | Compile a history of construction | Yes | A History of Construction report was prepared for Ash Pond No. 1 and Ash Pond No. 2, in addition to other CCR surface impoundments at COF [4]. | Yes | A letter listing updates to the History of Construction Report is provided in Attachment C . | |
| | al Stability Assessmen | | 1 | 1 | 1 | | |
| 5 | §257.73(d)(1)(i) | Stable foundations and abutments | Yes | Foundations was found to be stable. Abutments were not present [9]. | Yes | No changes were identified that may affect this requirement. | |
| | §257.73(d)(1)(ii) | Adequate slope protection | Yes | Slope protection was adequate [9]. | Yes | No changes were identified that may affect this requirement. | |
| | \$257.73(d)(1)(iii) | Sufficiency of dike compaction | Yes | Dikes compaction was sufficient for expected ranges in loading conditions [9] . | Yes | No changes were identified that may affect this requirement. | |
| | \$257.73(d)(1)(iv) | Presence and condition of slope vegetation | Yes | Vegetation was present on interior and exterior slopes and was maintained [9]. | Yes | No changes were identified that may affect this requirement. | |
| | §257.73(d)(1)(v)(A) and (B) | Adequacy of spillway design and management | Yes | Spillways were adequately designed and constructed and were expected to adequately manage flow during 1,000-year flood [9]. | Yes | Spillways were found to be adequately designed and constructed and are expected to adequately manger flow during the 1,00-year flood, after performing updated hydrologic and hydraulic analyses. | |
| | §257.73(d)(1)(vi) | Structural integrity of hydraulic structures | No | Requirement could not be certified due to inability to complete a CCTV inspection of the recycle intake pipe due to high sustained pipe flows needed for plant operations. Inspection of this pipe was recommended as soon as feasible [9]. | | cation of \$257.73(d)(1)(vi) was by Luminant in 2020 [10] | |
| | \$257.73(d)(1)(vii) | Stability of downstream slopes inundated by water body. | Not Applicable | Inundation of exterior slopes were not expected. This requirement was not applicable [9]. | Yes | No changes were identified that may affect this requirement. | |
| Safety F | actor Assessment | , | | 11 - 13 | | 1 | |
| 6 | \$257.73(e)(1)(i) | Maximum storage pool safety factor must be at least 1.50 | Yes | Safety factors were calculated to be 1.50 and higher [9]. | Yes | No changes were identified that may affect this requirement. | |
| | \$257.73(e)(1)(ii) | Maximum surcharge pool safety factor must be at least 1.40 | Yes | Safety factors were calculated to be 1.49 and higher [9]. | Yes | No changes were identified that may affect this requirement. | |
| | §257.73(e)(1)(iii) | Seismic safety factor must be at least 1.00 | Yes | Safety factors were calculated to be 1.03 and higher [9]. | Yes | No changes were identified that may affect this requirement. | |
| | §257.73(e)(1)(iv) | For dike construction of soils that have susceptible to liquefaction, safety factor must be at least 1.20 | Not Applicable | Dike soils were not susceptible to liquefaction. This requirement was not applicable [9]. | Yes | No changes were identified that may affect this requirement. | |
| | esign Flood Control S | - | | | | | |
| 7 | §257.82(a)(1), (2), (3) | Adequacy of inflow design control system plan. | Yes | Flood control system adequately managed inflow and peak discharge during the 1,000-year, 24-hour, Inflow Design Flood | Yes | The flood control system was found to adequately manage inflow and peak discharge during the 1,000-year, 24-hour Inflow Design Flood, after performing updated hydrologic and hydraulic analyses. | |
| | \$257.82(b) | Discharge from CCR Unit | Yes | Discharge from the CCR Unit into Waters of the United States were not expected during normal or 1,000-year, 24-hour Inflow Design Flood conditions [9]. | Yes | Discharge from the CCR Unit into Waters of the United States were not expected during normal or 1,000-year, 24-hour Inflow Design Flood conditions, after performing updated hydrologic and hydraulic analyses. | |

SECTION 1

INTRODUCTION AND BACKGROUND

This Periodic United States Environmental Protection Agency (USEPA) Coal Combustion Residual (CCR) Rule [1] Certification Report was prepared by Geosyntec Consultants (Geosyntec) for Illinois Power Generating Company (IPGC) to document the re-certification of the Ash Pond No. 1 (AP1) at the Coffeen Power Plant (CPP), also known as the Coffeen Power Station (COF), located at 134 Cips Lane in Coffeen, Illinois, 62017. The location of CPP is provided in **Figure 1**, and a site plan showing the location of AP1, among other closed and open CCR units and non-CCR surface impoundments, is provided in **Figure 2**.

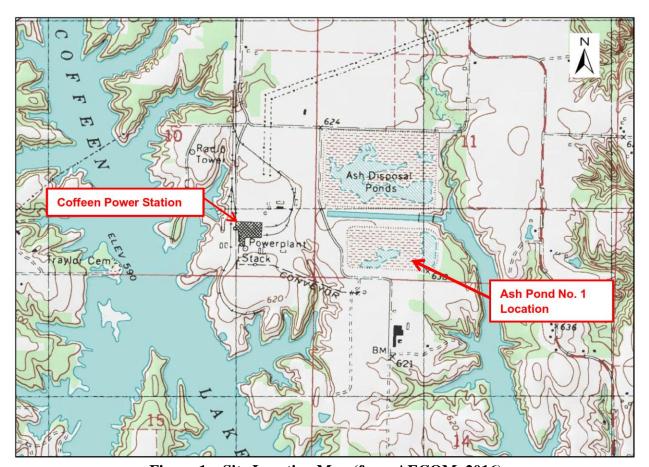


Figure 1 – Site Location Map (from AECOM, 2016)



Figure 2 – Site Plan (modified from AECOM, 2016)

1.1 **AP1 Description**

CPP was retired in 2019. Prior to retirement, three active CCR surface impoundments: the GMF Pond, the GMF Gypsum Recycle Pond, and AP1 and one CCR landfill were used for managing CCRs generated at CPP. AP1 has a Significant hazard potential, based on the initial hazard potential classification assessment performed by Stantec in 2016 in accordance with §257.73(a)(2) ([2], [9]).

AP1 formerly served as the primary wet impoundment basin for bottom ash produced at CPP. AP1 was utilized as a flow-through structure, where outflow was ultimately discharged to Coffeen

Lake, until approximately 1981, when the pond was modified by abandoning the penetrating discharge pipe in the northeast corner of the impoundment, adding a recycle intake structure in the northwest corner, removing some of the accumulated bottom ash, and regrading the remainder of the bottom ash to form a new impoundment flow.

When CPP was operational, outflow from AP1 flowed into the recycle intake structure (outlet pipe) and was transferred back to CPP for use as process water. An approximately 1,300-ft long interior dike creates an interior channel leading to the recycle intake structure. AP1 was operated as a closed-loop hydraulic system as outflow was transmitted back to CPP during normal operational conditions. Bottom ash was mechanically excavated from the southwest corner of AP1 for offsite beneficial use [9].

Sluiced bottom ash from CPP entered AP1 through three steel sluice pipes, which discharged along the western embankment, on the south side of the interior dike. Additional clear water inflow from CPP entered AP1 through two pipes, which discharged at a concrete structure approximately 120 feet north of the sluice pipes, and a 12-in. diameter iron pipe located at the northwest corner of the embankment. Outflow water was transmitted back to CPP via a concrete riser recycle intake structure and 48-in. diameter steel recycle intake pipe located at the northwest corner of AP1, which function as the primary outflow pipe for AP1. The pool level is controlled by a steel spillway gate, which allowed for pool levels ranging from El. 624.5 ft to 631.0 ft³ However, a berm was constructed with bottom ash around the inlet to the spillway after plant closure in 2019 to provide freeze protection for the gate while still allowing overflow during higher pool levels. A secondary 24-in. diameter pipe, which starts as a corrugated metal pipe (CMP) and transitions to steel, is connected to the 48-in. diameter steel recycle intake pipe within the embankment, and was used to discharge excess flow into the process water flume during upset conditions and act as an overflow pipe., but the pipe did not transmit outflow during [9].

The surface area of AP1 is approximately 26.2 acres. The embankment portion of AP1 is comprised of a ring dike with a total length of approximately 4,350 ft and has a maximum height above exterior grade of 30 ft. The embankment was constructed as a homogenous earthen structure with well-compacted clayey fill. An approximately 570-ft long, Hoesch 2500k steel sheet pile wall, is located at the toe of the northeast corner of AP1, to separate the embankment from the plant process water flume. The process water flume was used to transmit plant cooling water back to Coffeen Lake over a series of weirs. The water level in the process water flume was surveyed to be approximately El. 600 ft in 2020, after plant closure [11]. The sheet pile wall was installed around 2000 and driven approximately 13 feet into the foundation soils and has a maximum exposed height of 13.8 feet, for a total pile length of approximately 27 ft. Downstream dike slopes, outside of the sheet pile wall area, range from approximately 1.4H:1V (horizontal to vertical) to 3H:1V and generally are covered in vegetation. Interior embankment slopes are partially covered in bottom ash, vegetation, or gravel and exhibit an approximately 2H:1V orientation. The

5

³ Assumed to be the NGVD29 datum, based on the date of the design drawings, but all other elevations in this report are in the North American Vertical Datum of 1988 (NAVD88), unless otherwise noted.

embankment crest width varies from approximately 14 to 22 feet. An engineered liner system is not present beneath AP1 [9].

The normal maximum normal operating pool of AP1 was 631.0 ft when the plant was operational, as controlled by the recycle intake structure and emergency outflow pipes. The maximum normal operating pool may be different now due to the bottom ash berm placed around the recycle intake structure. The minimum crest elevation is 635.0 ft [9].

Initial certifications for AP1 for Hazard Potential Classification (§257.73(a)(2)), History of Construction (§257.73(c)), Structural Stability Assessment (§257.73(d)), Safety Factor Assessment (§257.73(e)(1)), and Inflow Design Flood Control System Plan (§257.82) were completed by Stantec and AECOM in 2016 and 2017 and subsequently posted to IPGC's CCR Website ([2], [3], [4], [5], [6], [7]). Additional documentation for the initial certifications included detailed operating record reports containing calculations and other information prepared for the hazard potential classification by Stantec [8] and for the structural stability assessment, safety factor assessment, and inflow design flood control system plan by AECOM [9]. These operating record reports were not posted to IPGC's CCR Website.

1.2 Report Objectives

The following objectives are associated with this report:

- Compare site conditions from 2015/2016 to site conditions in 2020/2021, and evaluate if updates are required to the:
 - o §257.73(a)(2) Hazard Potential Classification [2];
 - o §257.73(c) History of Construction [4];
 - o §257.73(d) Structural Stability Assessment [5];
 - o §257.73(e) Safety Factor Assessment [6], and/or
 - o §257.82 Inflow Design Flood Control System Plan [7].
- Independently review the Hazard Potential Classification ([2], [8]), Structural Stability Assessment ([5], [9]), Safety Factor Assessment ([6], [9]), and Inflow Design Flood Control System Plan ([7], [9]) to evaluate whether updates are required based on technical considerations.
- The History of Construction report [4] was not independently reviewed for technical consideration, as this report contained historical information primarily developed prior to promulgation of the CCR Rule [1] for the CCR units at CPP, and did not include

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calculations or other information used to certify performance and/or integrity of the impoundments under §257.73(a)(2)-(3), §257.73(c)-(e), or §257.82.

• Confirm that AP1 meets all of the requirements associated with §257.73(a)(2)-(3), (c), (d), (e), and §257.82, or, if AP1 does not meet any of the requirements, provide recommendations for compliance with that section of the CCR Rule [1].

SECTION 2

COMPARISION OF INITIAL AND PERIODIC SITE CONDITIONS

2.1 Overview

This section describes the comparison of conditions at AP1 between the start of the initial CCR certification program in 2015 and subsequent collection of periodic certification site data in 2020 and 2021.

2.2 Review of Annual Inspection Reports

Annual onsite inspections of AP1 were performed between 2016 and 2020 ([12], [13], [14], [15], [16]) and were certified by a licensed professional engineer in accordance with §257.83(b). Each inspection report stated the following information, relative to the previous inspection:

- A statement that no changes in geometry of the impounding structure were observed since the previous inspection;
- Information on maximum recorded instrumentation readings and water levels;
- Approximate volumes of impounded water and CCR at the time of inspection;
- A statement that no appearances of actual or potential structural weakness or other disruptive conditions were observed; and
- A statement that no other changes which may have affected the stability or operation of the impounding structure were observed.

In summary, the reports did not indicate any significant changes to AP1 between 2015 and 2020. No signs of instability, structural weakness, or changes which may have affected the operation or stability of the AP1 were noted in the inspection reports. The 2019 report [15] indicated that approximately 5 acre-feet (8,100 cubic yards) of CCR was removed from AP1 in 2019 for beneficial use, and the 2020 report noted that CPP had closed in 2019.

2.3 Review of Instrumentation Data

Eight piezometers, COF-P000, COF-P001, COF-P002, COF-P003, COF-P005, COF-P006, COF-P007, and COF-P008, are present at AP1 have been monitored monthly by CPP staff since August 29, 2015. Geosyntec reviewed the piezometer data collected through April 22, 2021 to evaluate if significant fluctuations, partially increases in phreatic levels, may have occurred between development of the initial structural stability and factor of safety certifications ([9], [5], [6]) and April 22, 2021. Available piezometer readings are plotted in **Attachment A**.

In summary, only minor changes in phreatic conditions were observed in the available piezometric data. Phreatic levels typically varied by one to five feet for most piezometers, with average levels remaining steady and not exhibiting any sustained trends of increase or decrease. These changes do not indicate significantly different phreatic levels than those utilized for the initial structural stability and factor of safety certifications ([9], [5], [6]).

2.4 Comparison of Initial to Periodic Surveys

The initial survey of AP1, conducted by Weaver Consultants (Weaver) in 2015 [17], was compared to the periodic survey of AP1, conducted by IngenAE, LLC (IngenAE) in 2020 [11], using AutoCAD Civil3D 2021 software. This comparison quantified changes in the volume of CCR placed within AP1 and considered volumetric changes above and below the starting water surface elevation (SWSE) used for the initial §257.82 inflow design flood control plan hydraulic analysis [7]. Potential changes to embankment geometry were also evaluated.

This comparison is presented in side-by-side views of each survey in **Drawing 1** and a plan view isopach map denoting changes in ground surface elevation in **Drawing 2**. A summary of the water elevations and changes in CCR volumes is provided in **Table 1**.

Table 2 – 2015 and 2020 Survey Comparison

| Initial Surveyed Pool Elevation (ft) | 629.9 |
|--|--------|
| Periodic Surveyed Pool Elevation (ft) | 629.2 |
| Initial §257.82 Starting Water Surface Elevation (SWSE) (ft) | 631.0 |
| Total Change in CCR Volume (CY) | +3,550 |
| Change in CCR Volume Above SWSE (CY) | +2,877 |
| Change in CCR Volume Below SWSE (CY) | +673 |

The comparison indicated that approximately 2,900 CY of CCR was placed in AP1 between 2015 and 2020 above the SWSE, thereby leading to a potential for the peak water surface elevation (PWSE) to increase slightly during the inflow design 1,000-year flood event. No significant changes to embankment geometry appeared to have occurred between the initial and periodic surveys, although changes in CCR disposal grades within the impoundment were noted, reportedly due to excavation of bottom ash for beneficial use.

2.5 <u>Comparison of Initial to Periodic Aerial Photography</u>

Initial aerial photographs of AP1 collected by Weaver in 2015 [17] were compared to periodic aerial photographs collected by IngenAE in 2020 [17] to visually evaluate if potential site changes (i.e., changes to the embankment, outlet structures, limits of CCR, other appurtenances) may have occurred. A comparison of the aerial photographs is provided in **Drawing 3**, and the following change was identified:

• The water level within the cooling water discharge channel leading to Coffeen Lake was observed to be lower (approximately El. 600 ft, as indicated by the 2020 survey [11]), likely due to closure of the CPP power plant and cessation of cooling water discharge.

2.6 Comparison of Initial to Periodic Site Visits

An initial site visit to AP1 was conducted by AECOM in 2015 and documented with a Site Visit Summary and corresponding photographs [18]. A periodic site visit was conducted by Geosyntec on May 28, 2021, with Mr. Lucas P. Carr, P.E. conducting the site visit. The site visit was intended to evaluate potential changes at the site since the initial certifications were prepared (i.e., modification to the embankment, outlet structures or other appurtenances, limits of CCR, maintenance programs, repairs), in addition to performing visual observations of AP1 to evaluate if the structural stability requirements (§257.73(d)) were still met. The site visit included walking the perimeter of AP1, visually observing conditions, recording field notes, and collecting photographs. The site visit is documented in a field observation form and photographic log provided in **Appendix A**. A summary of significant findings from the periodic site visit is provided below:

- Overall site maintenance appeared to have improved since 2015, with the exception of continued tree growth at the top of the sheet pile wall. Geosyntec recommended cutting the trees to IPGC staff as part of routine site maintenance activities.
- A berm of bottom ash was observed to have been installed around the inlet to the Recycle Intake Structure, reportedly to reduce freeze-thaw concerns.
- Seepage was observed at the east and south dikes of AP1. Geosyntec recommended to IPGC staff that the seepage be monitored during routine inspections.
- No signs of structural instability or erosion were observed during the site visit.

2.7 <u>Interview with Power Plant Staff</u>

An interview with Mr. John Romang of CPP was conducted by Mr. Lucas P. Carr, P.E. of Geosyntec on May 28, 2021. Mr. Romang had been employed, at the time of the interview, by CPP for approximately 20 years as the environmental and chemistry manager and supervisor. His responsibilities included general oversight and environmental compliance, including weekly impoundment inspections and identifying items requiring repair. The interview included a discussion of potential changes that may have occurred at AP1 since the development of the initial certifications ([2], [8], [3], [4], [9], [5], [6], [7]).

• Were any construction projects completed for AP1 between 2015 and 2021, and, if so, are design drawings and/or details available?

- No construction projects were completed.
- Were there any changes to the purpose of AP1 between 2015 and 2017?
 - o CPP was closed in October of 2019 and CCR placement stopped at that time.
 - Beneficial use contractors continued mining the AP1 for some time after closure, until CCR viable for beneficial use was no longer encountered.
- Were there any changes to the to the instrumentation program and/or physical instruments for AP1 between 2015 and 2021?
 - No known changes occurred.
- Were there any changes to spillways and/or diversion features for AP1 completed between 2015 and 2021?
 - The inlet to the Recycle Intake Structure was partially blocked with a berm of bottom ash in 2019, after plant closure, to provide freeze protection. Overflow into the Recycle Intake Structure will still occur at higher pool levels.
- Were there any changes to construction specifications, surveillance, maintenance, and repair procedures for AP1 between 2015 and 2021?
 - No known changes occurred.
- Were there any instances of dike and/or structural instability for AP1 between 2015 and 2021?
 - o No known instance of dike and/or structural instability occurred.

SECTION 3

HAZARD POTENTIAL CLASSIFICATION - §257.73(A)(2)

3.1 Overview of Initial HPC

The Initial Hazard Potential Classification (Initial HPC) was prepared by Stantec Consulting Services, Inc. (Stantec) in 2016 ([2], [8]), following the requirements of §257.73(a)(2). The Initial HPC included the following information:

- Results of two breach analyses using HEC-HMC software [19], using pool levels estimated
 within AP1 during the Probable Maximum Precipitation (PMP) rainfall event, for breaches
 occurring at the northeast and northwest corners of AP1.
- Evaluating potential effects of flooding in multiple areas, including breach flood wave velocities, flood depths, and/or pool increases, for the following locations:
 - Coffeen Lake, including the eastern cove (east of AP1) and the main lake (west of AP1),
 - o Coffeen Lake Dam,
 - o Coffeen Power Plant, including the building and parking lots,
 - o AP1 recycle pump house,
 - o Coal yard maintenance buildings near AP1, and
 - o Abandoned coal mining structures south of AP1.
- While a breach map is not included within the Initial HPC, it is included within the §257.73(a)(3) Initial Emergency Action Plan (Initial EmAP) [2].

The breach analysis concluded that a breach of AP1 would impact non-occupied CPP structures and lightly used access roads, where the populations at risk were considered transient and there would be no probable loss of life. Probable loss of life differentiates high hazard potential from significant hazard potential classification. The analysis found that a breach could impact several buildings with regular occupancy, but that the depth-velocity relationships of the breach wave did not constitute a probable loss of life. The Initial HPC concluded that neither breach would be likely to result in a probable loss of human life, although the breach could cause CCR to be released into the Coffeen Lake, thereby causing environmental damage. The Initial HPC therefore recommended a "Significant" hazard potential classification for AP1 [2].

3.2 **Review of Initial HPC**

Geosyntec performed a review of the Initial HPC ([2], [8]), in terms of technical approach, input parameters, and assessment of results. The review included the following tasks:

- Reviewing the rainfall depths utilized in the breach analysis for appropriateness,
- Reviewing the breach assessment inputs for appropriateness,
- Reviewing the selected HPC for appropriateness based on the results of the breach analysis, including flow velocities and depths,
- Reviewing the HPC vs. applicable requirements of the CCR Rule.

No significant technical issues were noted within the technical review; a detailed review (e.g., check) of the calculations was not performed.

3.3 Summary of Site Changes Affecting the Initial HPC

Geosyntec did not identify any changes at the stie that may affect the HPC. No new structures, infrastructure, frequently occupied facilities/areas, or waterways were present in the probable breach area indicated in the Initial EmAP [3]. Additionally, no significant changes to the topography in the probable breach were identified.

3.4 Periodic HPC

Geosyntec recommends retaining the "Significant" hazard potential classification for AP1, per §257.73(a)(2), based on the lack of site changes potentially affecting the Initial HPC occurring since the initial HPC was developed, as described in **Section 3.3**, and the lack of significant review comments, as described in **Section 3.2**. Updates to the Initial HPC reports ([2], [8]) are not recommended at this time.

HISTORY OF CONSTRUCTION REPORT - §257.73(C)

4.1 Overview of Initial HoC

The Initial History of Construction report (Initial HoC) was prepared by AECOM in 2016 [4], following the requirements of §257.73(c), and included information on all CCR surface impoundments at CPP, including AP1, AP2, the GMF Pond, and the GMF Recycle Pond. The Initial HoC included the following information for each CCR surface impoundment:

- The name and address of the owner/operator,
- Location maps,
- Statements of purpose,
- The names and size of the surrounding watershed,
- A description of the foundation and abutment materials,
- A description of the dike materials,
- Approximate dates and stages of construction,
- Available design and engineering drawings,
- A summary of instrumentation,
- Area-capacity curves for AP1,
- Information on spillway structures,
- Construction specifications,
- Inspection and surveillance plans,
- Information on operational and maintenance procedures, and
- Information on past sloughs in the embankments for AP1.

4.2 Summary of Site Changes Affecting the Initial HoC

Several significant changes at the site were identified since development of the initial HoC and required updates to the HoC report. Each change is described below.

- A state identification number (ID) of W1350150004-01 was assigned to AP1 by the Illinois Environmental Protection Agency (IEPA).
- Electricity generation at the CPP ceased in 2019 and AP1 is no longer being used to actively store CCR generated by CPP as CCR is no longer being generated. Additionally, AP1 no longer receives regular process water inflows or outflows.
- A berm of bottom ash was constructed around the AP1 recycle intake structure.
- Revised area-curves and spillway design calculations for AP1 were prepared as part of the updated Periodic Inflow Design Flood Control System Plan, as described in **Section 6.3**.

A letter documenting changes to the HoC report is provided in **Attachment C**.

STRUCTURAL STABILITY ASSESSMENT - §257.73(D)

5.1 Overview of Initial SSA

The Initial Structural Stability Assessment (Initial SSA) was prepared by AECOM in 2016 [9], following the requirements of §257.73(d)(1), and included the following evaluations:

- Stability of dike foundations, dike abutments, slope protection, dike compaction, and slope vegetation;
- Spillway stability including capacity, structural stability and integrity, including using closed-circuit television (CCTV) equipment to inspect the interior of the 24-in. diameter secondary overflow pipe;
- An evaluation of the effects of liquefaction in the foundation soils using a slope stability analysis considering post-cyclic softening in the foundation soils; and
- Downstream slope stability under sudden drawdown conditions for a downstream water body.

The Initial SSA concluded that AP1 met all structural stability requirements for §257.73(d)(1)(i)-(v) and (vii), but recommended inspection of the 48-in. diameter recycle intake pipe to verify that AP1 meets the stability and structural integrity criteria for hydraulic outfall structures, per §257.73(d)(1)(vi). An inspection of this spillway pipe was not performed in 2015 or 2016 due to high sustained flows in the pipe being critical for plant operations.

A periodic certification of the structural stability and structural integrity of hydraulic outfall structures (§257.73(d)(1)(vi)) was performed by Luminant in 2020 [10]. This certification independently determined that the criteria was met due to the condition of the spillway pipes and the soil types within the embankment. Therefore, the review and certification of §257.73(d)(1)(vi) was not included within the scope of this report.

The Initial SSA referenced the results of the Initial Structural Factor Assessment (Initial SFA) ([6], [9]), to demonstrate stability of the stability of foundations and abutments (§257.73(d)(1)(i)) and sufficiency of dike compaction (§257.73(d)(1)(iii)) portions of the SSA criteria. This included stating that slope stability analyses for slip surfaces passing through the foundation met or exceeded the criteria listed in §257.73(e)(1), for the stability of foundations and abutments. For the sufficiency of dike compaction, this included stating that slope stability analyses for slip surfaces passing through the dike also met or exceeded the §257.73(e)(1) criteria.

5.2 **Review of Initial SSA**

Geosyntec performed a review of the Initial SSA ([5], [9]) in terms of technical approach, calculation input parameters and methodology, recommendations, and completeness. The review included the following tasks:

- Reviewing photographs collected in 2015 and used to demonstrate compliance with §257.73(d)(1)(i)-(vii).
- Reviewing geotechnical calculations used to demonstrate the stability of foundations, per §257.73(d)(1)(i) and sufficiency of dike compaction, per §257.73(d)(1)(iii), in terms of supporting geotechnical investigation and testing data, input parameters, analysis methodology, selection of critical cross-sections, and loading conditions.
- Review of the methodology used to demonstrate that a downstream water body that could induce a sudden drawdown condition, per §257.73(d)(1)(vii), is not present.
- Reviewing the contents vs. the applicable CCR Rule requirements [1].

No significant technical issues were noted within the technical review of the Initial SSA. A detailed review (e.g., check) of the calculations was not performed.

5.3 Summary of Site Changes Affecting the Initial SSA

Several changes at the site that occurred after development of the Initial SSA were identified. These changes required updates to the Initial SSA and are described below:

• The Initial SSA utilized the results of the Initial Inflow Design Flood Control System Plan (IDF) to demonstrate compliance with the adequacy of spillway design and management (§257.73(d)(1)(v)(A)-(B)). The Initial IDF was subsequently updated to develop a Periodic IDF, based on site changes, as discussed in **Section 7**.

5.4 Periodic SSA

The Periodic IDF (**Section 7**) indicates that spillways are adequately designed and constructed to adequately manage flow during the 1,000-year flood, as the spillways can adequately manage flow during peak discharge from the 1,000-year storm event without overtopping of the embankments. Therefore, the requirements of \$257.73(d)(1)(v)(A)-(B) are met for the Periodic SSA.

Certification of §257.73(d)(1)(vi) was independently performed by Luminant [10].

SAFETY FACTOR ASSESSMENT - §257.73(E)(1)

6.1 Overview of Initial SFA

The Initial Safety Factor Assessment (Initial SFA) was prepared by AECOM in 2016 ([6], [9]), following the requirements of §257.73(e)(1). The Initial SFA included the following information:

- A geotechnical investigation program with in-situ and laboratory testing;
- An assessment of the potential for liquefaction in the dike and foundation soils;
- The development of five slope stability cross-sections for limit equilibrium stability analysis utilizing GeoStudio SLOPE/W software; and
- The analysis of each cross-section for maximum storage pool, maximum surcharge pool, and seismic loading conditions.
 - Liquefaction loading conditions were not evaluated as liquefaction-susceptible soil layers were not identified in the either the embankments or foundation soils.

The Initial SFA concluded that AP1 met all safety factor requirements, per §257.73(e), as all calculated safety factors were equal to or higher than the minimum required values.

6.2 Review of Initial SFA

Geosyntec performed a review of the Initial SFA ([6], [9]) in terms of technical approach, calculation input parameters and methodology, recommendations, and completeness. The review included the following tasks:

- Reviewing geotechnical calculations used to demonstrate the acceptable safety factors, per §257.73(e)(1), in terms of:
 - Completeness and adequacy of supporting geotechnical investigation and testing data;
 - o Completeness and approach of liquefaction triggering assessments; and
 - Input parameters, analysis methodology, selection of critical cross-sections, and loading conditions utilized for slope stability analyses.
 - o Phreatic conditions based on piezometric data collected between August 29, 2015 and April 22, 2021 as discussed in **Section 2.3**.

No significant technical issues were noted within the technical review. A detailed review (e.g., check) of the calculations was not performed.

6.3 Summary of Site Changes Affecting the Initial SFA

No changes since development of the Initial SFA were identified that would require updates to the Initial SFA ([6], [9]). For example, starting and peak water surface elevations from the updated Periodic IDF (**Section 7**) were both calculated to be less than level levels used within the slope stability analyses associated with the Initial SFA. Therefore, the water levels within the Initial SFA slope stability analyses are conservative and updates to the analyses were not recommended and were not performed.

INFLOW DESIGN FLOOD CONROL SYSTEM PLAN - §257.82

7.1 Overview of Initial IDF

The Initial Inflow Design Flood Control System Plan (Initial IDF) was prepared by AECOM in 2016 ([7], [9]) following the requirements of §257.82. The Initial IDF included the following information:

- A hydraulic and hydrologic analysis, performed for the 1,000-year design flood event because of the hazard potential classification of "Significant", which corresponded to 9.13 inches of rainfall over a 24-hour period.
- The Initial IDF utilized a HydroCAD Version 10 model to evaluate spillway flows and pool level increases during the design flood, with a SWSE of 631.0 ft.

The Initial IDF concluded that AP1 met the requirements of §257.82, as the peak water surface estimated by the HydroCAD model was El. 632.0 ft, relative to the minimum AP1 dike crest elevation of 635.0 ft. Therefore, overtopping was not expected. The Initial IDF also evaluated the potential for discharge from the CCR unit and determined that discharge from the unit was note expected, as AP1 does not discharge into waters of the United States and overtopping of the AP1 embankments was not expected during the 1,000-year inflow design flood.

7.2 Review of Initial IDF

Geosyntec performed a review of the Initial IDF ([7], [9]) in terms of technical approach, calculation input parameters and methodology, recommendations, and completeness. The review included the following tasks:

- Reviewing the return interval used vs. the hazard potential classification.
- Reviewing the rainfall depth and distribution for appropriateness.
- Performing a high-level review of the inputs to the hydrological modeling.
- Reviewing the hydrologic model parameters for spillway parameters, starting pool elevation, and storage vs. the reference data.
- Reviewing the overall Initial IDF vs. the applicable requirements of the CCR Rule [1].

Several comments were identified during review of the Initial IDF. The comments are described below:

- The Initial IDF utilized the National Resource Conservation Service (NRCS) Type II rainfall distribution type [20]. Geosyntec utilized the Huff 3rd Quartile distribution for areas less than 10 square miles [21] for the reasons listed below.
 - Huff 3rd Quartile distribution was identified to be a more appropriate representation of a 1,000-year, 24-hour storm event per the Illinois State Water Survey (ISWS)
 Circular 173 [22] which developed standardized rainfall distributions from compiled rainfall data at sites throughout Illinois.
 - OWR) [23] recommends use of the Huff Quartile distributions in Circular 173 when using frequency events to determine the spillway design flood inflow hydrograph, "The suggested method to distribute this rainfall is described in the ISWS publication, Circular 173, "Time Distributions of Heavy Rainstorms in Illinois".

7.3 Summary of Site Changes Affecting the Initial IDF

Several changes at the site that occurred after development of the Initial IDF were identified. These changes required updates to the Initial IDF and are described below:

- A bottom ash berm was constructed around the recycle outlet structure, thereby the outlet structure configuration utilized in the Initial IDF was no longer consistent with conditions observed in 2020.
- Approximately 2,900 CY of CCR were placed in AP1 above the SWSE utilized for the Initial IDF, thereby altering the stage-storage curve for AP1 relative to the Initial IDF. Process inflows to AP1 have ceased due to the closure of the CPP power plant, thereby the process inflow conditions utilized in the Initial IDF were no longer consistent with conditions observed in 2020.

7.4 Periodic IDF

Geosyntec revised the HydroCAD model associated with the Initial IDF to account for the revised rainfall distribution type, increase in SWSE, and additional CCR placement, as described in **Sections 7.2** and **7.3**. The following approach and input data were used for the revised analyses and are referenced in **Attachment D** as appropriate:

• Updated the time of concentration associated with Ash Pond No. 1 from 5 minutes to 6 minutes in accordance with TR-20 [24].

- Updated stage-storage curve for Ash Pond No. 1 based on the 2020 site survey [11].
 - O A revised stage-volume curve for Ash Pond No. 1 was prepared based on measuring the storage volume of Ash Pond No. 1 at every one-foot increment of depth from an elevation just beneath the SWSE (630.0 ft) to the perimeter dike embankment crest elevation (636.0 ft). This analysis identified an overall increase of 539,887 cf (12 ac-ft) of storage volume at Ash Pond No. 1 from 2016 to 2021 relative to the SWSE used in the Initial IDF.

• Starting Water Surface Elevation

- o Based on information provided by site personnel, a bottom ash berm is located 30 inches below the top of the concrete outlet structure. A top of concrete elevation of 632.7 ft for the outlet structure was assumed based on the 2015 site survey [25]; therefore, a top of berm elevation of 630.2 ft was used for the bottom ash berm. For this analysis, the SWSE was updated from 631.0 ft to 630.2 ft to reflect the top elevation of the bottom ash berm as described by site personnel, and the lowest free discharge elevation was set at 632.7 ft based on the surveyed 24-inch riser elevation in 2015 [25]. The 2020 site survey showed a WSE of 629.17 ft; however, the top elevation of the bottom ash berm is higher than the surveyed WSE and was used as the SWSE to provide conservatism in the model.
- The rainfall distribution type was updated to the Huff 3rd Quartile for areas less than 10 square miles storm type provided by HydroCAD [26].
- The precipitation depth for the 1,000-yr, 24-hr design storm event was updated from 9.13 in. to 9.14 in. per NOAA Atlas 14 precipitation frequency estimates **Invalid source specified.**.
- The outlet structure for AP1 was updated as follows:
 - The discharge multiplier for the weir (i.e., top of the riser structure) was updated from 0 to 1.
 - The top of riser structure elevation was updated from 631.0 ft to 632.7 ft (i.e., top of concrete) per the 2015 site survey. The assumption that 100 percent of the flow is routed through the 24-inch circular horizontal orifice was maintained for conservatism in the model.
 - The length of 48-inch steel pipe was updated from 100 linear feet (LF) to 10 LF to account for a tee into the 24-inch cast iron pipe as described by site personnel. The pipe was assumed to be blocked beyond the tee as the CPP is no longer active and the recycle pump house downstream of the tee is no longer pumping water out of AP1. A slope of 0.17 ft/ft was maintained, and the outlet invert was updated from 607.0 ft to 622.3 ft based on the presumed tee elevation.

- O Added 92 LF of 24-inch cast iron pipe and 171 LF of 24-inch corrugated metal pipe based on an overflow assessment conducted in 2011. The inlet invert was set at 622.3 ft based on the approximate tee location, and the outlet invert was set at 600.0 ft per the 2020 site survey.
- All other input data and settings from the Initial IDF HydroCAD model were utilized, including, but not limited to software package and version, runoff method, analysis time span and analysis time step.

The results of the Updated IDF are summarized in **Table 4** and confirm that AP1 meets the requirements of §257.82(a)-(b), as the peak water surface elevation does not exceed the minimum perimeter dike crest elevation, as long as the SWSE is maintained ate El. 630.2 ft or lower. Based on the Periodic IDF analysis, the peak WSE is 631.4 ft, which is below the riser opening elevation of 632.7. Therefore, there is no discharge from AP1 during normal and inflow design flood conditions and discharge into Waters of the United States is not expected during either normal or inflow design flood conditions. Updated area-capacity curves and HydroCAD model output is provided in **Attachment D**.

Table 3 - Water Levels from Periodic IDF

| | Ash Pond No. 1 | | | |
|---|------------------------|--------------------|--------------------|--|
| | Starting Water Surface | Peak Water Surface | Minimum Dike Crest | |
| Analysis | Elevation (ft) | Elevation (ft) | Elevation (ft) | |
| Initial IDF | 631.0 | 632.0 | 636.0 | |
| Periodic IDF Update | 630.2 | 631.4 | 636.0 | |
| Initial to Periodic Change ¹ | -0.8 | -0.6 | 0.0 | |

Notes:

¹Positive change indicates increase in the WSE relative to the Initial IDF; negative changes indicate decrease in the WSE, relative to the Initial IDF.

CONCLUSIONS

AP1 at CPP was evaluated relative to the USPEPA CCR Rule periodic assessment requirements for:

- Hazard potential classification (§257.73(a)(2));
- History of Construction reporting (§257.73(d));
- Structural stability assessment (§257.73(d)), with the exception of §257.73(d)(1)(vi) that was independently certified by Luminant [10];
- Safety factor assessment (§257.73(e)); and
- Inflow design flood control system planning (§257.82).

Based on the evaluations presented herein, the referenced requirements are satisfied.

CERTIFICATION STATEMENT

CCR Unit: Illinois Power Generating Company, Coffeen Power Plant, Ash Pond No. 1

I, Lucas P. Carr, being a Registered Professional Engineer in good standing in the State of Illinois, do hereby certify, to the best of my knowledge, information, and belief that the information contained in this 2021 USEPA CCR Rule Periodic Certification Report, has been prepared in accordance with the accepted practice of engineering. I certify, for the above-referenced CCR Unit, that the periodic assessment of the hazard potential classification, history of construction report, structural stability, safety factors, and inflow design flood control system planning, dated October 2021, were conducted in accordance with the requirements of 40 CFR §257.73(a)(2), (c), (d), (e), and §257.82, with the exception of §257.73(d)(1)(vi)) that was independently certified by others.

Lucas P. Carr

10/11/2021

- 1.6

Date

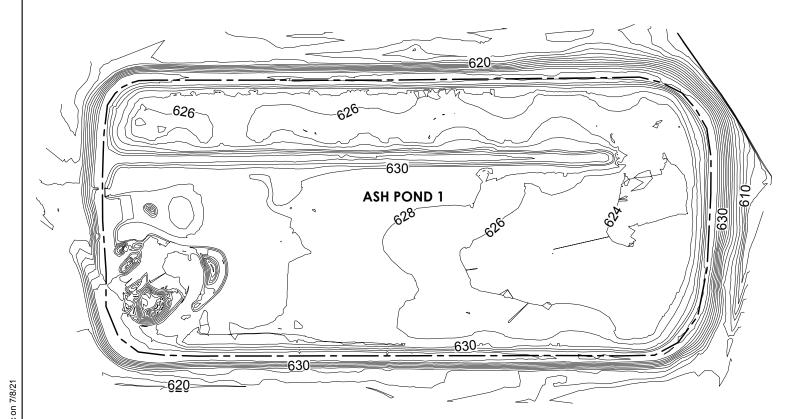
REFERENCES

- [1] United States Environmental Protection Agency, 40 CFR Parts 257 and 261; Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities; Final Rule, 2015.
- [2] Stantec Consulting Services, Inc., "Initial Hazard Potential Classification Assessment, EPA Final CCR Rule, Ash Pond No. 1, Coffeen Power Station, Montgomery County, Illinois," Fenton, Mo, October 12, 2016.
- [3] Stantec Consulting Services, Inc., "Illinois Power Generating Company, Coffeen Power Station, Montgomery County, Illinois, Emergency Action Plan (EAP)," Fenton, MO, April 13, 2017.
- [4] AECOM, "History of Construction, USEPA Final CCR Rule, 40 CFR §257.73(c), Coffeen Power Station, Coffeen, Illinois," October 2016.
- [5] AECOM, "CCR Rule Report: Initial Structural Stability Assessment for Ash Pond No. 1 at Coffeen Power Station," St. Louis, MO, October 2016.
- [6] AECOM, "CCR Rule Report: Initial Safety Factor Assessment For Ash Pond No. 1 at Coffeen Power Station," St. Louis, MO, October 2016.
- [7] AECOM, "CCR Rule Report: Initial Inflow Design Flood Control System Plan For Ash Pond No. 1 at Coffeen Power Station," St. Louis, MO, October 2016.
- [8] Stantec Consulting Services, Inc., "Documentation of Initial Hazard Potential Classification Assessment, Ash Pond No. 1, Coffeen Power Station, Montgomery County, Illinois," October 12, 2016.
- [9] AECOM, "CCR Certification Report: Initial Structural Stability Assessment, Initial Safety Factor Assessment, and Initial Inflow Design Flood Control System Plan for Ash Pond No. 1 at Coffeen Power Station," St. Louis, MO, October 2016.
- [10] V. Modeer, "Ash Pond No. 1 Structural Stability Assessment, Illinois Power Resrouces Generationg, LLC, Coffeen Power Station," Luminant, November 30, 2020.
- [11] IngenAE, "Luminant, Illinois Power Generating Company, Coffeen Power Station, December 2020 Topography," February 26, 2021.
- [12] J. Knutelski and J. Cambpbell, *Annual CCR Surface Impoundment Inspection (per 40 CFR 257.83(b)(2)), Coffeen Power Station, Ash Pond No. 1, January 18, 2017.*
- [13] J. Knutelski and J. Campbell, Annual CCR Surface Impoundment Inspection Report (per 40 CFR 257.83(b)(2)), Coffeen Power Station, Ash Pond No. 1, February 7, 2018.
- [14] J. Knutelski, *Inspection by a Qualified Professional Engineer*, 40 CFR §257.73(b), Coffeen Power Station, Ash Pond No. 1, December 28, 2018.
- [15] J. Knutelski, Annual Inspection by a Qualified Professional Engineer, 40 CFR §257.73(b), Coffeen Power Station, Ash Pond No. 1, January 8, 2020.

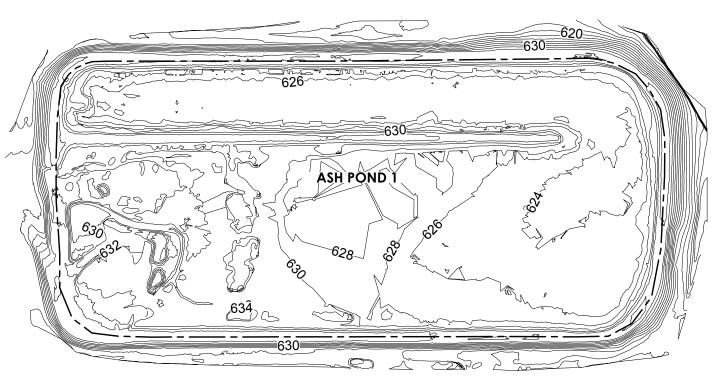
- [16] J. Knutelski, Annual Inspection by a Qualified Professional Engineer, Coffeen Power Station, Ash Pond No. 1, January 6, 2021.
- [17] Weaver Consultants Group, "Dynegy, Collinsville, IL, 2015 Coffeen Topography," December 1, 2015.
- [18] AECOM, "CCR Unit Initial Site Visit Summary, Dynegy CCR Compliance Program, Coffeen Power Station Ash Pond No. 1," June 18, 2015.
- [19] US Army Corps of Engineers, "Hydrologic Modeling System (HEC-HMS), Version 4.0," Hydrologic Engineering Center, 2013.
- [20] C. E. D. National Resources Conservation Service, "Urban Hydrology for Small Watersheds (TR-55)," United States Department of Agriculture, 1985.
- [21] F. A. Huff and J. R. Angel, "Frequency Distributions and Hydroclimatic Characteristics of Heavy Rainstorms in Illinois," State Water Survey Division, Department of Energy and Natural Resources, Champaign, Illinois, 1989.
- [22] F. Huff, "Time Distributions of Heavy Rainstorms in Illinois," State Water Survey Division, Department of Energy and Natural Resources, Champaign, Illinois, 1990.
- [23] Office of Natural Resources, "Procedural Guidelines for Preparation of Technical Data to be included in Applications for Permits for Construction and Maintenance of Dams," Department of Natural Resoruces, State of Illinois, Springfield, Illinois, Undated.
- [24] U. N. R. C. Service, "WinTR-20 Project Formulation Hydrology, Verion 3.20".
- [25] Weaver Consultants Group, *Dynegy Collinsville*, *IL*, 2015 Coffeen Topography, December, 2015.
- [26] L. HydroCAD Software Solutions, "HydroCADTM Stormwater Modeling System, Version 10," Chocorua, New Hampshire, 2016.

DRAWINGS





INITIAL SURFEY 12-01-2015 TOPOGRAPHY



PERIODIC SURVEY 02-26-2021 TOPOGRAPHY

NOTES:

- 1. THE INITIAL SURVEY WAS TAKEN FROM THE DRAWING PACKAGE TITLED "DYNEGY, COLLINSVILLE, ILLINOIS, 2015 COFFEEN TOPOGRAPHY", PREPARED BY WEAVER CONSULTANTS GROUP, DATED DECEMBER 1, 2015.
- 2. THE PERIODIC SURVEY WAS TAKEN FROM THE DRAWING PACKAGE TITLED "LUMINANT, ILLINOIS POWER GENERATING COMPANY, COFFEEN POWER STATION, DECEMBER 2020 TOPOGRAPHY", PREPARED BY INGENAE, DATED FEBRUARY 26, 2021.
- 3. ALL SURVEY DATA WAS COLLECTED IN THE NORTH AMERICAN VERTICAL DATUM OF 1988 (NAVD88) AND NORTH AMERICAN DATUM OF 1983 (NAD83) FOR VERTICAL AND HORIZONTAL COORDINATES, RESPECTIVELY.



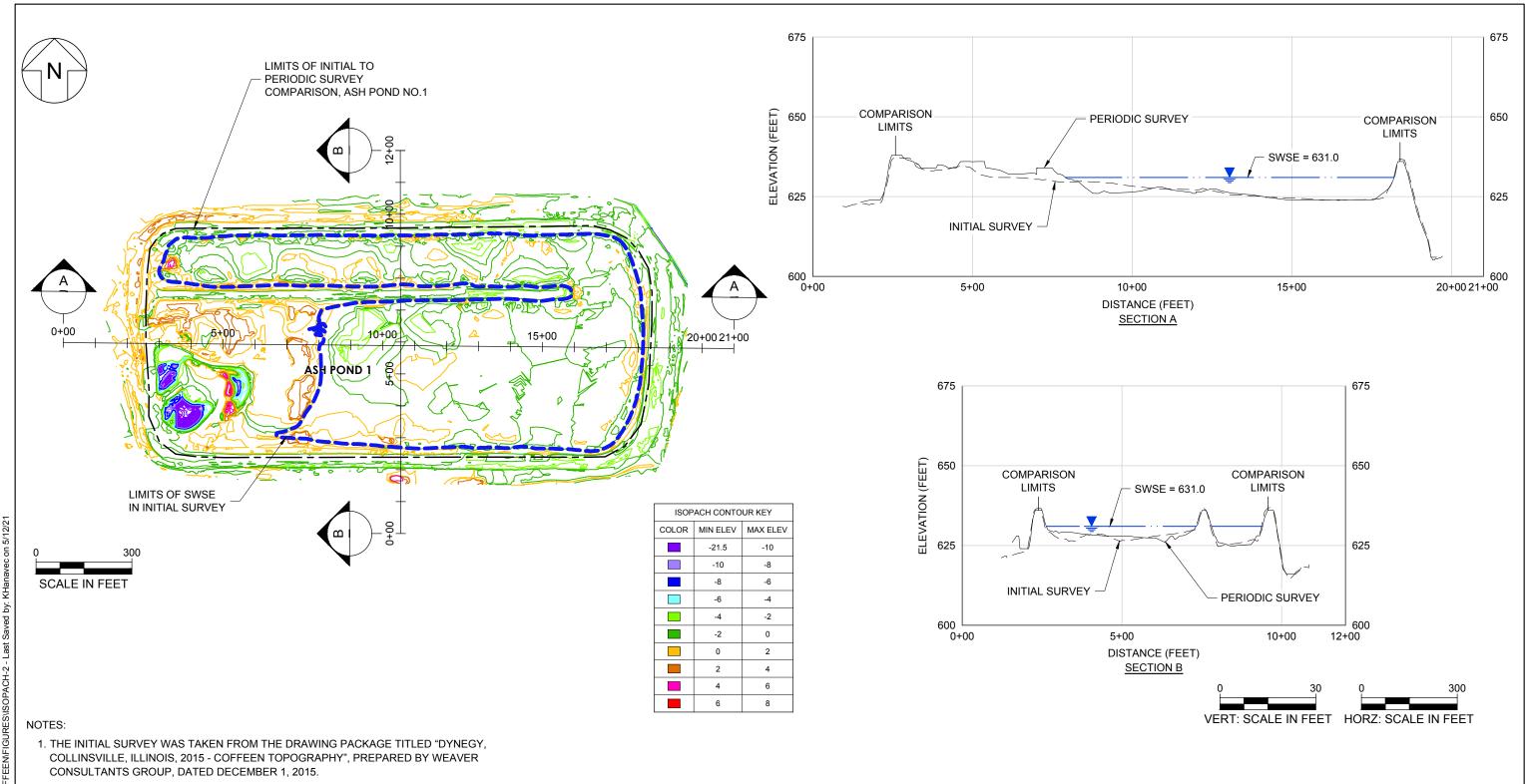
INITIAL TO PERIODIC SURVEY COMPARISON
PLANT ASH POND 1
COFFEEN POWER PLANT
COFFEEN, ILLINOIS

| Geosyntec ^D | |
|------------------------|--|
| consultants | |

GLP8027.02

JULY 2021

DRAWING



- 2. THE PERIODIC SURVEY WAS TAKEN FROM THE DRAWING PACKAGE TITLED "LUMINANT, ILLINOIS POWER GENERATING COMPANY, COFFEEN POWER STATION, DECEMBER 2020 TOPOGRAPHY", PREPARED BY INGENAE, DATED FEBRUARY 26, 2021.
- 3. ALL SURVEY DATA WAS COLLECTED IN THE NORTH AMERICAN VERTICAL DATUM OF 1988 (NAVD88) AND NORTH AMERICAN DATUM OF 1983 (NAD83) FOR VERTICAL AND HORIZONTAL COORDINATES, RESPECTIVELY.
- 4. THE MAXIMUM OPERATING POOL ELEVATION OF ASH POND NO. 1 IS EL. 631.0 FT, AS NOTED IN THE REPORT TITLED "CCR CERTIFICATION REPORT: INITIAL STRUCTURAL STABILITY ASSESSMENT, INITIAL SAFETY FACTOR ASSESSMENT, AND INITIAL INFLOW DESIGN FLOOD CONTROL SYSTEM PLAN FOR ASH POND NO. 1 AT COFFEEN POWER STATION", PREPARED BY AECOM, DATED OCTOBER, 2016.

| INITIAL TO PERIODIC SURVEY COMPARISON SUMMARY | | | | | |
|---|--------|--------|---------------|--|--|
| SURFACE IMPOUNDMENT | CUT | FILL | NET (CU. YD.) | | |
| ASH POND 1 | 20,726 | 24,277 | 3,550 (FILL) | | |
| ABOVE SWSE | 9,611 | 12,488 | 2,877 (FILL) | | |
| BELOW SWSE | 11,118 | 11,789 | 673 (FILL) | | |

SURVEY COMPARISION ISOPACH
ASH POND 1
COFFEEN POWER PLANT
COFFEEN, ILLINOIS

GLP8027.02 MAY 2021

GLP8027.02 MAY 2021

DRAWING





INITIAL AERIAL 12-01-2015 IMAGERY PERIODIC AERIAL 02-26-2021 IMAGERY



NOTES:

- 1. THE INITIAL IMAGERY WAS TAKEN FROM THE DRAWING PACKAGE TITLED "DYNEGY, COLLINSVILLE, ILLINOIS, 2015 - COFFEEN TOPOGRAPHY", PREPARED BY WEAVER CONSULTANTS GROUP, DATED DECEMBER 1, 2015.
- 2. THE PERIODIC IMAGERY WAS TAKEN FROM THE DRAWING PACKAGE TITLED "LUMINANT, ILLINOIS POWER GENERATING COMPANY, COFFEEN POWER STATION, DECEMBER 2020 TOPOGRAPHY", PREPARED BY INGENAE, DATED FEBRUARY 26, 2021.

INITIAL TO PERIODIC AERIAL IMAGERY COMPARISON ASH POND 1 **COFFEEN POWER PLANT** COFFEEN, ILLINOIS

Geosyntec consultants

GLP8027.02

MAY 2021

3

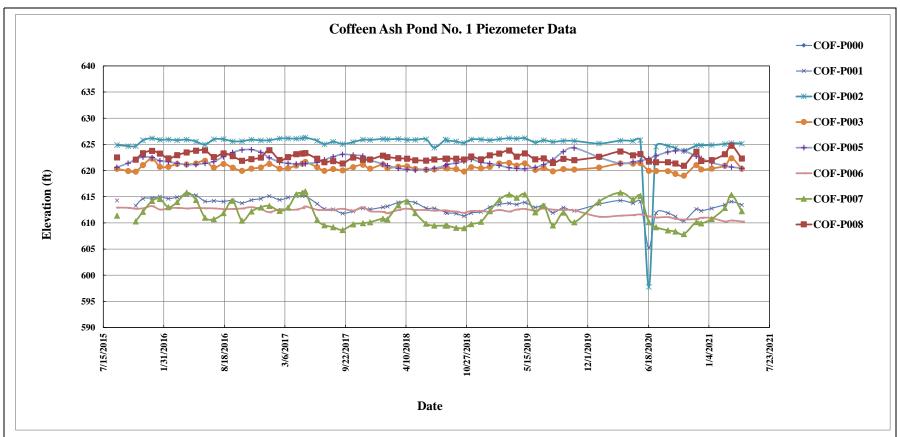
DRAWING

Periodic USEPA CCR Rule Certification Report Ash Pond No. 1 – Coffeen Power Plant October 11, 2021

ATTACHMENTS

Attachment A

AP1 Piezometer Data Plots



NOTES:

- 1. The average of preceding and following readings was applied in this graph for specific missed measurments on 5/2/2017, 8/18/2018 and 8/23/2018.
- 2. Piezometer data was taken from the spreadsheet titled "2021 Coffeen Piezo Measurements", provided by the Coffeen Power Station.

| PIEZOMETER DATA PERIODIC CERTIFICATION, ASH POND NO.1 COFFEEN POWER PLANT COFFEEN, ILLINOIS | | | | |
|---|-----------|--------|--|--|
| Geosyntec Consultants | | Figure | | |
| GLP8027 | 5/18/2021 | A-1 | | |

Periodic USEPA CCR Rule Certification Report Ash Pond No. 1 – Coffeen Power Plant October 11, 2021

Attachment B

AP1 Site Visit Photolog

Geosyntec consultants

Site Owner: Illinois Power Generating Company **Project Number:** GLP8027

CCR Unit: Ash Pond #1 (AP#1) Site: Coffeen Power Plant

Photo: 01

Date: 05/28/2021

Direction Facing:

Е

Comments:

Bottom ash berm installed around the recycle intake structure (primary spillway) inlet.



Photo: 02

Date: 05/28/2021

Direction Facing:

NW

Comments:

Recycle pipe penetration through

the berm.



1

Geosyntec consultants

Site Owner: Illinois Power Generating Company **Project Number:** GLP8027

CCR Unit: Ash Pond #1 (AP#1) Site: Coffeen Power Plant

Photo: 03

Date: 05/28/2021

Direction Facing:

Down

Comments:

Interior of recycle intake structure.



Photo: 04

Date: 05/28/2021

Direction Facing:

E

Comments:

North AP1 embankment overview



Geosyntec consultants

Site Owner: Illinois Power Generating Company Project Number: GLP8027

CCR Unit: Ash Pond #1 (AP#1) Site: Coffeen Power Plant

Photo: 05

Date: 05/28/2021

Direction Facing:

E

Comments:

North interior slope of AP1. Slope coverings included bottom ash, gravel, and vegetation in some areas.



Photo: 06

Date: 05/28/2021

Direction Facing:

N

Comments:

Wet area at north embankment toe, as noted in previous site visit reports by others.



Geosyntec consultants

Site Owner: Illinois Power Generating Company **Project Number:** GLP8027

CCR Unit: Ash Pond #1 (AP#1) Site: Coffeen Power Plant

Photo: 07

Date: 05/28/2021

Direction Facing:

NE

Comments:

North embankment

overview



Photo: 08

Date: 05/28/2021

Direction Facing:

SE

Comments:

North interior embankment overview



GEOSYNTEC CONSULTANTS

Geosyntec consultants

Site Owner: Illinois Power Generating Company **Project Number:** GLP8027

CCR Unit: Ash Pond #1 (AP#1) Site: Coffeen Power Plant

Photo: 09

Date: 05/28/2021

Direction Facing:

SE

Comments:

Northeast embankment exterior overview



Photo: 10

Date: 05/28/2021

Direction Facing:

F

Comments:

Crest of northeast embankment sheet pile wall. Note growth of small trees. Geosyntec recommended cutting of the trees as part of routine site maintenance.



Geosyntec consultants

Site Owner: Illinois Power Generating Company **Project Number:** GLP8027

CCR Unit: Ash Pond #1 (AP#1) Site: Coffeen Power Plant

Photo: 11

Date: 05/28/2021

Direction Facing:

S

Comments:

East embankment toe overview. Some seepage was noted on the embankment face. Geosyntec recommended observing the seepage as part of routine inspections.



Photo: 12

Date: 05/28/2021

Direction Facing:

W

Comments:

Sheet pile wall overview at northeast embankment toe. Note tree growth. Geosyntec recommended cutting of the trees as part of routine site maintenance



GEOSYNTEC CONSULTANTS

Geosyntec consultants

Site Owner: Illinois Power Generating Company Project Number: GLP8027

CCR Unit: Ash Pond #1 (AP#1) Site: Coffeen Power Plant

Photo: 13

Date: 05/28/2021

Direction Facing:

S

Comments:

East embankment interior overview



Photo: 14

Date: 05/28/2021

Direction Facing:

SW

Comments:

Southeast Ash Pond 1 interior

overview



Geosyntec consultants

Site Owner: Illinois

Power Generating **Project Number:** GLP8027

Company

CCR Unit: Ash Pond #1 (AP#1)

Site: Coffeen Power Plant

Photo: 15

Date: 05/28/2021

Direction Facing:

W

Comments:

South embankment exterior overview.
The embankment toe is reportedly always wet in this area.



Photo: 16

Date: 05/28/2021

Direction Facing:

W

Comments:

South embankment interior overview.



GEOSYNTEC CONSULTANTS

Geosyntec consultants

Site Owner: Illinois

Power Generating

Project Number: GLP8027

Company

CCR Unit: Ash Pond #1 (AP#1)

Site: Coffeen Power Plant

Photo: 17

Date: 05/28/2021

Direction Facing:

W

Comments:

South embankment exterior overview



Photo: 18

Date: 05/28/2021

Direction Facing:

SW

Comments:

Exterior toe of the south embankment. Note wet conditions, which are typical per previous site visit reports.



Geosyntec consultants

Site Owner: Illinois Power Generating Company Project Number: GLP8027

CCR Unit: Ash Pond #1 (AP#1) Site: Coffeen Power Plant

Photo: 19

Date: 05/28/2021

Direction Facing:

N

Comments:

Exterior toe of the south embankment. Note wet conditions, which are typical per pervious site visit reports.



Photo: 20

Date: 05/28/2021

Direction Facing:

NW

Comments:

AP1 sluice line discharge location.



Geosyntec consultants

Site Owner: Illinois Power Generating Company Project Number: GLP8027

CCR Unit: Ash Pond #1 (AP#1) Site: Coffeen Power Plant

Photo: 21

Date: 05/28/2021

Direction Facing:

NW

Comments:

Southwest embankment

exterior overview



Photo: 22

Date: 05/28/2021

Direction Facing:

NW

Comments:

Sluice pipe penetrations through the embankment.



GEOSYNTEC CONSULTANTS

Geosyntec consultants

Site Owner: Illinois Power Generating Company Project Number: GLP8027

CCR Unit: Ash Pond #1 (AP#1) Site: Coffeen Power Plant

Photo: 23

Date: 05/28/2021

Direction Facing:

Down

Comments:

Culvert under the crest access road.



Photo: 24

Date: 05/28/2021

Direction Facing:

N

Comments:

West exterior embankment overview



Geosyntec consultants

Site Owner: Illinois Power Generating Company Project Number: GLP8027

CCR Unit: Ash Pond #1 (AP#1) Site: Coffeen Power Plant

Photo: 25

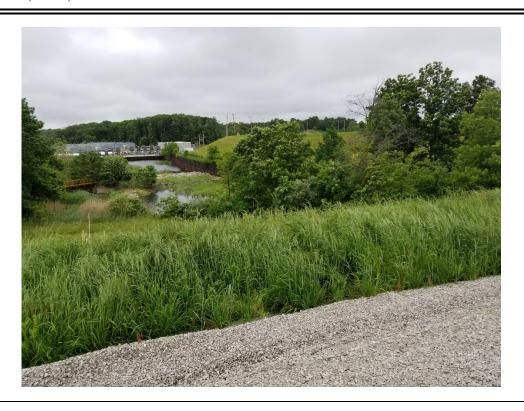
Date: 05/28/2021

Direction Facing:

SE

Comments:

Overview of sheet pile wall from AP2. Note 1 tree growth. Geosyntec recommended cutting trees as part of routine site maintenance.



Periodic USEPA CCR Rule Certification Report Ash Pond No. 1 – Coffeen Power Plant October 11, 2021

Attachment C

Periodic History of Construction Report Update Letter





October 11, 2021

Illinois Power Generating Company 134 Cips Lane Coffeen, Illinois 62017

Subject: Periodic History of Construction Report Update Letter

USEPA Final CCR Rule, 40 CFR §257.73(c)

Coffeen Power Plant Coffeen Illinois

At the request of Illinois Power Resources Generation Company (IPRG), Geosyntec Consultants (Geosyntec) has prepared this Letter to documents updates to the Initial History of Construction (HoC) report for the Coffeen Power Plant (CPP), also known as the Coffeen Power Station (COF). The Initial HoC report was prepared by AECOM in October of 2016 [1] in accordance with 40 Code of Federal Regulations (CFR) §257.73(c) of the United States Environmental Protection Agency (USEPA) Coal Combustion Residuals Rule, known as the CCR Rule [2]. This letter also includes information required by Section 845.220(a)(1)(B) (Design and Construction Plans) of the state-specific Illinois Environmental Protection Agency (IEPA) Part 845 CCR Rule [3] that is not expressly required by §257.73(c).

BACKGROUND

The CCR Rule required that, by October 17, 2016, Initial HoC reports to be compiled for existing CCR surface impoundments with: (1) a height of five feet or more and a storage volume of 20 acre-feet or more, or (2) a height of 20 feet or more. The Initial HoC report was required to contain, to the extent feasible, the information specified in 40 CFR §257.73(c)(1)(i)-(xii). The Initial HoC report for CPP, which included four existing CCR surface impoundments, Ash Pond No. 1 (AP1), Ash Pond No. 2 (AP2), the GMF Gypsum Stack Pond (GMF GSP, also known as the GMF Pond), and the GMF Recycle Pond (GMF RP), was prepared and subsequently posted to IPGC's CCR Website prior to October 17, 2016.

The CCR Rule requires that Initial HoC to be updated if there is a significant change to any information complied in the Initial HoC report, as listed below:

Illinois Power Resources Generating Company October 2021 Page 2

§ 257.73(c)(2): If there is a significant change to any information complied under paragraph (c)(1) of this section, the owner or operator of the CCR unit must update the relevant information and place it in the facility's operating record as required by § 257.105(f)(9).

IPRG retained Geosyntec to review the Initial HoC report, review reasonably and readily available information for AP1, AP2, the GMF GSP, and the GMF RP generated since the Initial HoC report was prepared, and perform a site visit to CPP to evaluate if significant changes may have occurred since the Initial HoC report was prepared. This Letter contains the results of Geosyntec's evaluation and documents significant changes that have occurred at AP1, AP2, the GMF GSP, and the GMF RP, as they pertain the requirements of §257.73(c)(1)(i)-(xii).

UPDATES TO HISTORY OF CONSTRUCTION REPORT

Geosyntec's evaluation for the CPP AP1, AP2, GMF GSP, and GMF RP determined that no known significant changes requiring updates to the information in the Initial HoC report pertaining to §257.73(c)(1)(ii), (iv), (v), (vi), (vii), (xi), and (xii) of the CCR Rule had occurred since the Initial HoC report was developed.

However, Geosyntec's evaluation determined that significant changes at the CPP AP1, AP2, GMF GSP, and GMF RP, pertaining to §257.73(c)(1)(i), (iii), (viii), (ix), and (x) of the CCR Rule had occurred since the Initial HoC report had been developed. Additionally, information how long the CCR surface impoundments have been operating and the types of CCR in the surface impoundments, as required by Section 845.220(a)(1)(B) of the Part 845 Rule were not included in the Initial HoC report, as this information is not required by the CCR Rule. Each change and the subsequent updates to the Initial HoC report is described within this section.

Section 845.220(a)(1)(B): A statement of ... how long the CCR surface impoundment has been in operation, and the types of CCR that have been placed in the surface impoundment.

Ash Pond No. 1

The AP1 was in operation from 1964 until CPP was retired in 2019 and received CCR for approximately 55 years. As of the date of this report, the AP1 has been present for approximately 57 years [4].

CCR placed in the AP1 included bottom ash [4].

Ash Pond No. 2

The AP2 was in operation from 1971 to 1984, for a total of approximately 13 years. The AP2 was closed in 1984-1985 by installing a clay cover and has not since been active or

received CCR. As of the date of this report, AP2 has been present for approximately 50 years. [4].

CCR placed in the AP2 was used to store and dispose of fly ash and bottom ash [4].

GMF Gypsum Pond

The GMF GSP was in operation from 2010 until CPP was retired in 2019 and received CCR for approximately 9 years. As of the date of this report, the GMF GSP has been present for a total of approximately 11 years [4].

CCR placed in GMF GSP included gypsum [4].

GMF Recycle Pond

The GMF RP was in operation from 2010 until CPP was retired in 2019, for a total of 9 years [4]. As of the date of this report, the GMF RP has been present for approximately 11 years.

 \S 257.73(c)(1)(i): The name and address of the person(s) owning or operating the CCR unit; the name associated with the CCR unit; and the identification number of the CCR unit if one has been assigned by the state.

State identification numbers (IDs) for AP1, AP2, the GMF GSP, and the GMF RP have been assigned by the Illinois Environmental Protection Agency (IEPA). Each ID is listed in **Table 1**.

 CCR Surface Impoundment
 State ID

 Ash Pond No. 1 (AP1)
 W1350150004-01

 Ash Pond No. 2 (AP2)
 W1350150004-02

 GMF Gypsum Stack Pond (GMF GSP)
 W1350150004-03

 GMF Recycle Pond (GMF RP)
 W1350150004-04

Table 1 – IEPA ID Numbers

§ 257.73(c)(1)(iii): A statement of the purpose for which the CCR unit is being used.

AP2 was closed in 2020, in substantial compliance with the written closure plan posted to IPRG's CCR Website [5], and as documented by a certified Notification of Completion of Closures posted to DMG's CCR Website [6].

The CPP was retired in December of 2019, with the generation of electricity ceased at that time. Therefore, AP1, the GMF GSP, and the GMF RP are no longer being used to store and dispose of new CCR that is actively generated by CPP, as CCR generation as ceased. All three impoundments still contain CCR and liquids that was present at the time of plant

retirement. The GMF RP also previously received dewatering discharge from AP2; this inflow was ceased after AP2 was closed in 202.

 $\S 257.73(c)(1)(viii)$: A description of the type, purpose, and location of existing instrumentation.

Instrumentation monitoring at AP2 is no longer required as the CCR surface impoundment was closed in accordance with §257.102 [6], and the instrumentation network was modified at that time. Therefore, the instrumentation locations shown in Appendix C of the Initial HoC report are no longer applicable to AP2.

 \S 257.73(c)(1)(ix): Area-capacity curves for the CCR unit.

Updated area-capacity curves were prepared for AP1, the GMF GSP, and the GMF RP in 2021 and are provided in **Figures 1**, **2**, and **3**, respectively.

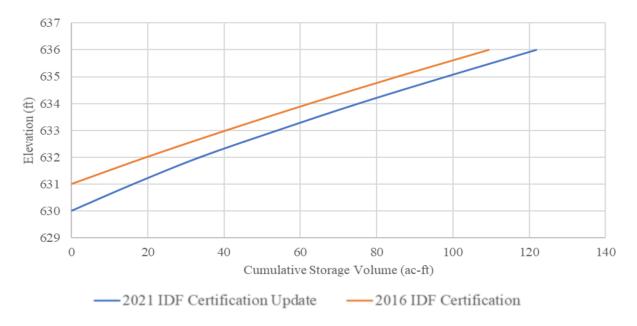
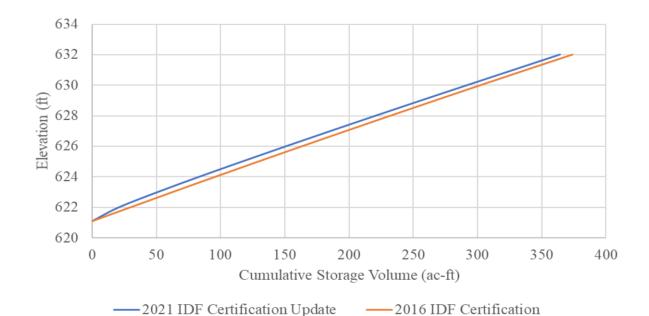


Figure 1 – Area-Capacity Curve for AP1



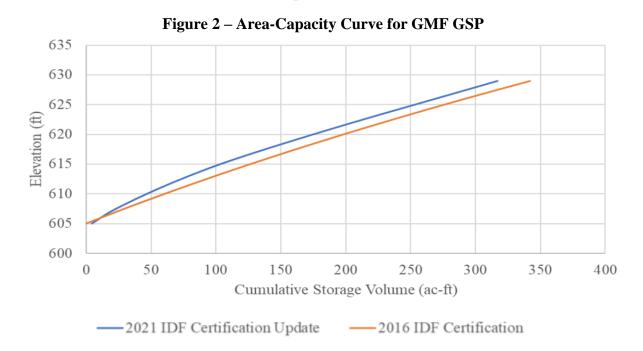


Figure 3 – Area-Capacity Curve for GMF RP

§ 257.73(c)(1)(x): A description of each spillway and diversion design features and capacities and calculations used in their determination.

The primary spillway structure for AP1 was modified in 2020 by constructing a berm of bottom ash around the entrance to the spillway, to reduce the potential for freezing around the spillway during post-CPP closure conditions, with a berm crest elevation of

approximately 630 ft. Design drawings for the bottom ash berm are not reasonably or readily available.

The transfer channel between the GMF GSP and the GMF RP was modified in 2020 by constructing a geomembrane-lined berm, in order to allow the normal pool level of the GMF GSP to be increased. Design drawings for the berm are not reasonably or readily available. However, survey data [3] indicates the berm has an elevation of approximately 628 ft, a top width (perpendicular to the flow direction) of approximately 75 ft, a total length (parallel to the flow direction) of 25 ft, and side slopes of approximately 4 horizontal to 1 vertical.

Valves were installed on the intake pipes for the GMF RP after the CPP was closed and plant process water intake pumping was ceased. Design drawings for these valves are not reasonably or readily available.

Updated discharge capacity calculations for the existing spillways of AP1, the GMF GSP, and the GMF RP were prepared in 2021 using HydroCAD 10 modeling software. The calculations indicate that the AP1 and the GMF RP have sufficient storage capacity and will not overtop the embankments during the 1,000-year, 24-hour, storm event. The calculations also indicate that the GMF GSP has sufficient storage capacity and will not overtop the embankments during the Probable Maximum Precipitation (PMP), 24-hour storm event. The results of the calculations are provided in **Table 2**.

Table 2 – Results of Updated Discharge Capacity Calculations

| | AP1 | GMF GSP | GMF RP |
|--|--------------|-------------|--------------|
| Approximate Berm Minimum Elevation ¹ , ft | 636.0 | 632.0 | 629.0 |
| Approximate Emergency Spillway Elevation ¹ , ft | Not Present | Not Present | 624.0 |
| Starting Water Surface Elevation ¹ (SWSE), ft | 630.2 | 625.2 | 622.1 |
| Peak Water Surface Elevation ¹ (PWSE), ft | 631.4 | 626.7 | 623.9 |
| Time to Peak, hr | No Discharge | 10.6 | No Discharge |
| Surface Area ² , ac | 18.1 | 34.8 | 16.1 |
| Storage ³ , ac-ft | 19.5 | 52.9 | 29.0 |

Notes:

AP2 no longer retains free water as the CCR surface impoundments was closed in 2020 [6]. Therefore, the spillways are no longer present and the information regarding these structures, as presented in the Initial HoC report, is no longer applicable to AP2.

¹Elevations are based on the NAVD88 datum

²Surface area is defined as the water surface area at the PWSE

³Storage is defined as the volume between the SWSE and PWSE

Illinois Power Resources Generating Company October 2021 Page 7

CLOSING

This letter has been prepared to document Geosyntec's evaluation of changes that have occurred at AP1, AP2, the GMF GSP, and the GMF RP since the Initial HoC was developed, based on reasonably and readily available information provided by IPRG, observed by Geosyntec during the site visit, or generated by Geosyntec as part of subsequent calculations.

Sincerely,

Lucas P. Carr, P.E.

2- 8/

Senior Engineer

John Seymour, P.E.

Senior Principal

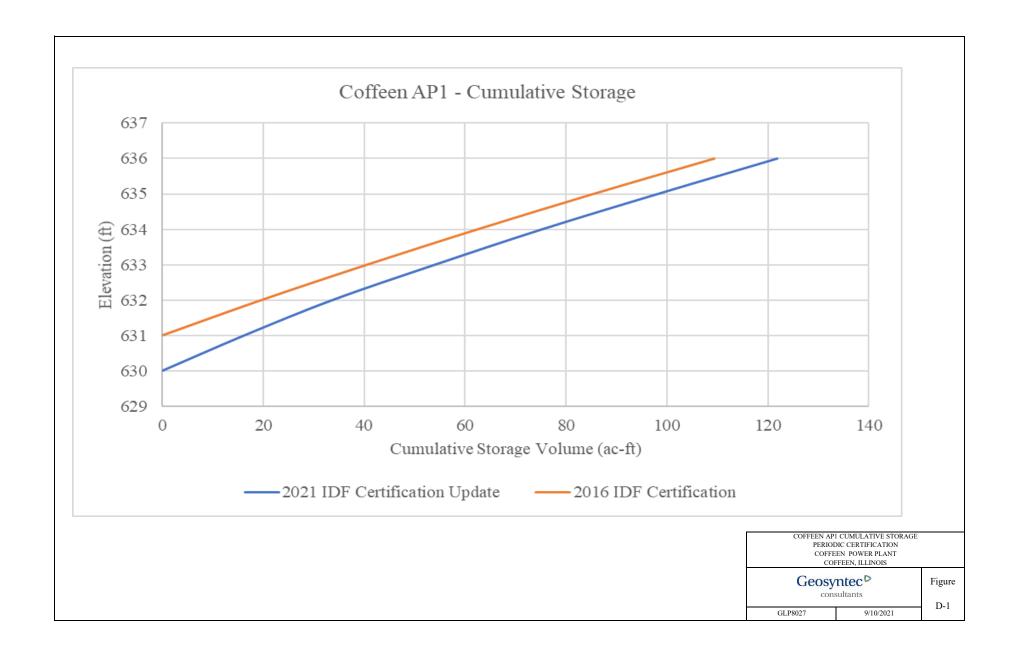
REFERENCES

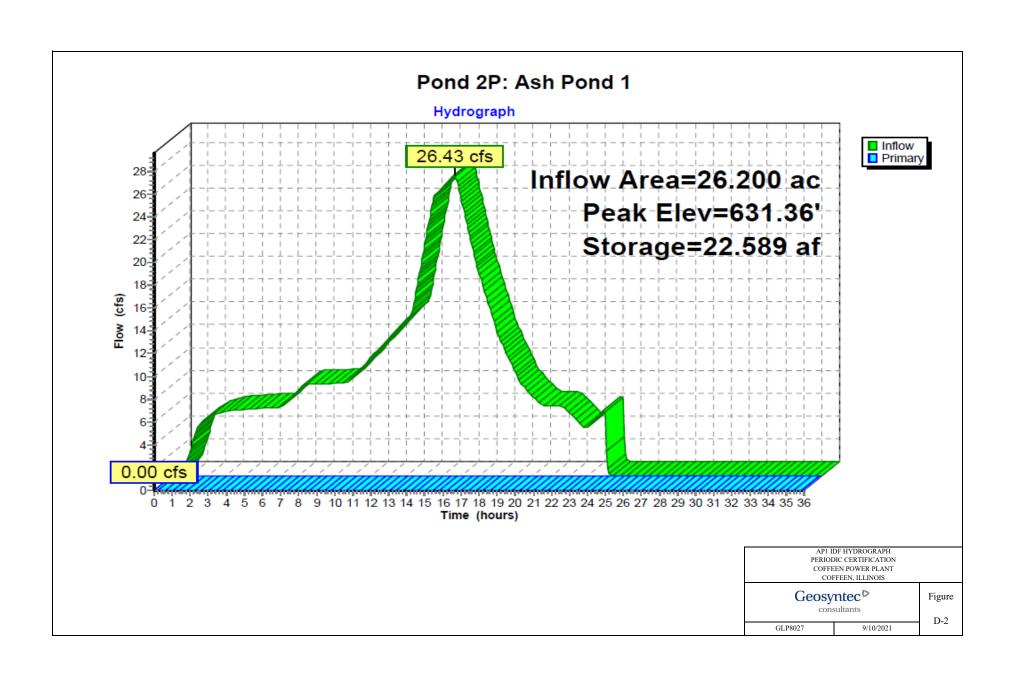
- [1] AECOM, "History of Construction, USEPA Final CCR Rule, 40 CFR § 257.73(c), Coffeen Power Station, Coffeen, Illinois," October 2016.
- [2] United Stated Environmental Protection Agency, "40 CFR Parts 257 and 261, Hazardous and Solid Waste Management System, Disposal of Coal Combustion Residuals from Electric Utilities, Final Rule, 2015," 2015.
- [3] Illinois Environmental Protection Agency, "35 Ill. Adm. Code Part 845, Standards for the Disposal of Coal Combustion Residuals in Surface Impoundments," Springfield, IL, 2021.
- [4] AECOM, "History of Construction, USEPA Final CCR Rule, 40 CFR § 257.73(c), Hennepin Power Station, Hennepin, Illinois," October 2016.
- [5] V. Modeer, "Closure Plan for Existing CCR Surface Impoundment, Coffeen Power Station, Illinois Power Generating Company, Ash Pond No. 2," October 17, 2016.
- [6] D. Tickner, "Coffeen Power Station; Ash Pond No. 2; Notification of Completion of Closure," December 17, 2020.

Periodic USEPA CCR Rule Certification Report Ash Pond No. 1 – Coffeen Power Plant October 11, 2021

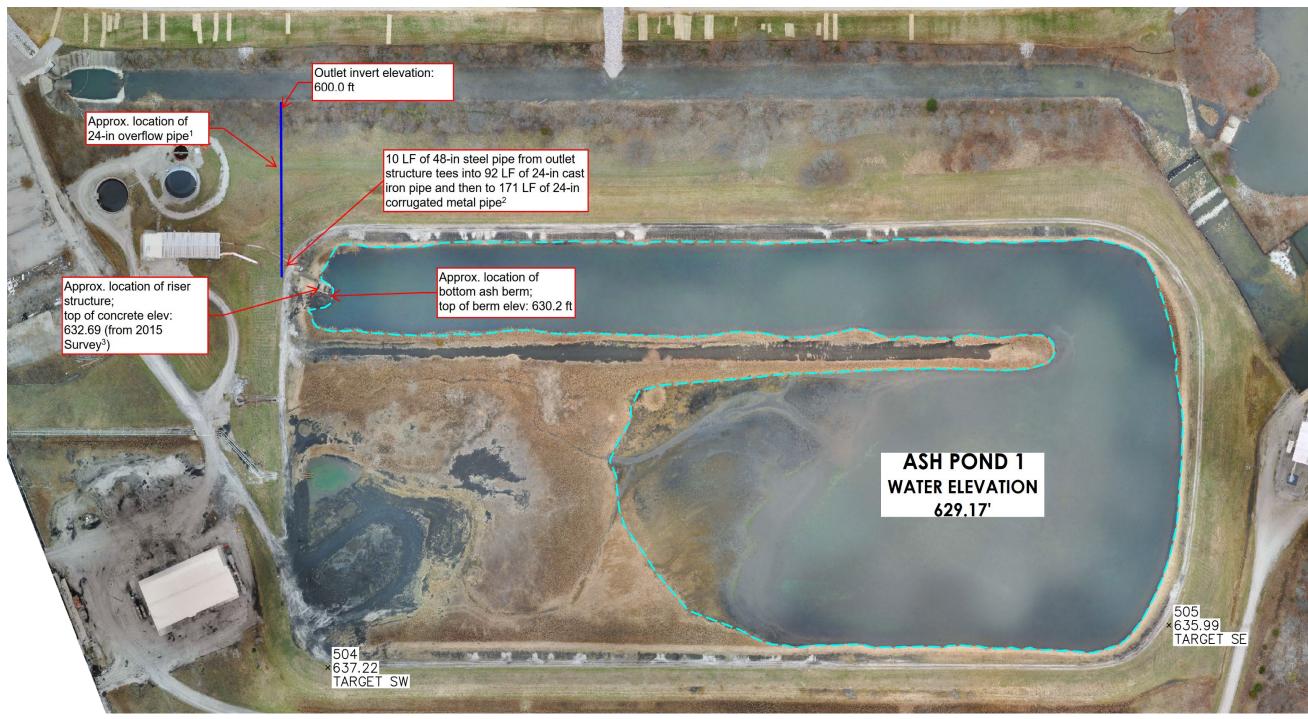
Attachment D

Periodic Inflow Design Flood Control System Plan Analyses









¹Outlet pipe configuration provided by site personnel on 29 June 2021

Figure based on IngenAE 2020 Site Topo

NOT TO SCALE

Coffeen Power Plant Ash Pond 1 Hydrologic Workmap

Geosyntec[▶] consultants

Figure

D-3

GLP8027

September 2021

²Emergency Overflow Assessment (2011); see Figure D-4

³Weaver Consultants Group, "Dynegy, Collinsville, IL, 2015 - Coffeen Topography," December 1, 2015.

BODINE SERVICES OF MASSILE US 3322 Tower Drive Newburgh, IN 47720 Phone 812 423-5106 Fax 812 422-1996

WORK

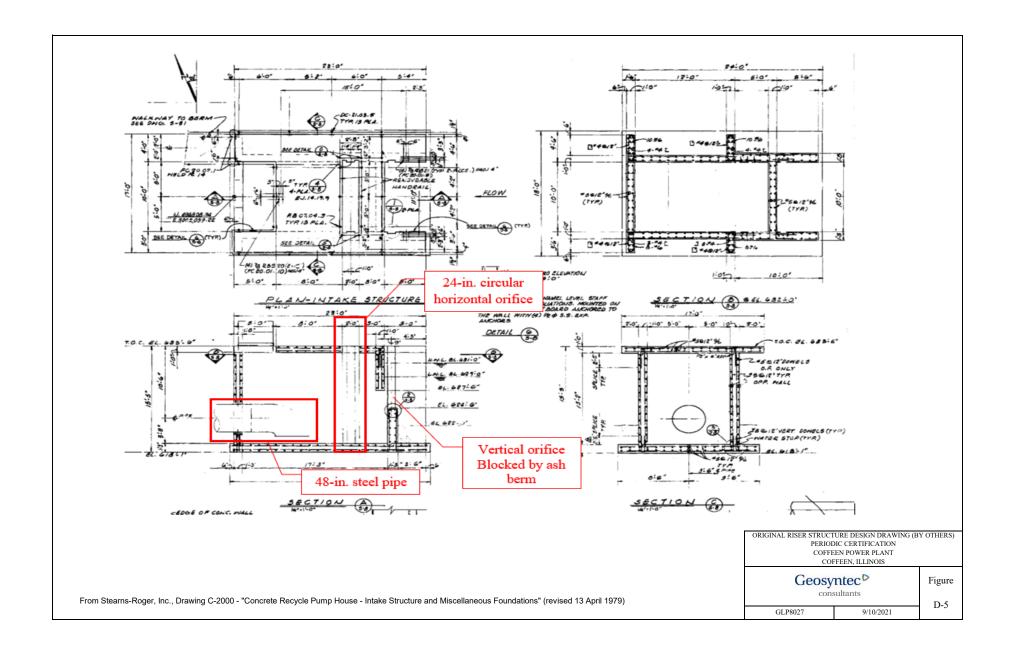
| D HD HOFTS | LE NO. VISUA | ergency Overfill TO MANHO NT PIPE SIZE QPX 24" | LENO. | TORIVER | |
|---------------------|---------------------|---|-----------------------------------|-------------------------------------|-----------|
| RECTION B | VERTO PLA | NT PIPE SIZE QPX 24" | PIPE TYPE C | Corrugated + | Cast pipe |
| Distance Reading | Quadrani 1 2 3 4 | Observations | 7; infiltration/ inflow GPO | Recommended Correction Action | Photo No. |
| 77+ | | Light buildup Bottier | n of pipe | 1. | |
| 7 fT | | Spirt in pipe | 1011 | | 1 |
| 13+T | | Light buildupon B | ottomot più | 200 | |
| 27FT | | Junt in sige | | | |
| IntT | Titi | JOINT INDIANA Light | thuilding | Lottempfair | be . |
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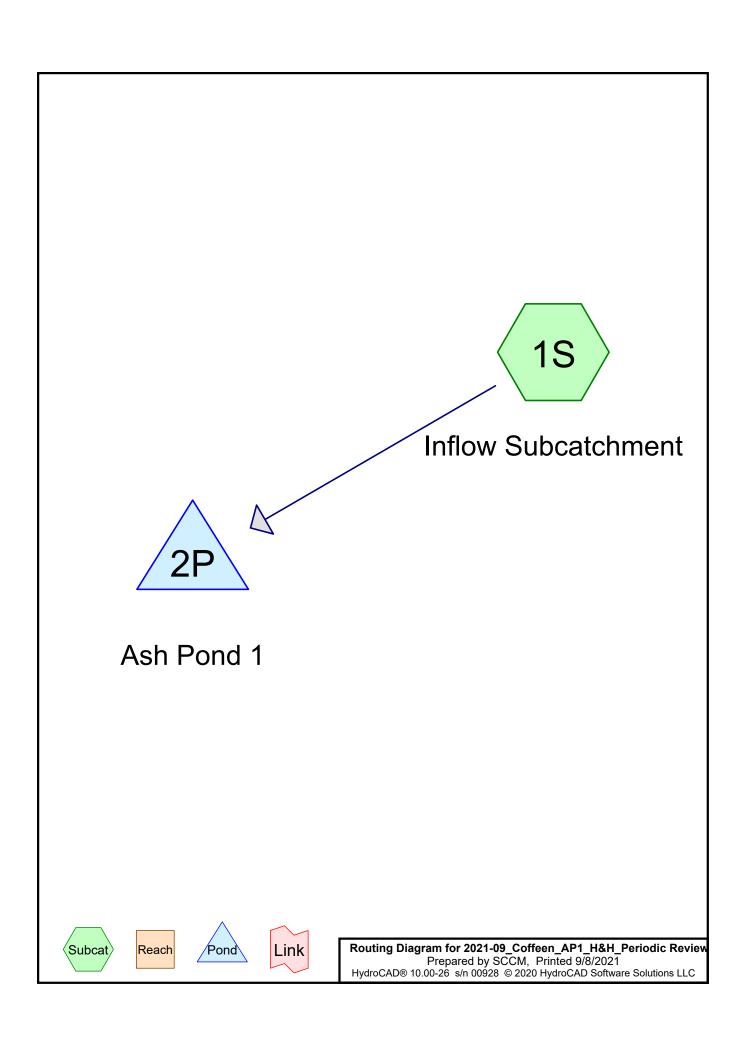
2011 EMERGENCY OVERFLOW ASSESSMENT (BY OTHERS)
PERIODIC CERTIFICATION
COFFEEN POWER PLANT
COFFEEN, ILLINOIS

Geosyntec consultants

GLP8027 9/10/2021 D-4

Figure





Printed 9/8/2021

Page 2

Area Listing (all nodes)

| Area | CN | Description |
|---------|----|----------------------------|
| (acres) | | (subcatchment-numbers) |
| 26.200 | 98 | Water Surface and Ash (1S) |
| 26.200 | 98 | TOTAL AREA |

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Page 3

Soil Listing (all nodes)

| Area | Soil | Subcatchment |
|---------|-------|-------------------|
| (acres) | Group | Numbers |
| 0.000 | HSG A | |
| 0.000 | HSG B | |
| 0.000 | HSG C | |
| 0.000 | HSG D | |
| 26.200 | Other | 1S |
| 26.200 | | TOTAL AREA |

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Page 4

Ground Covers (all nodes)

| HSG-A | HSG-B | HSG-C | HSG-D | Other | Total | Ground | Subcatchment |
|---------|---------|---------|---------|---------|---------|-----------------------|--------------|
| (acres) | (acres) | (acres) | (acres) | (acres) | (acres) | Cover | Numbers |
| 0.000 | 0.000 | 0.000 | 0.000 | 26.200 | 26.200 | Water Surface and Ash | 1S |
| 0.000 | 0.000 | 0.000 | 0.000 | 26.200 | 26.200 | TOTAL AREA | |

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Pipe Listing (all nodes)

| Line# | Node | In-Invert | Out-Invert | Length | Slope | n | Diam/Width | Height | Inside-Fill |
|-------|--------|-----------|------------|--------|---------|-------|------------|----------|-------------|
| | Number | (feet) | (feet) | (feet) | (ft/ft) | | (inches) | (inches) | (inches) |
| 1 | 2P | 614.50 | 600.00 | 171.0 | 0.0848 | 0.025 | 24.0 | 0.0 | 0.0 |
| 2 | 2P | 622.30 | 614.50 | 92.0 | 0.0848 | 0.013 | 24.0 | 0.0 | 0.0 |
| 3 | 2P | 624.00 | 622.30 | 10.0 | 0.1700 | 0.012 | 48.0 | 0.0 | 0.0 |

Page 5

Time span=0.00-36.00 hrs, dt=0.05 hrs, 721 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: Inflow Subcatchment Runoff Area=26.200 ac 100.00% Impervious Runoff Depth=8.93" Tc=6.0 min CN=98 Runoff=26.43 cfs 19.502 af

Pond 2P: Ash Pond 1 Peak Elev=631.36' Storage=22.589 af Inflow=26.43 cfs 19.502 af Outflow=0.00 cfs 0.000 af

Total Runoff Area = 26.200 ac Runoff Volume = 19.502 af Average Runoff Depth = 8.93" 0.00% Pervious = 0.000 ac 100.00% Impervious = 26.200 ac

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Page 7

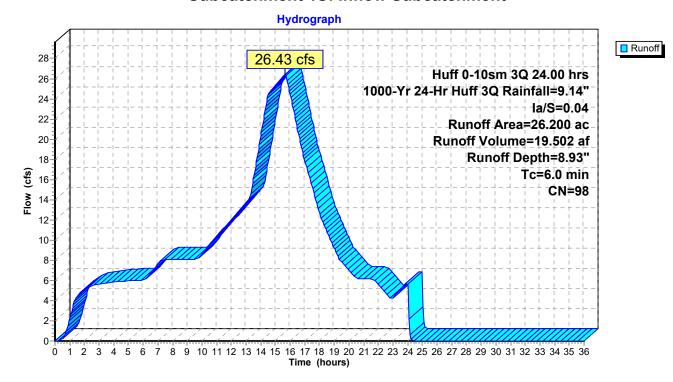
Summary for Subcatchment 1S: Inflow Subcatchment

Runoff = 26.43 cfs @ 15.65 hrs, Volume= 19.502 af, Depth= 8.93"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.05 hrs Huff 0-10sm 3Q 24.00 hrs 1000-Yr 24-Hr Huff 3Q Rainfall=9.14", Ia/S=0.04

| | Area | (ac) | CN | Desc | cription | | |
|---|-------------|------|----|------------------|----------------------|-------------------|---|
| * | 26. | 200 | 98 | Wate | er Surface | and Ash | |
| | 26. | 200 | | 100. | 00% Impe | rvious Area | · |
| | Tc (min) | Leng | | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
| _ | 6.0 | • | , | | , | , , | Direct Entry, Minimal - Direct Entry into Impoundment |

Subcatchment 1S: Inflow Subcatchment



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Page 8

Summary for Pond 2P: Ash Pond 1

Inflow Area = 26.200 ac,100.00% Impervious, Inflow Depth = 8.93" for 1000-Yr 24-Hr Huff 3Q event

Inflow = 26.43 cfs @ 15.65 hrs, Volume= 19.502 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.05 hrs

Starting Elev= 630.19' Surf.Area= 0.000 ac Storage= 3.087 af

Peak Elev= 631.36' @ 24.40 hrs Surf.Area= 0.000 ac Storage= 22.589 af (19.502 af above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Avail.Storage Storage Description

Center-of-Mass det. time= (not calculated: no outflow)

Invert

Volume

| | | | <u> </u> | |
|---------------------|-----------------------|------------|-------------------------------|--|
| #1 | 630.00' | 121.815 af | Custom Stage DataListed below | |
| Elevation (feet) | Cum.Stor (acre-fee | | | |
| 630.00 | 0.00 | 0 | | |
| 631.00 | 16.24 | 8 | | |
| 632.00 | 33.72 | 2 | | |
| 633.00 | 54.03 | 8 | | |
| 634.00 | 75.24 | .0 | | |
| 635.00 | 98.17 | 4 | | |
| 636.00 | 121.81 | 5 | | |

| Device | Routing | Invert | Outlet Devices |
|--------|----------|---------|--|
| #1 | Primary | 614.50' | 24.0" Round Culvert - 24" CMP L= 171.0' Ke= 1.000 |
| | - | | Inlet / Outlet Invert= 614.50' / 600.00' S= 0.0848 '/' Cc= 0.900 |
| | | | n= 0.025 Corrugated metal, Flow Area= 3.14 sf |
| #2 | Device 1 | 622.30' | 24.0" Round Culvert - 24" Cast Iron L= 92.0' Ke= 1.000 |
| | | | Inlet / Outlet Invert= 622.30' / 614.50' S= 0.0848 '/' Cc= 0.900 |
| | | | n= 0.013 Cast iron, coated, Flow Area= 3.14 sf |
| #3 | Device 2 | 624.00' | 48.0" Round Culvert - 48" Steel L= 10.0' Ke= 1.000 |
| | | | Inlet / Outlet Invert= 624.00' / 622.30' S= 0.1700 '/' Cc= 0.900 |
| | | | n= 0.012 Steel, smooth, Flow Area= 12.57 sf |
| #4 | Device 3 | 632.69' | 24.0" Horiz. Orifice/Grate C= 0.600 |
| | | | Limited to weir flow at low heads |

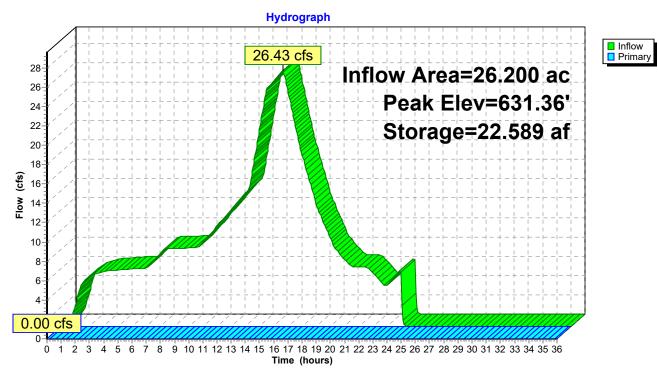
Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=630.19' (Free Discharge)

-1=Culvert - 24" CMP (Passes 0.00 cfs of 42.58 cfs potential flow)

-2=Culvert - 24" Cast Iron (Passes 0.00 cfs of 29.78 cfs potential flow)
-3=Culvert - 48" Steel (Passes 0.00 cfs of 92.89 cfs potential flow)

4=Orifice/Grate (Controls 0.00 cfs)

Pond 2P: Ash Pond 1





Office Memorandum

Date: November 30, 2020

To: Cynthia Vodopivec

Matt Ballance Jason Campbell Charles Koudelka

From: Vic Modeer

cc:

Ash Pond No. 1 Structural Stability Assessment

Illinois Power Resources Generating, LLC

Subject: Coffeen Power Station

BACKGROUND

The Coffeen Power Station was retired in November 2019. The October 2016 certified "CCR Rule Report: Initial Structural Stability Assessment for Ash Pond No. 1 at the Coffeen Power Station" (CCR Certification Report) prepared by AECOM for Illinois Power Resources Generating (IPRG) describes the outlets for the spillway system for Ash Pond No. 1. The spillway system includes a concrete recycle intake structure with a gated inlet to a 48-inch diameter steel recycle intake pipe, which acts as the primary outflow pipe for Ash Pond No. 1, and a secondary 24-inch corrugated metal (CMP) overflow pipe that flows into the recycle intake pipe, which are all constructed of non-erodible materials designed to carry sustained flows. AECOM's 2016 report states that the Ash Pond No. 1 hydraulic structures cannot be structurally certified due to inability to complete a closed-circuit television (CCTV) inspection of the 48-inch steel recycle intake pipe. However, the 48-inch pipe and 24-inch CMP have been inspected numerous times thereafter and found to be structurally sufficient. Thus, both hydraulic structures for Ash Pond No. 1 are structurally sufficient.

Specifically, AECOM's 2016 report states that the 24-inch CMP overflow pipe was able to be internally inspected via a CCTV inspection and "found to be free of significant deterioration, deformation, distortion, bedding deficiencies, sedimentation, and debris." In addition, the AECOM report states that "[e]valuation of design drawings and operational and maintenance procedures for [the 24-inch pipe] also did not identify any issues." However, AECOM could not certify that the 48-inch inch pipe met the requirements of § 257.73(d)(1)(vi) due to the inability to visually inspect the pipe as a result of the high flow volume while the plant was in operation. Notwithstanding, the 48-inch pipe was observed in the field by AECOM, and no structural defects were found as noted in AECOM's 2016 report.

Dike Structural Stability. The stability of the Coffeen Ash Pond No. 1 embankment section at the 48-inch recycle intake pipe (Cross Section 13+00, "CCR Certification Report") had calculated factors of safety of 1.77, (§257.73(e)(1)(i) Minimum FS = 1.50), 1.77 (§257.73(e)(1)(ii) Minimum = 1.40) and 1.18 (§257.73(e)(1)(iii) Minimum = 1.00). The inspection history does not reveal any seepage at the standpipe spillway section.

48-inch Recycle Intake Pipe Stability. The embankment at the recycle intake pipe is stable as shown by visual inspection and the above listed calculations. The plant is no longer in operation, and the impoundment water level has been lowered to an elevation at or below the base of the intake pipe. There is no possibility of a pipe failure causing a release of CCR material.

Accordingly, both the 24-inch CMP overflow pipe and 48-inch recycle intake pipe are structurally sufficient and meet the requirements of § 257.73(d)(1)(vi).

Please let me know if you have any questions.

molen

Sincerely,

Vic Modeer, PE, D.GE (IL, MO, IN, KY, OH, LA) Consulting Engineer